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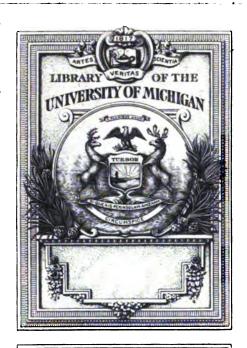
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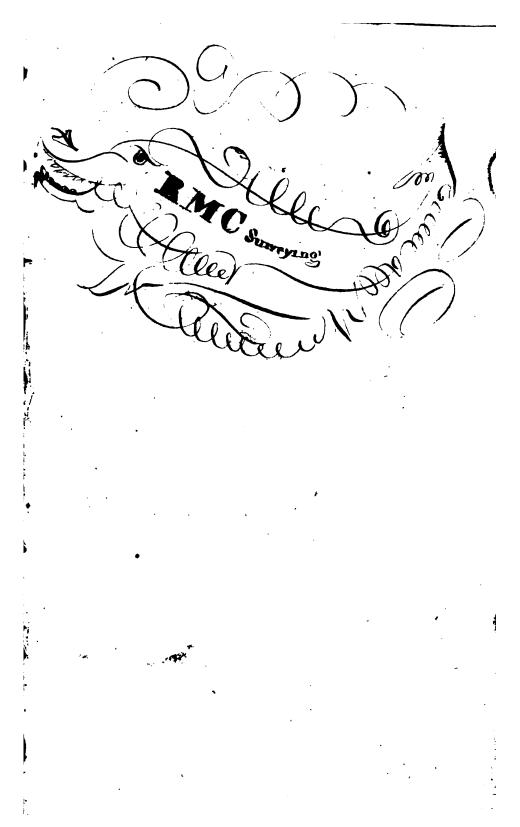
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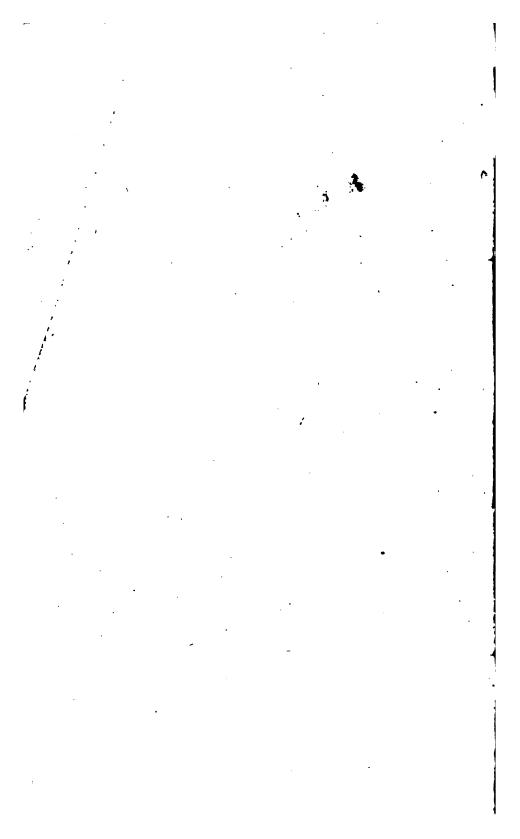
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THE

THEORY AND PRACTICE

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SURVEYING;

CONTAINING

All the Instructions requisite for the skilful practice of this Art.

21

ROBERT GIBSON.

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THE

WHOLE CORRECTED, NEWLY ARRANGED, AND GREATLY ENLARGED;
WITH USEFUL SELECTIONS,

AND A NEW SET OF ACCURATE

MATHEMATICAL TABLES.

By D. P. ADAMS,
TEACEER OF THE MATERIATION.

NEW-YORK:

PUBLISHED BY EVERT DUYCKINCK, NO. 103 PRABLETREET.

G. Long, printer.

1814.

District of Nord-York, ex.

BE IT REMEMBERED, That on the twenty-eighth day of March, in the thirty-fifth year of the Independence of the United States of America, *Evert Dwyckinck*, of the said district, hath deposited in this office the title of a book, the right whereof he claims as proprietor, in the words following, to wit:

"The Theory and Practice of Surveying; containing all the Instructions requisite for the skilful passine of this Art. By Robert Gibson. Illustrated by Copper-Plates. The whole corrected, newly arranged, and greatly enlarged, with useful Selections, and a new set of accurate Mathematical Tables. By D. P. Adams, Teacher of the Mathematica."

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EXPLANATION

Of the Mathematical Characters used in this Works

+ signifies plus, or addition.

- . . minus, or subtraction.

× or . , . multiplication.

🚓 . division.

: 4:: . proportion.

- . equality.

√ . . square root.

. . cube root, &c.

o . . diff. between two numbers when it is not known which is the greater.

Thus,

5 + 3, denotes that 3 is to be added to 5.

6 - 2, denotes that 2 is to be taken from 6.

 7×3 , or $7 \cdot 3$, denotes that 7 is to be multiplied by 3.

8 ÷ 4, denotes that 8 is to be divided by 4.

2:3::4:6, shows that, 2 is to 3 as 4 is to 6.

6 + 4 = 10, shows that the sum of 6 and 4 is equal to 10.

√ 3, or 3½, denotes the square root of the number 3.

 $\frac{3}{4}$ 5, or $5\frac{1}{3}$, denotes the cube root of the number 5.

72, denotes that the number 7 is to be squared.

83, denotes that the number 8 is to be cubed.

&c.

THEORY AND PRACTICE

SURVEYING.

THE word Surveying, in the Mathematics, signifies the art of measuring land, and of

delineating its boundaries on a map.

The Surveyor, in the practice of this art, directs his attention, at first, to the tracing and measuring of lines; secondly, to the position of these lines in respect to each other, or the angles formed by them; thirdly, to the plan, or representation of the field, or tract, which he surveys; and fourthly, to the calculation of its area, or super-When this art is employed in ficial content. observing and delineating Coasts and Harbours, in determining their variation of the Compass, their Latitude, Longitude and soundings, together with the bearings of their most remarkable places from each other, it is usually denominated Maritime Surveying. This branch of Surveying, however, demands no other qualifications than those, which should be thoroughly acquired by every Land-Surveyor, who aspires to the character of an accomplished and skilful practitioner. Surveying, therefore, requires an intimate acquaintance with the several parts of the Mathematics, which are here inserted as an introduction to this treatise.

PART 1.

Containing Decimal Fractions, Involution and Evolution, the Nature and Use of Logarithms, Geometry and Plane Trigonometry.

SECTION I.

DECIMAL FRACTIONS.

If we suppose unity or any one thing to be divided into any assigned number of equal parts, this number is called the denominator; and if we chuse to take any number of such parts less than the whole, this is called the numerator of a fraction.

The numerator, in the vulgar form, is always written over the denominator, and these are separated by a small line thus 2, or 4; the first of these is called three-fourths, and the latter five-eighths of an inch, yard, &c. or of whatever the whole thing originally consisted: the 4 and the 8 are the denominators, showing into how many equal parts the unit is divided; and the three and the five are the numerators, showing how many of those parts are under consideration.

Fractions are expressed in two forms, that is,

either vulgarly or decimally.

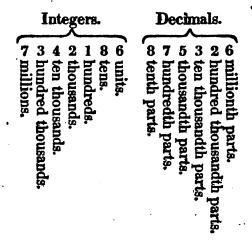
All fractions whose denominators do not consist of a cipher, or ciphers, set after unity, are called vulgar; and their denominators are always written under their numerators. The treatment of these, however, would be foreign to our present purpose. But fractions whose denominators consist of an unit prefixed to one or more ciphers, are called decimal fractions; the numerators of which are written without their denominators, and are distinguished from integers by a point prefixed: thus $\frac{2}{10}$, $\frac{4}{100}$ and $\frac{170}{100}$, in the decimal form, are expressed by .2 .42 .172.

The denominators of such fractions consisting always of an unit, prefixed to as many ciphers as there are places of figures in the numerators, it follows, that any number of ciphers put after those numerators, will neither increase nor lessen, their value: for \$\frac{1}{10}\$, \$\frac{100}{100}\$ and \$\frac{1000}{1000}\$ are all of the same value, and will stand in the decimal form thus .3 .30 .300; but a cipher, or ciphers prefixed to those numerators lessen their value in a tenfold proportion: for \$\frac{1}{10}\$, \$\frac{100}{100}\$ and \$\frac{1000}{1000}\$, which in the decimal form we denote by .3 .03 and .003, are fractions, of which the first is ten times greater than the second; and the second, ten times greater than the third.

Hence it appears, that as the value and denomination of any figure, or number of figures, in common arithmetic is enlarged, and becomes ten, or an hundred, or a thousand times greater, by placing one or two, or three ciphers after it; so in decimal arithmetic, the value of any figure, or number of figures, decreases, and becomes ten, or a hundred, or a thousand times less, while the denomination of it increases, and becomes so many times greater, by prefixing one, or two, or three ciphers to it: and that any number of ciphers, before an integer, or after a decimal fraction, has no effect in changing their values.

DECIMAL FRACTIONS.

SCALE OF NOTATION.



ADDITION OF DECIMALS.

Write the numbers under each other according to the value or denomination of their places; which position will bring all the Decimal points into a column, or vertical line, by themselves. Then, beginning at the right hand column of figures, add in the same manner as in whole numbers, and put the decimal point, in the sum directly beneath the other points.

EXAMPLES.

Add 4.7832 3.2543 7.8251 6.03 2.857 and 3.251 together. Place them thus,

4.7832

3.2543

7,8251

6,03

2.857

3.251

Sum=28,0006.

Add 6.2 121.306 .75 2.7 and .0007 together. 121.306

.75 2.7

.0007

Sum = 130.9567

What is the sum of 6.57 1.026 .75 146.5 8.7 526. 3.97 and .0271?

Answer 693.5431.

What is the sum of 4.51 146.071 .507 .0006 132. 62.71 .507 7.9 and .10712 ?

Answer 354.31272.

SUBTRACTION OF DECIMALS.

Write the figures of the subtrahend beneath those of the minuend according to the denomination of their places, as directed in the rule of addition; then, beginning at the right hand, subtract as in whole numbers, and place the decimal point in the difference exactly under the other two points,

EXAMPLES.

From 38.765 take 25.3741 25.3741

Difference =13.3909

From 2.4 take .8472 .8472

Diff. = 1.5528

From 71.45 take 8.4837248.

Difference = 62.9662752.

From 84 take 82.3412.

Diff. = 1.6588.

MULTIPLICATION OF DECIMALS.

Set the multiplier under the multiplicand without any regard to the situation of the decimal point; and having multiplied as in whole numbers, cut off as many places for decimals in the product, counting from the right hand towards the left, as there are in both the multiplicand and multiplier: but if there be not a sufficient number of places in the product, the defect may be supplied by prefixing ciphers thereto.

For the denominator of the product being an unit, prefixed to as many ciphers, as the denominators of the multiplier and multiplicand contain of ciphers, it follows, that the places of decimals in the product, will be as many as in the numbers

from whence it arose.

EXAMPLES.

DECIMAL FRACTIONS.

Multiply 121.6 by 2.76 2.76

> 7296 8512 2432

Product = 335.616

Multiply .0089789 by 1085 Product = 9.7421065

Multiply .248723 by .13587 Product = .03379399401.

DIVISION OF DECIMALS.

Divide as in whole numbers; observing that the divisor and quotient together must contain as many decimal places as there are in the dividend. If. therefore, the dividend have just as many places of decimals as the divisor has, the quotient will be a whole number without any decimal figures. If there be more places of decimals in the dividend, than there are in the divisor, point off as. many figures in the quotient for decimals, as the decimal places in the dividend exceed those in the divisor; the want of places in the quotient being supplied by prefixing ciphers. But if there be more decimal places in the divisor, than in the dividend, annex ciphers to the dividend, so that the decimal places here may be equal, in number, to those in the divisor; and then the quotient will be a whole number, without fractions.

When there is a remainder, after the division has been thus performed, annex ciphers to this remainder, and continue the operation till nothing remains, or till a sufficient number of decimals shall be found in the quotient.

DECIMAL FRACTIONS:

EXAMPLES.

Divide .144 by .12

.12).144(1.2 = quotient.

Divide 63.72413456922 by 2718 2718)63.72413456922(.02344522979 = quotient.

There being 11 decimal figures in the dividend, and none in the divisor, 11 figures are to be cut off in the quotient; but as the quotient itself consists of but 10 figures, prefix to them a cipher to complete that number.

Divide 1.728 by .012

.012)1.728(144 = quotient.

Because the number of decimal figures in the divisor and dividend, are alike, the quotient will be integers.

Divide 2 by 3.1416

3.1416)2.0000,0(0.636618+=quotient.

1 8849 6

9012+

In this example there are four decimal figures in the divisor, and none in the dividend; therefore, according to the rule, four ciphers are annexed to the dividend, which in this condition, is yet less than the divisor. A cipher must then be put in the quotient, in the place of integers, and other ciphers annexed to the dividend; and the division being now performed, the decimal figures of the quotient are obtained.

Divide	7234.5 by 6.5 Quotient=1113.
Divide	476.520 by .423 ——== 1126.5+
Divide	.45695 by 12.5
Divide	2.3 by 96 ———————————————————————————————————
Divide	87446071 by .004387 —=19933000000.
Divide	.624672 by 482== .001296.

REDUCTION OF DECIMALS.

RÙLE I.

To reduce a Vulgar Fraction to a Decimal of the same value.

Having annexed a sufficient number of ciphers, as decimals, to the numerator of the vulgar fraction, divide by the denominator; and the quotient thence arising, will be the decimal fraction required.

EXAMPLES.

Reduce \(\frac{3}{4} \) to a decimal fraction. \(\frac{4}{3} \).00

.75 = decimal required.

For $\frac{3}{4}$ of one acre, mile, yard, or any thing, is equal to $\frac{1}{4}$ of 3 acres, miles, yards, &c. there-

fore if 3 be divided by 4, the quotient is the answer required.

Reduce $\frac{1}{2}$, $\frac{1}{3}$, $\frac{1}{4}$, $\frac{1}{4}$, and so on to $\frac{1}{40}$, to their corresponding decimal fractions; and in this operation the various modes of interminate decimals may be easily observed.

RULE II.

To reduce Quantities of the same, or of different Denominations to Decimal Fractions of higher denominations,

If the given quantity consist of one denomination only, write it as the numerator of a vulgar fraction; then consider how many of this make one of the higher denomination, mentioned in the question, and write this latter number under the former, as the denominator of a vulgar fraction. When this has been done, divide the numerator by the denominator, as directed in the foregoing rule, and the quotient resulting will be the decimal fraction required.

But if the given quantity contain several denominations, reduce them to the lowest term for the numerator; reduce likewise that quantity, whose fraction is sought, to the same denomination for the denominator of a vulgar fraction; then divide as before directed.

EXAMPLES.

Reduce 9 inches to the Decimal of a foot,

The foot being equal to 12 inches, the vulgar fraction will be $\frac{1}{12}$; then 12)9.00

.75=decimal frac-[tion required.

Reduce 8 inches to the decimal of a yard.
8 inches.

1 yard × 3 × 12 = 36 inches.
36)8.0(.22 + = Answer.

$$\frac{72}{80}$$

 $\frac{72}{8}$

Reduce 5 furlongs 12 perches to the decimal of a mile.

Reduce 21 minutes 54 seconds to the decimal of a degree. Ans. .365
Reduce .056 of a pole to the decimal of an Acre. Ans. .00035

Reduce 13 cents to the decimal of an Eagle. Ans. .013

Reduce 14 minutes to the decimal of a day. Ans. .00972+

Reduce 3 hours 46 minutes to the decimal of a week. Ans. .0224206+

RULE III.

To find the value of Decimal Fractions in terms of the lower denominations.

Multiply the given decimal by the number of the next lower denomination, which makes an integer of the present, and point off as many places at the right hand of the product, for a remainder, as there are figures in the given decimal. Multiply this remainder by the number of the next inferior denomination, and point off a remainder, as before. Proceed in this manner through all the parts of the integer, and the several denominations, standing on the left hand, are the value required.

EXAMPLES.

Required the value of .3375 of an acre.

 $\frac{4 = \text{number of roods}}{\text{[in an acre.}}$

1.3500

 $\frac{40 = \text{number of perch}}{\text{[es in a rood.]}}$

14.0000

The value, therefore, is 1 rood 14 perches.

What is the value of .6875 of a yard?

3=number of feet in a yard.

2.0625

12=number of inches in [a foot.

.7500

12=number of lines in _____ [an inch.

9.0000

The answer here is 2 feet 9 lines.

What is the value of .084 of a furlong? Ans. 3 per. 1 yd. 2 ft. 11 in.

What is the value of .683 of a degree? Ans. 40 m. 58 sec. 48 thirds.

What is the value of .0053 of a mile? Ans. I per. 3 yds. 2 ft. 5 in.+

What is the value of .036 of a day? Ans. 51' 50" 24"".

PROPORTION

IN DECIMAL FRACTIONS.

Having reduced all the fractional parts in the given quantities to their corresponding decimals, and having stated the three known terms, so that the fourth, or required quantity, may be as much greater, or less than the third, as the second term is greater, or less than the first, then multiply the second and third terms together, and divide the product by the first term, and the quotient will be the answer;—in the same denomination with the third term.

EXAMPLES.

If 3 acres 3 roods of land can be purchased for 93 dollars 60 cts. how much will 15 acres 1 rood cost at that rate?

3 acs. 3 rds. = 3.75 acres.15 acs. 1 rd. = 15.25 acres\$93, 60 cts. = \$93.60Then 3.75: 15.25:: 93.60: 15.25 468 00 - 18720 46800 9360 3.75)1427.4000(380.64=Answer. 1125 3024 3000 2400 2250 1500

If a clock gain 14 seconds in 5 days 6 hours, how much will it gain in 17 days 15 hours? Ans. 47 seconds.

1500

If 187 dollars 85 cents gain 12 dollars 33 cents interest in a year, at what rate per cent is this interest? Ans. 6.56+

SECTION II.

INVOLUTION AND EVOLUTION.

Involution is the method of raising any number, considered as the root, to any required power.

Any number, whether given, or assumed at pleasure, may be called the root, or first power of this number; and its other powers are the products, that result from multiplying the number by itself, and the last product by the same number again; and so on to any number of multiplications.

The index, or exponent, is the number donoting the height, or degree of the power, being always greater by one, than the number of multiplications employed in producing the power. It is usually written above the root, as in the following example, where the method of involution is plainly exhibited.

Required the fifth power of 8 } the root, or first first multiply by - - 8 } = power.

then multiply the product $64 = 8^{\circ} = \text{square}$, or by $8 = \{\text{second power.}\}$

&c. $512 = 8^3 = \text{cube}$, or third power.

4096 = 84= biquadrate 8 [or fourth power.

 $32768 = 8^{s} = Answer.$

EXAMPLES FOR EXERCISE.

What is the second power of 3.05? Ans. 9.3025 What is the third power of 85.3? Answer, 620650.477

What is the fourth power of .073? Answer, 090028398241

What is the eighth power of .09? Answer, .00.00.00,0043046721

Note. When two, or more powers are multiplied together, their product is that power, whose index is the sum of the indices of the factors, or powers multiplied.

Evolution is the method of extracting any re-

quired root from any given power.

Any number may be considered as a power of some other number; and the required root of any given power is that number, which, being multiplied into itself a particular number of times, produces the given power; thus if 81 be the given number, or power, its square, or second root, is 9; because $9 \times 9 = 9^2 = 81$; and 3 is its biquadrate, or fourth root, because $3 \times 3 \times 3 \times 3 = 3^4 = 81$. Again, if 729 be the given power, and its cube root be required, the answer is 9, for $9 \times 9 \times 9 = 729$; and if the sixth root of that number be required, it is found to be 3, for $3 \times 3 \times 3 \times 3 \times 3 = 729$.

The required power of any given number, or root, can always be obtained exactly, by multiplying the number continually into itself; but there are many numbers, from which a proposed root can never be completely extracted;—yet by approximating with decimals, these roots may be found as exact as necessity requires. The roots that are found complete, are denominated rational roots, and those, which cannot be found completed, or which only approximate, are called surd, or irrational roots.

Roots are usually represented by these characters or exponents;

√, or ‡ which signifies the square root; thus,

$$\checkmark$$
 9, or 9½ = 3
 \checkmark or \checkmark cube root; \checkmark 64, or 64 \checkmark = 4
 \checkmark , or \checkmark biquadrate root; \checkmark 16, or 16 \checkmark = 2 &c.

Likewise 8³ signifies the square root of 8 cubed; and, in general, the fractional indices imply, that the given numbers are to be raised to such powers as are denoted by their numerators, and that such roots are to be extracted from these powers, as are denoted by their denominators.

RULE

For extracting the Square Root.

Separate the given number into periods of two figures, by putting a point over the place of units, another over the place of hundreds, and so on, over every second figure, both toward the left hand in whole numbers, and toward the right hand in the Decimal places.—When the number of integral places is odd, the first, or left hand period, will consist of one figure only.

Find the greatest square in the first period on the left hand, and write its root on the right hand of the given number, in the manner of a quotient

figure in division.

Subtract the square, thus found, from the said period, and to the remainder annex the two figures of the next following period, for a dividend.

Double the root above mentioned for a divisor, and find how often it is contained in the said dividend, exclusive of its right hand figure, and set this quotient both in the place of the quotient and in the divisor.—The best way of doubling the root, to form each new divisor, is to add the last figure always to the last divisor, as it is done in the subsequent examples.

Multiply the whole augmented divisor by this last quotient figure, and subtract the product from the said dividend, bringing down to it the next period of the given number for a new dividend.

Repeat the same operation again; that is, find another new divisor, by doubling all the figures now found in the root; from which, and the last dividend, find the next figure of the root as before; and so on through all the periods to the last.

- Note 1. After the figures belonging to the given number are all exhausted, the operation may be continued in decimals, by annexing any number of periods or ciphers to the remainder.
- 2. The number of integral places in the root, is always equal to the number of periods in the integral part of the resolvend.
- 3. When vulgar fractions occur in the given power, or number, they may be reduced to decimals, then the operation will be the same as before dictated.

EXAMPLES.

Required the square root of 1710864.

Required the square root of 16007.3104.

1 16007.31	 104(126.52=Answer.
22 60 2 44	
246 1607 6 1476	
2525 1313 5 1262	
25302 506 506	04 04
·	

EXAMPLES FOR EXERCISE.

Required the square root of 298116. Ans. 546. Required the square root of 348.17320836. Ans. 18.6594.

Required the square root of 17.3056. Ans. 4.16. Required the square root of .000729. Ans. .027. Required the square root of 17% Ans. 4.168333+

A GENERAL RULE

For extracting any Root whatever.

Find by trial a number, which, when involved to the power denoted by the index of the required root, shall come nearest to the given number, whether greater or less; and let that number be called the assumed root, and when thus involved, the assumed power.

Let the given power, or number be represented by	G.
the index, or exponent, in the question by the assumed power, by	X.
the assumed root, by	Q.
and the required root by	R.

Then $\overline{X+1} \times A + \overline{X-1} \times G : \overline{X+1} \times G + \overline{X-1} \times A :: Q : R.$

That is, as the sum of X+1 times A and X—1 times G,

is to the sum of X+1 times G and X-1 times A,

so is the assumed root, Q,

to the required root, R,—nearly; and the operation may be repeated as many times as we chuse, by using always the root last found for the assumed root, and this, involved according to the given index, for the assumed power.*

EXAMPLES.

1. Required the Cube root of 789.

"" This is a very general approximating rule," says Dr. Hutton, "of which that for the cube root is a particular case, and is the best adapted for practice and for memory, of any that I have yet seen. It was first discovered in this form by myself, and the investigation and use of it were given at large in my Tracts—page 45 &cc."

Here G=789, X=3, Q=9, A=9 =729, $\overline{X+1}$ =4 and $\overline{X-1}$ =2. And $4 \times 729 = 2916$ $4 \times 789 = 3156$ $2 \times 789 = 1578$ $2 \times 729 = 1458$ Then 4494 : 4614 :: 9 : 9.240+9

4494)41526(9.2403+[Ans. 40446

918 &c.

13482

In the foregoing example the answer is strictly correct in its integral part and also in the three first decimal places; but if more decimals were wanted, and if their exactness were likewise requisite, the present answer might be taken for the assumed root, and the whole operation should be repeated.

2. Required the biquadrate root of 2.0743.

Here G=2.0743, Q=1.2,A= $\overline{1.2}$ =2.0736, X=4, $\overline{X+1}$ =5, and $\overline{X-1}$ =3. And $5 \times 2.0736 = 10.3680$ $5 \times 2.0743 = 10.3715$ $3 \times 2.0743 = 6.2229$ $3 \times 2.0736 = 6.2208$ Then 16.5909 : 16.5923

:: 1.2: 1.2001+Ans.

Required the fifth root of 21035.8 Ans. =7.3213±
Required the sixth root of 21035.8 Ans. =5.2540±
Required the cube root of 999 Ans. =9.9966±
Required the fourth root of 97.41 Ans. =3.1416
Required the cube root of .037 Ans. =.33322±
Required the cube root of 2 Ans. =1.2599±
Required the seventh root of 21035.8 Answer=
[4.1454.

SECTION III.

OF LOGARITHMS.

LOGARITHMS are a series of numbers, so contrived, that by them the work of multiplication may be performed by addition; and the operation of division may be done by subtraction. Or,—Logarithms are the indices, or series of numbers in arithmetical progression, corresponding to another series of numbers in geometrical progression. Thus,

(0,1,2,3, 4, 5, 6,&c. Indices or Logarithms. (1,2,4,8,16,32,64,&c. Geometrical progression. Or.

(0, 1, 2, 3, 4, 5, 6, &c. Ind. or Log. (1, 3, 9, 27, 81, 243, 729, &c. Geometrical Series.

(0, 1, 2, 3, 4, 5, 6,&c.I.orL. 1, 10, 100, 1000, 10000, 100000, 1000000, &c. Geometrical series,—where the same indices serve equally for any Geometrical series, or progression.

Hence it appears that there may be as many kinds of indices, or logarithms, as there can be taken kinds of geometrical series. But the Logarithms most convenient for common uses are those adapted to a geometrical series increasing in a ten-fold progression, as in the last of the foregoing

examples.

In the geometrical series 1, 10, 100, 1000, &c. if between the terms 1 and 10, the numbers 2, 3, 4, 5, 6, 7, 8, 9 were interposed, indices might also be adapted to them in an arithmetical progression, suited to the terms interposed between 1 and 10, considered as a geometrical progression. Moreover, proper indices may be found to all the numbers, that can be interposed between any two terms of the Geometrical series.

But it is evident that all the indices to the numbers under 10, must be less than 1; that is, they must be fractions. Those to the numbers between 10 and 100, must fall between 1 and 2; that is, they are mixed numbers, consisting of 1 and some fraction. Likewise the indices to the numbers between 100 and 1000, will fall between 2 and 3; that is, they are mixed numbers, consisting of 2 and some fraction; and so of the other indices.

Hereafter the integral part only of these indices will be called the Index; and the fractional part will be called the Logarithm. The computation of these fractional parts, is called making Logarithms; and the most troublesome part of this work is to make the Logarithms of Prime Numbers, or those which cannot be divided by any other numbers than themselves and unity.

RULE

For Computing the Logarithms of Numbers.

Let the sum of its proposed number and the next less number be called A. Divide 0.8685889638׆

[†] The number 0.86858896384 is the quotient of 2 divided by 2.302585093, which is the logarithm of 10, according to the first

by A, and reserve the quotient. Divide the reserved quotient by the square of A, and reserve this quotient. Divide the last reserved quotient by the square of A, reserving the quotient still; and thus proceed as long as division can be made. Write the reserved quotients orderly under one another, the first being uppermost. Divide these quotients respectively by the odd numbers 1, 3, 5, 7, 9, 11, &c.; that is, divide the first reserved quotient by 1, the second by 3, the third by 5, the fourth by 7, &c. and let these quotients be written orderly under one another; add them together, and their sum will be a logarithm. To this logarithm add the logarithm of the next less number, and the sum will be the logarithm of the number proposed.

form of Lord Napier, the inventor of logarithms. The manner in which Napier's logarithm of 10 is found, may be seen in most books of Algebra, but it is here omitted, because students of Surveying are too generally unacquainted with the principles of that science, and the subject is too extensive for the present treatise. Those, however, who have not an opportunity for entering thoroughly into this subject, may with more propriety grant the truth of one number, and thereby be enabled to try the correctness of any logarithm in the tables, than receive those tables, as truly computed, without any means of examining their accuracy.

EXAMPLE I.

Required the Logarithm of the number 2.

Here the next less number is 1, and 2+1=3= A. and A², or $3^2=9$; then

3)0.868588964

 $.9)0.289529654 \div 1 = 0.289529654$

9) $0.032169962 \div 3 = 0.010723321$

 $9)0.003574440 \div 5 = 0.000714888$

9) $0.000397160 \div 7 = 0.000056737$

 $9)0.000044129 \div 9 = 0.000004903$

 $9)0.000004903 \div 11 = 0.000000446$

9)0.000000545÷13=0.000000042

 $0.000000061 \div 15 = 0.000000004$

To this Logarithm 0.301029995 add the Logarithm of 1 = 0.000000000

Their Sum = 0.301029995 = Log. of 2.

The manner in which the division is here carried on, may be readily perceived by dividing, in the first place, the given decimal by A, and the succeeding quotients by A²; then letting these quotients remain in their situation, as seen in the example, divide them respectively by the odd numbers, and place the new quotients in a column by themselves. By employing this process, the operation is considerably abbreviated.

EXAMPLE 2.

Required the Logarithm of the number 3.

Here the next less number is 2; and 3+25=A, and $A^2=25$.

5)0.868588964

 $25)0.173717793 \div 1 = 0.173717793$

 $25)0.006948712 \div 3 = 0.002316237$

25)0.000277948 ÷ 5=0.000055599

 $25)0.000011118 \div 7 = 0.000001588$

25)0.000000445 ÷ 9=0.000000049

 $0.000000018 \div 11 = 0.000000002$

To this Logarithm 0.176091259 add the Logarithm of 2=0.301029995

Their Sum = 0.477121254 = Log. of 3.

Then, because the sum of the logarithms of numbers, gives the logarithm of their product; and the difference of the logarithms, gives the logarithm of the quotient of the numbers: from the two preceding logarithms, and the logarithm of 10, which is 1, a great many logarithms can be easily made, as in the following examples.

Example 3. Required the Logarithm of 4.

Since $4=2\times 2$, then to the Logarithm of 2=0.301029995 add the Logarithm of 2=0.301029995

The sum=Logarithm of 4=0.602059990

Example 4.	Required	ţhe	Logarithm	of	5.

10÷2 being=5, therefore from the Log. of 10=1.000000000 subtract the Log. of 2=0.301029995

the remainder is the Log. of 5=0.698970005

Example 5. Required the Logarithm of 6.

 $6=3\times2$, therefore to the Logarithm of 3=0.477121254 add the Logarithm of 2=0.301029995

their sun=Log. of 6=0.778151249

Example 6. Required the Logarithm of 8.

8=23, therefore multiply the Logarithm of 2=0.301029995 by 3

The product = Log. of 8=0.903089985

Example 7. Required the Logarithm of 9.

9=3, therefore the Logarithm of 3=0.477121254 being multiplied by 2

the product=Log. of 9=0.954242508

Example 8. Required the Logarithm of 7.

Here the next less number is 6, and 7+6=13= A, and $A^3=169$.

13)0.868588964

 $169)0.066814536 \div 1 = 0.066814536$

 $169)0.000395352 \div 3 = 0.000131784$

 $169)0.000002339 \div 5 = 0.000000468$

 $0.000000014 \div 7 = 0.0000000002$

To this Logarithm=0.066946790 add the Log. of 6=0.778151249

Their sum=
$$0.845098039$$
=Log. of 7.
of 12
of 14
of 15 is equal to the sum
of 16 of the Logs.
of 3 and 4.
of 3 and 5.
of 4 and 4.
of 3 and 6.
of 4 and 5.

The Logarithms of the prime numbers, 11, 13, 17, 19, &c. being computed by the foregoing general Rule, the Logarithms of the intermediate numbers are easily found by composition and division. It may, however, be observed, that the operation is shorter in the larger prime numbers; for when any given number exceeds 400, the first quotient, being added to the Logarithm of its next lesser number, will give the Logarithm sought, true to 8, or 9 places; and therefore it will be very easy to examine any suspected Logarithm in the Tables.

For the arrangement of Logarithms in a Table, the method of finding the Logarithm of any natural number, and of finding the natural number corresponding to any given Logarithm, therein: likewise for particular rules concerning the Indices, the reader will consult Table 1, with its explanation, at the end of this Treatise.

MULTIPLICATION,

Two, or more numbers being given, to find their product by Logarithms.

RULE.

Having found the Logarithms of the given numbers in the Table, add them together, and their sum is the Logarithm of the product; which Logarithm, being found in the Table, will give a na-

tural number, that is, the product required.

Whatever is carried from the decimal part of the Logarithm is to be added to the affirmative indices; but subtracted from the negative. Likewise the indices must be added together, when they are all of the same kind, that is, when they are all affirmative, or all negative; but when they are of different kinds, the difference must be found, which will be of the same denomination with the greater.

Example 1. Required the product of 86.25 multiplied by 6.48

Log. of 86.25=1.935759 Log. of 6.48=0.811575

Product=558.9=2.747334

Example 2. Required the product of 46.75 and .3275

Log. of 46.75 = 1.669782 Log. of .3275 = -1.515211

Product = 15.31 + = 1.184993

Example 3. Required the product of 3.768, 2.053 and .007693.

Log. of 3.768= 0.576111 Log. of 2.053= 0.312389 Log. of .007693=-3.886096

 $Product = .05951 \times = -2.774596$

Example 4. Required the product of 27.63, 1.859, .7258 and 0.3591.

Log. of 27.63 = 1.441381 Log. of 1.859 = 0.269279 Log. of .7258 = -1.860817 Log. of .03591 = -2.555215

Product nearly=1.339 = 0.126692

DIVISION.

Two numbers being given, to find how many times one is contained in the other, by Logarithms.

RULE.

From the Logarithm of the Dividend subtract the Logarithm of the Divisor, and the remainder will be the Logarithm, whose corresponding natural number will be the Quotient required.

In this operation, the Index of the Divisor must be changed from affirmative to negative, or from negative to affirmative; and then the difference of the affirmative and negative Indices must be taken for the index to the Logarithm of the Quotient. Likewise when one has been borrowed in the left hand place of the Decimal part of the Logarithm, add it to the Index of the Divisor, if affirmative; but subtract it, if negative; and let the

Index, thence arising, be changed and worked with, as before.

Example 1. Divide 558.9 by 6.48.

Log. of 558.9 =2.747334 Log. of 6.48 =0.811575

Quotient = 86.25 = 1.935759

Example 2. Divide 15.31 by 46.75.

Log. of 15.31 = 1.184975

Log. of 46.75= 1.669782

Quotient = .3275 = -1.515193

Example 3. Divide .05951 by .007693.

Log. of .05951 = -2.774590

Log. of .007693=-3.886096

Quotient=7.735 = 0.888494

Example 4. Divide .6651 by 22.5.

Log. of .6651 = -1.822887

Log. of 22.5 = 1.352183

Quotient = .02956 = -2.470704

PROPORTION,

Or the Rule of Three in Logarithms.

RULE.

Having stated the three given terms according to the rule in common Arithmetic, write them orderly under one another, with the signs of proportion; then add the Logarithms of the second and third terms together, and from their sum subtract the Logarithm of the first term, and the remainder will be the Logarithm of the fourth term, or Answer.

Or,—add together the Arithmetical Complement of the Logarithm of the first term, and the Logarithms of the second and third terms; the sum, rejecting 10 from the index, will be the Logarithm

of the fourth term, or term required.

N. B. The Arithmetical Complement of a Logarithm is what it wants of 10,000000, or 20,000000, and the easiest way to find it is to begin at the left hand, and subtract every figure from 9, except the last, which should be taken from 10; but if the index exceed 9, it must be taken from 19.—It is frequently used in the rule of Proportion and Trigonometrical calculations, to change Subtractions into Additions.

EXAMPLES.

1st. If a clock gain 14 seconds in 5 days 18 hours, how much will it gain in 17 days 15 hours?

5.75 days : Log.=0.759668

17.625 days :: Log.=1.246129 14 Seconds :: Log.=1.146128

2.392257

 \triangle nswer=42". 91 = 1.632589

Or thus; 5.75 days: Arith. Co. Log. = 9.240332

17.625 :: Log.=1.246129 14 Seconds: Log.=1.146128

Answer=42". 91 =1.632589

2d. Find a fourth proportional to 9.485, 1.969 and 347.2.

98.45 : Log.=1.993216

347.2 : Log.=2.540580 1.969 : Log.=0.294246

2.834826

Answer=6.944 = 0.841610

3d. What number will have the same proportion to .8538 as .3275 has to .0131

.0131 : Log. = -2.117271

.3275 :: Log.=-1.515211 .8538 : Log.=-1.931356

-1.446567

Answer=21.35= 1.329296

4th. Required a third proportional number to 9.642 and 4.821

9.642 : Log,=0.984167

4.821 : Log = 0.683137 4.821 : Log = 0.683137

1.366274

Answer=2,411 =0,382107

INVOLUTION.

To find any proposed power of a given number by Logarithms.

Rule. Multiply the Logarithm of the given number by the Index of the proposed power, and the

product will be the Logarithm, whose natural

number is the power required.

When a negative Index is thus multiplied, its product is negative, but what was carried from the decimal part of the Logarithm must be affirmative; consequently the difference is the index of the product, which difference must be considered of the same kind with the greater, or that which was made the minuend.

EXAMPLES.

1. What is the second power of 3.874?

Log. of 3.874=0.588160

Index = 2

Power required=15.01 =1,176320

2. Required the third power of the number 2.768.

Log. of 2.768=0.442166 Index = 3

Answer=21.21=1,326498

3. Required the second power of the number .2857.

Log. of .2857 = -1.455910 Index = 2

Answer = .08162 = -2.911820

4. Required the third power of the number .7916.

 $Log. of .791\hat{6} = -1.898506$ Index = 3

Answer = .4961 = -1.695518

EVOLUTION.

To extract any proposed Root of a given number by Logarithms.

RULE.

Find the Logarithm of the given number, and divide it by the Index of the proposed root; the quotient is a Logarithm, whose natural number is

the root-required.

When the index of the Logarithm to be divided, is negative, and does not exactly contain the divisor without some remainder, increase the index by such a number, as will make it exactly divisible by the index, carrying the units borrowed as so many tens to the left hand place of the decimal, and then divide as in whole numbers.

EXAMPLES.

1. Required the square root of 847. Index 2)2.927883=Log. of 847.

$$1.463941 = Quot = Log.of 29.103 + = ans.$$

2. Required the cube root of 847. Index 3)2.927883=Log. of the given number.

3. Required the square root of .093. Index 2)—2.968483—Log. of .093.

$$-1.484241 = Quot. = Log. of. 304959 = ans.$$

4. Required the cube root of 12345. Index 3)4.091491=Log. of 12345.

^{1.363830=}Quot.=Log. of 23.116.=Ans

SECTION IV.

ELEMENTS OF

PLANE GEOMETRY.

DEFINITIONS.

See PLATE I.

- 1. Geometry is that science wherein we consider the properties of magnitude.
- 2. A point is that which has no parts, being of itself indivisible; as A.
- 3. A line has length but no breadth; as AB. figures 1 and 2.
- 4. The extremities of a line are points, as the extremities of the line AB are the points A and B. figures 1 and 2.
- 5. A right line is the shortest that can be drawn between any two points, as the line AB. fig. 1. but if it be not the shortest, it is then called a curve line, as AB. fig. 2.
- 6. A superficies or surface is considered only as having length and breadth, without thickness, as *ABCD*. fig. 3.
 - 7. The extremities of a superficies are lines.
- 8. The inclination of two lines meeting one another (provided they do not make one continued

line) or the opening between them, is called an angle. Thus in fig. 4. the inclination of the line AB to the line BC meeting each other in the point B, or the opening of the two lines BA and BC, is called an angle, as ABC.

- Note, When an angle is expressed by three letters, the middle one is that at the angular point.
- 9. When the lines that form the angle are right ones, it is then called a right-lined angle, as ABC, fig. 4. If one of them be right and the other curved, it is called a mixed angle, as B. fig. 5. If both of them be curved, it is called a curved-lined or spherical angle, as C. fig. 6.
- 10. If a right line, CD (fig. 7.) fall upon another right line, AB, so as to incline to neither side, but make the angles ADC, CDB on each side equal to each other, then those angles are called right angles, and the line CD a perpendicular.
- 11. An obtuse angle is that which is wider or greater than a right one, as the angle ADE, fig. 7. and an acute angle is less than a right one, as EDB. fig. 7.
- 12. Acute and obtuse angles in general are called oblique angles.
- 13. If a right line CB. (fig. 8.) be fastened at the end C, and the other end B, be carried quite round, then the space comprehended is called a circle; and the curve line described by the point B, is called the circumference or the periphery of the circle; the fixed point C, is called its centre.

- 14. The describing line CB. (fig. 8.) is called the semidiameter or radius, so is any line from the centre to the circumference: whence all radii of the same or of equal circles are equal.
- 15. The diameter of a circle is a right line drawn thro' the centre, and terminating in opposite points of the circumference; and it divides the circle and circumference into two equal parts, called semicircles; and is double the radius, as AB or DE. fig. 8.
- 16. The circumference of every circle is supposed to be divided into 360 equal parts called degrees, and each degree into 60 equal parts called minutes, and each minute into 60 equal parts called seconds, and these into thirds, fourths, &c. these parts being greater or less as the radius is.
- 17. A chord is a right line drawn from one end of an arc or arch (that is, any part of the circumference of a circle) to the other; and is the measure of the arc. Thus the right line HG, is the measure of the arc HBG. fig. 8.
- 18. The segment of a circle is any part thereof, which is cut off by a chord: thus the space which is comprehended between the chord HG and the arc HBG, or that which is comprehended between the said chord HG and the arc HDAEG are called segments. Whence it is plain, fig. 8.
- 1. That any chord will divide the circle into two segments.
- 2. The less the chord is, the more unequal are the segments.

- 3. When the chord is greatest it becomes a diameter, and then the segments are equal; and each segment is a semicircle.
- 19. A sector of a circle is a part thereof less than a semicircle, which is contained between two radii and an arc: thus the space contained between the two radii *CH*, *CB*, and the arc *HB* is a sector. fig. 8.
- 20. The right sine of an arc, is a perpendicular line let fall from one end thereof, to a diameter drawn to the other end: thus *HL* is the right sine of the arc *HB*.

The sines on the same diameter increase till they come to the centre, and so become the radius; hence it is plain that the radius CD is the greatest possible sine, and thence is called the whole sine.

Since the whole sine CD (fig. 8.) must be perpendicular to the diameter (by def. 20.) therefore producing DC to E, the two diameters AB and DE cross one another at right angles, and thus the periphery is divided into four equal parts, as BD, DA, AE, and EB; (by def. 10.) and so BD becomes a quadrant or the fourth part of the periphery: therefore the radius DC is always the sine of a quadrant, or of the fourth part of the circle BD.

Sines are said to be of as many degrees as the arc contains parts of 360: so the radius being the sine of a quadrant becomes the sine of 90 degrees, or the fourth part of the circle, which is 360 degrees.

- 21. The versed sine of an arc is that part of the diameter that lies between the right sine and the circumference: thus LB is the versed sine of the arc HB. fig. 8.
- 22. The tangent of an arc is a right line touching the periphery, being perpendicular to the end of the diameter, and is terminated by a line drawn from the centre through the other end: thus BK is the tangent of the arc HB. fig. 8.
- 23. And the line which terminates the tangent, that is, CK, is called the secant of the arc HB. fig. 8.
- 24. What an arc wants of a quadrant is called the complement thereof: Thus **DH** is the complement of the arc **HB**. fig. 8.
- 25. And what an arc wants of a semicircle is called the supplement thereof: thus AH is the supplement of the arc HB. fig. 8.
- 26. The sine, tangent, or secant of the complement of any arc, is called the co-sine, co-tangent, or co-secant of the arc itself: thus FH is the sine, DI the tangent, and CI the secant of the arc DH: or they are the co-sine, co-tangent, or co-secant of the arc HB. fig. 8.
- 27. The sine of the supplement of an arc, is the same with the sine of the arc itself; for drawing them according to def. 20, there results the self-same line; thus *HL* is the sine of the arc *HB*, or of its supplement *ADII*. fig. 8.
- 28. The measure of a right-lined angle, is the arc of a circle swept from the angular point, and

contained between the two lines that form the angle: thus the angle HCB (fig. 8.) is measured by the arc HB; and is said to contain so many degrees as the arc HB does; so if the arc HB is 60 degrees, the angle HCB is an angle of 60 degrees.

Hence angles are greater or less according as the arc described about the angular point, and terminated by the two sides, contains a greater or less number of degrees of the whole circle.

- 29. The sine, tangent, and secant of an arc, is also the sine, tangent, and secant of an angle whose measure the arc is: thus because the arc HB is the measure of the angle HCB, and since HL is the sine, BK the tangent, and CK the secant, BL the versed sine, HF the co-sine, DI the co-tangent, and CI the co-secant, &c. of the arc BH; then HL is called the sine, BK the tangent, CK the secant, &c. of the angle HCB, whose measure is the arc HB. fig. 8.
- 30. Parallel lines are such as are equi-distant from each other, as AB, CD. fig. 9.
- 31. A figure if a space bounded by a line or lines. If the lines be right it is called a rectilineal figure, if curved it is called a curvilineal figure; but if they be partly right and partly curved lines, it is called a mixed figure.
- 32. The most simple rectilineal figure is a triangle, being composed of three right lines, and is considered in a double capacity; 1st, with respect to its sides; and 2d, to its angles.
- 33. In respect to its sides it is either equilateral, having the three sides equal, as A. fig. 10.

- 34. Or isosceles, having two equal sides, as B. fig. 11.
- 35. Or scalene, having the three sides unequal, as C. fig. 12.
- 36. In respect to its angles, it is either right-angled, having one right angle, as D. fig. 13.
- 37. Or obtuse angled, having one obtuse angle, as E. fig. 14.
- 38. Or acute angled, having all the angles acute, as F. fig. 15.
- 39. Acute and obtuse angled triangles are in general called oblique angled triangles, in all which any side may be called the base, and the other two the sides.
- 40. The perpendicular height of a triangle is a line drawn from the vertex to the base perpendicularly: thus if the triangle ABC, be proposed, and BC be made its base, then if from the vertex A the perpendicular AD be drawn to BC, the line AD will be the height of the triangle ABC, standing on BC as its base. Fig. 16.

Hence all triangles between the same parallels have the same height, since all the perpendiculars are equal from the nature of parallels.

- 41. Any figure of four sides is called a quadrilateral figure.
- 42. Quadrilateral figures, whose opposite sides are parallel, are called parallelograms: thus

ABCD is a parallelogram. Fig. 3. 17, and AB. fig. 18 and 19.

- 43. A parallelogram whose sides are all equal and angles right, is called a square, as ABCD. fig. 17.
- 44. A parallelogram whose opposite sides are equal and angles right, is called a rectangle, or an oblong, as *ABCD*. fig. 3.
- 45. A rhombus is a parallelogram of equal sides, and has its angles oblique, as A. fig. 18. and is an inclined square.
- 46. A rhomboides is a parallelogram whose opposite sides are equal and angles oblique; as *B*. fig. 19. and may be conceived as an inclined rectangle.
- 47. Any quadrilateral figure that is not a parallelogram, is called a trapezium. Plate 7. fig. 3.
- 48. Figures which consist of more than four sides are called polygons; if the sides are allequal to each other, they are called regular polygons. They sometimes are named from the number of their sides, as a five-sided figure is called a pentagon, one of six sides a hexagon, &c. but if their sides are not equal to each other, then they are called irregular polygons, as an irregular pentagon, hexagon, &c.
- 49. Four quantities are said to be in proportion when the product of the extremes is equal to that of the means: thus if A multiplied by D, be equal to B multiplied by C, then A is said to L to B as C is to D.

POSTULATES OR PETITIONS.

- 1. That a right line may be drawn from any one given point to another.
- 2. That a right line may be produced or continued at pleasure.
- 3. That from any centre and with any radius, the circumference of a circle may be described.
- 4. It is also required that the equality of lines and angles to others given, be granted as possible: that it is possible for one right line to be perpendicular to another, at a given point or distance; and that every magnitude has its half, third, fourth, &c. part.

Note, Though these postulates are not always quoted, the reader will easily perceive where, and in what sense they are to be understood.

AXIOMS or self-evident TRUTHS.

- 1. Things that are equal to one and the same thing, are equal to each other.
 - 2. Every whole is greater than its part. .
- 3. Every whole is equal to all its parts taken together.
- 4. If to equal things, equal things be added, the whole will be equal.
- 5. If from equal things, equal things be deducted, the remainders will be equal.

- 6. If to or from unequal things, equal things be added or taken, the sums or remainders will be unequal.
 - 7. All right angles are equal to one another.
- 8. If two right lines not parallel, be produced towards their nearest distance, they will intersect each other.
- 9. Things which mutually agree with each other, are equal.

NOTES.

A theorem is a proposition, wherein something is proposed to be demonstrated.

A problem is a proposition, wherein something is to be done or effected.

A lemma is some demonstration, previous and necessary, to render what follows the more easy.

A corollary is a consequent truth, deduced from a foregoing demonstration.

A scholium, is a remark or observation made upon something going before.

GEOMETRICAL THEOREMS.

THEOREM I.

Pz. 1, fig. 20.

IF a right line falls on another, as AB, or EB, does on CD, it either makes with it two right angles, or two angles equal to two right angles.

- 1. If AB be perpendicular to CD, then (by def. 10.) the angles CBA, and ABD, will be each a right angle.
- 2. But if EB fall slantwise on CD, then are the angles DBE+EBC=DBE+EBA (=DBA)+ ABC, or two right angles. Q. E. D.
- Corollary 1. Whence if any numbers of right lines were drawn from one point, on the same side of a right line; all the angles made by these lines will be equal to two right lines.
 - 2. And all the angles which can be made about a point, will be equal to four right angles.

THEO. II.

PL. 1. fig. 21.

If one right line cross another, (as AC does BD) the opposite angles made by those lines, will be equal to each other: that is, ABB to CED, and BEC to AED.

By theorem 1. BEC + CED = 2 right angles and CED + DEA = 2 right angles.

Therefore (by axiom 1.) BEC+CED=CED+

DEA: take CED from both, and there remains BEC=DEA. (by axiom 5.) Q. E. D.

After the same manner CED + AED = 2 right angles; and AED + AEB = two right angles; wherefore taking AED from both, there remains CED = AEB. Q. E. D.

THEO. III.

PL. 1. fig. 22.

If a right line cross two parallels, as GH dees AB and CD, then,

- 1. Their external angles are equal to each other, that is, GEB = CFH.
- 2. The alternate angles will be equal, that is, AEF = EFD and BEF = CFE.
- 3. The external angle will be equal to the internal and opposite one on the same side, that is, GEB = EFD and AEG = CFE.
- 4. And the sum of the internal angles on the same side, are equal to two right angles; that is, BEF + DFE are equal to two right angles, and AEF + CFE are equal to two right angles.
- 1. Since AB is parallel to CD, they may be considered as one broad line, crossed by another line, as GH; (then by the last thee.) GEB = CFH, and AEG = HFD.
- 2. Also GEB = AEF, and CFH = EFD; but GEB = CFH (by part 1. of this theo.) therefore AEF = EFD. The same way we prove FEB = EFC.
- 3. AEF=EFD; (by the last part of this theo.) but AEF=GEB (by theo. 2.) Therefore GEB=EFD. The same way we prove AEG=CFE.

4. For since GEB = EFD, to both add FEB, then (by axiom 4.) GEB + FEB = EFD + FEB, but GEB + FEB, are equal to two right angles (by theo. 1.) Therefore EFD + FEB are equal to two right angles: after the same manner we prove that AEF + CFE are equal to two right angles. Q.E.D.

THEO. IV.

PL. 1. fig. 23.

In any triangle ABC, one of its legs, as BC, being produced towards D, it will make the external angle ACD equal to the two internal opposite angles taken together. Viz. to B and A.

Through C, let CE be drawn parallel to AB; then since BD cuts the two parallel lines BA, CE; the angle ECD = B, (by part 3. of the last theo.) and again, since AC cuts the same parallels, the angle ACE = A (by part. 2. of the last.) Therefore ECD + ACE = ACD = B + A. Q. E. D.

THEO. V.

PL. 1. fig. 23.

In any triangle ABC, all the three angles, taken together, are equal to two right angles, viz. A + B + ACB = 2 right angles.

Produce CB to any distance, as D, then (by the last) ACD = B + A; to both add ACB; then ACD + ACB = A + B + ACB; but ACD + ACB = 2 right angles (by theo. 1.); therefore the three angles A + B + ACB = 2 right angles. Q.E.D.

Cor. 1. Hence if one angle of a triangle be known, the sum of the other two is also known: for since the three angles of every triangle contain two right ones, or 180 degrees, therefore 180 —the given angle will be equal to the sum of the other two; or 180—the sum of two given angles, gives the other one.

Cor. 2. In every right-angled triangle, the two acute angles are = 90 degrees, or to one right angle: therefore 90 — one acute angle, gives the other.

THEO. VI.

PL. 1. fig. 24.

If in any two triangles, ABC, DEF, there be two sides, AB. AC in the one, severally equal to DE, DF in the other, and the angle A contained between the two sides in the one, equal to D in the other; then the remaining angles of the one, will be severally equal to those of the other, viz. B = E and C = F: and the base of the one BC, will be equal to EF, that of the other.

If the triangle ABC be supposed to be laid on the triangle DEF, so as to make the points A and B coincide with D and E, which they will do, because AB = DE (by the hypothesis); and since the angle A = D, the line AC will fall along DF, and inasmuch as they are supposed equal, C will fall in F; seeing therefore the three points of one coincide with those of the other triangle, they are manifestly equal to each other; therefore the angle B = E and C = F, and BC = EF. Q. E. D.

LEMMA.

Ps. 1. fig. 11.

If two eider of a triangle a b c be equal to each other, that is, ac = cb, the angles which are opposite to those equal sides, will also be equal to each other; viz. a = b.

For let the triangle a b c be divided into two

triangles a c d, d c b, by making the angle a c d = d c b (by postulate 4.) then because a c = b c, and cd common, (by the last) the triangle a d c = d c b; and therefore the angle a = b. Q. E. D.

Cor. Hence if from any point in a perpendicular which bisects a given line, there be drawn right lines to the extremeties of the given one, they with it will form an isosceles triangle.

THEO. VII.

PL. 1. fig. 25.

The angle BCD at the centre of a circle ABED, is double the angle BAD at the circumference, standing upon the same are BED.

Through the point A, and the centre C, draw the line ACE: then the angle ECD = CAD, + CDA; (by theo. 4.) but since AC=CD being radii of the same circle, it is plain (by the preceding lemma) that the angles subtended by them will be also equal, and that their sum is double to either of them, that is, DAC + ADC is double to CAD, and therefore ECD is double to CAD; after the same manner BCE is double to CAB, wherefore, BCE + ECD, or BCD is double to BAC + CAD or to BAD. Q. E. D.

Cor. 1. Hence an angle at the circumference is measured by half the arc it subtends or stands on.

Fig. 26.

Cor. 2. Hence all angles at the circumference of a circle which stands on the same chord as AB, are equal to each other, for they are all measured by half the arc they stand on, vis. by half the arc AB.

Fig. 26.

Cor. 3. Hence an angle in a segment greater than a semicircle is less than a right angle; thus ADB is measured by half the arc AB, but as the arc AB is less than a semicircle, therefore half the arc AB, or the angle ADB is less than half a semicircle, and consequently less than a right angle.

Fig. 27.

Cor. 4. An angle in a segment less than a semicircle, is greater than a right angle, for since the arc AEC is greater than a semicircle, its half, which is the measure of the angle ABC, must be greater than half a semicircle, that is, greater than a right angle.

Fig. 28.

Cor. 5. An angle in a semicircle is a right angle, for the measure of the angle ABD, is half of a semicircle AED, and therefore a right angle.

THEO. VIII.

PL. 1. fig. 29.

If from the centre C of a circle ABE, there be let fall the fierhendicular CD on the chord AB, it will bisect it in the point D.

Let the lines AC and CB be drawn from the centre to the extremities of the chord, then since CA = CB, the angles CAB = CBA (by the lemma.) But the triangles ADC, BDC are right angled ones, since the line CD is a perpendicular; and so the angle ACD = DCB; (by cor. 2. theo. 5.) then have we AC, CD, and the angle ACD in one triangle; severally equal to CB, CD, and the angle

BCD in the other: therefore (by theo. 6.) A = DB. Q. E. D.

Cor. Hence it follows, that any line bisecting a chord at right angles, is a diameter; for a line drawn from the centre perpendicular to a chord, bisects that chord at right angles; therefore, conversely, a line bisecting a chord at right angles must pass through the centre, and consequently be a diameter.

THEO. IX.

PL. 1. fig. 29.

If from the centre of a circle ABE there be drawn a perpendicular CD on the chord AB, and produced till it meets the circle in F, that line CF, will bisect the arc AB in the point F.

Let the lines AF and BF be drawn, then in the triangles ADF, BDF; AD=BD (by the last;) DF is common, and the angle ADF=BDF being both right, for CD or DF is a perpendicular. Therefore (by theo. 6.) AF=FB; but in the same circle, equal lines are chords of equal arcs, since they measure them (by def. 19.): whence the arc AF=FB, and so AFB is bisected in F, by the line CF.

Cor. Hence the sine of an arc is half the chord of twice that arc. For AD is the sine of the arc AF, (by def. 22.) AF is half the arc, and AD half the chord AB (by theo. 8.) therefore the corollary is plain.

THEO. X.

PL. 1. fig. 30.

In any triangle ABD, the half of each side is the sine of the opposite angle.

Let the circle ADB be drawn through the points A, B, D; then the angle DAB is measured by half the arc BKD, (by cor 1 theo. 7.) viz. the chord of BK is the measure of the angle BAD; therefore (by cor. to the last) BE the half of BD is the sine of BAD: the same way may be proved that half of AD is the sine of ABD, and the half of AB the sine of ADB. Q. E. D.

THEO. XL

PL. 1. fig. 22.

If a right line GH cut two other right lines AB, CD, so at to make the alternate angles AEF, EFD equal to each other, then the lines AB and CD will be parallel.

If it be denied that AB is parallel to CD, let IK be parallel to it; then IEF = (EFD) = AEF (by part 2. theo. 3.) a greater to a less, which is absurd, whence IK is not parallel; and the like we can prove of all other lines but AB; therefore AB is parallel to CD. Q. E. D.

THEO. XII.

PL. 1. fig. 3.

If two equal and parallel lines AB, CD, be joined by two other lines AD, BC, those shall be also equal and parallel.

Let the diameter or diagonal BD be drawn, and we will have the triangles ABD, CBD: whereof AB in one is=to CD in the other, BD common to both, and the angle ABD=CDB (by part 2 theo. 3.;) therefore (by theo. 6.) AD=CB, and the angle CBD=ADB, and thence the lines AD and BC are parallel, by the preceding theorem.

Cor. 1. Hence the quadrilateral figure ABCD is a parallelogram, and the diagonal BD bisects the

same, inasmuch as the triangle ABD = BCD, as now proved.

- Cor. 2. Hence also the triangle ABD on the same base AB, and between the same parallels with the parallelogram ABCD, is half the parallelogram.
- Cor. 3. It is hence also plain, that the opposite sides of a parallelogram are equal; for it has been proved that ABCD being a parallelogram, AB will be = CD and AD = BC.

THEO. XIII.

PL. 1. fig. 31.

All parallelograms on the same or equal bases and between the same parallels, are equal to one another, that is, if BD = GH, and the lines BH and AF parallel, then the parallelogram ABDC = BDFE = EFHG.

For AC=BD=EF (by cor. the last;) to both add CE then AE=CF. In the triangles ABE, CDF; AB=CD and AE=CF and the angle BAE=DCF (by part 3. theo. 3.;) therefore the triangle ABE=CDF, (by theo. 6.) let the triangle CKE be taken from both, and we will have the trapezium ABKC=KDFE; to each of these add the triangle BKD, then the parallelogram ABCD=BDEF; in like manner we may prove the parallelogram EFGH=BDEF. Wherefore ABDC=BDEF=EFHG. Q. E. D.

Cor. Hence it is plain that triangles on the same or equal bases, and between the same parallels, are equal, seeing (by cor. 2. theo. 12.) they are the halves of their respective parallelogram.

THEO. XIV.

PL. 1. fig. 32.

In every right-angled triangle, ABC, the equare of the hypothenuse or longest side, BC, or BCMH, is equal to the sum of the equares made on the other two sides AB and AC, that is, ABDE and ACGF.

Through A draw AKL perpendicular to the hypothenuse BC, join AH, AM, DC and BG; in the triangles, BDC, ABH, BD = BA, being sides of the same square, and also BC = BH, and the included angles DBC = ABH, (for DBA =CBH being both right, to both add ABC, then DBC = ABH) therefore the triangle DBC =ABH (by theo. 6.) but the triangle DBC is half of the square ABDE (by cor. 2 theo. 12.) and the triangle ABH is half the parallelogram BKLH. The same way it may be proved, that the square ACGF, is equal to the parallelogram KCLM. So ABDE + ACGF the sum of the squares = BKLH+ KCML, the sum of the two parallelograms or square BCMH; therefore the sum of the squares on AB and AC is equal to the square on BC. **Q**. **E**. **D**.

- Cor. 1. Hence the hypothenuse of a right-angled triangle may be found by having the sides; thus, the square root of the sum of the squares of the base and perpendicular, will be the hypothenuse.
- Cor. 2. Having the hypothenuse and one side given to find the other; the square root of the difference of the squares of the hypothenuse and given side, will be the required side.

THEO. XV.

Ps. 1. fig. 33.

In all circles the chord of 60 degrees is always equal in length to the radius.

Thus in the circle AEBD, if the arc AEB be an arc of 60 degrees, and the chord AB be drawn: then AB = CB = AC.

In the triangle ABC, the angle ACB is 60 degrees, being measured by the arc AEB; therefore the sum of the other two angles is 120 degrees (by Cor. 1. theo. 5.) but since AC=CB, the angle CAB=CBA (by lemma preceding theo. 7.) consequently each of them will be 60, the half of 120 degrees, and the three angles will be equal to one another, as well as the three sides: wherefore AB=BC=AC. Q. E. D.

Cor. Hence the radius, from whence the lines on any scale are formed, is the chord of 60 degrees on the line of chords.

THEO. XVI.

PL. 1. fig. 34.

If in two triangles ABC, abc, all the angles of one be each respectively equal to all the angles of the other, that is, A=a, B=b, C=c: then the sides opposite to the equal angles will be proportional, viz.

AB: ab:: AC: ac AB: ab:: BC: bc and AC: ac:: BC: be

For the triangles being inscribed in two circles, it is plain since the angle A=a, the arc $BDC=b\ d\ c$, and consequently the chord BC is to $b\ c$, as the radius of the circle ABC is to the radius of the circle $a\ b\ c$; (for the greater the radius is, the greater is the circle described by that radius; and consequently the greater any particular arc of that circle is, so the chord, sine, tangent, &c. of that arc will be also greater. Therefore, in general, the chord, sine, tangent, &c. of any arc is proportional to the radius of the circle;) the same way the chord

AB is to the chord ab, in the same proportion. So AB:ab::BC:bc; the same way the rest may be proved to be proportional.

THEO. XVIL

PL. 1. fig. 35.

If from a point A without a circle DBCE there be drawn two lines ADE, ABC, each of them cutting the circle in two points; the product of one whole line into its external part, viz. AC into AB, will be equal to that of the other line into its external part, viz. AE into AD.

Let the lines DC, BE, be drawn in the two triangles ABE, ADC; the angle AEB = ACD (by cor. 2. theo. 7.) the angle A is common, and (by cor. 1. theo. 5.) the angle ADC = ABE; therefore the triangles ABE, ADC, are mutually equiangular, and consequently (by the last) AC : AE :: AD : AB; wherefore AC multiplied by AB, will be equal to AE multiplied by AD. Q. E. D.

THEO. XVIIL

PL. 2. fig. 1.

Triangles ABC, BCD, and parallelograms ABCF and BDEC, having the same altitude, have the same proportion between themselves as their bases BA and BD.

Let any aliquot part of AB be taken, which will also measure BD: suppose that to be Ag, which will be contained twice in AB, and three times in BD, the parts Ag, gB, Bh, hi, and iD being all equal, and let the lines gC, hC, and iC, be drawn: then (by cor. to theo. 13.) all the small triangles AgC, gCB, BCh, &c. will be equal to each other; and will be as many as the parts into which their bases were divided; therefore it will be as the sum of the parts in one base, is to the

sum of those in the other, so will be the sum of the small triangles in the first, to the sum of the small triangles in the second triangle; that is, AB:BD:ABC:BDC.

Whence also the parallelograms ABCF and BDEC, being (by cor. 2. theo. 12.) the doubles of the triangles, are likewise as their bases. Q.E.D.

Note. Wherever there are several quantities connected with the sign (::) the conclusion is always drawn from the first two and last two proportionals,

THEO. XIX.

PL. 2. fig. 2,

Triangles ABC, DEF, standing upon equal bases AB and DE, are to each other as their altitudes CG and FH.

Let BI be perpendicular to AB and equal to CG, in which let KB = FH, and let AI and AK be drawn.

The triangle AIB = ACB (by cor. to theo. 13.) and AKB = DEF; but (by theo. 18.) BI: BK: ABI: ABK. That is, CG: FH: ABC: DEF, Q. E. D,

THEO. XX.

P L. 2. fig. 3.

If a right line BE be drawn parallel to one side of a triangle ACD, it will cut the two other sides proportionally, viz. AB; BC:: AE: ED.

Draw CE and BD; the triangles BEC and EBD being on the same base BE and under the same parallel CD, will be equal (by cor. to theo. 13.)

therefore (by theo. 18) AB : BC :: (BEA : BEC) or BEA : BED) :: AE : ED. Q. E. D.

- Cor. 1. Hence also AC: AB:: AD: AE:For AC: AB:: (AEC: AEB:: ABD: AEB):: AD: AE.
- Cor. 2. It also appears that a right line, which divides two sides of a triangle proportionally, must be parallel to the remaining side.
- Cor. 3. Hence also, theo. 16. is manifest; since the sides of the triangles \boldsymbol{ABE} , \boldsymbol{ACD} , being equiangular, are proportional.

THEO. XXI.

PL. 2. fig. 4.

If two triangles ABC, ADE, have an angle BAC, in the one, equal to an angle DAE, in the other, and the sides about the equal angles, proportional; that is, AB:AD:AC:AE; then the triangles will be mutually equiangular.

In AB take Ad = AD, and let de be parallel to BC, meeting AC in e.

THEO. XXIL

PL. 2. fig. 5.

Equiangular triangles ABC, DEP, are to one another in

a duplicate proportion of their homologous or like sides; or as the squares AK, and DM of their homologous sides.

Let the perpendiculars CG and FH be drawn as well as the diagonals BI and EL.

The perpendiculars make the triangles ACG and DFH equiangular, and therefore similar (by theo. 16.) for because the angle CAG=FDH, and the right angle AGC=DHF, the remaining angle ACG=DFH, (by cor. 2. theo. 5.)

Therefore GC: FH: (AC: DF::)AB: DE, or which is the same thing, GC: AB::FH: DE for FH multiplied by AB = AB multiplied by FH.

By theo. 19. ABC: ABI:: (CG: AI or AB as before:: FH DE or DL::) DFE: DLE, therefore <math>ABC: ABI:: DFE: DLE, or ABC: AK:: DFE: DM, for AK is double the triangle ABI, and DM double the triangle DEL, by cor. 2. theo. 12. Q.E.D.

THEO. XXIII.

PL. 2. fig. 6.

Like folygons ABCDE, a b c d e, are in a dufticate proportion to that of the sides AB, a b, which are between the equal angles A and B and a and b, or as the squares of the sides AB, ab.

Draw AD, AC, ad, ac.

By the hypothesis AB : ab :: BC : bc, and thereby also the angle B = b; therefore (by theo. 21.) BAC = b a c; and ACB = a c b: in like manner EAD = e a d, and EDA = e da. If therefore from the equal angles A, and a, we take the equal ones

EAD + BAC = e a d, + b a c the remaining angle DAC = dac, and if from the equal angles D and d, EDA = e da, be taken, we shall have ADC = a dc: and in like manner if from C and c be taken BCA, = b c a, we shall have ACD = a c d; and so the respective angles in every triangle, will be equal to those in the other.

By theo. 22. ABC: a b c:: the square of AC to the square of ac, and also ADC: adc:: the square of AC, to the square of ac; therefore from equality of proportions ABC: abc:: ADC: a d c; in like manner we may shew that ADC: a d c: EAD: c a d: Therefore it will be as one antecedent is to one consequent, so are all the antecedents to all the consequents. That is, ABC is to abc as the sum of the three triangles in the first polygon, is to the sum of those in the last. Or ABC will be to abc, as polygon to polygon.

The proportion of ABC to abc (by the foregoing theo.) is as the square of AB is to the square of ab, but the proportion of polygon to polygon, is as ABC to abc, as now shown: therefore the proportion of polygon to polygon is as the square of AB to the square of ab.

THEO. XXIV.

PL. 1. fig. 8.

Let DHB be a quadrant of a circle described by the radius CB; HB an arc of it, and DH its complement; HL or FC the sine, FH or CL its co-sine, BK its tangent, DI its co-tangent; CK its secant, and CI its co-secant. Fig. 8.

1. The co-sine of an arc is to the sine, as the radius is to the tangent.

- 2. The radius is to the tangent of an arc, as the co-sine of it is to the sine.
- 3. The sine of an arc is to its co-sine, as the radius to its co-tangent;
- 4. Or the radius is to the co-tangent of an arc, as its sine to its co-sine.
- 5. The co-tangent of an arc is to the radius, as the radius to the tangent.
- 6. The co-sine of an arc is to the radius, as the radius is to the secant.
- 7. The sine of an arc is to the radius, as the tangent is to the secant.

The triangles CLH and CBK, being similar, (by theo. 16.)

- 1. CL : LH : : CB : BK.
- 2. Or, CB : BK : : CL : LH.

The triangles CFH and CDI, being similar.

- 3. CF (or LH): FH: CD: DI.
- **4.** CD : DI : CF (or LH) : FH.

The triangles CDI and CBK are similar: for the angle CID = KCB, being alternate ones (by part 2, theo. 3.) the lines CB and DI being parallel: the angle CDI = CBK being both right, and consequently the angle DCI = CKB, wherefore,

5. DI : CD :: CB : BK.

And again, making use of the similar triangle CLH and CBK.

6. CL : CB : : CH : CK.

7. HL: CH: BK: CK.

GEOMETRICAL PROBLEMS.

PROB. I.

PL. 2. fig. 7.

To make a triangle of three given right lines BO, LB, LO, of which any two must be greater than the third.

Lay BL from B to L; from B with the line BO, describe an arc, and from L with LO describe another arc; from O, the intersecting point of those arcs, draw BO and OL, and BOL is the triangle required.

This is manifest from the construction.

PROB. II.

Pt. 2. fig. 8.

At a point B in a given right line BC, to make an angle equal to a given angle A.

Draw any right line ED to form a triangle, as EAD, take BF = AD, and upon BF make the triangle BFG, whose side BG = AE, and GF = ED (by the last) then also the angle B = A; if we suppose one triangle be laid on the other, the sides

will mutually agree with each other, and therefore be equal; for if we consider these two triangles to be made of the same three given lines, they are manifestly one and the same triangle.

Otherwise,

Upon the centres A and B, at any distance, let two arcs, DE, FG, be described; make the arc FG = DE, and through B and G draw the line BG, and it is done.

For since the chords ED, GF, are equal, the angles A and B are also equal, as before (by def.17.)

PROB. III.

PL. 2. fig. 9.

To bisect or divide into two equal parts, any given rightlined angle, BAC.

In the lines AB and AC, from the point A set off equal distances AE,=AD, then, with any distance more than the half of DE, describe two arcs to cut each other in some point F; and the rightline AF, joining the points A and F, will bisect the given angle BAC.

For if DF and FE be drawn, the triangles ADF, AEF, are equilateral to each other, viz. AD=AE, DF=FE, and AF common, wherefore DAF=EAF, as before.

PROB. IV.

PL. 2. fig. 10.

To bisect a right-line. AB.

With any distance, more than half the line, from

A and B, describe two circles CFD, CGD, cutting each other in the points C and D; draw CD intersecting AB in E, then AE = EB.

For, if AC, AD, BC, BD, be drawn, the triangles ACD, BCD, will be mutually equilateral, and consequently the angle ACE=BCE: therefore the triangle ACE, BCE, having AC=BC, CE common, and the angle ACE=BCE; (by theo. 6.) the base AE the base BE.

Cor. Hence it is manifest, that CD not only bisects AB, but is perpendicular to it, (by def. 11.)

PROB. V.

PL. 2. fig. 11.

On a given point A, in a right line EF, to erect a perpendicular.

From the point A lay off on each side, the equal distances, AC, AD; and from C and D, as centres, with any interval greater than AC or AD, describe two arcs intersecting each other in B; from A to B draw the line AB, and it will be the perpendicular required.

For, let CB, and BD be drawn; then the triangles CAB, DAB, will be mutually equilateral and equiangular, so CAB = DAB, a right angle, (by def. 10.)

PROB. VI.

PL. 2. fig. 12.

To raise a perpendicular on the end B of a right line AB.

From any point D not in the line AB, with the distance from D to B, let a circle be described cut-

ting AB in E; draw from E through D the right line EDC, cutting the periphery in C, and join CB; and that is the perpendicular required.

EBC being a semicircle, the angle EBC will be a right angle (by cor. 5. theo. 7.)

PROB. VII.

PL. 2. fig. 13.

From a given point A, to let fall a perpendicular upon a given right line BC.

From any point D, in the given line, take the distance to the given point A, and with it describe a circle AGE, make GE=AG, join the points A and E, by the line AFE, and AF will be the perpendicular required.

Let DA, DE, be drawn; the angle ADF=FDE, DA=DE, being radii of the same circle, and DF common; therefore (by theo. 6.) the angle DFA=DFE, and FA a perpendicular. (By def. 10.)

PROB. VIII.

PL. 2. fig. 14.

Through a given point A, to draw a right line AB, parallel to a given right line CD.

From the point A, to any point F, in the line CD, draw the line AF; with the interval FA, and one foot of the compasses in F, describe the arc AE, and with the like interval and one foot in A, describe the arc BF, making BF = AE; through A and B draw the line AB, and it will be parallel to CD.

By prob. 2. The angle BAF=AFE, and by theo. 11. BA and CD are parallel.

PROB. IX.

PL. 1. fig. 17.

Upon a given line AB to describe a square ABCD.

Make BC perpendicular and equal to AB; and from A and C, with the line AB, or BC, let two arcs be described, cutting each other in D; from whence to A and C, let the lines AD, DC be drawn; so is ABCD the square required.

For all the sides are equal by construction; therefore the triangles ADC and BAC, are mutually equilateral and equiangular, and ABCD is an equilateral parallelogram, whose angles are right. For B being right, D is also right, and DAC, DCA, BAC, ACB, each half a right angle, (by lemma preceding theo. 7. and cor. 2. theo. 5.) whence DAB and BCD will each be a right angle, and (by def. 44.) ABCD is a square.

SCHOLIUM.

By the same method a rectangle or oblong, may be described, the sides thereof being given.

PROB. X.

PL. 2. fig. 15.

To divide a given right line AB, into any proposed number of equal parts.

Draw the indefinite right line AP, making any angle with AB, also draw BQ parallel to AP, in

each of which, let there be taken as many equal parts AM, MN, &c. Bo, on, &c. as you would have AB divided into; then draw Mm, Nn, &c. intersecting AB in E, F, &c. and it is done.

For MN and mn being equal and parallel, FN will be parallel to EM; and in the same manner, GO to FN (by theo. 12.) therefore AM, MN, NO, being all equal by construction, it is plain (from theo. 10.) that AE, EF, FG, &c. will likewise be equal.

PROB. XI.

PL. 2. fig. 16.

To find a third proportional to two given right lines, A and B.

Draw two indefinite blank lines CE, CD, anywise to make any angle. Lay the line A, from C to F; and the line B, from C, to G; and draw the line FG; lay again the line A, from C to H; and through H, draw HI parallel to FG (by prob. 8.) so is CI the third proportional required.

For by cor. 1. theo. 20, CG: CH:: CF: CI.

Or, B:A::A:CI,

PROB. XII.

PL. 2. fig. 17.

Three right lines A, B, C, given to find a fourth proportional.

Having made an angle DEF anywise, by two indefinite blank right lines, ED, EF, as before; lay the line A; from E to G; the line B, from E to I; and draw the line IG; lay the line C, from E to

H, and (by prob. 8.) draw HK parallel thereto, so will EK be the fourth proportional required.

For, by cor. 1. theo. 20. EG: EI: EH: EK.

Or, A:B::C:EK.

PROB. XIII.

PL. 3. fig. 1.

Two right lines, A and B, given to find a mean proportional.

Draw an indefinite blank line, as AF, on which lay the line A, from B to B, and the line B, from B to C, on the point B, which is the joining point of the lines A and B; erect a perpendicular BD (by prob. 5.) bisect AC in E (by prob. 4.) and describe the semicircle ADC; and from the point D, where the periphery cuts the perpendicular BD, draw the line BD, and that will be the mean proportional required.

For if the lines AD, DC, be drawn, the angle ADC is a right angle (by cor. 5. theo. 7.) being an angle in a semicircle.

The angles ABD, DBC, are right ones (by def. 10.) the line BD being a perpendicular; wherefore the triangles ABD, DBC, are similar: thus the angle ABD = DBC, being both right, the angle DAC is the complement of BDA to a right angle (by cor. 2. theo. 5.) and is therefore equal to BDC, the angle ADC being a right angle as before; consequently (by cor. 1. theo. 5.) the angle ADB = DCB, wherefore (by theo. 16.)

AB:BD::BD:BC. Or, A:BD:BD:B.

PROB. XIV.

PL. 3. fig. 2. .

To divide a right line AB, in the point E, so that AE shall have the same proportion to EB, as two given lines C and D have.

Draw an indefinite blank line, AF, to the extremity of the line AB, to make with it any angle; lay the line C, from A to C; and D, from C to D; and join the points B and D, by the line BD; through C draw CE parallel to BD (by prob. 8.) so is E the point of division.

For, by cor. 1. theo. 20. AC: AD:: AE: AB. Or, C: D:: AE: EB.

PROB. XV.

PL. 3. fig. 3.

To describe a circle about a triangle ABC, or (which is the same thing) through any three points, A, B, C, which are not situated in a right line.

By prob. 4. Bisect the line AC by the perpendicular DE, and also CB, by the perpendicular FG, the point of intersection H, of these perpendiculars, is the centre of the circle required; from which take the distance to any of the three points A, B, C, and describe the circle ABC, and it is done.

For, by cor. to theo. 8. The lines DE and FG, must each pass through the centre, therefore, their point of intersection H, must be the centre.

SCHOLIUM.

By this method the centre of a circle may be found, by having only a segment of it given.

PROB, XVI.

PL. 3. fig. 4.

To make an angle of any number of degrees, at the point A, of the line AB, suppose of 45 degrees.

From a scale of chords take 60 degrees, for 60° is equal to the radius (by cor. theo. 15.) and with that distance from A, as a centre, describe a circle from the line AB; take 45 degrees, the quantity of the given angle, from the same scale of chords, and lay it on that circle from a to b; through A and b, draw the line AbC, and the angle A will be an angle of 45 degrees, as required.

If the given angle be more than 90°, take its half (or divide it into any two parts less than 90) and lay them after each other on the arc, which is described with the chord of 60 degrees; through the extremity of which, and the centre, let a line be drawn, and that will form the angle required, with the given line.

PROB. XVII.

P1, 3. fig. 5.

To measure a given angle, ABC.

If the lines which include the angle, be not as long as the chord of 60° on your scale, produce them to that or a greater length, and between them so produced, with the chord of 60° from B, describe the arc ed, which distance ed, measured on the same line of chords, gives the quantity of the angle BAC, as required; this is plain from def. 17.

PROB. XVIII.

PL. 3. fig. 6.

To make a triangle BCE equal to a given quadrilateral figure ABCD.

Draw the diagonal AC, and parallel to it (by prob. 8.) DE, meeting AB produced in E; then draw CE, and ECB will be the triangle required.

For the triangles ADC, AEC, being upon the same base AC, and under the same parallel ED, (by cor. to theo. 13.) will be equal, therefore if ABC be added to each, then ABCD = BEC.

PROB. XIX.

PL. 3. fig. 7,

To make a triangle DFH, equal to a given five-sided figure ABCDE.

Draw DA and DB, and also EH and CF, parallel to them (by prob. 8.) meeting AB produced in H and F; then draw DH, DF, and the triangle HDF is the one required.

For the triangle DEA = DHA, and DBC = DFB (by cor. to theo. 13.) therefore by adding these equations, DEA + DBC = DHA + DFB if to each of these ADB be added; then DEA + ADB + DBC = ABCDE = (DHA + ABD + DFB) = DHF.

PROB. XX.

PL. 3, fig. 8.

To project the lines of chords, sines, tangents and secants, with any radius.

On the line AB, let a semicircle ADB be described; let CDF be drawn perpendicular to this line from the centre C; and the tangent BE perpendicular to the end of the diameter; let the quadrants, AD, DB, be each divided into 9 equal parts, every one of which will be 10 degrees; if then from the centre C, lines be drawn through 10, 20, 30, 40, &c. the divisions of the quadrant BD, and continued to BE, we shall there have the tangents of 10, 20, 30, 40, &c. and the secants C 10, C 20, C 30, &c. are transferred to the line CF, by describing the arcs 10, 10: 20, 20: 30, 30, &c. If from 10, 20, 30, &c. the divisions of the quadrant BD, there be let fall perpendiculars, let these be transferred to the radius CB, and we shall have the sines of 10, 20, 30, &c. and if from A we describe the arcs 10, 10: 20, 20: 30, 30, &c. from every division of the arc AD: we shall have a line of chords. The same way we may have the sine, tangent, & c. to every single degree on the quadrant, by subdividing each of the 9 former divisions into 10 equal parts. By this method the sines, tangents, &c. may be drawn to any radius; and then, after they are transferred to lines on a rule, we shall have the scales of sines, tangents, &c. ready for use.

MATHEMATICAL

DRAWING INSTRUMENTS.

The strictness of geometrical demonstration admits of no other instruments, than a rule and a pair of compasses. But, in proportion as the practice of geometry was extended to the different arts, either connected with, or dependent upon it, new instruments became necessary, some to answer peculiar

purposes, some to facilitate operation, and others

to promote accuracy.

As almost every artist, whose operations are connected with mathematical designing, furnishes himself with a case of drawing instruments suited to his peculiar purposes, they are fitted up in various modes, some containing more, others, fewer instruments. The smallest collection put into a case, consists of a plane scale, a pair of compasses with a moveable leg, and two spare points, which may be applied occasionally to the compasses; one of these points is to hold ink; the other, a porte crayon, for holding a piece of black-lead pencil.

What is called a full pocket case, contains the

following instruments.

A pair of large compasses with a moveable point, an ink point, a pencil point, and one for dotting; either of those points may be inserted in the compasses, instead of the moveable leg.

A pair of plain compasses somewhat smaller

than those with the moveable leg.

A pair of bow compasses.

A drawing pen with a protracting pin in the upper part.

A sector.

A plain scale.

A protractor.

A parallel rule.

A pencil and screw-driver.*

* Large collections are called, magazine cases of instru-

ments; these generally contain

A pair of six inch compasses with a moveable leg, an ink point, a dotting point, the crayon point, so contrived as to hold a whole pencil, two additional pieces to lengthen occasionally one leg of the compasses, and thereby enable them to measure greater extents, and describe circles of a larger radius.

A pair of hair compasses.

A pair of bow compasses.

A pair of triangular compasses.

In a case with the best instruments, the protractor and plain scale are always combined. The instruments in most general use are those of six inches; instruments are seldom made longer, but often Those of six inches are, however, to be smaller. preferred, in general, before any other size; they will effect all that can be performed with the shortest ones, while, at the same time, they are better adapted to large work.

OF DRAWING COMPASSES.

Compasses are made either of silver or brass, but with steel points. The joints should always be framed of different substances; thus, one side, or part, should be of silver or brass, and the other of

A sector.

A parallel rule.

A protractor.

A pair of proportional compasses, either with or without an adjusting screw.

A pair of wholes and halves. Two drawing pens, and a pointril.

A pair of small hair compasses, with a head similar to those of the bow compasses.

A knife, a file, key, and screw-driver, or the compasses in one piece.

A small set of fine water colours.

To these some of the following instruments are often added.

A pair of beam compasses. A pair of gunners callipers.

A pair of elliptical compasses.

A pair of spiral ditto.

A pair of perspective compasses.

A pair of compasses with a micrometer screw.

A rule for drawing lines, tending to a centre at a great distante.

A protractor and parallel rule.

One or more parallel rules.

A pantographer, or Pentagraph.

A pair of sectoral compasses, forming, at the same time, a pair of beam and calliper compasses.

steel. The difference in the texture and pores of the two metals causes the parts to adhere less together, diminishes the wear, and promotes uniformity in their motion. The truth of the work is ascertained by the smoothness and equality of the motion at the joint, for all shake and irregularity is a certain sign of imperfection. The points should be of steel, so tempered, as neither to be easily bent or blunted; not too fine and tapering, and yet meeting closely when the compasses are shut.

As an instrument of art, compasses are so well known, that it would be superfluous to enumerate the various uses; suffice it then to say, that they are used to transfer small distances, measure given

spaces, and describe arches and circles.

If the arch or circle is to be described obscurely, the steel points are best adapted to the purpose; if it is to be in ink or black lead, either the draw-

ing pen, or crayon points are to be used.

To use a pair of compasses. Place the thumb and middle finger of the right hand in the opposite hollows in the shanks of the compasses, then press the compasses, and the legs will open a little way; this being done, push the innermost leg, with the third finger, elevating, at the same time, the furthermost, with the nail of the middle finger, till the compasses are sufficiently opened to receive the middle and third finger; they may then be extended at pleasure, by pushing the furthermost leg outwards with the middle, or pressing it inwards with the four finger. In describing circles, or arches, set one foot of the compasses on the centre, and then roll the head of the compasses between the middle and four finger, the other point pressing at the same time upon the paper. They should be held as upright as possible, and care should be taken not to press forcibly upon them, but rather to let them act by their own weight; the legs should never be so far extended, as to form

an obtuse angle with the paper or plane, on which

they are used.

The ink and crayon points have a joint just under that part which fits into the compasses; by this they may be always so placed as to be set nearly perpendicular to the paper; the end of the shank of the best compasses is framed so as to form a strong spring, to bind firmly the moveable points, and prevent them from shaking. This is found to be a more effectual method than that by a screw.

Two additional pieces are often applied to these compasses; these, by lengthening the leg, enable them to strike larger circles, or measure greater extents, than they would otherwise perform, and that without the inconveniences attending longer compasses. When compasses are furnished with this additional piece, the moveable leg has a joint, that it may be placed perpendicular to the paper.

The bow compasses, are a small pair, usually with a point for ink; they are used to describe small arches or circles, which they do much more conveniently than large compasses, not only on account of their size, but also from the shape of the head, which rolls with great ease between the fingers.

Of the drawing pen and protracting pin. The pen part of this instrument is used to draw strait lines: it consists of two blades with steel points fixed to a handle; the blades are so bent, that the ends of the steel points meet, and yet leave a sufficient cavity for the ink; the blades may be opened more or less by a screw, and, being properly set, will draw a line of any assigned thickness. One of the blades is framed with a joint, that the points may be separated, and thus cleaned more conveniently; a small quantity only of ink should be put at one time into the drawing pen, and this should be placed in the cavity, between the blades, by a common pen, or feeder; the drawing pen acts

better, if the pen, by which the ink is inserted, be made to pass through the blades. To use the drawing pen, first feed it with ink, then regulate it to the thickness of the required line by the screw. In drawing lines, incline the pen a small degree, taking care, however, that the edges of both the blades touch the paper, keeping the pen close to the rule, and in the same direction during the whole operation: the blades should always be wiped very clean, before the pen is put away.

These directions are equally applicable to the ink point of the compasses, only observing, that when an arch or circle is to be described, of more than an inch radius, the point should be so bent, that the blades of the pen may be nearly perpendicular to the paper, and both of them touch it at

the same time.

The protracting pin, is only a short piece of steel wire, with a very fine point, fixed at one end of the upper part of the handle of the drawing pen. It is used to mark the intersection of lines, or to set off divisions from the plotting scale, and protractor.

OF THE SECTOR.

Amidst the variety of mathematical instruments that have been contrived to facilitate the art of drawing, there is none so extensive in its use, or of such general application, as the sector. It is an universal scale, uniting, as it were, angles and parallel lines, the rule and the compass, which are the only means that geometry makes use of for measuring, whether in speculation or practice. The real inventor of this valuable instrument is unknown; yet of so much merit has the invention appeared, that it was claimed by Galileo, and disputed by nations.

This instrument derives its name from the tenth definition of the third book of *Euclid*, where he defines the sector of a circle. It is formed of two equal rules called legs; these legs are moveable about the centre of a joint, and will, consequently, by their different openings, represent every possible variety of plane angles. The distance of the extremities of these rules are the subtenses or chords.

or the arches they describe.

Sectors are made of different sizes, but their length is usually denominated from the length of the legs when the sector is shut. Thus a sector of six inches, when the legs are close together, forms a rule of 12 inches when opened; and a foot sector is two feet long, when opened to its greatest extent. In describing the lines usually placed on this instrument, I refer to those commonly laid down on the best six-inch brass sectors. But as the principles are the same in all, and the differences little more than in the number of subdivisions, it is to be presumed that no difficulty will occur in the application of what is here said to sectors of a larger radius.

The scales, or lines graduated upon the faces of the instrument, and which are to be used as sectoral lines, proceed from the centre; and are, 1. Two scales of equal parts, one on each leg, marked LIN. or L. Each of these scales, from the great extensiveness of its use, is called the line of lines.

2. Two lines of chords, marked cho. or c. 3. Two lines of secants, marked sec. or s. A line of polygons, marked pol. Upon the other face, the sectoral lines are, 1. Two lines of sines marked sin. or s. 2. Two lines of tangents, marked tan. 3. Between the lines of tangents and sines, there is another line of tangents to a lesser radius, to supply the defect of the former, and extending from

45° to 75°.

Each pair of these lines (except the line of polygons) is so adjusted as to make equal angles at the centre, and consequently at whatever distance the sector be opened, the angles will be always respectively equal. That is, the distance between 10 and 10 on the line of lines, will be equal to 60 and 60 on the line of chords, 90 and 90 on the line of sines, and 45 and 45 on the line of tangents.

Besides the sectoral scales, there are others on each face, placed parallel to the outward edges, and used as those of the common plain scale. There are on the one face, 1. A line of inches. 2. A line of latitudes. 3. A line of hours. 4. A line of inclination of meridians. 5. A line of chords. On the other face, three logarithmic scales, namely, one of numbers, one of sines, and one of tangents; these are used when the sector is fully opened, the legs forming one line.

To read and estimate the divisions on the sectoral lines. The value of the divisions on most of the lines are determined by the figures adjacent to them; these proceed by tens, which constitute the divisions of the first order, and are numbered accordingly; but the value of the divisions on the line of lines, that are distinguished by figures, is entirely arbitrary, and may represent any value that is given to them; hence the figures 1, 2, 3, 4, &c. may denote either 10, 20, 30, 40; or 100, 200, 300, 400, and so on.

The line of lines is divided into ten equal parts, numbered 1, 2, 3, to 10; these may be called divisions of the first order; each of these are again subdivided into 10 other equal parts, which may be called divisions of the second order; and each of these is divided into two equal parts, forming divisions of the third order.

The divisions on all the scales are contained between four parallel lines; those of the first order extend to the most distant; those of the third, to the least; those of the second, to the intermediate

parallel.

When the whole line of lines represents 100, the divisions of the first order, or those to which the figures are annexed, represent tens; those of the second order, units; those of the third order, the halves of these units. If the whole line represents ten, then the divisions of the first order are units; those of the second, tenths, and the thirds, twentieths.

In the line of tangents, the divisions to which the numbers are affixed, are the degrees expressed by those numbers. Every fifth degree is denoted by a line somewhat longer than the rest; between every number and each fifth degree, there are four divisions, longer than the intermediate adjacent ones, these are whole degrees; the shorter ones, or those of the third order, are 30 minutes.

From the centre, to 60 degrees, the line of sines is divided like the line of tangents; from 60 to 70, it is divided only to every degree; from 70 to 80, to every two degrees; from 80 to 90, the division

must be estimated by the eye.

The divisions on the line of chords are to be es-

timated in the same manner as the tangents.

The lesser line of tangents is graduated every two degrees from 45 to 50; but from 50 to 60, to every degree; from 60 to the end, to half degrees.

The line of secants from 0 to 10, is to be estimated by the eye; from 20 to 50 it is divided to every two degrees; from 50 to 60, to every degree; and from 60 to the end, to every half degree.

The solution of questions on the sector is said to be simple, when the work is begun and ended on the same line; compound, when the operation begins on one line, and is finished on the other.

The operation varies also by the manner in which the compasses are applied to the sector. If a measure be taken on any of the sectoral lines, beginning at the centre, it is called a lateral distance. But if the measure be taken from any point in one line, to its corresponding point on the line of the same denomination, on the other leg, it is called a transverse or parallel distance.

The divisions of each sectoral line are bounded by three parallel lines; the innermost of these is that on which the points of the compasses are to be placed, because this alone is the line which goes to the centre, and is alone, therefore, the sectoral

line.

We shall now proceed to give a few general instances of the manner of operating with the sector.

Multiplication by the line of lines. Make the lateral distance of one of the factors the parallel distance of 10; then the parallel distance of the

other factor is the product.

Example. Multiply 5 by 6, extend the compasses from the centre of the sector to 5 on the primary divisions, and open the sector till this distance become the parallel distance from 10 to 10 on the same divisions; then the parallel distance from 6 to 6, extended from the centre of the sector, shall reach to 3, which is now to be reckoned 30. At the same opening of the sector, the parallel distance of 7 shall reach from the centre to 35, that of 8 shall reach from the centre to 40, &c.

Division by the line of lines. Make the lateral distance of the dividend the parallel distance of the divisor, the parallel distance of 10 is the quotient. Thus, to divide 30 by 5, make the lateral distance of 30, viz. 3 on the primary divisions, the parallel distance of 5 of the same divisions; then the parallel distance of 10, extended from the centre,

shall reach to 6.

Proportion by the line of lines. Make the lateral distance of the second term the parallel distance

of the first term; the parallel distance of the third

term is the fourth proportional.

Example. To find a fourth proportional to 8, 4, and 6, take the lateral distance of 4, and make it the parallel distance of 8; then the parallel distance of 6, extended from the centre, shall reach

to the fourth proportional 3.

In the same manner a third proportional is found to two numbers. Thus, to find a third proportional to 8 and 4, the sector remaining as in the former example, the parallel distance of 4, extended from the centre, shall reach to the third proportional 2. In all these cases, if the number to be made a parallel distance be too great for the sector, some aliquot part of it is to be taken, and the answer multiplied by the number by which the first number was divided. Thus, if it were required to find a fourth proportional to 4, 8, and 6; because the lateral distance of the second term 8 cannot be made the parallel distance of the first term 4, take the lateral distance of 4, viz. the half of 8, and make it the parallel distance of the first term 4; then the parallel distance of the third term 6, shall reach from the centre to 6, viz. the half of 12. Any other aliquot part of a number may be used in the same way. In like manner, if the number proposed be too small to be made the parallel distance, it may be multiplied by some number, and the answer is to be divided by the same number.

To protract angles by the line of Chords. Case
1. When the given degrees are under 60. 1. With
any radius on a centre, describe the arch. 2. Make
the same radius a transverse distance between 60
and 60 on the line of chords. 3. Take out the
transverse distance of the given degrees, and lay
this on the arch, which will mark out the angular

distance required.

Case 2. When the given degrees are more than

60. 1. Open the sector, and describe the arch as before. 2. Take $\frac{1}{3}$ or $\frac{1}{3}$ of the given degrees, and take the transverse distance of this $\frac{1}{3}$ or $\frac{1}{3}$, and lay it off twice, if the degrees were halved, three times if the third was used as a transverse distance.

Case 3. When the required angle is less than 6 degrees; suppose 3. 1. Open the sector to the given radius, and describe the arch as before. 2. Set off the radius. 3. Set off the chord of 57 degrees backwards, which will give the arc of three degrees.

Given the radius of a circle, (suppose equal to two inches,) required the sine and tangent of 280 30'

to that radius.

Solution. Open the sector so that the transverse distance of 90 and 90 on the sines, or of 45 and 45 on the tangents, may be equal to the given radius, viz. two inches; then will the transverse distance of 38° 30', taken from the sines, be the length of that sine to the given radius; or if taken from the tangents; will be the length of that tangent to the given radius.

But if the secant of 280 30' was required?

Make the given radius, two inches, a transverse distance to 0 and 0, at the beginning of the line of secants; and then take the transverse distance of the degrees wanted, viz. 28° 30'.

A tangent greater than 45° (suppose 60°) is

found thus.

Make the given radius, suppose two inches, a transverse distance to 45 and 45 at the beginning of the scale of upper tangents; and then the required number 60°00 may be taken from this scale.

Given the length of the sine, tangent, or secant of any degrees; to find the length of the radius to that

sine, tangent, or secant.

Make the given length a transverse distance to its given degrees on its respective scale: then,

In the sines. The transverse distance of 90 and

90 will be the radius sought.

In the lower tangents. The transverse distance of 45 and 45, near the end of the sector, will be the radius sought.

In the upper tangents. The transverse distance of 45 and 45, taken towards the centre of the sector on the line of upper tangents, will be the centre sought.

In the secant. The transverse distance of 0 and 0, or the beginning of the secants, near the centre of the sector, will be the radius sought.

Given the radius and any line representing a sine, tangent, or secant; to find the degrees corresponding to that line.

SOLUTION. Set the sector to the given radius, according as a sine, or tangent, or secant is concerned.

Take the given line between the compasses; apply the two feet transversely to the scale concerned, and slide the feet along till they both rest on like divisions on both legs; then will those divisions shew the degrees and parts corresponding to the given line.

To find the length of a versed sine to a given number of degrees, and a given radius.

Make the transverse distance of 90 and 90 on

the sines, equal to the given radius.

Take the transverse distance of the sine com-

plement of the given degrees.

If the given degrees are less than 90, the difference between the sine complement and the radius gives the versed sine.

If the given degrees are more than 90, the sum of the sine complement and the radius gives the

versed sine.

To open the legs of the sector, so that the corres-

ponding double scales of lines, chords, sines, and

tangents, may make each a right angle.

On the lines, make the lateral distance 10, a distance between eight on one leg, and six on the other leg.

On the sines, make the lateral distance 90 a transverse distance from 45 to 45; or from 40 to 50; or from 30 to 60; or from the sine of any degrees to their complement.

Or on the sines, make the lateral distance of 45

a transverse distance between 30 and 30.

OF THE PLAIN SCALE.

The divisions laid down on the plain scale are of two kinds, the one having more immediate relation to the circle and its properties, the other being merely concerned with dividing straight lines.

Though arches of a circle are the most natural measures of an angle, yet in many cases right lines are substituted, as being more convenient; for the comparison of one right line with another, is more natural and easy, than the comparison of a right line with a curve; hence it is usual to measure the quantities of angles not by the arch itself, which is described on the angular point, but by certain lines described about that arch.

The lines laid down on the plain scales for the measuring of angles, or the protracting scales, are, 1. A line of chords marked CHO. 2. A line of sines marked SIN. of tangents marked TAN. of semitangents marked SIN. and of secants marked SEC. this last is often upon the same line as the sines, because its gradations do not begin till the sines end.

There are two other scales, namely, the rhumbs, marked RU. and longitudes, marked LON. Scales of latitude and hours are sometimes put upon the

plain scale; but, as dialling is now but seldom

studied, they are only made to order.

The divisions used for measuring straight lines are called scales of equal parts, and are of various lengths for the convenience of delineating any figure of a large or smaller size, according to the fancy or purposes of the draughts-man. They are, indeed, nothing more than a measure in miniature for laying down upon paper, &c. any known measure, as chains, yards, feet, &c. each part on the scale answering to one foot, one yard, &c. and the plan will be larger or smaller, as the scale contains a smaller or a greater number of parts in an inch. Hence a variety of scales is useful to lay down lines of any required length, and of a convenient proportion with respect to the size of the drawing. If none of the scales happen to suit the purpose. recourse should be had to the line of lines on the sector; for, by the different openings of that instrument, a line of any length may be divided into as many equal parts as any person chooses.

Scales of equal parts are divided into two kinds,

the one simple, the other diagonally divided.

Six of the simply divided scales are generally placed one above another upon the same rule; they are divided into as many equal parts as the length of the rule will admit of; the numbers placed on the right hand, shew how many parts in an inch each scale is divided into. The upper scale is sometimes shortened for the sake of introducing another, called the line of chords.

The first of the larger, or primary divisions, on every scale is subdivided into 10 equal parts, which small parts are those which give a name to the scale: thus it is called a scale of 20, when 20 of these divisions are equal to one inch. If, therefore, these lesser divisions be taken as units, and each represents one league, one mile, one chain, or one yard.

&c. then will the larger divisions be so many tens; but if the subdivisions are supposed to be tens, the

larger divisions will be hundreds.

To illustrate this, suppose it were required to set off from either of the scales of equal parts 16, 36, or 360 parts, either miles or leagues. Set one foot of your compasses on 3, among the larger or primary divisions, and open the other point till it falls on the 6th subdivision, reckoning backwards or towards the left hand. Then will this extent represent, 16, 36, or 360 miles or leagues, &c. and bear the same proportion in the plan as the line measured does to the thing represented.

To adapt these scales to feet and inches, the first primary division is often duodecimally divided by an upper line; therefore, to lay down any number of feet and inches, as for instance, eight feet eight inches, extend the compasses from eight of the larger to eight of the upper small ones, and that distance laid down on the plan will repre-

sent eight feet eight inches.

Of the scale of equal parts diagonally divided. The use of this scale is the same as those already described. But by it a plane may be more accurately divided than by the former; for any one of the larger divisions may by this be subdivided into 100 equal parts; and, therefore, if the scale contains 10 of the larger divisions, any number under

1000 may be laid down with accuracy.

The diagonal scale is seldom placed on the same side of the rule with the other plotting scale. The first division of the diagonal scale, if it be a foot long, is generally an inch divided into 100 equal parts, and at the opposite end there is usually half an inch divided into an 100 equal parts. If the scale be six inches long, one end has commonly half an inch, the other a quarter of an inch subdivided into 100 equal parts.

N

The nature of this scale will be better understood by considering its construction. For this

purpose:

First. Draw eleven parallel lines at equal distances; divide the upper of these lines into such a number of equal parts, as the scale to be expressed is intended to contain; from each of these divisions draw perpendicular lines through the eleven parallels.

Secondly. Subdivide the first of these divisions into ten equal parts, both in the upper and lower

lines.

Thirdly. Subdivide again each of these subdivisions, by drawing diagonal lines from the 10th below to the 9th above; from the 8th below to the 7th above; and so on, till from the first below to the 0 above; by these lines each of the small divisions is divided into ten parts, and, consequently, the whole first space into 100 equal parts; for, as each of the subdivisions is one-tenth part of the whole first space or division, so each parallel above it is one-tenth of such subdivision, and, consequently, one-hundreth part of the whole first space: and if there be ten of the larger divisions, one-thousandth part of the whole space.

If, therefore, the larger divisions be accounted as units, the first subdivisions will be tenth parts of an unit, and the second, marked by the diagonal upon the parallels, hundreth parts of the unit. But, if we suppose the larger divisions to be tens, the first subdivisions will be units, and the second tenths. If the larger are hundreds, then will the

first be tens, and the second units.

The numbers therefore, 576, 57,6, 5,76, are all expressible by the same extent of the compasses: thus setting one foot in the number five of the larger divisions, extend the other along the sixth parallel to the seventh diagonal. For, if the five

larger divisions be taken for 500, seven of the first subdivisions will be 70, which upon the sixth parallel, taking in six of the second subdivisions for units, makes the whole number 576. Or, if the five larger divisions be taken for five tens, or 50, seven of the first subdivisions will be seven units, and the six second subdivisions upon the sixth parallel, will be six tenths of an unit. Lastly, if the five larger divisions be only esteemed as five units, then will the seven first subdivisions be seven tenths, and the six second subdivisions be the six hundredth parts of an unit.

Of the line of chords. This line is used to set off an angle from a given point in any right line, or to measure the quantity of an angle already

laid down.

Thus to draw a line that shall make with another line an angle, containing a given number of

degrees, suppose 40 degrees.

Open your compasses to the extent of 60 degrees upon the line of chords, (which is always equal to the radius of the circle of projection,) and setting one foot in the angular point, with that extent describe an arch; then taking the extent of 40 degrees from the said chord line, set it off from the given line on the arch described; a right line drawn from the given point, through the point marked upon the arch, will form the required angle.

The degrees contained in an angle already laid down, are found nearly in the same manner; for instance, to measure an angle. From the centre describe an arch with the chord of 60 degrees, and the length of the arch, contained between the lines measured on the line of chords, will give the num-

ber of degrees contained in the angle.

If the number of degrees are more than 90, they must be measured upon the chords at twice: thus, if 120 degrees were to be practised, 60 may be taken from the chords, and those degrees be laid off

twice upon the arch. Degrees taken from the chords are always to be counted from the begin-

ning of the scale.

Of the rhumb line. This is, in fact, a line of chords constructed to a quadrant divided into eight parts or points of the compass, in order to facilitate the work of the navigator in laying

down a ship's course.

Of the line of longitudes. The line of longitudes is a line divided into sixty unequal parts, and so applied to the line of chords, as to shew, by inspection, the number of equatorial miles contained in a degree on any parallel of latitude. The graduated line of chords is necessary, in order to shew the latitudes; the line of longitude shews the quantity of a degree on each parallel in sixtieth parts of an equatorial degree, that is, miles.

The lines of tangents, semitangents, and secants, serve to find the centres and poles of projected circles in the stereographical projection of the sphere.

The line of sines is principally used for the or-

thographic projection of the sphere.

The lines of latitudes and hours are used conjointly, and serve very readily to mark the hour lines in the construction of dials; they are generally on the most complete sorts of scales and sectors; for the uses of which see treatises on dialling.

OF THE PROTRACTOR.

This is an instrument used to protract, or lay down an angle containing any number of degrees, or to find how many degrees are contained in any given angle. There are two kinds put into cases of mathematical drawing instruments; one in the form of a semicircle, the other in the form of a parallelogram. The circle is undoubtedly the only natural measure of angles; when a straight line is therefore used, the divisions thereon are derived

from a circle, or its properties, and the straight line is made use of for some relative convenience: it is thus the parallelogram is often used as a protractor, instead of the semicircle, because it is in some cases more convenient, and that other scales, &c.

may be placed upon it.

The semicircular protractor, is divided into 180 equal parts or degrees, which are numbered at every tenth degree each way, for the conveniency of reckoning either from the right towards the left, or from the left towards the right; or the more easily to lay down an angle from either end of the line, beginning at each end with 10, 20, &c. and proceeding to 180 degrees. The edge is the diameter of the semicircle, and the mark in the middle points out the centre, in a protractor in the form of a parallelogram: the divisions are as in the semicircular one, numbered both ways; the blank side represents the diameter of a circle. The side of the protractor to be applied to the paper is made flat, and that whereon the degrees are marked, is chamfered or sloped away to the edge, that an angle may be more easily measured, and the divisions set off with greater exactness.

Application of the protractor to use. 1. A number of degrees being given, to protract, or lay down an angle, whose measure shall be equal thereto.

Thus, to lay down an angle of 60 degrees from the point of a line, apply the diameter of the protractor to the line, so that the centre thereof may coincide exactly with the extremity; then with a protracting pin make a fine dot against 60 upon the limb of the protractor; now remove the protractor, and draw a line from the extremity through that point, and the angle contains the given number of degrees.

2. To find the number of degrees contained in a

given angle.

Place the centre of the protractor upon the angular point, and the fiducial edge, or diameter, exactly upon the line; then the degree upon the limb that is cut by the line will be the measure of the given angle, which, in the present instance, is found to be 60 degrees.

3. From a given point in a line, to erect a perpen-

dicular to that line.

Apply the protractor to the line, so that the centre may coincide with the given point, and the division marked 90 may be cut by the line; then a line drawn against the diameter of the protractor will be the perpendicular required.

OF PARALLEL RULES.

Parallel lines occur so continually in every species of mathematical drawing, that it is no wonder so many instruments have been contrived to delineate them with more expedition than could be effected by the general geometrical methods. For this purpose, rules of various constructions have been made; and particularly recommended by their inventors; their use however is so apparent as to need no explanation.

GUNTER'S SCALE.

The scale generally used is a ruler of two feet in length, having drawn upon it equal parts, chords, sines, tangents, secants, &c. These are contained on one side of the scale, and the other side contains the logarithms of these numbers. Mr. Edmund Gunter was the first who applied the logarithms of numbers, and of sines and tangents to straight lines drawn on a scale or ruler; with which, proportions in common numbers, and trigonometry, may be solved by the application of a pair of compasses

only. The method is founded on this property, That the logarithms of the terms of equal ratios are equidifferent. This was called Gunter's Proportion, and Gunter's Line; hence the scale is generally called the Gunter.

Of the Logarithmical Lines, or Gunter's Scale. The logarithmical lines, on Gunter's scale, are

the eight following:

S. Rhumb, or fine rhumbs, is a line containing the logarithms of the natural sines of every point and quarter point of the compass, numbered from a brass pin on the right hand towards the left with 8, 7, 6, 5, 4, 3, 2, 1.

T*Rhumb, or tangent rhumbs, also corresponds to the logarithm of the tangent of every point and quarter point of the compass. This line is numbered from near the middle of the scale with 1.2.3.4 towards the right hand, and back again with the numbers 5, 6, 7 from the right hand towards the left. To take off any number of points below four, we must begin at 1, and count towards the right hand; but to take off any number of points above four, we must begin at four, and count towards the left hand.

Numbers, or the line of numbers, is numbered from the left hand of the scale towards the right, with 1, 2, 3, 4, 5, 6, 7, 8, 9, 1 which stands exactly in the middle of the scale; the numbers then go on 2, 3, 4, 5, 6, 7, 8, 9, 10 which stands at the right hand end of the scale. These two equal parts of the scale are divided equally, the distance between the first or left hand 1, and the first 2, 3, 4, &c. is exactly equal to the distance between the middle 1 and the numbers 2, 3, 4, &c. which follow it. The subdivisions of these scales are likewise similar, viz. they are each one-tenth of the primary divisions, and are distinguished by lines of about half the length of the primary divisions.

These subdivisions are again divided into ten parts, where room will permit; and where that is not the case, the units must be estimated, or guessed at, by the eye, which is easily done by a little

practice.

The primary divisions on the second part of the scale, are estimated according to the value set upon the unit on the left hand of the scale: If you call it one, then the first 1, 2, 3, &c. stand for 1, 2, 3, &c. the middle 1 is 10, and the 2. 3. 4. &c. following stand for 20, 30, 40, &c. and the ten at the right hand is 100: If the first 1 stand for 10, the first 2, 3, 4, &c. must be counted 20, 30, 40, &c. the middle 1 will be 100, the second 2, 3, 4, 5, &c. will stand for 200, 300, 400, 500, &c. and the ten at the right hand for 1000.

If you consider the first 1 as $\frac{1}{10}$ of an unit, the 2, 3, 4, &c. following will be $\frac{2}{10}$, $\frac{3}{10}$, &c. the middle 1 will stand for an unit, and the 2, 3, 4, &c. following will stand for 2, 3, 4, &c. also the division at the right-hand end of the scale will stand for 10. The intermediate small divisions must be estimated according to the value set upon the primary ones.

Sine. The line of sines is numbered from the left hand of the scale towards the right, 1, 2, 3, 4, 5, &c. to 10; then 20, 30, 40, &c. to 90, where it terminates just opposite 10 on the line of numbers.

Versed sine. This line is placed immediately under the line of sines, and numbered in a contrary direction, viz. from the right hand towards the left 10, 20, 30, 40, 50, to about 169; the small divisions are here to be estimated according to the number of them to a degree. By comparing the line of versed sines with the line of sines, it will appear that the versed sines do not belong to the arches with which they are marked, but are the half versed sines of their supplements. Thus, what is marked the versed sine of 90 is only half the versed sine of 90,

the versed sine of 120° is half the versed sine of 60°, and the versed sine marked 100° is half the versed sine of 80°, &c.

The versed sines are numbered in this manner to render them more commodious in the solution of trigonometrical, and astronomical problems.

Tangents. The line of tangents begins at the left hand, and is numbered 1, 2, 3, &c. to 10, then 20, 30, 45, where there is a little brass pin just under 90 in the line of sines; because the sine of 90° is equal to the tangent of 45°. It is numbered from 45° towards the left hand 50, 60, 70, 80, &c. The tangents of arches above 45° are therefore counted backward on the line, and are found at the same points of the line as the tangents of their complements.

Thus, the division at 40 represents both 40 and 50, the division at 30 serves for 30 and 60, &c.

Meridional Parts. This line stands immediately above a line of equal parts, marked Equal Pt. with which it must always be compared when used. The line of equal parts is marked from the right hand to the left with 0, 10, 20, 30, &c.; each of these large divisions represents 10 degrees of the equator, or 600 miles. The first of these divisions is sometimes divided into 40 equal parts, each re-

presenting 15' minutes or miles.

The extent from the brass pin on the scale of meridional parts to any division on that scale, applied to the line of equal parts, will give (in degrees) the meridional parts answering to the latitude of that division. Or the extent from any division to another, on the line of meridional parts, applied to the line of equal parts, will give the meridional difference of latitude between the two places denoted by the divisions. These degrees are reduced to leagues by multiplying by 20, or to miles by multiplying by 60.

The use of the logarithmical lines on Gunter's Scale. By these lines and a pair of compasses, all the problems of Trigonometry, &c. may be solved.

These problems are all solved by proportion; Now in natural numbers, the quotient of the first term by the second is equal to the quotient of the third by the fourth: therefore logarithmically speaking the difference between the first and second term is equal to the difference between the third and fourth, consequently on the lines on the scale, the distance between the first and second term will be equal to the distance between the third and fourth. And for a similar reason, because four proportional quantities are alternately proportional, the distance between the first and third terms, will be equal to the distance between the second and fourth. Hence the following

General.Rule.

The extent of the compasses from the first term to the second, will reach, in this same direction, from the third to the fourth term. Or, the extent of the compasses from the first term to the third, will reach, in the same direction, from the second to the fourth.

By the same direction in the foregoing rule, is meant that if the second term lie on the right hand of the first, the fourth will lie on the right hand of the third, and the contrary. This is true, except the two first or two last terms of the proportion are on the line of tangents, and neither of them under 45°; in this case the extent on the tangents is to be made in a contrary direction: For had the tangents above 45° been laid down in their proper direction, they would have extended beyond the length of the scale towards the right hand; they are therefore as it were folded back up-

on the tangents below 45°, and consequently lie in a direction contrary to their proper and natural order.

If the two last terms of a proportion be on the line of tangents, and one of them greater and the other less than 45°; the extent from the first term to the second will reach from the third beyond the To remedy this inconvenience, apply the extent between the two first terms from 45° backward upon the line of tangents, and keep the left hand point of the compasses where it falls; bring the right hand point from 45° to the third term of the proportion; this extent now in the compasses applied from 45° backward will reach to the fourth term, or the tangent required. For, had the line of tangents been continued forward beyond 45°, the divisions would have fallen above 45° forward; in the same manner as they fall under 45° backward.

SECTION V.

TRIGONOMETRY.

The word Trigonometry signifies the measuring of triangles. But, under this name is generally comprehended the art of determining the positions and dimensions of the several unknown parts of extension, by means of some parts, which are already known. If we conceive the different points, which may be represented in any space, to be joined together by right lines, there are three things offered for our consideration; 1. the length of these lines; 2 the angles which they form with one another; 3 the angles formed by the planes, in which these lines are drawn, or are supposed to be traced. On the comparison of these three objects,

depends the solution of all questions, that can be proposed concerning the measure of extension, and its parts; and the art of determining all these things from the knowledge of some of them, is reduced to the solution of these two general questions.

1. Knowing three of the six parts, the sides and angles—which constitute a rectilineal triangle; to

find the other three.

2. Knowing three of the six parts, which compose a spherical triangle; that is a triangle formed on the surface of a sphere by three arches of circles, which have their centre in the centre of the

same sphere—to find the other three.

The first question is the object of what is called Plane Trigonometry, because the six parts, considered here, are in the same plane: it is also denominated Rectilineal Trigonometry. The second question belongs to Spherical Trigonometry, wherein the six parts are considered in different planes. But the only object here is to explain the solutions of the former question: viz.

PLANE TRIGONOMETRY.

Plane Trigonometry is that branch of geometry, which teaches how to determine, or calculate three of the six parts of a rectilineal triangle by having the other three parts given or known. It is usually divided into Right angled and Oblique angled Trigonometry, according as it is applied to the mensuration of Right or Oblique angled Triangles.

In every triangle, or case in trigonometry, three of the parts must be given, and one of these parts, at least, must be a side; because, with the same angles, the sides may be greater or less in any

proportion,

RIGHT ANGLED PLANE TRIGONOMETRY.

· PL.5. Fig. 1.

1. In every right-angled plane triangle ABC, if the hypothenuse AC be made the radius, and with it a circle, or an arc of one, be described from each end; it is plain (from def. 20.) that BC is the sine of the angle A, and AB is the sine of the angle C; that is, the legs are the sines of their opposite angles.

Fig. 2.

If one leg AB be made the radius, and with it, on the point A, an arc be described; then BC is the tangent, and AC is the secant of the angle A, by def. 22 and 25.

Fig. 3.

3. If BC be made the radius, and an arc be described with it on the point C; then is AB the tangent, and AC is the secant of the angle C, as before.

Because the sine, tangent, or secant of any given arc, in one circle, is to the sine, tangent, or secant of a like arc (or to one of the like number of degrees) in another circle; as the radius of the one is to the radius of the other; therefore the sine, tangent, or secant of any arc is proportional to the sine, tangent, or secant of a like arc, as the radius of the given arc is to 10.000000, the radius from whence the logarithmic sines, tangents, and secants, in most tables, are calculated, that is;

If AC be made the radius, the sines of the angle A and C, described by the radius AC, will be proportional to the sines of the like arcs, or angles in the circle, that the tables now mentioned were

calculated for. So if BC was required, having the angles and AB given, it will be,

Fig. 1.

 $\mathbf{As} \ S.C : AB :: S.A : BC.$

That is, as the sine of the angle C in the tables, is to the length of AB; (or sine of the angle C, in a circle whose radius is AC;) so is the sine of the angle A in the tables, to the length of BC. (or sine of the same angle, in the circle, whose radius is AC.)

In like manner the tangents and secants represented by making either leg the radius, will be proportional to the tangents and secants of a like arc, as the radius of the given arc is to 10.000000,

the radius of the tables aforesaid.

Hence it is plain, that if the name of each side of the triangle be placed thereon, a proportion will arise to answer the same end as before: thus if AC be made the radius, let the word radius be written thereon; and as BC and AB, are the sines of their opposite angles; upon the first let SA, or sine of the angle A, and on the other let SC, or sine of the angle C, be written. Then,

When a side is required, it may be obtained by

this proportion, viz.

As the name of the side given

is to the side given,

So is the name of the side required

to the side required.

Thus, if the angles A and C, and the hypothenuse AC were given, to find the sides; the proportion will be

Fig. 1.

1. R : AC :: S.A : BC.

That is, as radius is to AC, so is the sine of the angle A, to BC. And,

 $\mathbf{Z}. \ \mathbf{R} : \mathbf{AC} :: \mathbf{S.C} : \mathbf{AB}.$

That is, as radius is to AC, so is the sine of the angle C to AB.

When an angle is required, we use this propor-

tion, viz.

As the side that is made the radius,

is to radius,

So is the other given side,

to its name.

Thus, if the legs were given to find the angle A, and if AB be made the radius, it will be

Fig. 2.

AB:R::BC:TA.

That is, as AB, is to radius, so is BC, to the tan-

gent of the angle A.

After the same manner, the sides or angles of all right angled plane triangles may be found, from their proper data.

We here, in plate 4, give all the proportion requisite for the solution of the six cases in rightangled trigonometry; making every side possible

the radius.

In the following triangles this mark — in an angle denotes it to be known, or the quantity of degrees it contains to be given; and this mark on a side, denotes its length to be given in feet, yards, perches, or miles, &c. and this mark, either in an angle or on a side, denotes the angle or side to be required.

From these proportions it may be observed; that to find a side, when the angles and one side are given, any side may be made the radius; and

to find an angle, one of the given sides must be made the radius. So that in the 1st, 2d, and 3d cases, any side as well required as given may be made the radius, and in the first statings of the 4th, 5th, and 6th cases, a given side only is made the radius.

RIGHT ANGLED TRIANGLES.

CASE I.

The angles and hypothenuse given, to find the base and perfendicular.

PL. 5. Fig. 4.

In the right angled triangle ABC, suppose the angle $A=46^{\circ}$. 30°. and consequently the angle $C=43^{\circ}$. 30°. (by cor. 2. theo. 5.); and AC 250 parts, (as feet, yards, miles, &c.) required the sides AB and BC.

1st. by construction.

Make an angle of 46°. 30', in blank lines, (by prob. 16. geom.) as CAB; lay 250, which is the given hypothenuse, from a scale of equal parts, from A to C; from C, let fall the perpendicular (BC, by prob. 7. geom.) and that will constitute the triangle ABC. Measure the lines BC, and AB, from the same scale of equal parts that AC was taken from; and you have the answer.

2d. BY CALCULATION.

1. Making AC the radius, the required sides are found by these propositions, as in plate 4, case 1.

R:AC :: S.A : BC.R:AC :: S.C : AB.

That is, as radius,	=90°	10.000000
is to AC	=250	2.397940
is to AC So is the sine of	of $A = 46^{\circ}$. $30'$	9.860562
to BC,	=181. 4	2.258502
As radius,	=90°	10.000000
is to AC ,	· =250 .	2.397940
So is the sine		9.837812
to AB,	=172. 1	2.235752

If from the sum of the second and third logs. that of the first be taken, the number will be the log. of the fourth; the number answering to which will be the thing required; but when the first log. is radius, or 10.000000, reject the first figure of the sum of the other two logs. (which is the same thing as to subtract 10.000000;) and that will be the log. of the thing required.

2. Making AB the radius.

Secant A:AC::R:AB. Secant A:AC::T.A:BC.

That is, As the secant	of $A = 46^{\circ} 30'$	
is to AC,	=250	2.397940
So is the radius	≕90°	10.000000
	•	12.397940
to AB ,	=172. 1	2.235762

As the secant of A is to AC , So is the tangent of A	=46° 30′ = 250 =46° 30′	10.162188 2.397940 10.022750
		12.420690
to <i>BC</i> ,	=181.34.	2.258502

3. Making BC the radius.

Sec. C : AC : Sec. C : AC :		2 ·
That is, as the secant of is to AC, So is tadius	of $C=43^{\circ}3$ $= 25$	o' 10.13943 8
•	•	12.397940
to BC , As the secant of C is to AC ,	= 181.3 = 43° 3¢ = 25	0' 10.139438
So is the tangent of	C =43° 30	
		12.375190

to AB, = 172. 1 2.235752 Or, having found one side, the other may be obtained by cor. 2. theo. 14. sect. 4.

3d. By Gunter's scale.

The first and third terms in the foregoing proportions, being of a like nature, and those of the second and fourth being also like to each other; and the proportions being direct ones, it follows; that if the third term be greater or less than the first, the fourth term will be also greater or less

than the second; therefore the extent in your compasses, from the first to the third term, will reach from the second to the fourth.

Thus, to extend the first of the foregoing proportions;

- 1. Extend from 90° to 46° 30′, on the line of sines; that distance will reach from 250 on the line of numbers, to 181, for BC.
- 2. Extend from 90° to 43° 30′, on the line of sines; that distance will reach from 250 on the line of numbers, to 172, for AB.

If the first extent be from a greater to a less number; when you apply one point of the compasses to the second term, the other must be turned to a less; and the contrary.

By def. 20. sect. 4. The sine of 90° is equal to the radius; and the tangent of 45° is also equal to the radius; because if one angle of a right angled triangle be 45°, the other will be also 45°; and thence (by the lemma preceding theo. 7. sect. 4.) the tangent of 45° is equal to the radius: for this reason the line of numbers of 10.000000, the sine of 90°, and tangent of 45° being all equal, terminate at the same end of the scale.

The two first statings of this case, answers the question without a secant: the like will be also made evident in all the following cases.

4th. Solution by Natural Sines.

From the foregoing analogies, or statements, it

is obvious that if the hypothenuse be multiplied by the natural sine of either of the acute angles, the product will be the length of the side opposite to that angle; and multiplied by the natural cosine of the same angle, the product will be the length of the other side, or that which is contiguous to the angle. Thus:

the given ang. =47° 36′. Nat. Sine =.725374 Hyp. = 250	Nat. Cos. =.688355 250
36268700	34417750
1450748	1376710
Perpend.=181.343500	Base=172.088750

CASE II.

The base and angles given; to find the perpendicular and kypothenuse.

PL. 5. fig. 5.

In the triangle ABC there is the angle A 42° 20′, and of course the angle C 47° 40′ (by cor. 2. theo. 5,) and the side AB 190, given; to find BC and AC.

1st. By Construction.

Make the angle CAB (by prob. 16. sect. 4.) in blank lines, as before. From a scale of equal parts lay 190 from A to B: on the point B, erect a perpendicular BC (by prob. 5. sect. 4.) the point where this cuts the other blank line of the angle, will be C: so is the triangle ABC constructed; let AC and BC be measured from the same scale of equal parts that AB was taken from, and the answers are found.

2d. By Calculation.

1. Making AC the radius.

S.C : AB : : R : AC. S.C : AB : : S.A : BC.

That is, as the sine of C=47° 40′ 9.868785 is to AB, 190 2.278754So is radius 900 10.000000 12.278754 2.409969 As the sine of C=47° 40′ 9.868785 is to AB. 190 2.278754 So is the sine of $A = 42^{\circ} 20'$ 9.828301 12.107055 to BC, =173.12.238270

2. Making AB the radius.

R:AB::T.A:BC.R:AB::Sec.A:AC.

That is, as radius 90. 10.000000 is to AB, 190 **2.278754** So is the tangent of $A=42^{\circ}$ 20' 9.959516 to BC, =173.12.238270 **=90** As radius 10.000000 is to AB. =1902.278754 So is the secant of $A = 42^{\circ} 20'$ 10.131215 to AC, 257 2.409969

3. Making BC the radius.

$T. C: AB:: Sec. C: AC.$ $T. C: AB:: R: BC.$ That is, as the tangent of $C=47^{\circ}$ 40' is to $AB, = 190$ So is the Secant of $C=47^{\circ}$ 40'	10.040484 2.278754 10.171699
	12.450453
to AC , = 257 As the tangent of $C=7^{\circ}$ 40 is to AB , = 190 So is the radius = 90°	2.409969 10.040484 2.278754 10.000000
	12.278754
to $BC = 173.1$	2.238270

Or, having found one of the required sides, the other may be obtained, by one, or the other of the cors. to theo. 14. sect. 4.

3d. By Gunter's Scale:

1. When AC is made the radius.

Extend from 47° 40′, to 90° on the line of sines; that distance will reach from 190 to 257, on the line of numbers, for AC.

2. When AB is made the radius, the first stating

is thus performed:

Extend from 45° on the tangents (for the tangent of 45° is equal to the radius, or to the sine of 90° as before) to 42° 20′; that extent will reach from 190, on the line of numbers, to 173, for BC.

3. When BC is made the radius, the second stating is thus performed:

Extend from 47° 40' on the line of tangents, to 45° , or radius; that extent will reach from 190 to 173, on the line of numbers, for BC; for the tangent of 47° 40', is more than the radius, therefore the fourth number must be less than the second, as before.

The two first statings of this case, answer the question without a secant.

4th. Solution by Natural Sines.

$$\frac{AB \times R.}{S \text{ of } C.} = AC; \text{ and } \frac{AB \times S \text{ of } A}{S \text{ of } C.} = BC.$$
Nat. S of C, side $AB \times R$.
Thus .739239) 190.0000000 (257.02 &c.=AC.
147.8478
$$\frac{4215220}{2606105}$$

> 1557700 1478478

and, .673443=Nat. S. of A. 190=side AB.

60609870

Nat. S. of C. 673443

.739239) 127.954170 (173.09=BC. 739239

5403027 5174673

> 2283540 2217717

> > 6502300 6653151

CASE III.

The angle's and perpendicular given; to find the base and hypothenuse.

PL. 5. fig. 6.

In the triangle ABC, there is the angle A 40°, and consequently the angle C 50°, with BC 170, given: to find AC and AB.

1st. By Construction.

Make an angle CAB of 40° in blank lines; (by prob. 16, sect. 4.) with BC 170, from a line of equal parts draw the lines EF parallel to AB (by prob. 8, sect. 4.) the lower line of the angle, and from the point where it cuts the other line in C, let fall a perpendicular BC (by prob. 7, sect 4.) and the triangle is constructed: the measures of AC and AB, from the same scale that BC was taken, will answer the question.

What has been said in the two foregoing cases, is sufficient to render the operations in this, both by calculation, Gunter's scale, and Natural sines, so obvious, that it is needless to insert them; however, for the sake of the learner, we give for

Answers; AC 264. 5, and AB 202. 6.

CASE IV.

The base and hypothenuse given; to find the angles and perpendicular.

PL. 5. fig. 7.

In the triangle ABC, there is given, AB 300 and AC 500: the angles A and C, and the perpendicular BC, are required.

1st. By Construction.

From a scale of equal parts lay 300 from A to B; on B erect an indefinite blank perpendicular line, with AC 500, from the same scale, and one foot of the compass, in A, cross the perpendicular line in C; and the triangle is constructed.

By prob. 17. sect. 4. measure the angle A, and let BC be measured from the same scale of equal parts that AC and AB were taken from; and the answers are obtained.

2d. By Calculation.

1. Making AC the radius:

AC: R:: AB: S.C. R: AC:: S.A.: BC.

That is, as AC	==	500	2.698970
is to radius,	===	` 90 •	10.000000
So is AB	=	300	2.477121
			12.477121
to the sine	e of <i>C</i> ,	=36° 52′	9.778151
By cor. 2. theo. angle A .	5. 90%-	36° 52′ =	= 53°08′ the
As radius =	90°		10.000000
is to AC , $=$	500)	2.698970
So is the sine of A	= 53°	08'	9.903108
to BC,	= 400)	2.602078

2. Making AB the radius.

 $\overrightarrow{AB} : R : : AC : sec. A.$ R : AB : : T.A : BC.

That is, as AB	==	300	2 477121
is to radius	===	90°	10.000000
So is AC	=	500	2.698970
	•		12.698970
to the seca	nt of A,	=53°. 08′	10.221849
As radius	=	90°	10.000000
is to AB ,	===	300	2.477121
So is the tange	ent of A	=53°. 08′	10.124990
to BC ,	=	400	2.602111

Or BC may be found from cor. 2. theo. 14. sect. 4.

3d. By Gunter's Scale.

1. Making AC the radius.

Extend from 500 to 300, on the line of numbers; that extent will reach from 90°, on the line of sines, to 36°. 52' for the angle C.

Again, extend from 90° to 53°. 08′, on the line of sines, that extent will reach from 500 to 400, on the line of numbers, for BC.

2. Making AC the radius, the second stating is thus performed.

Extend from radius, or the tangent of 45°, to 53°. 08', that extent will reach from 300 to 400, for BC.

4th. Solution by Natural Sines.

$$\frac{R \times AB.}{AC} = S \text{ of } C; \text{ and } \frac{AC \times S \text{ of } A.}{R} = BC.$$
Thus, $AC AB$

$$5,00) 300,0000,00$$

$$600000 = \text{Nat. sine } 36^{\circ} 52'$$

and,

Nat. sine of
$$A = 53^{\circ} 8' = .800034$$

 $AC = 500$
 $400.017000 = BC$

CASE F.

The perpendicular and hypothenuse given, to find the angles and base.

PL. 5. fig. 8.

In the triangle ABC there is BC 306, and AC 370 given; to find the angles A and C; and the base AB.

1st. By Construction.

Draw a blank line from any point, in which, at B, erect a perpendicular, on which lay BC 306, from a scale of equal parts: from the same scale, with AC 370, in the compasses, cross the first drawn blank line in A, and the triangle ABC is constructed.

Measure the angle A (by prob. 17. sect. 4.); and also AB, from the same scale of equal parts the other sides were taken from, and the answers are now found.

The operations by calculation, the square root, Gunter's scale, and Natural sines, are here omitted, as they have been heretofore fully explained: the statings, or proportions, must also be obvious, from what has already been said.

Answers; The angle A 55° 48'; therefore the angle C 34° 12', and AB 208.

CASE VI.

The base and perpendicular given; to find the angles and hypothenuse.

PL. 5. fig. 9.

In the triangle ABC, there is AB 225, and BC 272, given; to find the angles A and C, and the hypothenuse AC.

1st. By Construction,

Draw a blank line, on which lay AB 225, from a scale of equal parts; at B, erect a perpendicular; on which lay BC, 272, from the same scale: join A and C, and the triangle is constructed.

As before, let the angle A, and the hypothenuse AC be measured; in order to find the answers.

2d. By Calculation.

1. Making AB the radius.

AB:R::BC:T.A.R.:AB::sec.A:AC.

2. Making BC the radius.

BC:R::AB:T.C.R.:BC::Sec.C:AC.

By calculation; the answers from the foregoing proportions are easily obtained, as before.

But because AC, by either of the said proportions is found by means of a secant; and since there is no line of secants on Gunter's scale; after

having found the angles as before, let us suppose AC the radius, and then

1. S.
$$A : BC :: R. : AC$$
. or 2. S. $C : AB :: R : AC$.

These proportions may be easily resolved, either by calculation, or Gunter's scale, as before; and thus the hypothenuse AC may be found without a secant.

From the two given sides, the hypothenuse may be easily obtained, from cor. 1. theo. 14. sect. 4.

Thus the square of
$$AB = 50625$$

Add the square of $BC = 73984$
$$124609 (353 = AC)$$
$$9$$
$$65)346$$
$$325$$
$$703)2109$$
$$2109$$

From what has been said on logarithms, it is plain,

1. That half the logarithm of the sum of the squares of the two sides, will be the logarithm of the hypothenuse. Thus,

The sum of squares, as before, is 124609; its log. is 5.095549, the half of which is 2.547774.;

and the corresponding number to this, in the tables, will be 353, for AC.

2. And that half of the logarithm of the difference of the squares of AC and AB, or of AC and BC, will be the logarithm of BC, or of AB.

The following examples are inserted for the ex-

ercise of the learner.

1. Given,
$$\left\{\begin{array}{c} \text{the angle } C \ 64^{\circ} \ 40' \\ AC \ 3876 \end{array}\right\} \left\{\begin{array}{c} AB \\ BC \end{array}\right\}$$
 required.

2. Given, $\left\{\begin{array}{c} \text{the angle } C \ 47^{\circ} \ 20' \\ AB \ 17 \end{array}\right\} \left\{\begin{array}{c} AC \\ BC \end{array}\right\}$ required.

3. Given, $\left\{\begin{array}{c} \text{the angle } C \ 28^{\circ} \ 30' \\ BC \ 27187 \end{array}\right\} \left\{\begin{array}{c} AB \\ AC \end{array}\right\}$ required.

4. Given, $\left\{\begin{array}{c} AB \ 2 \\ AC \ 3 \end{array}\right\} \left\{\begin{array}{c} \text{the angles required.} \\ \text{and } BC \end{array}\right\}$ required.

5. Given, $\left\{\begin{array}{c} BC \ 17 \\ AC \ 21.6 \end{array}\right\} \left\{\begin{array}{c} \text{the angles nequired.} \\ \text{and } AB \end{array}\right\}$ required.

6. Given, $\left\{\begin{array}{c} AB \ 2871.64 \\ BC \ 3176.2 \end{array}\right\} \left\{\begin{array}{c} \text{the angles required.} \\ \text{and } AC \end{array}\right\}$ required.

The answers are omitted, that the learner may pesolve them for himself by the foregoing methods; by which means he will find and see more distinctly their mutual agreements: and become more expert, and better acquainted with the subject.

OBLIQUE ANGLED

PLANE TRIGONOMETRY.

BEFORE we proceed to the solution of the four cases of Oblique angled triangles, it is necessary to premise the following theorems.

THEO. I.

PL. 5. fig. 10.

In any plane triangle ABC, the sides are proportional to the sines of their opposite angles; that is, S. C: AB:: S. A: BC, and S. C: AB:: S. B: AC; also S. B: AC:: S. A: BC.

By theo. 10. sect. 4. the half of each side is the sine of its opposite angle; but the sines of those angles, in tabular parts, are proportional to the sines of the same in any other measure; and therefore the sines of the angles will be as the halves of their opposite sides; and since the halves are as the wholes, it follows, that the sines of their angles are as their opposite sides; that is, S. C: AB: S. A: BC, &c. Q. E. D.

THEO. II.

Fig. 11.

In any filane triangle ABC, the sum of the two given sides AB and BC, including a given angle ABC, is to their difference, as the sangent of half the sum of the two unknown angles A and C is to the tangent of half their difference.

Produce AB, and make HB = BC, and join HC: let fall the perpendicular BE, and that will bisect

the angle HBC (by theo. 9. sect. 4.) through B draw BD parallel to AC, and make HF = DC, and join BF; take BI = BA, and draw IG parallel to BD or AC.

It is then plain that AH will be the sum, and HI the difference of the sides AB and BC: and since HB=BC, and BE perpendicular to HC, therefore HE=EC (by theo. 8. sect. 4.); and since BA = BI, and BD and IG parallel to AC, therefore GD = DC = FH, and consequently HG = FD, and $\frac{1}{2}HG = \frac{1}{2}FD$ or ED. Again, EBC being half HBC, will be also half the sum of the angles A and C (by theo. 4. sect. 4.) also, since HB, HF, and the included angle H, are severally equal to BC, **CD**, and the included angle **BCD**: therefore (by theo. 6. sect. 4.) HBF = DBC = BCA (by part 2. theo. 3. sect. 4.) and since HBD=A (by part. 3. theo. 3. sect. 4.) and HBF=BCA: therefore BFDis the difference, and EBD, half the difference of the angles A and C: then making BE the radius, it is plain, that EC will be the tangent of half the sum, and ED the tangent of half the difference of the two unknown angles A and C: now IG being parallel to AC; AH: IH: CH: GH. (by cor. 1. theo. 20. sect. 4.) But the wholes are as their halves, that is, AH: IH: CE: ED, that is as the sum of the two sides AB and BC, is to their difference; so is the tangent of half the sum of the two unknown angles A and C, to the tangent of half their difference. Q. E. D.

THEO. III.

Fig. 12.

In any right lined plane triangle ABD; the base AD will be to the sum of the other sides, AB, BD, as the difference of those sides is to the difference of the segments of the base, made by the perpendicular BE; viz. the difference between AE and ED.

Produce BD, till BG=AB the lesser leg; and on B as a centre, with the distance BG or BA, describe a circle AGHF; which will cut BD, and AD in the points H and F; then it is plain, that GD will be the sum, and HD the difference of the sides AB and BD; also since AE=EF (by theo. 8. sect. 4.) therefore, FD is the difference of AE ED, the segments of the base; but (by theo. 17. sect. 4.) AD: GD: HD: FD; that is, the base is to the sum of the other sides, as the difference of those sides is to the difference of the segments of the base. Q. E. D.

THEO. IV.

Fig. 13.

If to half the sum of two quantities, be added half their difference; the sum will be the greatest of them; and if from half the sum be subtracted half their difference; the remainder will be the least of them.

Let the two quantities be represented by AB and BC: (making one continued line;) whereof AB is the greatest, and BC the least; bisect the whole line AC in E; and make AD = BC; then

it is plain, that AC is the sum, and DB the difference of the two quantities; and AE or EC, their half sum, and DE or EB their half difference. Now if to AE we add EB, we shall have AB the greatest quantity; and if from EC we take EB, we shall have BC the least quantity. Q, E, D.

Cor. Hence, if from the greatest of two quantities, we take half the difference of them, the remainder will be half their sum; or if to half their difference be added the least quantity, their sum will be half the sum of the two quantities.

OBLIQUE ANGLED TRIANGLES.

CASE I.

TWO sides, and an angle opposite to one of them given; to find the other angles and side.

PL. 5. fig. 11.

In the triangle ABC, there is given AB 240, the angle A 46° 30°, and BC 200; to find the angle C, being acute, the angle B, and the side AC.

1st. By Construction.

Draw a blank line, on which set AB 240, from a scale of equal parts; at the point A, of the line AB, make an angle of 46° 30, by an indefinite blank line; with BC 200, from a like scale of equal parts that AB was taken, and one foot in B, describe the arc DC to cut the last blank line in the points D and C. Now if the angle C had been required obtuse, lines from D to B, and to A, would constitute the triangle; but as it is required acute,

draw the lines from C to B and to A, and the triangle ABC is constructed. From a line of chords let the angles B and C be measured; and AC from the same scale of equal parts that AB and BC were taken; and you will have the answers required.

2d. By Calculation.

This is performed by theo. 1. of this sect. thus;

As $BC = $ is to the sine of $A = $ So is $AB = $	200 46°. 30′ 240	2.301030 9.860562 2.380211
to the sine of C_{*}	60°. 31′	12.240773 9.939743

180°—the sum of the angles A and C, will give the angle B, by cor. 1. theo. 5, sect. 4.

A 46°. 30′ C 60. 31

180° — 107°. 1'=72°. 59' = B. As the sine of $A = 46^{\circ}$. 30' is to BC , = 200 So is the sine of $B = 72^{\circ}.59'$			9.860562 2.301030 9.980555
		·	12.281585
to AC,	=	263 , 7	2.421023

3d. By Gunter's Scale.

Extend from 200 to 240, on the line of numbers; that distance will reach from 46° 30′ on the line of sines, to 60° 31′ for the angle C₁

Extend from 46° 30′, to 72° 59′, on the line of sines; that distance will reach from 200 to 263.7 on the line of numbers, for AC.

Note. The method by Natural Sines will be obvious from the foregoing analogies.

CASE II.

Two angles and a side given; to find the other sides.

PL. 5. fig. 15.

In the triangle ABC, there is the angle A 46° 30' AB 230; and the angle B 37° 30', given to find AC and BC.

1st. By Construction.

Draw a blank line, upon which set AB 230, from a scale of equal parts; at the point A of the line AB, make an angle of 46°30′, by a blank line; and at the point B of the line AB make an angle of 37°30′, by another blank line: the intersection of those lines gives the point C, then the triangle ABC is constructed. Measure AC and BC from the same scale of equal parts that AB was taken; and you have the answer required.

2d. By Calculation.

By (cor. 1. theo. 5. sect. 4.) 180°—the sum of the angles A and B=C.

A 46° 30′

B 37. 30

 $180^{\circ} - 84^{\circ}$. $00' = 96^{\circ}$ 00' = C.

By def. 27. sect. 4. The sine of 96°=the sine of 84°, which is the supplement thereof; therefore instead of the sine of 96°, look in the tables for the sine of 84°.

By theo. 1. of this sect.

As the sine of $C = $ is to AB , $= $ So is the sine of $A = $	96° 00′ 230 46° 30′	9.997614 2.361728 9.860562
		12.222290
to BC , $=$	167.8	2.224676
As the sine of $C =$	96° 00′	9.997614
is to AB , =	230	2.361728
So is the sine of $B =$	37° 30′	9.784447
	·	12.146175
to AC , =	140.8	2.148561

3d. By Gunter's Scale.

Extend from 84° (which is the supplement of 96°) to 46° 30′ on the sines; that distance will reach from 230 to 168, on the line of numbers, for BC.

Extend from 84° to 37°. 30°, on the sines; that extent will reach from 230 to 141, on the line of numbers, for AC.

CASE III.

Two sides and a contained angle given; to find the other angles and side.

PL. 5. fig. 16.

In the triangle ABC, there is AB 240, the angle A 36° 40' and AC 180, given; to find the angles & and B, and the eide BC.

1st. By Construction.

Draw a blank line, on which from a scale of equal parts, lay AB 240; at the point A of the line AB, make an angle of 36° 40′, by a blank line; on which from A, lay AC 180, from the same scale of equal parts; measure the angles C and B, and the side BC, as before; and you have the answers required.

2d. By Calculation.

By cor. 1. theo. 5. sect. 4. 180° —the angle A 36° . $40' = 143^{\circ}$. 20' the sum of the angles C and B: therefore half of 143° . 20', will be half the sum of the two required angles, C and B.

By theo. 2. of this sect.

As the sum of the two sides AB and AC = 420 is to their difference, = 60

So is the tangent of half the sum of the two unknown angles C and B = 71° 40° to the tangent of half their difference = 23° 20°

By theo. 4.

To half the sum of the angles C and $B=71^{\circ}$ 46. Add half their difference as now found = 23 20.

The sum is the greatest angle, or ang. C=9500

Subtract, and you have the least angle, or B=4820

The angle C and B being found; BC is had, as before, by theo. 1. of this sect. Thus,

S. B : AC : : S : A : BC. 48° 20′ : 180 : : 36° 40 : 143. 9.

3d. By Gunter's Scalo.

Because the two first terms are of the same kind, extend from 420 to 60 on the line of numbers; lay that extent from 45° on the line of tangents, and keeping the left leg of your compasses fixed, move the right leg to 71°. 40′; that distance laid from 45° on the same line will reach to 23°. 30′, the half difference of the required angles. Whence the angles are obtained, as before.

The second proportion may be easily extended, from what has been already said.

CASE IV.

PL. 5. fig. 17.

The three sides given, to find the angles.

In the triangle ABC, there is given, AB 64, AC 47, BC 34; the angles A, B, C, are required.

1st. By Construction.

The construction of this triangle must be manifest, from prob. 1. sect. 4.

2d. By Calculation.

From the point C, let fall the perpendicular CD on the base AB; and it will divide the triangle into two right angled ones, ADC and CBD; as well as the base AB, into the two segments, AD and DB.

AC 47
BC 34
Sum 81
—
Difference 13

By theo. 3. of this sect.

As the base or the longest side, AB is to the sum of the other sides, AC a	64 nd <i>BC</i> , 81
So is the difference of those sides	13
to the difference of the segments of the base $AD DB$.	16.46

By theo. 4. of this sect.

To half the base, or to half the sum	32
of the segments AD and DB .	·
Add half their difference, now found,	8.23

Their sum will be the greatest segment AD 40.23

Subtract, and their difference will be the least segment DB,

In the right angled triangle ADC, there is AC47, and AD 40. 23, given, to find the angle A.

This is resolved by case 4. of right angled plane trigonometry, thus,

AD: **R**:: **AC**: Sec. **A** 40. 23: 90°: : 47: 31° 08′

Or it may be had by finding the angle ACD, the complement of the angle A; without a secant, thus,

AC: R:: AD: S. ACD. 47:90°::40_23:58°52'

 $90 - 58^{\circ} 52' = 31^{\circ}$. 08', the angle A.

Then by theo. 1. of this sect.

BC: S. A: AC: S. B. 34: 31° 08': : 47: 45° 37.

By cor. 1. theo. 5. sect. 4. 180° —the sum of A and B=C.

A 31°. 08′ B 45. 37

180°-76. 45=103°. 15′, the angle C:

3d. By Gunter's Scale.

The first proportion is extended on the line of numbers; and it is no matter whether you extend from the first to the third, or to the second term, since they are all of the same kind: If you extend to the second, that distance applied to the third, will give the fourth; but if you extend from the first to the third, that extent will reach from the second to the fourth.

The methods of extending the other proportions have been already fully treated of.

An example in each case of oblique angled triangles.

1. Given,
$$\begin{cases} AC & 290 \\ C69 & 30' \\ AB & 350 \end{cases} \stackrel{A}{B}$$
 required.
2. Given, $\begin{cases} C & 24^{\circ} \cdot 20' \\ B & 128^{\circ} \cdot 30 \\ AC & 3246 \end{cases} \stackrel{AB}{BC}$ required.
3. Given, $\begin{cases} AC & 6 \\ C & 124^{\circ} \cdot 30' \\ BC & 4 \cdot 5 \end{cases} \stackrel{A}{B}$ required.
4. Given, $\begin{cases} AB & 46 \\ AC & 92 \\ BC & 52 \end{cases} \stackrel{A}{C}$ required.

Additional Exercises with their Answers.

QUESTIONS FOR EXERCISE.

1. Given the Hypothenuse 108 and the Angle opposite the Perpendicular 25° 36; required the Base and Perpendicular.

Answer. The Base is 97.4, and the Perpendi-

cular 46.66.

2. Given the Base 96 and its opposite Angle 71. 45'; required the Perpendicular and the Hypothenuse.

Answer. The Perpendicular is 31.66 and the Hypothenuse 101.1.

3. Given the Perpendicular 360 and its opposite Angle 58° 20'; required the Base and the Hypothenuse.

Answer. The Base is 222, and the Hypothenuse 423.

- 4. Given the Base 720 and the Hypothenuse 980; required the Angles and the Perpendicular. Answer. The Angles are 47° 17′. and 42° 43′, and the Perpendicular 664.8
- 5. Given the Perpendicular 110.3 and the Hypothenuse 176.5; required the Angles and the Base.

Answer. The Angles are 38°41' and 51°19', and the Base 137.8.

6. Given the Base 360 and the Perpendicular 480; required the Angles and the Hypothenuse.

Answer. The Angles are 53°8′ and 36°52′, and the Hypothenuse 600.

7. Given one Side 129, an adjacent Angle 56° 30, and the opposite Angle 81° 36′: required the third Angle and the remaining Sides.

Answer. The third Angle is 41° 54', and the

remaining Sides are 108.7 and 87.08.

8. Given one Side 96.5, another Side 59.7, and the Angle opposite the latter Side 31°30′: required the remaining Angles and the third Side.

Answer. This Question is ambiguous; the given Side opposite the given Angle being less than the other given Side (see Rule I.;) hence, if the Angle opposite the Side 96.5 be acute, it will be 57° 38', the remaining Angle 90° 52', and the third Side 114.2; but if the Angle opposite the Side 96.5 be obtuse, it will be 122° 22', the remaining Angle 26° 8', and the third Side 50.32.

9. Given one Side 110, another Side 102, and the contained Angle 113° 36: required the remaining Angles and the third Side.

Answer. The remaining Angles are 34° 37' and

31° 47', and the third Side is 177.5.

10. Given the three Sides respectively, 120.6, 125.5, and 146.7: required the Angles.

Answer. The Angles are 51° 53', 54° 58', and

73° 9′. ''

The student, who has advanced thus far in this work with diligence and active curiosity, is now prepared to study, with ease and pleasure, the following part; which comprehends all the necessary directions for the practice of Surveying.

PART II.

Or the Practical Surveyor's Guide.

SECT. I.

Containing a particular Description of the several Instruments used in Surveying, with their respective Uses.

THE CHAIN,

THE stationary distance, or merings of ground, are measured either by Gunter's chain of four poles or perches, which consists of 100 links; (and this is the most natural division) or by one of 50 links, which contains two poles or perches: but because the length of a perch differs in many places, therefore the length of chains and their respective links will differ also.

The English statute-perch is 5½ yards, the two-pole chain is 11 yards, and the four-pole one is 22 yards; hence the length of a link in a statute-chain is 7.92 inches.

There are other perches used in different parts of England, as the perch of *noodland measure*, which is 6 yards; that of *church-land measure*, which is 7 yards, and the *forest measure perch*, which is 8 yards.

For the more ready reckoning the links of a four-pole chain, there is a large ring, or sometimes a round piece of brass, fixed at every 10 links; and at 50 links, or in the middle, there are two large In such chains as have a brass piece at every 10 links, there is the figure 1 on the first piece, 2 on the second, 3 on third, &c. to 9. leading therefore that end of the chain forward which has the least number next to it, he who carries the hinder end may easily determine any number of links: thus, if he has the brass piece number 8, next to him, and six links more in a distance. that distance is 86 links. After the same manner 10 may be counted for every large ring of a chain which has not brass pieces on it; and the number of links is thus readily determined.

The two-pole chain has a large ring at every 10 links, and in its middle, or at 25 links, there are 2 large rings; so that any number of links may be the more readily counted off, as before.

The surveyer should be careful to have his chain measured before he proceeds on business, for the rings are apt to open by frequently using it, and its length is thereby increased, so that no one can be too circumspect in this point,

In measuring a stationary distance, there is an object fixed in the extreme point of the line to be measured; this is a direction for the hinder chainman to govern the foremost one by, in order that the distance may be measured in a right line; for if the hinder chainman causes the other to cover the object, it is plain the foremost is then in a right line towards it. For this reason it is necessary to have a person that can be relied on, at the hinder

end of the chain, in order to keep the foremost man in a right line; and a surveyor who has no such person, should chain himself. The inaccuracies of most surveys arise from bad chaining, that is, from straying out of the right line, as well as from other omissions of the hinder chainman: no person, therefore, should be admitted at the hinder end of the chain, of whose abilities in this respect, the surveyor was not previously convinced; since the success of the survey, in a grest measure, depends on his care and skill.

In setting out to measure any stationary distance, the foreman of the chain carries with him 10 iron pegs pointed, each about ten inches long; and when he has stretched the chain to its full length, he at the extremity thereof sticks one of those pegs perpendicularly in the ground; and leaving it there, he draws on the chain till the hinder man checks him when he arrives at that peg: the chain being again stretched, the fore man sticks down another peg, and the hind man takes up the former; and thus they proceed at every chain's length contained in the line to be measured, counting the surplus links contained between the last peg, and the object at the termination of the line, as before: so that, the number of pegs taken up by the hinder chainman, expresses the number of chains; to which, if the odd links be annexed, the distance line required in chains and links is obtained, which must be registered in the field book, as will hereafter be shewn.

If the distance exceeds 10, 20, 30, &c. chains, when the leader's pegs are all exhausted, the hinder chainman, at the extremity of the 10 chains, delivers him all the pegs; from whence they pro-

ceed to measure as before, till the leader's pegs are again exhausted, and the hinder chainman at the extremity of these 10 chains again delivers him the pegs; from whence they proceed to measure the whole distance line in the like manner; then it is plain, that the number of pegs the hinder chainman has, being added to 10, if he had delivered all the pegs once to the leader, or to 20 if twice, or to 30 if thrice, &c. will give the number of chains in that distance; to which if the surplus links be added, the length of the stationary distance is known in chains and links.

It is customary, and indeed necessary, to have red, or other coloured cloth, fixed to the top of each peg, that the hinder man at the chain may the more readily find them; otherwise, in chaining through corn, high grass, briars, rushes, &c. it would be extremely difficult to find the pegs which the leader puts down: by this means no time is lost, which otherwise must be, if no cloths are fixed to the pegs, as before.

It will be necessary here to observe, that all slant, or inclined surfaces, as sides of hills, are measured horizontally, and not on the plane or surface of the hill, and is thus effected.

PL. 8, Ag. 4.

Let ABC be a hill, the hindmost chainman is to hold the end of the chain perpendicularly over the point A (which he can'the better effect with a plummet and line, than by letting a stone drop, which is most usual) as d is over A, while the leader puts down his peg at e: the eye can direct the horizontal position near enough, but if greater accuracy

were required, a quadrant applied to the chain, would settle that. In the same manner the rest may be chained up and down; but in going down, it is plain the leader of the chain must hold up the end thereof, and the plummet thence suspended, will mark the point where he is to stick his peg. The figure is sufficient to render the whole evident; and to shew that the sum of the chains will be the horizontal measure of the base of the hill; for de = Ao, fg = op, hi = pq, &c. therefore $de \times fg \times hi$, &c. = $Ao \times op \times pq$, &c. = AC, the base of the hill. If a whole chain cannot be carried horizontally, half a chain, or less, may, and the sum of these half chains, or links, will give the base, as before.

If the inclined side of the hill be the plane surface, the angle of the hill's inclination may be taken, and the slant height may be measured on the surface; and thence (by case 1. of right-angled trigonometry) the horizontal line answering to the top, may be found; and if we have the angle of inclination given on the other side, with those already given; we can find the horizontal distance across the hill, by case 2. of oblique trigonometry.

All inclined surfaces are considered as horizontal ones; for all trees which grow upon any inclined surface, do not grow perpendicular thereto, but to the plane of the horizon: thus if Ad, ef, gh, &c. were trees on the side of a hill, they grow perpendicular to the horizontal base AC, and not to the surface AB: hence the base will be capable to contain as many trees as are on the surface of the hill, which is manifest from the continuation of them thereto. And this is the reason that the area of the base of a hill, is considered to be equal in value to the hill itself.

Besides, the irregularities of the surfaces of hills in general are such, that they would be found impossible to be determined by the most able mathematicians. Certain regular curve surfaces have been investigated with no small pains, by the most eminent; therefore an attempt to determine in general the infinity of irregular surfaces which offer themselves to our view, to any degree of certainty, would be idle and ridiculous, and for this reason also, the horizontal area is only attempted.

Again, if the circumjacent lands of a hill be planned or mapped, it is evident we shall have a plan of the hill's base in the middle: but were it possible to put the hill's surface in lieu thereof, it would extend itself into the circumjacent lands, and render the whole an heap of confusion: so that if the surfaces of hills could be determined, no more than the base could be mapped

Roads are usually measured by a wheel for that purpose, called the Perambulator, to which there is fixed a machine, at the end whereof there is a spring, which is struck by a peg in the wheel, once in every rotation; by this means the number of rotations is known; if such a wheel were 3 feet 4 inches in diameter, one rotation would be 101 feet, which is half a plantation perch; and because 320 perches make a mile, therefore 640 rotations will be a mile also; and the machinery is so contrived, that by means of a hand, which is carried round by the work, it points out the miles, quarters, and perches, or sometimes the miles, furlongs, and perches.

Or roads may be measured by a chain more accurately; for 80 four-pole, 160 two-pole chains, or 320 perches, make a mile as before: and if roads

are measured by a statute-chain, it will give you the miles English, but if by a plantation chain, the miles will be Irish. Hence an English mile contains 1760, and an Irish mile 2240 yards; and because 14 half yards is an Irish, and 11 half yards is an English perch, therefore 11 Irish perches, or Irish miles, are equal to 14 English ones.

Since some surveys are taken by a four-pole, and others by a two-pole chair; and as ground for houses is measured by feet, we will shew how to reduce one to the other, in the following problems.

PROB. I.

To reduce two-hole chains and links to four-hole ones.

If the number of chains be even, the half of them will be the four-pole ones, to which annex the given links, thus,

Ch. L.

1. In 16. 37 of two pole chains, how many fourpole ones?

Ch. L. Answer 8, 37.

But if the number of chains be odd, take the half of them for chains, and add 50 to the links, and they will be four-pole chains and links, thus,

Ch. L.

2. In 17. 42 of two-pole chains, how many four-pole ones?

Ch. L, Answer 8. 92,

PROB. H.

To reduce four-fiele chains and links, to two-field over:

Double the chains, to which annex the links, if they be less than 50; but if they exceed 50, double the chains, add one to them, and take 50 from the links, and the remainder will be the links, thus,

Ch. L.

1. In 8. 37 of four-pole chains, how many two-pole ones?

16. 37

Ch. L.

2. In 8. 82 of four-pole chains, how many 2. 50 two-pole ones?

17. 32 Answer,

PROB. III.

To reduce four-pole chains and links, to perches and decimals of a perch.

The links of a four-pole chain are decimal parts of it, each link before the hundreth part of a chain; therefore if the chain and links be multiplied by 4, (for 4 perches are a chain) the product will be the perches and decimal parts of a perch. Thus,

How many perches in 13. 64 of four pole chains,

Answer 54, 56 perches.

PROB. IV.

To reduce two-pole chains and links, to perches and decimals of a perch.

They may be reduced to four-pole ones (by prob. 1.) and thence to perches and decimals (by the last,) or,

If the links be multiplied by 4, carrying one to the chains, when the links are, or exceed 25; and the chains by 2, adding one, if occasion be; the product will be perches, and decimals of a perch. Thus,

Ch. L.
1. In 17. 21 of two-pole chains, how many

2. 4 perches.

Answer, 34. 84 perches.

Ch. L.

2. In 15. 38 of two-pole chains, how mnay 2. 4 perches.

Answer, 31. 52 perches.

PROB. V.

To reduce perches, and decimals of a perch, to four-pole chains and links.

Divide by 4, so as to have two decimal places in the quotient, and that will be four-pole chains and links. Thus, In 31. 52 perches, how many four-pole chains and links?

Ch. L. 4)31.52(7. 88 Answer.

35

32

PROB. VI.

To reduce perches and decimals of a perch, to two-pole chains and links.

The perches may be reduced to four-pole chains (by the last) and from thence to two-pole chains (by prob. 2.) or,

Divide the whole number by 2, the quotient will be chains; to the remainder annex the given decimals, and divide by 4, the last quotient will be the links. Thus,

In 31.52 perches, how many two-pole chains and links?

Ch. L. 2)31.52(15. 38 Answer.

11 4)152(38

32

PROB. VII.

To reduce chains and links, to feet and decimal parts of a foot.

If they be two-pole chains, reduce them to fourpole ones: (by prob. 1.) these being multiplied by the feet in a four-pole chain, will give the feet and decimals of a foot. Thus,

Ch. L. In 17. 21 of two-pole chains, how many feet?

Ch. L.
 71 of four-pole chains.
 66 feet = 1 chain.

5226. Feet Inches 5226 Answer 574. 104.

Feet 574.86 12 Inches 10.32 4 1.28

PROB. VIII.

To reduce feet and inches to chains and links.

Reduce the inches to the decimal of a foot, and annex that to the feet; that divided by the feet in a four-pole chain, will give the four-pole chains and

links in the quotient: these may be reduced to two-pole chains and links, if required, by prob. 2. Thus,

Feet. Inches.

In 217. 9 how many two-pole chains? 12)9.00.(75 the decimal of 9 inches.

60

66)217.75(3. 29 of four-pole chains, or

197 655 Ch. L. 656 6. 29

How to take a Survey by the CHAIN only.

PROB. I.

To survey a piece of ground, by going round it, and the men thod of taking the angles of the field, by the chain only.

PL. 6. fig. 6.

Let ABCDEFG be a piece of ground to be surveyed: beginning at the point A, let one chain be laid in a direct line from A, towards G, where let a peg be left, as at c; and again, the like distance from A in a direct line towards B; where another peg is also to be left, as at d: let the distance from d to c be measured, and placed in the field-book, in

بنج

the second column under the denomination of angles, in a line with station No. 1; and in the same line, under the title of distances, in the third column, let the measure of the line AB in chains and links be inserted. Being now arrived at B, let one chain be laid in a direct line from B towards A, where let a peg be left, as at f, and again, the like distance from B in a direct line towards C, where let also another peg be left, as ate; the distance from e to f is to be inserted in the field-book in the second column, under angles, in a line with station No. 2; and in the same line, under the title of distances in the third column, let the measure of the line BC, in chains and links, be inserted: after the same manner we may proceed from C to D, and thence to E; but because the angle at E, vis. FED, is an external angle, after having laid one chain from E to h, and to g, the distance from g to h is measured, and inserted in the column of angles, in a line with station No. 5. and on the side of the field-book against that station, we make an asterisk, thus *, or any other mark, to signify that to be an external angle, or one measured out of the ground. Proceed we then as before, from E to F, to G, and thence to A, measuring the angles and distances. and placing them as before, in the field-book, opposite to their respective stations; so will the fieldbook be completed in manner following.

N. B. After this manner the angles for inaccessible distances may be taken, and the method of constructing or laying them down, as well as the construction of the map, from the following field-notes, must be obvious from the method of taking them.

The form of the field-book, with the title.

A field-book of part of the land of Grange, in the parish of Portmarnock, barony of Coolock, and county of Dublin; being part of the estate of L. P. Esq. let to C. D. farmer. Surveyed January 30, 1782.

Taken by a four-pole chain.

Remarks.	No. Sta.	Angles Ch. L.	Distan. Ch. L.
Mr. J. D's part of Grange	1	1.80	17.65
	2	1.79	18.50
Mr. L. P's part of Portmar-		1.76	28.00
nock strand	4	1.411.	20.00
*	5	1.874	14.83
Widow J. G's part of Grange	6	1.14	19.41
	7	1.89	24.53
	Close at the first station.		

Explanation of the remarks.

Mr. J. D's part of Grange bounds, or is adjacent to the surveyed land from the first to the third station; Mr. L. P's part of Portmarnock bounds it from the third to the fourth station; the strand then is the boundary from thence to the sixth, and from the sixth to the first station, the widow J. G's part of Grange is the boundary.

It is absolutely necessary to insert the persons' names, and town-lands, strands, rivers, bogs, rivulets, &c. which bound or circumscribe the land which is surveyed, for these must be expressed in the map.

In a survey of a town-land, or estate, it is sufficient to mention only the circumjacent town-lands, without the occupiers' names: but when a part only of a town-land is surveyed, then it is necessary to insert the person or persons' names, who hold any particular parcel or parcels, of such townland, as bound the parts surveyed.

When an angle is very obtuse, as most in our present figure are, viz. the angles at A, B, C, E, and G: it will be best to lay a chain from the angular point, as at A, on each of the containing sides to c and to d; and any where nearly in the middle of the angle, as at c: measuring the distances c and c; and these may be placed for the angle in the field-book. Thus,

For when an angle is very obtuse, the chord line, as ed, will be nearly equal to the radii Ac and Ad; so if the arc ced be swept, and the chord line ed be laid on it, it will be difficult to determine exactly that point in the arc where ed cuts it: but if the angle be taken in two parts, as ce, the arc, and the angle thence, may be truly determined and constructed.

After the same manner any piece of ground may be surveyed by a two-pole chain.

PROB. II.

To take a survey of a piece of ground from any point within it, from whence all the angles can be seen; by the chain only.

PL. 6. fig. 6.

Let a mark be fixed at any point in the ground, as at H, from whence all the angles can be seen; let the measures of the lines HA, HB, HC, &c. be taken to every angle of the field from the point H; and let those be placed opposite to No. 1, 2, 3, 4, &c. in the second column of the radii: the measures of the respective lines of the mearing, viz. AB, BC, CD, DE, &c. being placed in the third column of distances, will complete the field-book. Thus,

Remarks.		dii Distan. L.Ch. L.
	1 20.0	00 17.65
	2 21.	72 18.50
	3 21.	74 28.00
•	4 25.	34 20.00
		20 14.83
	6 29.	62 19.41
	7 21.	2 0 24.5 3
	Close at the	first station.

If any line of the field be inaccessible, as suppose CD to be, then by way of proof that the distance CD is true, let the measure of the angle CHD be taken by the line oo, with the chain: if this angle corresponds with its containing sides, the length of the line DO truly obtained, and the whole work is truly taken.

Note, That in setting off an angle, it is necessary to use the largest scale of equal parts, vis. that of the inch, which is diagonally divided into 100 parts, in order that the angle should be accurately laid down; or if two inches were thus divided for angles, it would be the more exact; for it is by no means necessary that the angles should be laid from the said scale with the stationary distances.

PROB. III.

To take a survey by the chain only, when all the angles cannot be seen from one point within.

PL. 6. fig. 7.

Let the ground to be surveyed be represented by 1, 2, 3, 4, &c. Since all the angles cannot be seen from one point, let us assume 3 points, as A, B, C, from whence they may be seen; at each of which let a mark be put, and the respective sides of the triangle be measured and set down in the field-book; let the distance from A to 1, and from B to 1, be measured, and these will determine the point 1; let the other lines which flow from A, B, C, as well as the circuit of the ground, be then measured as the figure directs; and thence the map may be easily constructed.

There are other methods which may be used; as dividing the ground into triangles, and measuring the 3 sides of each; or by measuring the base and perpendicular of each triangle. But this we shall speak of hereafter.

PROB. IV.

How to take any inaccessible distance by the chain only.

PL. 8. fig. 8.

Suppose AB to be the breadth of a river, or any other inaccessible distance, which may be required.

Let a staff or any other object be set at B, draw yourself backward to any convenient distance C, so that B may cover A: from B, lay off any other distance by the river's side to E, and complete the parallelogram EBCD: stand at D, and cause a mark to be set at F, in the direction of A; measure the distance in links from E to F, and FB will be also given. Wherefore EF:ED::FB:AB. Since it is plain (from part 1. theo. 3. sect. 4. and theo. 2. sect. 4.) the triangles EFDBFA are mutually equiangular.

If part of the chain be drawn from B to C, and the other part from B to E; and if the ends at E and C be kept fast, it will be easy to turn the chain over to D, so as to complete a parallelogram; by reckoning off the same number of links you had in BC, from E to D, and pulling each part straight.

THE

CIRCUMFERENTOR.

HIS instrument is composed of a brass circular box, about five or six inches in diameter; within which is a brass ring, divided on the top into 360 degrees, and numbered 10, 20, 30, &c. to 360: in the centre of the box is fixed a steel pin finely pointed, called a centre-pin, on which is placed a needle touched by a loadstone, which always retains the same situation; that is, it always points to the North and South points of the horizon nearly, when the instrument is horizontal, and the needle at rest.

The box is covered with a glass lid, in a brass rim, to prevent the needle being disturbed by wind or rain, at the time of surveying: there is also a brass lid or cover, which is laid over the former to preserve the glass in carrying the instrument.

This box is fixed by screws, to a brass index, or ruler, of about 14 or 15 inches in length, to the ends whereof are fixed brass sights, which are screwed to the index, and stand perpendicular thereto: in each sight is a large and a small aperture, or slit, one over the other; but these are changed, that is, if the large aperture be uppermost in the one sight, it will be lowest in the other, and

so of the small ones: therefore the small aperture in one is opposite to the large one in the other; in the middle of which last, there is placed a horse hair, or fine silk thread.

The instrument is then fixed on a ball and socket; by the help of which and a screw, you can readily fix it horizontally in any given direction; the socket being fixed on the head of a three-legged staff, whose legs, when extended, support the instrument whilst it is used.

To take field notes by the Circumferentor.

PL. 6. fig. 6.

Let your instrument be fixed at any angle as A, your first station; and let a person stand at the next angle B, or cause a staff, with a white sheet, to be set there perpendicularly for an object to take your view to: then having placed your instrument horizontally (which is easily done by turning the box so that the ends of the needle may be equidistant from its bottom, and it traverses or plays freely) turn the flower-de-luce, or north part of the box, to your eye, and looking through the small aperture, turn the index about, till you cut the person or object in the next angle B, with the horse hair, or thread of the opposite sight; the degrees then cut by the south end of the needle, will give the number to be placed in the second column of your field-book in a line with station No. 1, and expresses the number of degrees the stationary line is from the north, counting quite round with the sun.

Most needles are pointed at the south end, and have a small ring at the north: such needles are

better than those which are pointed at each end, because the surveyor cannot mistake by counting to a wrong end; which error may be frequently committed, in using a two-pointed needle.

Two-pointed needles have sometimes a ring, but more usually a cross towards the north end: and the south end is generally bearded towards its extremity, and sometimes not, but its arm is a naked right line from the cap at the centre.

Having taken the degrees or bearing of the first stationary line AB, let the line be measured, and the length thereof in chains and links be inserted in the third column of your field-book, under the title of distances, opposite to station No. 1.

It is customary, and even necessary, to cause a sod to be dug up at each station, or place where you fix the instrument: to the end, that if any error should arise in the field-book, it may be the more readily adjusted and corrected, by trying over the former bearings and stationary distances.

Having done with your first station, set the instrument over the hole or spot where your object stood, as at B, for your second station, and send him forward to the next angle of the field, as at C; and having placed the instrument in an horizontal direction, with the sights directed to the object at C, and the north of the box next your eye, count your degrees to the south end of the needle, which register in your field-book, in the second column opposite to station No. 2; then measure the stationary distance BC, which insert in the third column, and thus proceed from angle to angle, sending your object before you, till you

return to the place where you began, and you will have the field-book complete; observing always to signify the parties names who hold the contiguous lands, and the names of the town-lands, rivers, roads, swamps, lakes, &c. that bound the land you survey, as before; and this is the manner of taking field-notes by what is called foresights.

But the generality of mearsmen frequently set themselves in disadvantageous places, so as often to occasion two or more stations to be made, where one may do, which creates much trouble and loss of time; we will therefore shew how this may be remedied, by taking back-sights, thus: let your object stand at the point where you begin your survey, as at A; leaving him there, proceed to your next angle B, where fix your instrument so, that you may have the longest view possible towards C. Having set the instrument in an horizontal position, turn the south part of the box next your eye, and having cut your object at A, reckon the degrees to the south point of the needle, which will be the same as if they were taken from the object to the instrument, the direction of the index being the same. Let the degree be inserted in the fieldbook, and the stationary distance be measured and annexed thereto, in its proper column; and thus proceed from station to station, leaving your object in the last point you left, till you return to the first station A.

By this method your stations are laid out to the best advantage, and two men may do the business of three, for one of those who chain, may be your object; but in fore-sights, you must have an object before you, besides two chainmen.

It was said before, that a surveyor should have a person with him to carry the hinder end of the chain, on whom he can depend: this person should be expert and ready at taking off-sets, as well as exact in giving a faithful return of the length of every stationary line. One who has such a person, and who uses back-sights, will be able to go over near double the ground he could at the same time, by taking fore-sights, because of overseeing the chaining; for should he take back-sights, he must be obliged, after taking his degree, to go back to the foregoing station, to oversee the chaining, and by this means to walk three times over every line, which is a labour not to be borne.

Or a back and a fore-sight may be taken at one station, thus; with the south of the box to your eye, observe from B the object A, and set down the degree in your field-book, cut by the south end of the needle. Again from B observe an object at C, with the north of the box to your eye, and set down the degree cut by the south point of the needle, so have you the bearings of the lines AB and BC; you may then set up your instrument at D, from whence take a back-sight to C, and a fore-sight to E: thus the bearings may be taken quite round, and the stationary distances being annexed to them, will complete the field-book.

But in this last method, care must be taken to see that the sights have not the least cast on either side; if they have, it will destroy all: and yet with the same sights you may take a survey by fore-sights, or by back-sights only, with as great truth as if the sights were ever so erect, provided the same cast continues without any alteration; but, upon the whole, back-sights only will be found the readiest method.

If your needle be pointed at each end, in taking fore-sights, you may turn the north part of the box to your eye, and count your degrees to the south part of the needle, as before; or you may turn the south of the box to your eye, and count your degrees to the north end of the needle.

But in back-sights you may turn the north of the box to your eye, and count your degrees to the north point of the needle; or you may turn the south of the box to your eye, and count your degrees to the south end of the needle.

The brass ring in the box is divided on the side into 360 degrees, thus; from the north to the east into 90, from the north to the west into 90, from the south to the east into 90, and from the south to the west into 90 degrees; so the degrees are numbered from the north to the east or west, and from the south to the east or west.

The manner of using this part of the instrument is this; having directed your sights to the object, whether fore or back, as before, observe the two cardinal points of your compass, the point of the needle lies between, (the north, south, east and west being called the four cardinal points, and are graved on the bottom of the box) putting down those points, together by their initial letters, and thereto annexing the number of degrees, counting from the north or south, as before, thus; if the point of your needle lies between the north and east, north and west, south and east, or south and west points in the bottom of the box, then put down NE, NW, SE, or SW, annexing thereto the number of degrees cut by the needle on the side of the ring, counting from the north or south as before.

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But if the needle point exactly to the north, south, east, or west, you are then to write down N, S, E, or W, without annexing any degree.

This is the manner of taking field notes, whereby the content of ground may be universally determined by calculation; and they are said to be taken by the quartered compass, or by the four nineties.

To find the number of degrees contained in any given angle.

Set up your instrument at the angular point, and thence direct the sights along each leg of the angle, and note down their respective bearings, as before; the difference of these bearings, if less than 180, will be the quantity of degrees contained in the given angle; but if more, take it from 360, and the remainder will be the degrees contained in the given angle.

THE

THEODOLITE.

THIS instrument is a circle, commonly of brass, of ten or twelve inches in diameter, whose limb is divided into 300 degrees, and those again are subdivided into smaller parts, as the magnitude of it will admit; sometimes by equal divisions, and sometimes by diagonals, drawn from one concentric circle of the limb to another.

In the middle is fixed a circumferentor, with a needle; but this is of little or no use, except in finding a meridian line, or the proper situation of the land.

Over the brass circle is a pair of sights, fixed to a moveable index, which turns on the centre of the instrument, and upon which the circumferentor-box is placed.

This instrument will either give the angles of the field, or the bearing of every stationary distance line, from the meridian; as the circumferentor and quartered compass do.

To take the angles of the field.

PL. 6. fig. 6.

Lay the ends of your index to 360°, and 180°; turn the whole about with the 360 from you; direct

the sights from A to G, and screw the instrument fast; direct them from A, to cut the object at B; the degree then cut by that end of the index which is opposite you, will be the quantity of the angle GAB, to place in your field-book; to which annex the measure of the line AB, in chains and links; set up your instrument at B, unscrew it, and lay the ends of your index to 360 and 180; turn the whole about with the 360 from you, or 180 next you, till you cut the object at A; screw the instrument fast, and direct your sights to the object at C, and the degree then cut by that end of the index which is opposite to you, will be the quantity of the angle ABC. Thus proceed from station to station, still laying the index to 360, turning it from you, and observing the object at the foregoing station, screwing the instrument fast, and observing the object at the following station, and counting the degrees to the opposite end of the index, will give you the quantity of each respective angle.

LEMMA.

All the angles of any holygon, are equal to twice as many right angles as there are sides less by four. Thus, all the angles A, B, C, D, E, F, G, are equal to twice as many right angles as there are sides in the figure, less by four.

PL. 6. fig. 6.

Let the polygon be disposed into triangles, by lines drawn from any assigned point H within it, as by the lines HA, HB, HC, &c. It is evident then (by theo. 2. sect. 4. part 1.) that the three angles of each triangle are equal to two right; and consequently, that the angles in all the triangles are twice as many right ones as there are sides:

but all the angles about the point H, are equal to four right (by cor. 2. theo. 1. sect. 4.); therefore the remaining angles are equal to twice as many right ones as there are sides in the figure, abating four. Q. E. D.

SCHOLIUM.

Hence we may know if the angles of a survey be truly taken; for if their sum be equal to twice as many right angles, as there are stations, abating four right angles, you may conclude that the angles were truly taken, otherwise not.

If you take the bearing of any line with the circumferentor, that bearing will be the number of degrees the line is from the north; consequently the north must be a like number of degrees from the line, and thus the north, and of course the south, as well as the east and west, or the situation of the land, is obtained.

To take the bearing of each respective line from the meridian; or to perform the office of the circumferentor, or quartered compass by the theodolite.

Set your instrument at the first station, and lay the index to 360° and 180°, with the flower-de-luce of the box next 360; unscrew the instrument, and turn the whole about, till the north and south points of the needle cut the north and south points in the box; then screw it fast, and the instrument is north and south, if there be no variation in the needle; but if there be, and its quantity known, it may be easily allowed.

The circumferentor-box may then be taken off.

Direct the sights to the object at the second station, and the degree cut by the opposite end of the index will be the bearing of that line from the north, and the same that the circumferentor would give.

After having measured the stationary distance, set up your instrument at the second station; unscrew it, and set either end of the index to the degree of the last line, and turning the whole about with that degree towards you, direct your sights to an object at the foregoing station, and screw the instrument fast; it will then be parallel to its former situation, and consequently north and south; direct then your sights to an object at the following station, and the degree cut by the opposite end of the index, will be the bearing of that line.

In like manner you may proceed through the whole.

If the brass circle be divided into four nineties, from 360 and 180, and the letters N, S, E, W, be applied to them; the bearings may be obtained by putting down the letters the far or opposite end of the index lies between, and annexing thereto the degrees from the N or S; and this is the same as the quartered compass.

If you keep the compass box on, to see the mutual agreement of the two instruments; after having fixed the theodolite north and south, as before; turn the index about with the north end or flower-de-luce next your eye, and count the degree to the opposite, or south end of the index, and this will correspond with the degree cut by the south end of the needle.

At the second, or next station, unscrew the instrument, and set the south of the index to the degree of the last station; turn the whole about, with the south of the index to you, and cut the object at the foregoing station; screw the instrument fast, and with the north of the index to you, cut the object at the next following station, the degree then cut by the south of the index, will correspond with the degree cut by the south end of the needle, and so through the whole.

Some theodolites have a standing pair of sights fixed at 360 and 180, besides those on the moveable index; if you would use both, look through the standing sights, with the 180 next you, to an object at the foregoing station: screw the instrument fast, and direct the upper sights on the moveable index, to the object at the following station, and the degree cut by the opposite end of the index, will give you the quantity of the angle of the field.

Two pair of sights can be of no use in finding the angles from the meridian; and inasmuch as one pair is sufficient to find the angles of the field, the second can be of no use: besides, they obstruct the free motion of the moveable index, and therefore are rather an incumbrance than of any real use. Some will have it, that they are useful with the others, for setting off a right angle, in taking an off-set: and surely this is as easily performed by the one pair on the moveable index: thus, if you lay the index to 360 and 180, and cut the object either in the last or following station, screw the instrument fast, and turn the index to 90 and 270, and then it will be at right angles with the line. So that the small sights, at those of the circle, can be

of no additional use to the instrument, and therefore should be laid aside as useless.

This instrument may be used in windy andrainy weather, as well as in mountainous and hilly grounds; for it does not require an horizontal position to find the bearing, or angle, as the needle doth; and therefore is preferred to any instrument that is governed by the needle.

THE SEMICIRCLE.

THIS instrument, as its name imports, is a half circle, divided from its diameter into 180 degrees, and from thence again, that is, from 0, to 360 degrees: it is generally made of brass, and is from 8 to 18 inches diameter.

On the centre there is a moveable index with sights, on which is placed a circumferentor-box, as in the theodolite.

This instrument may be used as the theodolite in all respects; but with this difference, when you are to reckon the degree to that end of the index which is off the semicircle, you may find it at the other end, reckoning the degree from 180 forwards,

THE

PLANE TABLE.

A PLANE TABLE is an oblong of oak, or other wood, about 15 inches long, and 12 broad; they are generally composed of 3 boards, which are easily taken asunder, or put together, for the convenience of carriage.

There is a box frame, with 6 joints in it, to take off and put on as occasion serves; it keeps the table together, and is likewise of use to keep down a sheet of paper which is put thereon.

The outside of the frame is divided into inches and tenths, which serve for ruling parallels or squares on the paper, or for shifting it, when occasion serves.

The inside of the frame is divided into 360 degrees, which, though unequal on it, yet are the degrees of a circle produced from its centre, or centre of the table, where there is a small hole.

The degrees are subdivided as small as their distance will admit; at every tenth degree are two numbers, one the number of degrees, the other its complement to 360.

There is another centre hole about \$\frac{1}{4}\$ of the table's breadth from one edge, and is in the mid-

dle between the two ends. To this centre hole on the other side of the frame, there are the divisions of a semicircle, or 180 degrees; and these again are subdivided into halves, or quarters, as the size of the instrument will admit.

That side of the frame on which the 360 degrees are, supplies the place of a theodolite, the other, that of a semicircle.

There is a circumferentor-box of wood, with a paper chart at the bottom, applied to one side of the table by a dove-tail joint, fastened by a screw. This box (besides its rendering the plane table capable of answering the end of a circumferentor) is very useful for placing the instrument in the same position every remove.

There is a brass ruler or index, of about two inches broad, with a sharp or fiducial edge, at each end of which is a sight; on the ruler are scales of equal parts, with and without diagonals, and a scale of chords; the whole is fixed on a ball and socket, and set on a three-legged staff.

To take the angles of a field by the table.

Having placed the instrument at the first station, turn it about till the north end of the needle be over the meridian, or flower-de-luce of the box, and there screw it fast. Assign any convenient point, to which apply the edge of the index, so as through the sights you may see the object in the last station, and by the edge of the index from the point draw a line. Again, turn about the index with its edge to the same point, and through the sights ob-

serve the object in the second station, and from the point, by the edge of the index, draw another line; so is the angle laid down; on that last line set off the distance to the second station, in chains and links; apply your instrument to the second station, taking the angle as before; and after the like manner proceed till the whole is finished.

This method may be used in good weather, if the needle be well touched and play freely; but if it be in windy weather, or the needle out of order, it is better, after having taken the first angle as before, and having removed your instrument to the second station, and placed the needle over the meridian line as before, to lay the index on the last drawn line, and look backward through the sights; if you then see the object in the first station, the table is fixed right, and the needle is true; if not, turn the table about, the index lying on the last line, till through the sights you see the object in the first station: and then screw it fast, and keeping the edge of the index to the second station, direct your sights to the next; draw a line by the edge - of the index, and lay off the next line; and proceed through the whole without using the needle, as you do with the theodolite.

If the sheet of paper on the table be not large enough to contain the map of the ground you survey, you must put on a clean sheet, when the other is full; and this is called shifting of paper, and is thus performed.

PL. 6. fig. 8.

Let ABCD represent the sheet of paper on the plane table, upon which the plot E, F, G, H, I,

K, L, M, is to be drawn; let the first station be E; proceed as before from thence to F, and to G; then proceeding to H, you find there is not room on your paper for the line GH; however draw as much of the line GH, as the paper can hold, or draw it to the paper's edge. Move your instrument back to the first station E, and proceed the contrary way to M, and to L; but in going from thence to K, you again find your sheet will not hold it; however, draw as much of the line LK on the sheet as it can hold.

Take that sheet off the table, first observing the distance oo of the lines GH and LK, by the edge of the table; take off that sheet, and mark it with No. 1, to signify it to be the first taken off. Having then put on another sheet, lay that distance oo on the contrary end of the table, and so proceed as before, with the residue of the survey, from o to H, to K, and thence to o; so is your survey complete.

In the like manner you may proceed to take off, and put on, as many sheets as are convenient; and these may afterwards be joined together with mouth glue, or fine white wafer, very thin.

If the index be fixed to the first centre, using the 360 side, it will then serve as a theodolite, and when to the second centre, using the 180 side, it will serve as a semicircle; by either of which you may survey in rainy weather, when you cannot have paper on the table.

To measure Angles of Altitude by the Circumferentor, Theodolite, Semicircle, or Plane Table.

1. To take an angle of altitude, by the circumferentor.

Let the glass lid be taken off, and let the instrument be turned on one side, with the stem of the ball into the notch of the socket, so that the circle may be perpendicular to the plane of the horizon; let the instrument be placed in this situation before the object, so that the top thereof may be seen through the sights; let a plummet be suspended from the centre pin, and the object being then observed, the complement of the number of degrees, comprehended between the thread of the plummet, and that part of the instrument which is next your eye, will give the angle of altitude required.

2. If an angle of altitude is to be taken by the theodolite, or semicircle, let a thread be run through a hole at the centre, and a plummet be suspended by it; turn the instrument on one side, by the help of the ball and notch in the socket for that purpose, so that the thread may cut 90, having 360 degrees next you; screw it fast in that position, and through the sights cut the top of the objects; and the degrees then cut by the end of the index next you, are the degrees of elevation required. An angle of depression is taken the contrary way.

7

170 OF ANGLES OF ELEVATION, &c.

3. By the plane table an angle of altitude is taken in the like manner, by suspending a plummet from the centre thereof, having turned the table on one side, and fixed the index to the centre by a screw, so as to move freely, let the thread cut 90, look through the sights as before, and you have the angle of elevation, and on the contrary that of depression.

THE

PROTRACTOR.

THE protractor is a semicircle annexed to a scale, and is made of brass, ivory, or horn; its diameter is generally about five or six inches.

The semicircle contains three concentric semicircles at such distances from each other, that the spaces between them may contain figures.

The outward circle is numbered from the right to the left hand, with 10, 20, 30, &c. to 180 degrees; the middlemost the same way, from 180 to 360 degrees; and the innermost from the upper edge of the scale both ways, from 10, 20, 30, &c. to 90 degrees.

It is easy to conceive that the protractor, though a semicircle, may be made to supply the place of a whole circle; for if a line be drawn, and the centre-hole of the protractor be laid on any point in that line, the upper edge of the scale corresponding with that line, the divisions on the edge of the semicircle will run from 0 to 180, from right to left: again, if it be turned the other way, or downwards, keeping the centre-hole thereof on the aforesaid point in the line, then the divisions will run from

180 to 360, and so completes an entire circle with the former semicircle.

The use of the protractor is to lay off angles, and to delineate or draw a map, or plan of any ground from the field notes; and is performed in the following manner.

To protract a field-book, when the angles are taken from the meridian.

PL. 6. fig. 9.

On your paper rule lines parallel to each other, at an inch asunder (being most usual), or at any other convenient distance; on the left end of the parallels put N. for north, and on the right S. for south; put E. at the top for east, and W. at the bottom of your paper for west.

Then let the following field-book be that which is to be profracted, the bearings being taken from the meridian, whether by a circumferentor, theodolite, or semicircle, and measured with a two-pole chain.

No.	Bearing.	Ch. L.
1	283½	55.20
2	3484	12.36
3	317	29.20
4	266	55.20
5	193	40.00
6	124	76.00
7	63 1	87.02

Close at the first station.

Pitch upon any convenient point on your paper for your first station, as at 1, on which lay the centre-hole of your protractor, with a protracting pin; then if the degrees be less than 180, turn the arc of your protractor downwards, or towards the west; but if more than 180, upwards, or towards the east.

Or if the right hand be made the north, and the left the south, the west will be then up, and the east down.

In this case, if the degree be less than 180, turn the arc of your protractor upwards, or towards the west; and if more, downwards, or towards the east.

By the foregoing field-book, the first bearing is 283½, turn the arc of your protractor upwards, keeping the pin in the centre-hole, move the protractor so that the parallel lines may cut opposite divisions, either on the ends of the scale, or or the degrees, and then it is parallel. This must be always first done, before you lay off your degrees.

Then by the edge of the semicircle, keeping the protractor steady, with the pin prick the first bearing $283\frac{1}{2}$, and from the centre point, through that point or prick, draw a blank line with the pin, on which from a scale of equal parts, or from the scale's edge of the protractor, lay off the distance $55C.\ 20L.$ so is that station protracted.

At the end of the first station, or at 2, which is the beginning of the second, with the pin place the centre of the protractor, turning the arc up, because the bearing of the second station is more

than 180, viz. 3484. Place your protractor parallel as before, and by the edge of the semicircle, with the pin prick at that degree, through which and the end of the foregoing station, draw a blank line, and on it set the distance of that station.

In the like manner proceed through the whole, only observe to turn the arc of your protractor down, when the degrees are less than 180.

If you lay off the stationary distances by the edge of the protractor, it is necessary to observe, that if your map is to be laid down by a scale of 40 perches to an inch, every division on the protractor's edge will be one two-pole chain; \(\frac{1}{2}\) a division will be 12\(\frac{1}{2}\) links.

If your map is to be laid down by a scale of 20 perches to an inch, two divisions will be one two-pole chain; one division will be 25 links; \frac{1}{2} a division 12\frac{1}{2} links, and \frac{1}{2} of a division will be 6\frac{1}{2} links.

In general, if 25 links be multiplied by the number of perches to an inch, the map is to be laid down by, and the product be divided by 20 (or which is the same thing, if you cut off one and take the half), you will have the value of one division on the protractor's edge, in links and parts.

Examples.

1. How many links in a division, if a map be laid down by a scale of 8 perches to an inch?

25 8 2|0)20|0

10 links. Answer.

2. How many links in a division, if a map be laid down by a scale of 10 perches to an inch?

25 10

20)250

12.5 or 121 links. Answer.

And so of any other.

To protract a field-book, taken by the angles of the field.

Note. We here suppose the land surveyed is kept on the right hand as you survey.

Draw a blank line with a ruler of a length greater than the diameter of the protractor; pitch upon any convenient point therein, to which apply the centre-hole of your protractor with your pin, turning the arc upwards if the angle be less than 180, and downwards if more; and observe to keep the upperedge of the scale, or 180 and 0 degrees upon the line: then prick off the number of degrees contained in the given angle, and draw a line from the first point through the point at the degrees; upon which lay the stationary distance. Let this line be lengthened forwards and backwards, keeping your first station to the right, and second to the left;

and lay the centre of your protractor over the second station, with your pin, turning the arc upwards, if the angle be less than 180, and downwards, if more; and keeping the 180 and 0 degrees on the line, prick off the number of degrees contained in the given angle, and through that point and the last station draw a line, on which lay the stationary distance; and in like manner proceed through the whole.

In all protractions, if the end of the last station falls exactly in the point you began at, the field-work and protraction are truly taken, and performed; if not, an error must have been committed in one of them: in such case make a second protraction; if this agrees with the former, and neither meet nor close, the fault is in the field-work, and not in the protraction; and then a re-survey must be taken.

REMARKS.

The accuracy of geometrical and trigonometrical mensuration, depends in a great degree on the exactness and perfection of the instruments made use of; if these are defective in construction, or difficult in use, the surveyor will either be subject to error, or embarrassed with continual obstacles. If the adjustments, by which they are to be rendered fit for observation, be troublesome and inconvenient, they will be taken upon trust, and the instrument will be used without examination, and thus subject the surveyor to errors, that he can neither account for, nor correct.

In the present state of science, it may be laid down as a maxim, that every instrument should be so contrived, that the observer may easily examine and rectify the principal parts; for however careful the instrument-maker may be, however perfect the execution thereof, it is not possible that any instrument should long remain accurately fixed in the position in which it came out of the maker's hand, and therefore the principal parts should be moveable, to be rectified occasionally by the observer.

AN ENUMERATION OF INSTRUMENTS USEFUL TO A SURVEYOR;

Fewer or more of which will be wanted, according to the extent of his work, and the accuracy required.

A case of good pocket instruments.

A pair of beam compasses.

A set of feather-edged plotting scales.

Three or four parallel rules.

A pair of proportional compasses.

A pair of triangular ditto.

A pantagraph.

A cross staff.

A circumferentor.

An Hadley's sextant.

An artificial horizon.

A theodolite.

A surveying compass.

Measuring chains, and measuring tapes.

King's surveying quadrant.

A perambulator, or measuring wheel.

A spirit level with telescope.

Station staves, used with the level

A protracter, with or without a nonius.

To be added for county and marine surveying;

An astronomical quadrant, or circular instrument.

178 LIST OF INSTRUMENTS.

A good refracting and reflecting telescope. A copying glass.

For marine surveying;

A station pointer.

An azimuth compass.

One or two boat compasses.

Besides these, a number of measuring rods, iron pins, or arrows, &c. will be found very convenient, and two or three offset staves, which are straight pieces of wood, six feet seven inches long, and about an inch and a quarter square; they should be accurately divided into ten equal parts, each of which will be equal to one link. These are used for measuring offsets, and to examine and adjust the chain.

Five or six staves of about five feet in length, and one inch and an half in diameter, the upper part painted white, the lower end shod with iron, to be struck into the ground as marks.

Twenty or more iron arrows, ten of which are always wanted to use with the chain, to count the number of links, and preserve the direction of the chain, so that the distance measured may be really in a straight line.

The pocket measuring tapes, in leather boxes, are often very convenient and useful. They are made to the different lengths of one, two, three, four poles, or sixty-six feet and 100 feet; divided, on one side, into feet and inches, and on the other into links of the chain. Instead of the latter, are sometimes placed the centesimals of a yard, or three feet into 100 equal parts.

SECTION IL

MENSURATION

OF HEIGHTS AND DISTANCES.

1st. Of Heights.

PL. 5. fig. 18.

HE instrument of least expence for taking heights, is a quadrant, divided into ninety equal parts or degrees; and those may be subdivided into halves, quarters, or eighths, according to the radius, or size of the instrument: its construction will be evident by the scheme thereof.

From the centre of the quadrant let a plummet be suspended by a horse hair: or a fine silk thread of such a length that it may vibrate freely, near the edge of its arc: by looking along the edge AC, to the top of the object whose height is required; and holding it perpendicular, so that the plummet may neither swing from it, nor lie on it; the degree then cut by the hair, or thread, will be the angle of altitude required.

If the quadrant be fixed upon a ball and socket on the three-legged staff, and if the stem from the ball be turned into the notch of the socket, so as to bring the instrument into a perpendicular position, the angle of altitude by this means, can be acquired with much greater certainty.

An angle of altitude may be also taken by any of the instruments used in surveying; as has been

particularly shown in treating of their description and uses.

Most quadrants have a pair of sights fixed on the edge AC, with small circular holes in them; which are useful in taking the sun's altitude, requisite to be known in many astronomical cases; this is effected by letting the sun's ray, which passes through the upper sight, fall upon the hole in the lower one; and the degree then cut by the thread, will be the angle of the sun's altitude; but those sights are useless for our present purpose, for looking along the quadrant's edge to the top of the object will be sufficient, as before.

PROB. I.

PL. 5. fg. 19.

To find the height of a perfendicular object at one station, which is on an horizontal plane.

A steeple.

Given, { The angle of altitude, 53 degrees. Distance from the observer to the foot of the steeple, or the base, 85 feet. Height of the instrument, or of the observer, 5 feet.

Required, the height of the steeple.

The figure is constructed and wrought, in all respects, as case 2. of right-angled trigonometry; only there must be a line drawn parallel to, and beneath AB of 5 feet for the observer's height, to represent the plane upon which the object stands;

to which the perpendicular must be continued, and that will be the height of the object.

Thus, AB is the base, A the angle of altitude, BC the height of the steeple from the instrument, or from the observer's eye, if he were at the foot of it; DC the height of the steeple above the borizontal surface.

Various statings for BC, as in case 2. of right-angled plane trigonometry.

- 1. S. C: AB:: S. A: BC. 37° 85 53° 112.8.
- 2. R.: AB:: T. A: BC. 90° 85 53° 112.8.
- 3. T.C: AB:: R.: BC. 37° 85 90° 112.8

To BC 112.8 Add DB 5. the height of the observer.

Their sum is 117. 8 or 118 feet, the height of the steeple required.

PROB. II.

PL. 5. fig. 20.

To find the height of a perpendicular object, on an horizontal plane; by having the length of the chadow given.

Provide a rod, or staff, whose length is given, let that be set perpendicular, by the help of a quadrant, thus; apply the side of the quadrant AC, to the rod, or staff; and when the thread cuts 90° it is then perpendicular; the same may be done by a carpenter's or mason's plumb.

Having thus set the rod or staff perpendicular; measure the length of its shadow, when the sun shines, as well as the length of the shadow of the object, whose height is required; and you have the proper requisites given. Thus,

ab, the length of the shadow of the staff, 15 feet.

, bc, the length of the staff, 10 feet.

 \boldsymbol{AB} , the length of the shadow of the steeple, or object, 135 feet.

Required BC, the height of the object.

The triangles abc, ABC, are similar, thus; the angle b=B, being both right; the lines ac, AC are parallel, being rays, or a ray of the sun; whence the angle a=A (by part 3. theo. 3. sect. 4.) and consequently c=C. The triangles being therefore mutually equiangular, are similar (by theo. 16. sect. 4) it will be,

ab : bc : : AB : BC.
15 10 135 90. the steeple's height, required.

The foregoing method is most to be depended on; however, this is mentioned for variety's sake.

PROB. III.

P1. 5. fig. 21.

To take the altitude of a perpendicular object, at the foot of a hill, from the hill's side.

Turn the centre A of the quadrant, next your eye, and look along the side AC, or 90 side, to the top and bottom of the object; and noting down the angles, measure the distance from the place of observation to the foot of the object. Thus,

Given, Angle to the foot of the object, 55% or 55°. 15'
Angle to the top of it, 31% or 31°. 15'
Distance to the foot of it, 250 feet.

Required, the height of the object.

By Construction.

Draw an indefinite blank line AD, at any point in which A make the angles EAB of 55°. 15′, and EAC of 31°. 15′; lay 250 from A to B; from B, draw the perpendicular BE (by prob. 7 of geometry (crossing AC in C; so will BC be the height of the object required.

In the triangle ABC there is given,

ABE the complement of EAB to 90°, which is 34°. 45′.

. CAB the difference of the given angle 24.00'.

The side AB, 250. Required, BC.

This is performed as case 2. of oblique angular trigonometry. Thus,

180—the sum of ABE 34°. 45′, and CAB 24°. 00′ = ACB 121°. 15′. Then,

S. ACB: AB:: S. CAB: BC.
121°. 15′ 250 24°. 00′ 119, the height required.

PROB. IV.

PL. 5, fg. 22.

To take the altitude of a perpendicular object, on the top of a hill, at one station; when the top and bottom of it can be seen from the fost of the hill.

As in prob I. take an angle to the top, and another to the bottom of the object; and measure from the place of observation to the foot of the object, and you have all the given requisites. Thus,

A Tower on a hill.

Given, Angle to the bottom, 48°. 36'.

Angle to the top, 67°.00'.

Dist. to the foot of the object, 136 feet.

Required, the height of the object.

By Construction.

Make the angle $DAB=48^{\circ}$ 30', and lay 136 feet from A to B; from B, let fall the perpendicular BD; and that will be the height of the hill; produce BD upwards by a blank line: again, at A, make the angle $DAC=67^{\circ}$ 00' by a blank line, and from C where that crosses the perpendicular produced, draw the line CB, and that will be the beight of the object required.

Let AC be drawn.

In the triangle ABC, there is given,

The angle ACD the complement of $DAC=23^{\circ}$. 00'.

CAB the difference between the two given angles=18°. 30'.

And the side AB 136. To find BC.

SC:: AB:: S.CAB: BC. 23° 136 18°. 30′ 110½.

If BD were wanted, it is easily obtained, by the first case of right-angled plane trigonometry.

PROB. V.

PL. 5. fig. 23.

To take an inaccessible perpendicular altitude, on a horizontal plane.

This is done at two stations, thus:

Let DC be a tower which cannot be approached by means of a moat or ditch, nearer than B; at B, take an angle of altitude, to C: measure any convenient distance backward to A, which note down; at A, take another angle to C; so have you the given requisites, thus:

Given, Stationary distance, 87 feet. Second angle, 37. 00'.

The height of the tower CD, is required.

By Construction.

Upon an indefinite blank line, lay off the stationary distance 87, from A to B; from B, set off your first; and from A, your second angle; from C, the point of intersection of the lines which form these angles, let fall the perpendicular CD; and that will be the height of the object required.

The external angle CBD, of the triangle ABC; is equal to the two internal opposite ones, A, and ACB (by theo. 4. sect. 4.): wherefore if one of the internal opposite angles be taken from the external angle, the remainder will be the other internal opposite one, thus;

 $CBD 55^{\circ} - A 37^{\circ} = ACB 18^{\circ}.$

Therefore in the triangle ABC; we have the angles A, and AGB, with the side AB given to find BC.

S. ACB: AB:: S. A: BC. 18° 87 37° 169.4 Having found BC, we have in the triangle BCD the angle CBD 55°, consequently BCD 35°, and BC 169.4; to find DC.

This is performed by the first case of right-angled trigonometry, three several ways; thus:

1. R: BC:: S. CBD: DC. 90° 169.4 55° 138.8. The height required.

2. Sec. CBD: BC:: T. CBD: DC. 55° 169.4 55° 138.8. The height required.

3. Sec. BCD : BC :: R : CD.
35° 169.4 90° 138.8.
The height required.

If BD, the breadth of the moat, were required; it may also be found, by three different statings, as in the first case of right-angled plane trigonometry.

PROB. VI.

PL. 5. fig. 24.

Let BC, a may-pole, whose height is 100 feet, be broken at D; the upper part of which, DC, falls upon an horizontal plane, so that its extremity, C, is 34 feet from the bottom or foot of the pole.

Required, the segments BD and DC.

By Construction.

Lay 34 feet from A to B; on B erect the perpendicular BC of 100 feet; and draw AC; bisect

AC (by prob. 4. geom.) with the perpendicular line, EF; and from D, where it cuts the perpendicular BC, draw AD, which will be the upper segment; and DB will be the lower.

By cor. to lemma, preceding theo. 7. geom. AD=DC; and (by the lemma) the angle C=CAD.

In the triangle ABC, find C as in case 6, of right-angled trigonometry, thus;

1. BC: R:: AB: T. C=GAD. 100 90° 34 18° 47′

By theo. 4. geom. The external angle $ABD = 37^{\circ} 34'$, or to twice the angle C, i. e. to C and GAD.

Then in the triangle ABD, there is ABD 37° 34′, therefore also its complement DAB 52° 26′, and AB 34, given, to find AD and BD.

By the second case of right-angled trigonometry.

2. S. ADB: AB:: R: AD or DC. 37° 34′ 34 90° 55.77.

BC—DC=BD. 100—55.77=44.23 required.

These may be had from other statings, as in the second case aforesaid.

PROB. VII.

PL. 5. fig. 25.

To take the altitude of a perpendicular object on a hill, from a plane beneath it.

This is done at two stations, thus;

Let the height DC, of a wind-mill on a hill be required.

From any part of the plane whence the foot of the object can be seen, let angles be taken to the foot and top; measure thence any convenient distance towards the object, and at the end thereof, take another angle to the top: and you have the proper requisites, thus;

First station. Angle to the foot DAB 21°00'.

Angle to the top CAB 35°00'.

Stationary distance AB 104 feet.

Second station.

Angle to the top 48° 30,

DC required.

By Construction.

On an indefinite blank line, lay the stationary distance AB 104 feet; from A, set off the second, and from B, the third given angle; and from the intersecting point C of the line formed by them, let fall the perpendicular CE; from A set off the first angle, and the line formed by it will determine the point D. Thus have we the height of the hill, as well as that of the wind-mill.

The angle CBE - A = ACB, as in the last prob. In the triangle ABC, find AC thus;

S. ACB: AB:: S. ACB (or sup. of CBE): AC 13°, 30': 104:: 131°, 30': 333.6

The angle CAE - DAE = CAD.

The angle $ACD = AED \times EAD$, by theo. 4.

In the triangle CAD, find CD thus,

S. ADC: AC: : S. CAD: DC 111*.: 333.6:: 14:: 86.46 required.

CE, BE, or DE, may be found by other various statings, as set forth in the first and second cases of right-angled trigonometry.

PROB. VIII.

Pt. 5. fig. 26.

To find the length of an object, that stands obliquely on the top of a hill, from a plane beneath.

Let CD be a tree whose length is required.

This is done at two stations.

Make a station at B, from whence take an angle to the foot, and another to the top of the tree; measure any convenient distance backward to A, from whence also let an angle be taken to the foot, and another to the top; and you have the requisites given. Thus,

First station. Angle to the foot $EBD=36^{\circ}$. 30'. Angle to the top $EBC=44^{\circ}$. 30'. Stationary distance AB=104 feet.

Second station. Angle to the foot $EAD=24^{\circ}$. 30'. Angle to the top $EAC=32^{\circ}$. 00'.

Let DC and DE be required.

The geometrical constructions of this and the next problem are omitted; as what has been already said, and the figures, are looked upon as sufficient helps.

EBC-A=ACB, or 44°. 30′—32°.=12°. 30′. as before.

In the triangle ABC, find BC. Thus,

1. S. ACB : AB : : S. A : BC. 12°. 30' 104 32° 254.7.

EBD-EAD=ADB, or 36°. 30'-24°. 30'=12° 00'

In the triangle ADB, find DB, thus;

2. S. ADB : AB : : S. DAB : DB. 12°00′ 104 24°. 30′. 207.4

CBE-DBE=CBD, or 44°. 30'-36°. 30'=8°00'

In the triangle CBD there is given, CB 254.7, DB 207.4, and the angle CBD 8°00'; to find DC.

This is performed as case 3. of oblique angled trigonometry, thus;

3. BC × BD : BC—BD:: T. of BDC+BCD : 462.1 47.3 86°. 00'. T. of BDC—BCD.

55°. 40′.

86°. 00′ + 55°. 40′ = 141°. 40′ = BDC. 86°. 00′ - 55°. 40′ = 30°. 20′ = BCD.

4. S. BCD: BD:: S. CBD: DC. 30°, 20' 207.4 8°. 06' 57.15 length of the tree.

To find DE in the triangle DBE.

Say R.: BD:: S. DBE: DE, 90°. 207.4 36°. 30′ 123.4 height of the hill.

PROB. 1X.

To find the height of an inaccessible object CD, on a hill BC, from ground that is not horizontal.

PL. 6. fig. 1.

From any two points, as G and A, whose distance GA, is measured, and therefore given; let the angles HGD, BAD, BAC, and EAG, be taken; because GH is parallel to EA (by part 2. theo. 3. geom.) the angle HGA=EAG; therefore $EAG \times HGD=AGD$: and (by cor. 1. theo. 1. geom) 180—the sum of EAG and BAD=GAD; and, (by cor. 1. theo. 5. geom. (180—the sum of the angles AGD and GAD=GDA: thus we have the angles of the triangle AGD, and the side AG given; thence (by case 2. of obl. ang. trig.) AD may be easily found. The angle DAB-CAB = DAC, and 90°—BAD=ADC; and 180°—the sum of DAC and ADC=ACD: so have we the

several angles of the triangle ACD given, and the side AD; whence (by case 2. of obl. trig.) CD may be easily found. We may also find AC, which with the angle BAC, will give CB the height of the hill.

The solutions of the several problems in heights and distances, by Gunter's scale, are omitted; because every particular stating has been already shewn by it, in trigonometry.

2d. OF DISTANCES.

THE principal instruments used in surveying, will give the angles or bearings of lines; which has been particularly shewn, when we treated of them.

PROB. I.

P1. 6. fig. 2.

Let A and B be two houses on one side of a river, whose distance asunder is 293 perches: there is a tower at C on the other side of the river, that makes an angle at A, with the line AB of 53° 20'; and another at B, with the line BA of 66° 20'; required the distance of the tower from each house, vis. AC and BC.

This is performed as case 2 of oblique angled trigonometry, thus;

1. S. C: AB:: S. A: BC. 60° 20′ 293 53° 20′ 270.5.

2. S. C : AB : : S. B : AC. 60° 20′ 293 66° 20′ 308.8.

PROB. II.

PL. 6. fig. 11.

Let B and C, be two houses whose direct distance as under, BC, is inaccessible: however it is

known that a house at A is 252 perches from B, and 230 from C; and that the angle BAC, is found to be 70°. What is the distance BC, between the two houses?

This is performed as case 3. of oblique angled trigonometry, thus;

5543°. 44'=58°. 44'=C. $55^{\circ}-3^{\circ}$. $44'=51^{\circ}$, 16=B.

2. S. C: AB:: S. A: BC. 58°. 44′ 252 70° 277.

PROB. 111.

PL. 6. fig. 3.

Suppose ABC a triangular piece of ground, which by an old survey we find to be thus; AB 260, AC 160, BC 150 perches, the mearing lines AC and BC, are destroyed or plowed down, and the line AB, only remaining. What angles must be set off at A and B, to run new mearings by exactly where the old ones were?

This is performed as in case 4. of oblique angled trigonometry, thus;

130 + 5.96 = 135.96 = AD. 130 - 5.96 = 124.04 = DB.

2. AD: R: AC: Sec. A. 136 90:: 160 312.47'.

3. BC: S. A:: AC: S. B. 150 31°. 47′ 160 34°. 10.

PROB. IV.

PL. 6. fig. 4.

Let D and C, be two trees in a bog, to which you can have no nearer access than at A and B; there is given, DAB 100°, CAB 36°. 30′, CBA 121°. DBA 49°, and the line AB 113 perches. Required, the distances of the trees DC.

180°—the sum of DBA and DAB=ADB=31°.
180°—the sum of CAB and CBA=ACB=22. 30.

In the triangle ABD, find DB, thus;

1. S. ADB: AB: S. DAB: DB. 31° 113:: 100° 216.

And in the triangle ABC, find BC, thus;

2. S. ACB : AB :: S. CAB : BC. 22° 30′ 113 36° 30′ 175.6.

In the triangle DBC, you have $DBC=ABC-ABD=72^{\circ}$; likewise the sides BD, BC, as before found, given to find DC.

3. BD+BC: BD—BC: T.of \(\frac{1}{2} \) DCB+CDB: 391.6 40.4

T. of $\frac{1}{2}$ DCB—CDB.

8 05'.

 $54^{\circ} + 8^{\circ} 05' = 62^{\circ} 05' = DCB$, $54^{\circ} - 8^{\circ} 05' = 45^{\circ} 55' = CDB$.

4. S. CDB : BC : S. DBC : DC. 45° 55′ 175.6 72° 232.5.

LEMMA.

PL. 6. fig. 12.

If from a point C, of a triangle ABC, inscribed in a circle, there be a perpendicular CD, let fall upon the opposite side AB; that perpendicular is to one of the sides, including the angle, as the other side, including the angle, is to the diameter of the circle, i. e. DC: AC:; GB: GE.

Let the diameter CE be drawn, and join EB; it is plain the angle CEB = CAB (by cor. 2. theo. 7. geom.) and CBE is a right angle (by cor. 5. theo. 7. geom.) and =ADC: whence ECB = ACD. The triangles CEB, CAD, are therefore mutually equiangular, and (by theo. 16. geom.) DC : AC : CB : CE, or DC : CB : AC : CE. Q. E. D.

PROB. V.

PL. 6. fig. 5.

Let three gentlemen's seats, A, B, C, be situate in a triangular form: there is given, AB 2.5 miles, AC 2.3, and BC 2. It is required to build a church at E, that shall be equi-distant from the seats A, B, C. What distance must it be from each seat, and by what angle may the place of it be found?

By Construction.

By prob. 15. geom. Find the centre of a circle that will pass through the points, A, B, C: and that will be the place of the church; the measure of which, to any of these points, is the answer for the distance: draw a line from any of the three points to the centre, and the angle it makes with either of the sides that contain the angle it was drawn to; that angle laid off by the direction of an instrument, on the ground, and the distance before found, being ranged thereon, will give the place of the church required.

By Calculation.

1.
$$AB : AC+BC : AC-BC : AD-DB$$
.
2.5 4.3 .3 .516.

1.25 + .258 = 1.508 = AD.

By cor. 2. theo. 14. geom. The square root of the difference of the squares of the hypothenuse AC, and given leg AD, will give DC.

That is, 5.29 - 2.274064 = 3.015936.

Its square root is 1.736 = CD.

Then by the preceding lemma,

2. CD: AC: CB: the diameter. 1.736 2.3 2 2.65.

the half of which, viz. 1.325 is the semi-diameter, or distance of the church from each seat, that is, AE, CE, BE.

From the centre E, let fall a perpendicular upon any of the sides as EF, and it will bisect in E: (by theo. 8. geom.)

Wherefore $AF = CF = \frac{1}{2}AC = 1.15$.

In the right angled triangle AFE, you have AF 1.15, and AE the radius 1.325 given, to find FAE, thus;

3. AF:/R.:: AE: Sec. FAE. 1.15 90° 1.325 29° 47′.

Wherefore directing an instrument to make an angle of 29° 47′, with the line AC; and measuring 1.325 or that line of direction, will give the place of the church, or the centre of a circle that will pass through A, B, and C.

The above angle FAE, may be had without a secant, as before, thus;

AE : R :: AF : S. AEF.1.325 90° .115 60°. 13′.

Its complement 29°. 47', will give FAE, as before.

The questions that may be proposed on this head, being innumerable, we have chosen to give only a few of the most useful.

SECTION III.

MENSURATION OF AREAS, OR THE VARIOUS ME-THODS OF CALCULATING THE SUPERFICIAL CONTENT OF ANY FIELD.

DEFINITION.

HE area or content of any plane surface, in perches, is the number of square perches which that surface contains.

PL. 7. fig. 1.

Let ABCD represent a rectangular parallelogram, or oblong: let the side AB, or DC, contain 8 equal parts; and the side AD, or BC, three of such parts; let the line AB be moved in the direction of AD, tillit has come to EF, where AE, or BF (the distance of it from its first situation) may be equal to one of the equal parts. Here it is evident, that the generated oblong ABEF, will contain as many squares as the side AB contains equal parts, which are 8; each square having for its side one of the equal parts, into which AB, or AD, is divided. Again, let AB move on till it comes to GH, so as GE, or HF, may be equal to AE, or BF; then it is plain that the oblong AGHB, will contain twice as many squares as the side AB contains equal parts. After the same manner it will appear, that the oblong ADCBwill contain three times as many squares as the side AB contains equal parts; and in general, that every rectangular parallelogram, whether square or oblong, contains as many squares as the product of the number of equal parts in the base, multiplied into the number of the same equal parts in the height, contains units, each square having for its side one of the equal parts.

Hence arises the solution of the following problems.

PROB. I.

To find the content of a square piece of ground.

1. Multiply the base in perches, into the perpendicular in perches, the product will be the content in perches; and because 160 perches make an acre, it must thence follow, that

Any area, or content in perches, being divided by 160, will give the content in acres; the remaining perches, if more than 40, being divided by 40, will give the roods, and the last remainder, if any, will be perches.

Or thus:

2. Square the side in four-pole chains and links, and the product will be square four-pole chains and links: divide this by 10, or cut off one more than the decimals, which are five in all, from the right towards the left: the figures on the left are acres; because 10 square four-pole chains make an acre, and the remaining figures on the right, are decimal parts of an acre. Multiply the five figures to the right by 4, cutting 5 figures from the product, and if any figure be to the left of them, it is a rood, or roods; multiply the last cut off figures by 40, cutting off five, or (which is the same thing) by 4, cutting off four; and the remaining figures to the left, if any, are perches.

1. The first part is plain, from considering that a piece of ground in a square form, whose side is a perch, must contain a perch of ground; and that 40 such perches make a rood, and four roods an

acre; or which is the same thing, that 160 square perches make an acre, as before.

2. A square four-pole chain (that is, a piece of ground four poles or perches every way) must contain 160 square perches; and 160 perches make an acre, therefore 10 times 16 perches, or 10 square four-pole chains, make an acre.

NOTE. The chains given, or required, in any of the following problems, are supposed to be twopole chains, that chain being most commonly used; but they must be reduced to four-pole chains or perches for calculation, because the links will not operate with them as decimals.

Examplés.

PL. 1. fig. 17.

Ch. L.

Let ABCD be a square field, whose side is 14 29, required the content in acres.

Ch. L.

By problem 4. section 1. part 2. 14. 29 are equal to 29.16 perches

29.16

17496

2916

26244

5832

160)850.3056(

A. R. P.

5. 1. 10. content.

40)50(1 rood.

10 perches.

Or thus:

Ch. L. Ch. L.

14. 29 are equal to 7. 29 of four-pole chains, by prob. 1. sect. 1. pt. 2. 7. 29

6561 1458 5103

A.R. P.

Acres 5|31441 cont. as before 5. 1. 10

4

Rood 1|25764

40

Perches 10|30560

It is required to lay down a map of this piece of ground, by a scale of twenty perches to an inch.

Take 29. 16 the perches of the given side, from the small diagonal on the common surveying scale, where 20 small, or two of the large divisions, are an inch: make a square whose side is that length (by prob. 9. geom.) and it is done.

PROB. II.

To find the side of a square, whose content is given.

Extract the square root of the given content in perches, and you have the side in perches, and consequently in chains.

EXAMPLE.

It is required to lay out a square piece of ground which shall contain 12A. 3R. 16P. Required the number of chains in each side of the square; and to lay down a map of it, by a scale of 40 perches to an inch.

A.	R.	P.
12.	3.	16.
. 4		
51		
40		
-		· Ch. L.
2056(4	5.34 - 1	$perches = 22. 33\frac{1}{2} \text{ by prob. 6.}$
85)456		[sect. 1. pt. 2.
903)3100)	
9064)391	00 &	C.

To draw the map.

From a scale where 4 of the large, or 40 of the small divisions are an inch, take 45.34, the perches of the side, of which make a square.

PROB, III.

To find the content of an oblong piece of ground.

Multiply the length by the breadth, for the content.

EXAMPLE.

PL. 1. fig. 3.

Let ABCD be an oblong piece of ground, whose length AB is 14C. 25L. and breadth 8C. 37L. required the content in acres, and also to lay down a map of it, by a scale of 20 perches to an inch.

Ch. L. Perches.

14.25=29.00
8.37=17.48

By prob. 4. sect. 1. pt. 2.

15732 3496

——— A. R. P. 160)506.9200(3. 0. 27. content.

26 perches, or near 27.

Or thus:

4 pole ch.

Ch. L. Ch. L. 14.25 = 7.25 8.37 = 4.37

By prob. 1. sect. 1. pt. 2.

5075 2175 2900

Acres 3|16825

4

Rood |67300

Perches 26|9200

To draw the map.

Make an oblong (by schol. to prob. 9. geom.) whose length, from a scale of 20 to an inch, may be 29 perches, and breadth, 17.48 perches.

PROB. IV.

The content of an oblong piece of ground, and one side given, to find the other.

Divide the content in perches, by the given side in perches, the quotient is the side required in perches; and thence it may be easily reduced to chains.

Example.

There is a ditch 14 Ch. 25 L. long, by the side of which it is required to lay out an oblong piece of ground, which shall contain 3A. 0R. 37P: what breadth must be laid off at each end of the ditch to enclose the 3A. 0R. 37P?

A. R. P.

3. 0. 27, $\frac{4}{12}$ $\frac{40}{-12}$ Perch. 6%. L.

29)507(17.48 = 8. 37. breadth. $\frac{217}{140}$

8

The map is constructed like the last.

PROB. V.

To find the content of a piece of ground, in form of an oblique ingular parallelogram; or of a rhombus, or rhomboides.

Multiply the base into the perpendicular height. The reason is plain from theo. 13. geom.

EXAMPLE.

PL. 7. fig. 2.

Let ABCD be a piece of ground in form of a rhombus, whose base AB is 22 chains, and perpendicular DE, or FC, 20 chains. Required the content.

Or,

0

The converse of this is done by prob. 4. and the map is drawn, by laying off the perpendicular on that part of the base from whence it was taken; joining the extremity thereof to that of the base by a right line, and thence completing the parallelogram.

PROB. VI.

To find the content of a triangular piece of ground.

Multiply the base by half the perpendicular, or the perpendicular by half the base; or take half the product of the base into the perpendicular.

The reason of this is plain, from cor. 2. theo. 12. geom.

EXAMPLE.

PL. 1. fig. 16. Let ABC be a triangular piece of ground, whose longest side or base BC, is 24C. 38L. and perpendicular AD, let fall from the opposite angle, is 13 Required the content. C. 28L.

Ch. L. Ch. L.

1. Base 24. 38 = 12. 38) 4 pole chains. ½ perp. 3. 39 (

> 11142 3714 3714

Acres 4 19682

Rood |78728

40

Perches 31|49120 A. R. P.

Content 4. 0. 31.

Ch. L. Ch. L. Perp. 13.28 = 6.78) four-pole chains by $\frac{1}{2}$ perp. 6.39 = 3.39 \ prob. 1. sect. 1. pt. 2. Or 2dly. Perp. 6.78 of four-pole chains. †base 6.19 6102 678 4068 R. 4|19682 = 4.Or 3dly. Base 12.38 four-pole chains. Perp. 6.78 9904 8666 7428 83.9364 Its! = 4|19682 = 4.0. 31.

Or the base and perpendicular may be reduced to perches; and the content may be thence obtained, thus:

```
Ch. L. Perches.
Perp. 13.28 = 27.12
                      By prob. 4. sect. 1. pt. 2.
Half the perp. 13.56
       Perches. Ch. L.
1: Base 49.52 = 24.38
 perp. 13.56
       29712
      24760
     14856
     4952
                   R.
 160)671.4912(4.
                   0.
                       31.
        31
         Perches.
   Perp. 27 12
Half base 24.76
         16272
        18984
       10848
       5424
                       R.
       671.4912 = 4.
                       0.
                           31.
```

But, square perches may be reduced to acres, &c. rather more commodiously, by dividing by 40 and 4, than by 160; thus,

4|0)67|1.

4)16. 31

A. 4. 0. 31

Perches.

3. Base 49.52
Perp. 27.12

9904
4952
34664
9904

1342.9824

671.4912 = 4. R. P.

The map may be readily drawn, having the distance from either end of the base, to the perpendicular given; as may be evident from the figure.

PROB. VII.

The content of a triangular piece of ground, and the base given, to find the perpendicular.

Divide the content in perches, by half the base in perches; and the quotient will give you the perpendicular, in perches and so in chains.

EXAMPLES.

PL. 1. fig. 16.

Let BC be a ditch, whose length is 24C. 40L. by which it is required to lay out a triangular piece of ground, whose content shall be 4A. 1R. 10P. Required the perpendicular.

Ch. L. Perches. Base 24.40 = 49.6Half the base = 24.8

A. R. P.
4. 1. 10.
4
17
40
Perches.
24.8)690(27.28

1940

2040

560

64

Perches. Ch. L.Answer perp. 27. 28. = 13.45.

This perpendicular being laid on any part of the base, and lines run from its extremity to the ends of the base, will lay out the triangle (by cor. to theo. 13. geom.) so that the perpendicular may be set on that part of the base which is most convenient and agreeable to the parties concerned.

LEMMA.

PL. 8. fig. 9.

If from half the sum of the sides of any plane triangle ABC, each particular side be taken; and if the half sum, and the three remainders be multiplied continually into each other, the square roof of this product will be the area of the triangle.

Bisect any two of the angles, as A and B, with the lines AB, BD meeting in D; draw the perpendiculars DE, DF, DG.

In the same way if A and C were bisected, the same point D would be had; therefore a line from D to C will bisect C, and thus the triangles DFC, DGC will be also equal.

Produce CA to H, till AH=EB or GB; so will HC be equal to half the sum of the sides, vis. to $\frac{1}{2}AB$, $+\frac{1}{4}AC+\frac{1}{2}BC$; for FC, FA, EB, are severally equal to CG, AE, BG; and all these together are equal to the sum of the sides of the triangle; therefore FC + FA + EB or CH, are equal to half the sum of the sides.

FC=CH-AB, for AF=AE, and HA=EB; therefore HF=AB; and AF=CH-BC; for CF

=CG, and AH=GB; therefore BC=HA+FC, and AH=CH-AH.

Continue DC, till it meets a perpendicular drawn upon H in K; and from K draw the perpendicular KI, and join AK.

Because the angles AHK and AIK are two right ones, the angles HIA and K together, are equal to two right; since the angles of the two triangles contain four right: in the same way FDE + FAE = (2 right angles) FAE + IAH; let FAE be taken from both, then FDE = IAH, and of course FAE = K; the quadrilateral figures AFDE, and KHAI, are therefore similar, and have the sides about the equal angles proportional; and it is plain the triangles CFD and CHK are also proportional: hence,

FD: HA:: FA: HK FD: FC:: HK: HC

Wherefore by multiplying the extreme, and means in both, it will be the square of $FD \times HK \times HC = FC \times FA \times HA \times HK$; let HK be taken from both, and multiply each side by CH; then the square of $CH \times$ by the square of $FD = FC \times FA \times HA \times CH$.

It is plain, by the foregoing problem, that $\frac{1}{2}AB \times DE$, $+\frac{1}{2}BC \times DG + \frac{1}{2}AC \times FD =$ the area of the triangle; or that half the sum of the sides, vis. $CH \times FD =$ the triangle; wherefore the square of $CH \times$ by the square of $FD = FC \times FA \times HA \times CH$, that is, the half sum multiplied continually into the differences between the half sum and each side, will be the square of the area of the triangle, and its root the area. Q. E. D.

Hence the following problem will be evident.

PROB. VIII.

The three sides of a plane triangle given to find the area.

RULE.

From half the sum of the three sides subtract each side severally; take the logarithms of half the sum and three remainders, and half their total will be the logarithm of the area: or, take the square root of the continued product of the half sum and three remainders for the area.

Examples.

Ps. 8. fig. 9.

1. In the triangle ABC, are

Given,
$$\begin{cases}
AB = 10.64 \\
AC = 12.28 \\
CB = 9.00
\end{cases}$$
 four-pole chains; required the area?

Sum 31.92

Half sum	15.96	Log.	1.203033
(5.32	_	0.725912
Remainders {	3.68		0.565848
(6.96	-	0.842609
•	•	•	2)3.337402

Answer, Sqr. Ch. 46.63 Log. 1.668701 or, 4.663 Acres.

Or, $15.96 \times 5.32 \times 3.68 \times 6.96 = 2174.71113216$;

the square root of which is 46.63, for the area as before.

2. What quantity of land is contained in a triangle, the 3 sides of which are, 80, 120 and 160 perches respectively? Answer, 29A. 7P.

PROB. IX.

Two sides of a plane-triangle and their included angle given, to find the area.

RULE.

To the log. sine of the given angle (or of its supplement to 180°, if obtuse) add the logarithms of the containing sides; the sum, less radius, will be the logarithm of the double area.

EXAMPLES.

PL. 5. fig. 16.

Suppose two sides, AB, AC, of a triangular lot ABC, form an angle of 30 degrees, and measure one 64 perches, and the other 40.5, what must the content be?

Given angle 30°. sine 9.698970
Containing sides \[\begin{pmatrix} 64. & \log. & 1.806180 \\ 40.5 & \log. & 1.607455 \\ \end{pmatrix} \]
\[\frac{2}{160}\text{648}(4A. 8P. answer. \]

- 2: Required the area of a triangle, two sides of which are 49.2 and 40.8 perches, and their contained angle 1441 degrees? Answer, 3A. 2R. 22P.
- 3. What quantity of ground is inclosed in an equilateral triangle, each side of which is 100 perches, either angle being 60 degrees? Answer, 27A. 10P.

Demonstration of this problem.

PL. 11. fig. 3.

Let AH be perpendicular to AB and equal to AC, and HE, FCG, parallel to AB; then making AH (= AC) radius, AF (= CD) will be the sine of CAD, and the parallelograms ABEH (the product of the given sides,) and ABGF the double area of the triangle) having the same base AB, are in proportion as their heights AH, AF; that is, as radius to the sine of the given angle; which proportion gives the operation as in the rule above.

PROB. X.

To find the area of a trapezoid, viz. a figure bounded by four right times, two of which are parallel, but unequal.

Rule.

Multiply the sum of the parallel sides by their perpendicular distance, and take half the product for the area.

Note. On this 10th problem are founded most of the calculations of differences by latitude and departure, and those by offsets, following in this treatise.

EXAMPLES.

1. Required the area of a trapezoid, of which the parallel sides are, respectively, 30 and 49 perches, and their perpendicular distance 61.6?

$$30+49 = \frac{61.6}{79.}$$
 Multiply. 2)4866.4

Answer, 2433.2=15A. 33.2P.

Ps. 9. Ag. 10.

2. In the trapezoid ABCD the parallel sides are, AD, 20 perches, BC, 32, and their perpendicular distance, AB, 26; required the content?

Answer, 4A. 36P.

PROB. XI.

To find the Content of a trapezium.

RULE.

Multiply the diagonal, or line joining the remotest opposite angles, by the sum of the two perpendiculars falling from the other angles to that diagonal, and half the product will be the area.

EXAMPLE.

PL. 7. fig. 3.

Let ABCD be a field in form of a trapezium, the diagonal AC 64.4 perches, the perpendicular Bb 13.6 and Dd 27.2, required the content?

Diagonal = 64.4 Multiply. 13.64+27.2 = 40.8

2)2627.52

160)131376(8A. 33[‡]P. Answer. 1280

33[‡] perches.

Note. The method of multiplying together the half sums of the opposite sides of a trapezium for the content is erroneous, and the more so the more oblique its angles are.

To draw the map set off Ab 28 perches, and Ad 34.4, and there make the perpendiculars to their proper lengths, and join their extremities to those of the diagonal.

PROB. XII.

To find the area of a circle, or an ellipsis.

RULE.

Multiply the square of the circle's diameter, or the product of the longest and shortest diameters of the ellipsis by .7854 for the area. Or, subtract 0.104909 from the double logarithm of the circle's diameter, or from the sum of the logarithms of those elliptic diameters, and the remainder will be the logarithm of the area.

Note. In any circle, the Diam multi. by 3.14159, produces the Cir. quotes the diam.

EXAMPLES.

1. How many acres are in a circle of a mile diameter?

1 Mile=320 per. log. 2.505150 2.505150 5.010300 0.104909 4|0)8042|5. log. 4.905391

4)2010.25

Answer, 502A. 2R. 25P.

2. A gentleman, knowing that the area of a circle is greater than that of any other figure of equal perimeter, walls in a circular deer park of 100 perches diameter, in which he makes an elliptical fish pond 10 perches long by 5 wide; required the length of his wall, content of his park, and area of his pond?

Answer, the wall 314.16 perches inclosing 49A. 14P. of which 39 $\frac{1}{4}$ perches, or $\frac{1}{4}$ of an acre nearly, is appropriated to the pond.

PROB. XIII.

The area of a circle given, to find its diameter.

Rule.

To the logarithm of the area add 0.104909, and half the sum will be the logarithm of the diameter. Or, divide the area by .7854, and the square-root of the quotient will be the diameter.

EXAMPLES.

A horse in the midst of a meadow suppose, Made fast to a stake by a line from his nose. How long must this line be, that feeding all round,

Permits him to graze just an acre of ground?

Area in perches 160 log. 2.204120
0.104909

2)2.309029

2)
Diameter, 14.2733 log. 1.154514

Answer, 7.13665 per. = 117F. 9 In.

PROB. XIV.

Allowance for roads.

It is customary to deduct 6 acres out of 106 for roads; the land before the deduction is made may be termed the gross, and that remaining after such deduction, the neat.

RULE.

The gross div. } by 1.06, { quotes the neat. prod. the gross.

EXAMPLES.

1. How much land must I inclose to have 850A2R. 20P. neat?

200

40|20. 4| 2.5 Acres. A. R. P. 850.625×1.06=901.6625=901.2.26. the ans.

2. How much neat land is there in a tract of 901A. 2R. 26P. gross?

40|26. 4| 2.65 Acres. A. R. P. 1.06)901.6625(850.625=850. 2. 20. the answ. 848 &c.

Note. These two operations prove each other.

PROB. XV.

To find the area of a piece of ground be it ever so irregular by dividing it into triangles and trapezia.

PL. 7. fig. 4.

We here admit the survey to be taken and protracted; by having therefore the map, and knowing the scale by which it was laid down, the content may be thus obtained.

Dispose the given map into triangles, by fine pencilled lines, such as are here represented in the scheme, and number the triangles with 1, 2, 3, 4, &c. Your map being thus prepared, rule a table with four columns; the first of which is for the number of the triangle, the second for the base of it, the third for the perpendicular, and the fourth for the content in perches.

Then proceed to measure the base of number 1, from the scale of perches the map was laid down, and place that in the second column of the table, under the word base; and from the angle opposite to the base, open your compasses so, as when one foot is in the angular point, the other being moved backwards and forwards, may just touch the base line, and neither go the least above or beneath it; that distance in the compasses measured from the same scale, is the length of that perpendicular, which place in the third column, under the word perpendicular.

If the perpendiculars of two triangles fall on one and the same base, it is unnecessary to put down the base twice, but insert the second perpendicular opposite to the number of the triangles in the table, and join it with the other perpendicular by a brace, as No. 1 & 2, 4 & 5, 6 & 7, 9 & 10, &c.

Proceed after this manner, till you have measured all the triangles; and then by prob. 6. find the content in perches of each respective triangle, which severally place in the table opposite to the number of the triangle, in the fourth column, under the word content.

But where two perpendiculars are joined together in the table, by a brace having both one and the same base; find the content of each (being a trapezium) in perches, by prob. 11. which place opposite the middle of those perpendiculars, in the fourth column, under the word content.

Having thus obtained the content of each respective triangle and trapezium, which the map contains, add them all together, and their sum will

be the content of the map in perches; which being divided by 160, gives the content in acres. Thus, for

EXAMPLES.

No.	Ease.	Perpend:	Content.
1	24.8	17.0	412.92
2	1	16.3	412.02
3	28.2	16.0	225.6
4	39.8	19.6	712.42
5		16.2 \$	112.42
6	49.4	29.0	1086,8
7		15.0 \$	1000.0
8	38.7	6.7	129.64
9	40.0	17.0 }	600.
10		13.0 \$	000.
11	42.8	10.2 }	481.5
12	1	12.3 \$	401.0
13	26.2	17.9	234.49
14	24.0	11.6	259.2
15	ł	10.0 }	203.2
Content in perches 4142.57			

This being divided by 160, will give 25A. 3R. 22P. the content of the map.

Let your map be laid down by the largest scale your paper will admit, for then the bases and perpendiculars can be measured with greater accuracy than when laid down by a smaller scale, and if possible measure from scales divided diagonally.

If the bases and perpendiculars were measured by four-pole chains, the content of every triangle and trapezium, may be had as before, in problems 6. and 11. and consequently the whole content of the map.

If any part of your map has short or crooked bounds, as those represented in plate 7. fig. 5. then by the straight edge of a transparent horn, draw a fine pencilled line as AB to balance the parts taken and left out, as also another, BC: these parts when small, may be balanced very nearly by the eye, or they may be more accurately balanced by method the third. Join the points A and C by a line, so will the content of the triangle ABC, be equal to that contained between the line AC, and the crooked boundary from A to B. and to C: by this method the number of triangles will be greatly lessened, and the content become more certain; for the fewer operations you have, the less subject will you be to err: and if an error be committed, the sooner it may be discovered.

The lines of the map should be drawn small, and neat, as well as the bases; the compasses neatly pointed, and scale accurately divided; without all which you may err greatly. The multiplications should be run over twice at least, as also the addition of the column content.

From what has been said, it will be easy to survey a field, by reducing it into triangles, and measuring the bases and perpendiculars by the chain. To ascertain the content only, it is not material to know at what part of the base the perpendicular was taken: since it has been shewn (in cor. to theo. 13. geom.) that triangles on the same base, and between the same parallels, are equal; but if you would draw a map from the bases and perpen-

G g

diculars, it is evident that you must know at what part of the base the perpendicular was taken, in order to set it off in its due position; and hence the map is easily constructed.

PROB. XVI.

To determine the area of a frieze of ground, having the man given, by reducing it to one triangle equal thereto, and thence finding its content.

PL. 8. fig. 5.

Let A B C D E F G H be a map of ground, which you would reduce to one triangle equal thereto.

Produce any line of the map, as AH, both ways, lay the edge of a parallel ruler, from A to C, having B above it; hold the other side of the ruler, or that next you, fast; open till the same edge touches B, and by it, with a protracting pin, mark the point b, on the produced line, lay the edge of the ruler from b to D, having C above it, hold the other side fast, open till the same edge touches C, and by it mark the point c, on the produced line. A line drawn from c to D will take in as much as it leaves out of the map.

Again lay the edge of the ruler from H to F, having G above it, keep the other side fast, open till the same edge touches G, and by it mark the point g, on the produced line; lay the edge of the ruler from g to E, having F above it, keep the other side fast, open till the same edge touches F, and by it mark the point f, on the produced line. Lay the edge of the ruler from f to D, having E

above it, keep the other side fast, open till the same edge touches E, and by it mark the point e, on the produced line. A line drawn from D to e, will take in as much as it leaves out. Thus have you the triangle c D e, equal to the irregular polygon A B C D E F G H.

If when the ruler's edge be applied to the points \mathcal{A} and \mathcal{C} , the point \mathcal{B} falls under the ruler, hold that side next the said points fast, and draw back the other to any convenient distance; then hold this last side fast, and draw back the former edge to \mathcal{B} , and by it mark \mathcal{b} , on the produced line; and thus a parallel may be drawn to any point under the ruler, as well as if it were above it. It is best to keep the point of your protracting pin in the last point in the extended line, till you lay the edge of the ruler from it to the next station, or you may mistake one point for another.

This may also be performed with a scale, or ruler, which has a thin sloped edge, called a fiducial edge; and a fine pointed pair of compasses. Thus,

Lay that edge on the points A and C, take the distance from the point B to the edge of the scale, so that it may only touch it, in the same manner as you take the perpendicular of a triangle; carry that distance down by the edge of the scale parallel to it, to b; and there describe an arc on the point b; and if it just touches the ruler's edge, the point b is in the true place of the extended line. Lay then the fiducial edge of the scale from b to D, and take a distance from C, that will just touch the edge of the scale; carry that distance along the edge, till the point which was in C, cuts the produced line in c; keep that foot in c, and

describe an arc, and if it just touches the ruler's edge, the point c is in the true place of the extended line. Draw a line from c to D, and it will take in and leave out equally: in like manner the other side of the figure may be balanced by the line c D.

Let the point of your compasses be kept to the last point of the extended line, till you lay your scale from it to the next station, to prevent mistakes from the number of points.

That the triangle c D c, is equal to the right-lined figure ABCDEFGH, will be evident from problems 18. 19. geom. for thereby, if a line were drawn from b to C, it will give and take equally, and then the figure b C D E F G H, will be equal to the map. Thus the figure is lessened by one side, and by the next balance line will lessen it by two, and so on, and will give and take equally. In the same manner an equality will arise on the other side.

The area of the triangle is easily obtained, as before, and thus you have the area of the map.

It is best to extend one of the shortest lines of the polygon, because if a very long line be produced, the triangle will have one angle very obtuse, and consequently the other two very acute; in which case it will not be easy to determine exactly the length of the longest side, or the points where the balancing lines cut the extended one.

This method will be found very useful and ready in small enclosures, as well as very exact; it may be also used in large ones, but great care must be taken of the points on the extended line, which will be crowded, as well as of not missing a station.

PROB. XVII.

A map with its area being given, and its scale omitted to be either drawn or mentioned; to find the scale.

OAST up the map by any scale whatsoever, and t will be.

As the area found
Is to the square of the scale by which you cast up,
:: The given area of the map
To the square of the scale by which it was laid
down.

The square root of which will give the scale.

EXAMPLE.

A map whose area is 126Å. 3R. 16P. being given; and the scale omitted to be either drawn or mentioned; to find the scale.

Suppose this map was cast up by a scale of 20 perches to an inch, and the content thereby produced be 31A. 2R. 34P.

As the area found, 31A.2R. 34P.=5074P.

Is to the square of the scale by which it was cast up, that is to 20×20=400,

:: The given area of the map 126A. 3R. 16P. = 20296P.

To the square of the scale by which it was laid down.

5074:400:: 20296: 1600 the square of the required scale.

Root. 1600(40 16 8(00

Answer. The map was laid down by a scale of 40 perches to an inch.

PROB. XVIII.

How to find the true content of a survey, though it be taken by a chain that is too long or too short.

Let the map be constructed, and its area found as if the chain were of the true length. And it will be,

As the square of the true chain
Is to the content of the map,
: The square of the chain you surveyed by
To the true content of the map.

Example.

If a survey be taken with a chain which is 3 inches too long; or with one whose length is 42 feet 3 inches, and the map thereof be found to contain 920A. 2R. 20P. Required the true content.

As the square of 42F. 0In.=the square of 504 inches=254016.

Is to the content of the map 920A. 1R. 20P. = 147260P.

:: The square of 42F. 3In. = the square of 507 inches = 257049.

To the true content.

P. P. 250416: 147260:: 257049: 149019
A. R. P. 160(149019(931. 1. 19 Answer.

501 219 40)59(1R. 19P. METHOD OF DETERMINING THE AREAS OF RIGHT-LINED FIGURES UNIVERSALLY, OR BY CALCULATION.

DEFINITIONS.

PL. 8. fig. 7.

- 1. MERIDIANS are north and south lines, which are supposed to pass through every station of the survey.
- 2. The difference of latitude, or the northing or southing of any stationary line, is the distance that one end of the line is north or south from the other end; or it is the distance which is intercepted on the meridian, between the beginning of the stationary line and a perpendicular drawn from the other end to that meridian. Thus, if N. S. be a meridian line passing through the point A of the line AB, then is Ab the difference of latitude or southing of that line,
- 3. The departure of any stationary line, is the nearest distance from one end of the line to a meridian passing through the other end. Thus Bb is the departure or easting of the line AB: but if CB be a meridian, and the measure of the stationary distance be taken from B to A; then is BC the difference of latitude, or northing, and AC the departure or westing of the line BA.

- 4. That meridian which passes through the first station, is sometimes called the first meridian; and sometimes it is a meridian passing on the east or west side of the map, at the distance of the breadth thereof, from east to west, set off from the first station.
- 5. The meridian distance of any station is the distance thereof from the first meridian, whether it be supposed to pass through the first station, or on the east or west side of the map.

THEO. I.

In every survey which is truly taken, the sum of the northings will be equal to that of the southings; and the sum of the eastings equal to that of the westings.

PL. 9. fig. 1.

Let a, b, c, e, f, g, h, represent a plot or parcel of land. Let a be the first station, b the second, c the third, &c. Let NS be a meridian line, then will all lines parallel thereto, which pass through the several stations, be meridians also; as ao, bs, cd, &c. and the lines bo, cs, de, &c. perpendicular to those, will be the east or west lines, or departures.

The northings, ei+go+hq=ao+bs+cd+fr the southings: for let the figure be completed; then it is plain that go+hq+rk=ao+bs+cd, and ei-rk=fr. If to the former part of this first equation ei-rk be added, and fr to the latter, then go+hq+ei=ao+bs+cd+fr; that is, the sum of the northings is equal to that of the southings.

Ηh

The eastings cs+qa=ob+de+if+rg+oh, the westings. For aq+yo (az) = de+if+rg+oh, and bo=cs-yo. If to the former part of this first equation, cs-yo be added, and bo to the latter, then cs+aq=ob+de+if+rg+oh; that is, the sum of the eastings is equal to that of the westings. Q. E. D.

SCHOLIUM.

This theorem is of use to prove whether the tield-work be truly taken, or not; for if the sum of the northings be equal to that of the southings, and the sum of the eastings to that of the westings, the field-work is right, otherwise not.

Since the proof and certainty of a survey depend on this truth, it will be necessary to shew how the difference of latitude and departure for any stationary line, whose course and distance are given, may be obtained by the table, usually called the Traverse Table.

To find the difference of Latitude and departure, by the Traverse Table.

This table is so contrived, that by finding therein the given course, and a distance not exceeding 120 miles, chains, perches, or feet, the difference of latitude and departure is had by inspection: the course is to be found at the top of the table when under 45 degrees; but at the bottom of the table when above 45 degrees. Each column signed with a course consists of two parts, one for the

difference of latitude, marked Lat the other for the departure, marked Dep. which names are both at the top and bottom of these columns. The distance is to be found in the column marked Dist. next the left hand margin of the page.

EXAMPLE.

In the use of this table, a few observations only are necessary.

- 1. If a station consist of any number of even chains or perches (which are almost the only measures used in surveying) the latitude and departure are found at sight under the bearing or course, if less than 45 degrees; or over it if more, and in a line with the distance.
- 2. If a station consist of any number of chains and perches, and decimals of a chain or perch, under the distance 10, the lat. and dep. will be found as above, either over or under the bearing; the decimal point or separatrix being removed one figure to the left, which leaves a figure to the right to spare.

If the distance be any number of chains or perches, and the decimals of a chain or perch, the lat and dep. must be taken out at two or more operations, by taking out the lat and dep. for the chains or perches in the first place; and then for the decimal parts.

To save the repeated trouble of additions, a judicious surveyor will always limit his stations to whole chains, or perches and lengths, which can commonly be done at every station, save the last.

1. In order to illustrate the foregoing observations, let us suppose a course or bearing, to be S. 35°. 15′ E. and the distance 79 four-pole chains. Under 35°. 15′, or 35¼ degrees; and opposite 79, we find 64. 52 for the latitude, and 45. 59 the departure, which signify that the end of that station differ in latitude from the beginning 64. 52 chains, and in departure 45. 59 chains.

Note. We are to understand the same things if the distance is given in perches or any other measures, the method of proceeding being exactly the same in every case.

Again, let the bearing be 54‡ degrees and distance as before; then over said degrees we find the same numbers, only with this difference, that the lat. before found, will now be the dep. and the dep. the lat. because 54‡ is the complement of 35‡ degrees to 90, vis. lat. 45. 59. dep. 64. 52.

2. Suppose the same course, but the distance 7 chains 90 links, or as many perches. Here we find the same numbers, but the decimal point must be removed one figure to the left.

Thus, under $35\frac{1}{4}$, and in a line with 79 or 7.9, are

Lat. 6. 45 Dep. 4. 56

the 5 in the dep. being increased by 1, because the 9 is rejected; but over 544 we get

Lat. 4. 56 Dep. 6. 45 3. Let the course be as before, but the distance 7.79, then opposite

Dep. 4. 43	Lat. 6. 29 7	7. 70 9
-		
4. 49	6. 36	7. 79
	-	

Or opposite

7. 00 . 79	Lat. 5. 72 . 64	Dep. 4. 03 . 46
7. 79	6. 36	4. 49

THEO. II.

When the first meridian passes through the map.

If the east meridian distances in the middle of each line be multiplied into the particular southing, and the west meridian distances into the particular northing, the sum of these products will be the area of the map.

PL. 10. fig. 1.

Let the figure abkm be a map, the lines, ab bk to the southward, and km ma to the northward, NS the first meridian line passing through the first station a.

The meridian
$$\begin{cases} sd \times ao \\ tu \times ox(by) \end{cases}$$
 = Area $\begin{cases} am \\ ow \end{cases}$

The meridian $\begin{cases} ef \times gx \\ hh \times ga(my) \end{cases}$ = Area $\begin{cases} xp \\ gl \end{cases}$

These four areas am + ow + xp + gl will be the area of the whole figure *cmsniprlc*, which is equal to the area of the map abkm. Complete the

figure.

The parallelograms am and ow, are made of the east meridian distances ds and tu, multiplied into the southings ao and ox. The parallelograms xp and gl are composed of the west meridian distances of and hh, multiplied into the northings xg and ga (my) but these four parallelograms are equal to the area of the map; for if from them be taken the four triangles marked Z, and in the place of those be substituted the four triangles marked O, which are equal to the former; then it is plain the area of the map will be equal to the four parallelograms. Q. E. D.

THEO. III.

If the meridian distance when east, he multiplied into the southings, and the meridian distance when west he multiplied into the northings, the sum of these less by the meridian distance when west, multiplied into the southings, is the area of the survey.

PL. 10. fig. 2.

Let ab c be the map.

The figure being completed, the rectangle af is made of the meridian distance eq when east, multiplied into the southing an; the rectangle yk is made of the meridian distance xw, multiplied into the northings cz or ya. These two rectangles, or parallelograms, af+yk, make the area of the figure dfnyikd, from which taking the rectangle oy, made of the meridian distance tu when west, into the southings oh or bm, the remainder is the area of the figure dfokkd, which is equal to the area of the map.

Let bou = Y, urih = L, ric = O, wrc = Z = akw = K, and efb = B, ade = A. I say, that Y+Z+B=K+L+A.

Y=L+O, add Z to both, then Y+Z=L+O+Z; but Z+O=K, put K instead of Z+O; then Y+Z=L+K, add to both sides the equal triangles B and A, then Y+Z+B=L+K+A. If therefore B+Y+Z be taken from abc, and in lieu thereof we put L+K+A, we shall have the figure dfohikd=abc, but that figure is made up of the meridian distance when east, multiplied into the southing, and the meridian distance, when west, multiplied into the northing less by the meridian distance, when west, multiplied into the southing. Q. E. D.

COROLLARY.

Since the meridian distance (when west) multiplied into the southing, is to be subtracted, by the same reasoning the meridian distance when east, multiplied into the northing, must be also subtracted.

SCHOLIUM.

From the two preceding theorems we learn how to find the area of the map, when the first meridian passes through it; that is, when one part of the map lies on the east and the other on the west side of that meridian. Thus,

RULE.

The merid. east {multiplied {southings}}
Dist. when } west { into the {northings}}
their sum is the area of the map.

But,

The merid. {east } multiplied {northings}
Dist. when {west} into the {southings}
the sum of these products taken from the former
gives the area of the map.

These theorems are true, when the surveyor keeps the land he surveys, on his right hand, which we suppose through the whole to be done; but if he goes the contrary way, call the southings northings, and the northings southings, and the same rule will hold good.

General Rule for finding the Meridian distances.

- 1. The meridian distance and departure, both east, or both west, their sum is the meridian distance of the same name.
- 2. The meridian distance and departure of different names; that is, one east and the other west, their difference is the meridian distance of the same name with the greater.

Thus in the first method of finding the area, as in the following field-book.

The first departure is put opposite the northing or southing of the first station, and is the first meridian distance of the same name. Thus if the first departure be east, the first meridian distance will be the same as the departure, and east also; and if west, it will be the same way.

The first meridian distance The next departure	6.61 E. 6.61 E.
The second meridian distance The next departure	13.22 E. 1.80 E.
The third meridian distance	15.02 E.

At station 5, the meridian distance The next departure	5.78 E. 7.76 W.
The next meridian distance	1,98 W.
At station 11, the meridian distance The next departure	0.12 W. 5.84 E.
The next meridian distance	5.72 E.

PL. 10. fig. 3.

In the 5th and 11th stations, the meridian distance being less than the departures, and of a contrary name, the map will cross the first meridian, and will pass as in the 5th line, from the east to the west line of the meridian; and in the 11th line it will again cross from the east to the west side, which will evidently appear, if the field-work be protracted, and the meridian line passing through the first station, be drawn through the map.

The field-book cast up by the first method, will be evident from the two foregoing theorems, and therefore requires no further explanation; but to find the area, by the second method, take this

RULE

When the meridian distances are east, put the products of north and south areas in their proper columns; but when west, in their contrary columns; that is, in the column of south area, when the difference of latitude is north; and in north when south: the reason of which is plain, from the two last theorems. The difference of these two columns will be the area of the map.

					•	
No. St.	Bearings	C. L.	Lat. and half Dep		Area.	Deduct.
1	NE 75	13.70	N 3.54 E 6.61	6.61 E 13.22 E		23.3994
2	NE 201	10.30		15.02 E 16.82 E		144.9430
3	East	16.20		2 4.92 E 33.02 E		
4	SW 333	35.30	S 29.44 W 9.74	23.28 E :3.54 E	68 <i>5</i> .3632	
5	SW 76	16.00	S 3.87 W 7.76	5.78 E 1.98 W	22.3686	
6	North	9.00	N 9.00 0.00	1.98 W 1.98 W	17.8200	
7	SW 84	11.60	S 1.21 W 5.77	7.75 W 13.52 W		9.3775
8	NW 584	11.60		18.16 W 22.80 W	126.0304	
9	NE 36#		N 15.38 E 5.74	1.06 W	262-3828	
10	NE 223	14.00	N 12.93 E 2.68	8.64 W 5.96 W	111.7152	
11	SE 763		S 2.75 E 5.84	0.12 W 5 72 E		0.3300
12	SW 15		S 10.48 W 1.40	4.32 E 2.92 E	45.2736	
13	SW 16‡		S 9.69 W 1.46	1.46 E 0.00	14.1474	
1285.1012 178.0499				178.0499		
Content in Chains, 1107.0513						

The foregoing Field-Book, Method II. 243

It is needless here to insert the columns of bearing or distances in chains, they being the same as before.

No.	Lat	. and	Merid.	lss .	
St.		Dep.	Dist.	N. Area.	S. Area,
1	N E	ن.54 6.61	6.61 E	23.3994	
2	N E	9.65	15.02 E	144.9430	
3	-	0.00	24.92 E		
1	1-	8.10 29.44	33.02 E 23.28 E		685.3532
5	w s	9.74 3.87	13.54 E 5.78 E		22.3686
-	W	7.76 9.00	1.98W 1.98W		17.8200
	s	0.00	1.98W 7.75W		
7	W	5.77	13.52W	9.3775	
-	w	4.64	22.80W		126.0308
9	NE	15.38 5.74	17.06W 11.32W		262.3828
10	N E	12.93 2.6 8	8.64W 5.96W		111.7152
. * *	S E	2.75 5.84	0.12W 5.72 E	0.3300	
12	Ś W	1.40	4.32 E 2.92 E		45.2736
13	s W	9.69	1.46 E 0.00		14.1474
		•	•	178.0499	284.1012
					178 0499
Aı	rea ir	chair	ıs, as befe	ore,	1107.0513

Construction of the Map from either the 1st or the 2d Tuble;

PL. 10. Ag. 3.

Draw the line NS for a north and south line. which call the first meridian; in this line assume any point, as 1, for the first station. Set the northing of that stationary line, which is 3.54, from 1 to 2, on the said meridian line. Upon the point 2 raise a perpendicular to the eastward, the meridian distance being easterly, and upon it set 13.22, the second number in the column of meridian distance from 2 to 2, and draw the line 1 2, for the first distance line: from 2 upon the first meridian, set the northing of the second stationary line, that is, 9.65 to 3, and on the point 3 erect a perpendicular eastward, upon which let the meridian distance of the second station 16.82, from 3 to 3, and draw the line 2 3, for the distance line of the second station. And since the third station has neither northing nor southing, set the meridian distance of it 33.02, from 3 to 4, for the distance line To the fourth station there of the third station. is 29.44, southing, which set from 3 to 5; upon the point 5, erect the perpendicular 5 5; on which lay 13.54, and draw the line 4 to 5.

In the like manner proceed to set the northings and southings on the first meridian, and the meridian distances upon the perpendiculars raised to the east or west; the extremities of which connected by right lines, will complete the map.

IND in the first place, by the Traverse Table, the lat. and dep. for the several courses and distances, as already taught; and if the survey be

A Specimen of the Pennsylvania Method of CALCULATION; which, for its Simplicity and Rase, in finding the Meridian Distances, is supposed to be preferable in Practice to any Thing here-tofore published on the Subject.

truly taken, the sums of the northings and southings will be equal, and also those of the eastings and westings. Then, in the next place, find the meridian distances, by choosing such a place in the column of eastings or westings, as will admit of a continual addition of one, and subtraction of the other; by which means we avoid the inconvenience of changing the denomination of either of the departures.

The learner must not expect that in real practice the columns of lat. and those of dep. will exactly balance when they are at first addedup, for little inaccuracies will arise, both from the observations taken in the field, and in chaining; which to adjust, previous to finding the meridian distances, we may observe, That if, in small surveys, the difference amount to two-tenths of a perch for every station, there must have been some error committed in the field; and the best way in this case, will be to rectify it on the ground by a re-survey, or at least as much as will discover the error. But when the differences are within those limits, the columns of northing, southing, easting, and westing, may be corrected as follows:

Add all the distances into one sum, and say, as that sum is to each particular distance, so is the difference between the sums of the columns of northing and southing to the correction of northing or southing belonging to that distance: the corrections thus found are respectively additive, when they belong to the column of northing or southing, which is the less of the two, and subtractive when they belong to the greater; if the course be due east or west, the correction is always additive to the less of the two columns of northing or southing. The corrections of easting and westing are found exactly in the same manner.

This rule was investigated two different ways, by N. Bowditch, Author of the Practical Navigator, and R. Adrain, Prof. Math. and N. Phil. Columbia Col. N. York, as may be seen in the Analyst No. IV. published in 1808.

The following example will sufficiently illustrate the manner of applying the rule.

In this example the sum of the distances is 791, and the difference between the columns of northing and southing, is .4, also the first distance is 70; say then,

which fourth proportional .04 is the first correction belonging to the southing 53.6, from which the correction .04 should be subtracted.

In this manner the several corrections of the southings

But as only two of these corrections amount to half a tenth, we must use .1 for each of the corrections .09 and .07, and neglect the correction .04; thus the correct southings become

In like manner from the remaining distances we obtain to

the northings
$$\begin{array}{c} 62.9 \\ 101.1 \\ 54.0 \\ 00.0 \end{array}$$
 the additive corrections .06 $\begin{array}{c} .04 \\ .05 \\ .07 \end{array}$

And consequently, by neglecting .04, and .03, and using .1 for each of the two .06 and .07, the northings

In obtaining these corrections, it is commonly unnecessary to use all the significant figures of the distances: thus, for the ratio of 791 to 70, we may say, as 80 to 7.

			1								7	1
				7	6	5	•	છ	22	-	<u>o</u>	L
		٠		West.	S. 8 W.	S. 81 E.	North.	N. 36 E.	N. 45 W.	S. 40° W.	No. Courses.	Field-Notes.
				130	187	186	2	125	89	70	Per.	
	Diff.		218.0				54.0	101.1	62.9		Z.	13
	1	218.0	218.4		1357	29.1				53.6	ŝ	om the
	:2	257.0	257.2			183.7		73.5			'n	From the Tables.
	Diff		257.0	130.0	19.1				62.9	45.0	₩.	مَعْ
•		-	257.0 218.2 218.2 257.1 257.1	00.1			54.0	101.2	62.9		Z	Î
			218.2		135 6	29.0				53.6	ç	Corrected.
			257.1			183.6		73.5			iii	cted.
			257.1	130.0	19.2			·	62.9	•5.0	₩.	

EXAMPLE OF CORRECTING A SURVEY

The latitudes and departures being thus balance ed, proceed to insert the meridian distances by the above method, where we still make use of the same field notes, only changing chains and links into perches and tenths of a perch. Then by looking along the column of departure, it is easy to observe, that in the columns of easting, opposite station 9, all the eastings may be added, and the westings subtracted, without altering the denomination of either. Therefore by placing 46.0, the east departure belonging to this station in the column of meridian distances, and proceeding to add the eastings and subtract the westings, according to the rule already mentioned, we shall find that at station 8, these distances will end in 0, 0, or a cypher, if the additions and subtractions be rightly made. Then multiplying the upper meridian distance of each station by its respective northing or southing, the product will give the north or south area, as in the examples already insisted on. and which is fully exemplified in the annexed specimen. When these products are all made out. and placed in their respective columns, their difference will give double the area of the plot, or twice the number of acres contained in the survey. Divide this remainder by 2, and the quotient thence arising by 160 (the number of perches in an acre), then will this last quotient exhibit the number of acres and perches contained in the whole survey; which in this example may be called 110 acres, 103 perches, or 110 acres, 2 quarters, 23 perches.

FIELD-NOTES, of the two foregoing Methods, as Practised in Pennsylvania.

Cast up by perches and tenths of a perch.

N.	Courses.	Dist	N.	Б.	E.	W.	MD.	N. Area.	S. Areas.
1	N 75.00 E	54.8	14.2		52.9		285.3 288.2	3341.26	
2	N 20.90 E	41.2	38.6		14.4		302.6 317.0	11680.36	
3	East.	64.8			64.8		381.8 446.6		
4	S 33.30 W	141.2		117.7		77.9	\$68.7 290.8		43595.99
5	8 76.00 W	64.0		15.5		62.1	228.7 166.0		3544.85
6	North.	36.0	\$6.0				166.6 166.6	5977.60	
7	S 84.00 W	46.4		4.9		46.1	1.0.5 74.4		590.45
8	N 58.15 W	46.4	27.8			37.2	37.2 00.0	1034.16	
9	N 36.45 E	76.8	61.5 '		46.0		46 .0 92 .0	2829.00	
19	N 22.30 E	56.0	51,7		21.4		113.4 154.8	5862.78	
11	8 76.45 E	48.0		11.0	46.7		181.5 928.2		1996.50
12	5 15,00 W	48.4		41.9		11.2	217.0 205.8		9092.30
13	S 16.45 W	40.5		88.8		11.7	194.1 184.4		7531.08
			229.8	229.8	246.2	:46.2		30745.16	36151.17 4.745.16
		•						2	>406.01
							Area	in perches.	1 7703 (6 05

SECTION IV.

OF OFF-SETS.

IN taking surveys it is unnecessary and unusual to make a station at every angular point, because the field-work can be taken with much greater expedition, by using off-sets and intersections, and with equal certainty; especially where creeks, &c. bound the survey.

Off-sets are perpendicular lines drawn or measured from the angular points of the land, that lie on the right or left hand to the stationary distance, thus,

PL. 11. fig. 2.

Let the black lines represent the boundaries of a farm or township: and let 1 be the first station; then if you have a good view to 2, omit the angular points between 1 and 2, and take the bearing and length of the stationary line 1, 2, and insert them in your field-book: but in chaining from 1 to 2, stop at d opposite the angular point a, and in your field-book insert the distance from 1 to d, which admit to be 4 C. 25L. as well as the measure of the off-set ad, which admit to be 1C. 12L. thus: by the side of your field-book in a line with the first station, say at 4C. 25L. L. 1C. 12L. that is, at 4C. 25L. there is an off-set to the left hand of 1C. 12L.

This done, proceed on your distance line to e opposite to the angle e, and measure e, supposing then 1 e to be 7C. 40L. and e 3C. 40L. say (still in a line with the first station in your field-book) at 7C. 40L. L. 3C. 40L." That is, at 7C. 40L. there is an off-set to the left of 3C. 40L. proceed then with your distance line to e opposite to the angle e, and measure e ; suppose then 1 e to be 13C. and e 1C. 25L. asy in the same line as before, at 13C. L. 1C. 25L. Then proceed from e to 2, ar 1 you will have the measure of the entire stationary line 1, 2, which insert in its proper column by the bearing.

In taking off-sets, it is necessary to have a perch chain, or a staff of half a perch, divided into links for measuring them; for by these means the chain in the stationary line is undisturbed, and the number of chains and links in that line from whence, or to which, the off-sets are taken, may be readily

known.

Having arrived at the second station, if you find your view will carry you to 3, take the bearing from 2 to 3, and in measuring the distance line, stop at l opposite g; admit 2l to be 4C. 10L. and the off-set lg 1C. 20L. then in a line with the second station in your field-book, say at 4C. 10L. R. 1C. 20L. that is, the off-set is a right hand one of 1C. 20L. Again at m, which suppose to be 10C. 25L. from 2; take the off-set mh of 1C. 15L. and in a line with the second station, say at 10C. 25L. R. 1C. 15L. In the same line when you come to the boundary at i, insert the distance 2i, 13C. 10L. thus, at 13C. 10L. 0; that is, at 13C. 10L. there is no off-set. At n, which is 15C. from 2, take the off-set nk 45L. and still opposite to the second station say at 15C. L. 45. L.

Let the line, 3, 6, represent the boundary, which by means of water, briers, or any other impediment, cannot be measured. In this case make one or more stations within or without the land, where the distances may be measured, and draw a line from the beginning of the first to the end of the last distance, thus; make stations at 3, 4, and 5, taking the bearings, and measuring the distances as usual, which insert in your field-book, and draw a mark like one side of a parenthesis, from the third to the fifth station, to shew that a line drawn from the third station to the farthest end of the fifth stationary line will express the boundary. Thus,

No. Sta.	Deg.	Ch. L.
(3	$172\frac{1}{2}$	5.45
4	200	13.25
$\begin{bmatrix} 3 \\ 4 \\ 4 \end{bmatrix}$	250	3.36

Suppose the point p of the boundary to be inaccessible, by means of the lines 6p or p7, being overflowed, or that of a quarry, furze, &c. might prevent your taking their lengths: in this case take the bearing of the line 6, 7, which insert opposite to the sixth station in your field-book with the other bearing; then direct the index to the point p, and insert its bearings on the left side of the field-book, opposite to the sixth station, annexing thereto the words Int. for boundary; and having measured and inserted the distance 6, 7, set the index in the direction of the line 7p, and insert its bearing on the left of the seventh station of the field-book, annexing thereto the words Int. for boundary: the crossing or intersection of these two bearings will determine the point p, and of course the boundary 6p7 is also determined.

If your view will then reach in the first station,

take its bearing, stationary line, and off-sets, as before, and you have the field-book completed. Thus,

The Field-Book.

Remarks and intersect.	N. St.	Deg.	C. L.	OFF-SETS.
318 Int. to a tower	1	358	22.12	At 4 C. 25 L. L. 1C. 12L. at 7C. 40L. L. 3C. 40L. at 13C. L. 1C. 25L.
231½ Int. to ditto	2	297 3	22.12	At 4C. 10L. R. 1C. 20L. at 10C. 25L. R. 1C. 51L. at 13C. 10L. 0. at 15C. L. 45L.
1551 Int. for bound. 274 Int. for ditto.	5	172 ¹ 200 250 125 105 ¹	13.25 3.36 15.15	 At 1C. 20L. L. 2C.

Close at the first station.

If you would lay down a tower, house, or any other remarkable object in its proper place; from any two stations take bearings to the object, and their intersection will determine the place where you are to insert it, in the manner that the tower is set out in the figure, from the intersection taken at the first and second stations of the above field-book.

A protraction of this will render all plain, on which lay off all your off-sets and intersections, and proceed to find the content by any of the methods in section the 4th.

The foregoing field-book may be otherwise kept, thus,

Remarks and intersection.	No St.	Deg.	L. han. Off-set Ch. L.		R. han. Off-set Ch. L.
318 Int. to a tower	ī	358	1.12 3.40 1.25	4.25 7.40 13.00 22.12	
232; Int. for ditto.	2	2971	0.45	4.10 10.25 13.10 15.00 21.21	1.20
155 Int. for bound.	3 4 5 6	1723 200 250 125		5.45 13.25 3.36 15.15	
274 In. for boundary.	7	105	2.20 2.32	1.20 7.45 11.25 12.25 15.10	0.36

How to east up off-sets by the pen.

PL. 11. fig. 2.

1,
$$2-1f=2f-1e=fe$$
, $1e-1d=ed$.

Then $1d \times \frac{1}{2}da = 1da$, by prob. 6, page 183, and $\frac{1}{2}cd \times da + fc = bcfc$, and $2f \times \frac{1}{2}fc = cf9$; the sum

of all which will be 1abc21; the area contained between the stationary line 1, 2, and the boundary, 1 abc 2.

In the same manner you may find the area of 2ihg2, of ik3i, as well as what is without and withinside of the stationary line 7, 1.

If therefore the left hand off-sets exceed the right hand ones, it is plain, the excess must be added to the area within the stationary lines, but if the right hand off-sets exceed the left hand ones, the difference must be deducted from the said area; if the ground be kept on the right hand, as we have all along supposed; or in words, thus;

To find the contents of off-sets.

- 1. From the distance line, take the distance to the preceding off-set, and from that the distance of the one preceding it, &c. in four-pole chains; so will you have the respective distances from off-set to off-set, but in a retrograde order.
- 2. Multiply the last of these remainders by is the first off-set, the next by is the sum of the first and second, the next by half the sum of the second and third, the next by half the sum of the third and fourth, &c. The sum of these will be the area produced by the off-sets.

Thus, in the foregoing field-book, the first stationary line is 22C. 12L. or 11C. 12L. of four-pole chains. See the figure.

• •	Ch. L.	Ch. L.	Ch. L	• •
From	11.12 = 1.2	6.50 = 1f	3.90 =	1 <i>e</i>
Take	6.50 = 1f	3.90 = 1e	2.25=	1 <i>d</i>
-	4.62=2f	2.60 = ef	1.65=	ed
ed=1.6 ef=2.60 2f=4.69 Content	5×1C. 26L.±0 0×1C. 32L.± 2×37L. half (the first off-set the sum of the 1s the sum of 2d a the last off-set = ets on the first le chains	st and 20 and 3d= =	
In lik The sur	e manner the n of the left	rest are perfo hand off-sets w right hand one	ill be	14.0856 3.6825
Excess	of left hand o	ff-sets in squ. 4		10.4031 1.04031
				.16124
•	1	Perc	hes	6.4496

Excess of left hand off-sets above the right hand ones, 1A. 0R. 6P. to be added to the area within the stationary lines.

SECTION V.

To find the area of a friece of Ground by intersections only, when all the angles of the field can be seen from any two Stations on the outside of the ground.

PL. 12. fig. 1.

LAET ABCDEFG be a field, H and I two places on the outside of it, from whence an object at every angle of the field may be seen.

Take the bearing and distance between H and I, set that at the head of your field-book, as in the annexed one. Fix your instrument at H, from whence take the bearings of the several angular points A, B, C, D, &c. as they are here represented by the lines HA, HB, HC, HD, &c. fix your instrument at I, and take bearings to the same angular points, represented by the lines IA, IB, IC, ID, &c. and let the first bearings be entered in the second column, and the second bearings in the third column, of your field-book; then it is plain that the points of intersection, made from the bearings in the second and third columns of every line, will be the angular points of the field, or the points A, B, C, D, &c. which points being joined by right lines, will give the plan ABCDEFGHA required.

L

		_							
Bear. 180 Dis. 28C. of the Sta. H and I.									
No. Bear. Bear.									
Ī		$261\frac{1}{2}$							
		265‡							
		248							
1		2384							
		$215\frac{1}{2}$							
		$208\frac{1}{2}$							
} (J	220	300						

The same may be done from any two stations within-side of the land, from whence all the angles of the field can be seen.

This method will be found useful in case the stationary distances from any cause prove inaccessible, or should it be required to be done by one party, when the other in whose possession it is, refuses to admit you to go on the land.

To find the content of a field by calculation, which was taken by intersection.

In the triangle AIH, the angles AHI, AIH, and the base HI being known, the perpendicular Aa, and the segments of the base Ha, AI may be obtained by trigonometry: and in the same manner all the other perpendiculars Bb, Cc, Dd, Ee, Ff, Gg, and the several segments at b, c, d, e, f, and g: if therefore the several perpendiculars be supposed to be drawn into the scheme (which are here omitted to prevent confusion arising from a multiplicity of lines) it is plain that if from bBCDEeb, there be taken bBAGFeb, the remainder will be the map ABCDEFGA.

As before half the sum of Bb, and Cc multiplied by bc, will be the area of the trapezium bBCc; after the same manner, half the sum of Cc, and Dd, multiplied by cd, will give the area of the trapezium cCDd; and again, half the sum of Dd, and Ec multiplied by dc, gives the area of the trapezium dDEc; and the sum of these three trapezia will be the area of the figure bBCDcb.

Again, in the same manner, half the sum of Bb and Aa multiplied by ah, will give the area of the trapezium BbAa; and half the sum of aA, and gG, by ag, gives the trapezium aAGg; to these add the trapezia gGFf, and fFEe, which are found in the like manner; and you will have the figure bBAGFEeb, and this taken from bBCDeb, will leave the map ABCDEFGA. Q. E. F.

It will be sufficient to protract this kind of work, and from the map to determine the area as well as in plate 10. fig. 3. to find the areas of the pieces, 3, 4, 5, 6, 3, and 6, 7, 7, 6, from geometrical constructions.

How to determine the station where a fault has been committed in a field book, without the trouble of going round the whole ground a second time.

From every fourth or fifth station, if they be not very long ones, or oftener if they are, let an intersection be taken to any object, as to any particular part of a castle, house, or cock of hay, &c. or if all these be wanting, to a long staff with a white sheet or napkin set thereon, to render the object more conspicuous, and let this be placed on the summit of the land, and let the respective intersections so

taken be inserted on the left hand side of the fieldbook, opposite to the stations from whence they were respectively taken.

In your protraction as you proceed, let every intersection be laid off from the respective stations from whence they were taken, and let these lines be continued; if they all converge or meet in one point, we thence conclude all is right, or so far as they do converge; but if we find a line of intersection to diverge or fly off from the rest, we may be sure that either a mistake has happened between the station the foregoing intersection was taken at, and the station from whence the intersection line diverges, or there must be an error in the intersection; but to be assured in which of these the fault is, protract on to the next intersection, and having set it off, if it converges with the rest, though the foregoing one did not, we may conclude the fault was committed in taking the last intersection but one, and none in any station, and that so far is true as is protracted; but if this as well as the foregoing intersection diverge or fly from the point of concourse or converging point of the rest, the error must have its rise from some station or stations, at or after that, from whence the last converging intersection line was taken: so that by going to that station on the ground, and proceeding on to that where the next, or from whence the following diverging intersection was taken, we can readily and with little trouble set all to rights.

But in most tracts of land, one object cannot be seen from every station, or from perhaps one fourth of them; in this case we are under the necessity to move the pole after we begin to lose sight of it, to some other part of the land, where

it may be seen from as many more stations as possible; which is easily done by viewing the boundary before it be surveyed: the pole then being fixed in an advantageous place, the first intersection to it is best to be made from the same station from whence the last one was taken, and then as often as may be thought convenient, as before; in like manner the whole may be done by the removal of the pole.

When we here speak of stations, we do not mean such as are usually taken at every particular angle of the field: for it is to be apprehended, that every skilful surveyor, particularly such who use calculation, will take the longest distances possible, not only to lessen the number of stations, for the ease of either protraction or calculation, but with greater certainty to account for the land passed by, on the right hand or on the left, which is taken by off-sets: and surely it will be allowed that any measure taken on the ground, and the content thence arithmetically computed, will be much more accurate than that which is obtained from any geometrical projection.

From what has been said it is plain, that from this method any fault committed in a survey can be readily determined, and therefore must be much preferable to the present method of taking diagonals, or the bearings and lengths of lines across land, to accomplish that end; which last method is too frequently used by surveyors to approximate or arrive near the content, which will ever remain uncertain, let these diagonals be ever so many, till the station or stations wherein the error or errors were committed, be found; and the fault or faults be corrected.

Where one diagonal is taken, it may perhaps close or meet with one part of the survey and not with the other; in this case, if the surveyor would discover his error, he must survey that part of the land which did not close, and this may be half or more, of the whole. And should the diagonal close with neither part, but be too long, or too short, or should it fall on either side of the assigned point it was to close with, he ought to go over the whole, and make a new survey of it in order to discover his error.

A number of diagonals are frequently taken, the sum of the lengths of which very often exceeds the circuit of the ground, and after all they are but approximations, and the content remains uncertain as before; therefore he who returns a map, made up by the assistance of diagonals, where there remains a misclosure in any one part, runs the risque of being detected in an error, and must suffer uneasiness in his mind, as he cannot be certain of the return he makes.

The frequent misclosures which are botched up by diagonals, occasion the many and frequent scandalous broils and animosities between surveyors, which tend to the loss of character of the one or the other, and indeed often to the disrepute of both, as well as to that of the science they profess.

But these may be easily remedied by intersections, and the bearing or line to be adjusted where the fault was committed, and till this be found, nothing can be certain.

SECTION VI.

TO ENLARGE OR DIMINISH MAPS.

To enlarge or diminish a man, or to reduce a man from one scale to another; also the manner of uniting separate mans of lands which join each other, into one Man of any assigned size.

LAY the map you would enlarge, over the paper on which you would enlarge it, and with a fine protracting pin, prick through every angular point of your map, join these points on your paper (laying the map you copy before you) by pencilled or popped lines, and you have the copy of the map you are to enlarge: in this manner any protractiom may be copied on paper, vellum, or parchment, for a fair map.

If you would enlarge a map to a scale which is double, or treble, or quadruple to that of the map to be enlarged, the paper you must provide for its enlargement must be two, or three, or four times as long and broad as the map; for which purpose in large things you will find it necessary to join several sheets of paper, and to cement them with white wafer or paste, but the former is best,

Then pitch upon any point in your copied map for a centre; from whence if distances be taken to its extreme points, and thence if those distances be set in a right line with (but from) the centre, and these last points fall within your paper, the map may be increased on it to a scale as large again as its own; and if the like distances be again set outwards in right lines from the centre, and if these last points fall within your paper, it will contain a map increased to a scale three times as large as its own, &c.

PL. 12. fig. 2.

Let the pricked or popped lines represent the copy of a down or old survey, laid down by a scale of 80 perches to an inch, and let it be required to enlarge it to one laid down by 40 to an inch.

Pitch upon your centre as Θ , from whence thro' a lay the fiducial edge of a thin ruler, with a fine pointed pair of compasses, take the distance from a to the centre Θ , and lay it by the ruler's edge from a to A: in the like manner take the distance from the next station b to the centre Θ , and lay it over in a right line from b to B, and join the points A and B by the right line AB; in the like manner set over the distance from every station to the centre, from that station outwards, and you will have every point to enlarge to; the joining of these constantly as you go on by right lines, will give you the enlarged map required.

In taking the distance from every station to the centre, set one foot of the compasses in the station, and the other very lightly over the centrepoint, so lightly as scarcely to touch it, otherwise the centre-point will become so wide, that it may occasion several errors in the enlarged map: for

if you err from the exact centre but a little, that error will become double, or treble, or quadruple, as you enlarge to a scale that is double, or treble, or quadruple of the given one; therefore great accuracy is required in enlarging a map.

When you have done with a station, give a dash with a pen or pencil to it, such as at the station a and b; by this means you cannot be disappointed in missing a station, or in laying your ruler over one station twice.

From what has been said it is plain, that if a map is to be enlarged to one whose scale is double the given one, that the distances from the respective stations to the centre, being set over by the ruler's edge, will give the points for the enlarged one. And thus may a map be enlarged from a scale of 160 to one of 80, from one of 80 to one of 40, from one of 20 to one of 10 perches to an inch, For to enlarge to a scale that is double, the number of perches to an inch for the enlarged map must be half of those to an inch for that to be enlarged: to enlarge to a scale that is treble the given one, the number of perches to an inch for the enlarged map, will be one third of those for the other; if to a scale that is quadruple the given one, the number of perches to an inch for the enlarged map, will be one fourth of those for the other, &c. therefore if you would enlarge a map which is laid down by a scale of 120 perches to an inch, to one of 40 perches to an inch, the distance from the several stations to the centre, being set twice beyond the said stations, will mark out the several points required, for these points will be three times further from the centre than the stationary points of the map are.

M m

In the same manner, if you would enlarge a map from a scale of 160, to one of 40 perches to an inch, the distance from the several stations to the centre, being set three times beyond said stations, will lay out the points for your enlarged map, for these points will be four times further from the centre than are the stations of the map.

When a map is enlarged to another, whose scale is double, or treble, or quadruple, &c. of the given one, every line, as well as the length and breadth of the enlarged map, will be double, or treble, or quadruple, &c. those of the given one, for it must be easy to conceive that those maps are like: but the area, if the scale be double, will be four times; if treble, nine times; if quadruple, sixteen times that of the given figure; that is, it will contain four, nine, or sixteen times as many square inches as the given one (for it has been shewn that like polygons are in a duplicate proportion with the homologous sides). Yet these figures being cast up by their respective scales will produce the same content.

Thus much is sufficient for enlarging maps, and from hence, diminishing of them will be obvious; for one fourth, one third, or half the distances from the several stations to the centre, will mark out points, which if joined, will compose a map similar to the given one, whose scale will be four times, three times, or twice as small as the given one.

Thus, if we would reduce a map from 40 to 80, from 20 to 40, from 10 to 20 perches to an inch, &c. half the distance of the stations from the centre will give the points requisite for drawing the

map; if we would reduce from 40 to 120, from 20 to 60, from 10 to 30 perches to an inch, &c. one third of the distances to the centre, will give the points for the map; and if we would reduce from 40 to 160, from 20 to 80, from 10 to 40 perches to an inch, &c. one fourth of the distances to the centre, will give the points for the map.

By the methods here laid down I have reduced a map from a scale of 40 to one of 20 perches to an inch, which contained upwards of 1200 acres, and consisted of 1224 separate divisions, without the least confusion from the lines; for none can arise if the methods here laid down be strictly observed.

I have also from the same methods reduced a large book of maps, each of which was an entire skin of parchment, and the whole contained upwards of 46000 acres, to a pocket volume; and afterwards connected all these maps into one map, which was contained in one skin of parchment: therefore upon the whole I do recommend these methods for reducing maps to be much more accurate than any of the methods commonly used, such as squaring of paper, using a parallelogram, proportionable compasses, or any other method I ever met with, though the figures to be reduced were ever so numerous, irregular, or complicated,

To unite esparate maps of lands which join each other, into one map of any assigned size.

If there be several large maps contained in a book, each of which suppose to take up a skin

of parchment, or a sheet of the largest paper; which maps of lands join each other; and it be required to reduce them to so small a scale, that all of them when joined together may be contained in one skin, half a skin, or any assigned sized piece of parchment, or paper.

Having pricked off and copied the several maps on any kind of paper, unite them by cutting with scissors along the edge of one boundary which is adjoining the other, but not cutting by the edge of both, and throw aside the parts cut off; then lay these together on a large table, or on the floor, and where the boundaries agree, they will fit in with each other as indentures do; and after this manner they are easily connected: measure then the length and breadth of the entire connected maps, and the length and breadth of the parchment or paper you are confined to; if the former be three, four, or five times greater (that is, longer and broader) than the latter, reduce each copied map severally to a scale that is three, or four, or five times less, as before; and the same parts of the boundaries you cut by in the large maps, by the same you must, also cut in small ones, and unite the small as the large ones were united; cementing them together with white wafer: thus will your map be reduced to the assigned size, which copy over fair, on the parchment, or paper you were confined to.

But it is not always that a person is confined to a given area of parchment, or paper; in such cases, if there are many large maps to be united into one, reduce each of them severally to a scale of 160 perches to an inch, and unite those by the contiguity or boundaries, as before: or if you have a few, it will be sufficient to reduce them to a scale of 120, &c. But having the maps given, and the scale by which they are laid down, your reason will be sufficient to direct you to know what scale they should be reduced to.

Directions concerning surveys in general.

If you have a large quantity of ground to survey, which consists of many fields or holdings, and that it be required to map and give the respective contents of the same, it is best to make a survey of the whole first, and to be satisfied that it is truly taken, as well as to find its content; and as you go round the land, to make a note on the side of your field-book at every station where the boundary of any particular field or holding intersects or meets the surround; then proceed from any one of those stations, and in your field-book say, "proceed from such a station," and when you have gone round that field or division, insert the station you close at, and so through the whole: a little practice can only render this sufficiently familiar, and the method of protraction must be evident from the field-notes. whole is protracted, and you are satisfied of the closes of the particular divisions, cast up each severally, and if the sum of their contents be equal to the content of the whole first found, you may safely conclude that all is right.

The protraction being thus finished and cast up, transfer it on clean paper, vellum, or parchment, as before; be careful to draw your lines with a fine pen, write on it the names of the circumjacent lands, and set No. 1, 2, 3, 4, &c. in every parti-

cular field or division; let every tenant's particular holding be distinguished by a different coloured paint being run finely along the boundaries; let all the roads, rivulets, rivers, bridges, bogs, ponds. houses, castles, churches, beacons (or whatever else may be remarkable on the ground) be distinguished on the map. Write the title of the map in a neat compartment either drawn, or done from a good copper-plate graving, with the gentleman's arms. Prick off one of your parallels with the map, and on it make a mariner's compass, and draw a flower-de-luce to the north, and this will represent the magnetical north; after which set off the variation, which express in figures, and through the centre of the compass. let a true meridian line be drawn of about 3 inches long, by which write True Meridian. Let a scale be drawn, or it is sufficient to express the number of perches to an inch, the map was laid down by. Draw a reference table of three, or, if occasion be, of four or more columns; in the first insert the number of the field or holding: in the next its name, and by whom occupied: in the third the quantity of acres, roods, and perches it contains: if you have unprofitable land, as bog or mountain. let the quantity be inserted in the fourth column; and, if it be required, you may make another column for statute measure, and then the map is completed.

SECTION VIL

THE METHOD OF DIVIDING LAND, OR OF TAKING OFF OR INCLOSING ANY GIVEN QUANTITY.

EXAMPLE 1.

PL. 12. fig. 1.

Let ABCD, &c. be a map of ground, containing 11 acres, it is required to cut off a piece as

DEFGID, that shall contain 5 acres.

Join any two opposite stations as D and G, with the line DG, (which you may nearly judge to be the partition line) and find the area of the part DEFG, which suppose may want 3R. 20P. of the quantity you would cut off: measure the line DG, which suppose to be 70 perches. Divide 3R. 20P. or 140P. by 25, the $\frac{1}{2}$ of DG, and the quotient 4 will be a perpendicular for a triangle whose base is 70, and the area 140P. Let HI be drawn parallel to DG, at the distance of the perpendicular 4, and from I, where it cuts the boundary, draw a line to D, and that line DI, will be the division line; or a line from G to H will have the same effect; all which must be evident from what has been already said.

But if hills, trees &c. obstruct the view of the points D and I from each other, it will be necessary in order to run a partition line, to know its bearing; and it may be proper on some occasions, to have its length; both these may be easily calculated from the common field-notes only, as in the following example, without the trouble of any other measurement on the ground, or any dependent.

dance on the map and scale.

Example 11.

P.L. 12. fig. 3.

Let ABCDEFGHIA be a tract of land, to be divided into two equal parts, by a right line from the corner I to the opposite boundary CD; required the bearing and length of the partition line IN, by calculation, from the following field-notes, viz.

Fi	Field-Notes and Area.									
Boun.		Beari	Perch.							
AB	N.	190.	o' E	. 108.						
BC	S.	77.	o E	91.						
CD	s.	27.	0 E	. 115.						
DE	S.	52.	oW	. 58.						
EF	S.	15.	30E	76.						
FG	İ	Wes	st.	70.9						
GH	N.	36.	o W	47.						
HI		Nor	64.3							
IA	N.	62.	15 W	. 59.						
	152	۹.	ıR.	25.9P.						

Operation.

1	IABCI		Per.	N.	S.	E.	W.	IZ
IA A B	N. 62° <u>‡</u> N. 19	w.	59	27.5			52.2	Ę.
BC	S. 77	Ē.	91	102.1	20.5	88.7		dist.
	a,8722.3	per	ches	129.6	109.1	123.9	123.9	ς.

152A. 1R. 25.9P.=24385.9 perch. half, to be divided off,=12192.9 the part IABCI = 8722.3 subt.

Triangle ICNI = 3470.6 perches.

ICDI.	Per.	N.	, s.	E.	w.	I
IC N.—E CDS. 27. E DI	115	1.001	102.5	71.7 52.2	123.9	erid. dist.
Arca, 6522.1	per.	109.1	109.1	122.9	123.9	8

Then, { .ICDI: CD: .ICNI: CN } Th. 18 as { 6522.1: 115::3470.6: 61.19 } Sec. 1 which determines the point N in CD.

ICNI.	Per.	N.	S.	E.	W.
IC as before CN S. 27 E.	61.2	109.1	54.6	17.7 27.8	
]***	 	-	54.6		99.5

As dif. lat. 54.6 | As S. Bear 61°15' : Radius S. 90 deg. : Depart. 99.5 : Radius S. 90 deg. : Distance 113.49

Answer, { IN runs N. 61 • 15' E. } 113.5 per.

In the part IABCI, the difference between the northings and the southings of the three lines, IA, AB and BC (109.1) is the difference of latitude, and that of their eastings and westings (71.7) the departure of the line CI, which is placed thereto, so as to balance the columns; see theo. 1. sect. 5. hence the content is obtained, as already taught, without the bearing or length of the line CI.

For the triangle ICDI, the diff. lat. and dep. of IC are taken from the preceding table, which in going from I to C will be northing and easting: those of CD are found by the bearing and distance, and of DI by balancing the columns, as before for CI.

The difference of latitude (54.6) and departure (99.5) of the line NI, in the third table, are found by balancing those of IC and CN; and as they are the base and perpendicular of a right angled triangle, of which the line NI is the hypothenuse, and the angle opposite to the departure, the bearing, we have the answer by two trigonometrical statings, as above; and thus may any tract be accurately divided, or any proposed quantity readily cut off or inclosed.

Now the student or practitioner may calculate the content of the part ABCNIA (the bearing and distance, or the diff. lat. and dep. of CN and of NI being known) and if it be found equal to the intended quantity, it proves the truth of the operation.

Example iil

Ps. 12. fig. 3.

It is proposed to cut off 38A. 16P₁, to the south end of this tract, by a line running from E due West 40 perches to a well at O, and from thence a right line to a point M in the boundary HI; the place of M, and the bearing and length of the line OM are required; the field-notes being as in example 2d.

Answer, { M from H, north, 43.23 } perchest OM, N. 78°7 W. 39.03 } perchest

In this example we find,

The area of	OEFGHO =	Perches. 5270 5
Consequently of	HOMH =	
Dif. lat. of the line	HO=HV=	35.2
Departure of ditto	=QV=	38.2

As HI happens to be a meridian, the area of HOMH divided by half OV(19.1) quotes HM(43.23) without finding the area of HOIH, as we did of ICDI in example 2d. and HM-HV=VM=8.03= dif. lat. of OM, which with its dep. VO=38.2. gives the bearing and distance as before.

EXAMPLE IV.

PL. 12. fig. 4.

A trapezoidal field ABCD, bounded as under specified, is to be divided into two equal parts by a right line EF parallel to AB or CD; required AF or BF?

Bou.	Bearing.	Per.		
AB BC CD DA		30. 60. 45.5 89.4		
13A. 3R. 7P.				

In the triangle CBG are given BC and all the angles (known by the bearings) to find BG, and thence the area by prob. 9. sect. 4. which that the area of ABCD = area of EFG; then as the area of CBG to that of EFG, so is the square of BG to the square of FG, and FG—BG=BF.

Operation at large.

Angle G 39° 30′, log. S. Co. Ar. Side BC 60 per. log. Angle C 40° 30′, sine	0.19649 1.77815 9.81254
Side <i>BG</i> 61'. 26 per. Side <i>BC</i> 60 per. Angle <i>B</i> 100° 0', sine	1.78718 1.77815 9.99335
2)3619.8, log.	3.55868
$As \ CBG = 1809.9 \text{ Co. Ar.}$ $1103.5 = BCEF$	6.74235
To $EFG = 2913.4$, log.	3.46440 >add
So sqr. BG 61. 26, log.	1.78718 1.78718
To sqr. FG 77.72 (2	2)3.78111
Ans. $BF = 16.46$ per.	1.89055

By the application of this method a tract of land may be divided accurately, in any proportion, by a line running in any assigned direction.

Note. When the practitioner would wish to be very accurate, it will be much better to work by four-pole chains and links than by perches and tenths; one tenth of a perch square being equal to 61 square links.

EXAMPLE V.

The following Field-Notes (from A. Burns) are of a piece of land, which is proposed, as an example, to be divided into three equal parts by two right-lines running from the sixth and seventh stations; and proved, by calculating the content of the middle part.

St.	Beari	ng.	P.C.
1,	N.E.	56°‡	21.60
2	N.E.	261	13.44
3	S.E.	714	18.96
4	S.E.	261	13.44
5	s.w.	711	18.96
6	S.E.	45	8.47
7	S.E.	63 }	13.44
8	N.E.	45	8.47
9	S.E.	26	13.44
-10	s.w.	45	8.47
11	s.w.	63	13.44
12	N.W.	76	24.73
1:	N.W.	364	30.00
A	A. rea 167	R. 1.	P. 24.

EXAMPLE VI.

PL. 8. fig. 5.

The plot ABCDEFGHA is proposed to be divided, geometrically, in the proportion of 2 to 3, by a right line from a given point in any boundary or angle thereof, suppose the point D.

Reduce the plot to the triangle cDe, as already taught; divide the base ce in the point N, so that eN be to Ne in the ratio of two or three, by prob. 14. page 53; draw DN, and it is done.

EXAMPLE VIL

PL. 12. fig. 3.

Example 2d may likewise be performed geometrically.

Produce CD both ways for a base, and reduce the whole to a triangle, making I the vertical point; then bisect the base in N, and draw IN. But.

Notwithstanding this geometrical method is demonstrably true in theory, it is not as safe, on practical occasions requiring accuracy, as the calculation, even when performed with the greatest care; for which reason we will not enlarge on it here.

Example viii.

Suppose 864 acres to be laid out in form of a right-angled parallelogram, of which the sides shall be in proportion as 5 to 3; required their dimensions?

For the greater side, multiply the area by the greater number of the given proportion, and divide

by the less, or, for the less side, multiply by the less number, and divide by the greater; the square root of the quotient will be the side required: thus,

864 A. = 138240P	1.38240		
· 5	3		
3)691200	5)414720		
Ånsw. ≠ 230400=480.	√ 82944=288.		

EXAMPLE IX.

If it be required to lay out any quantity of ground, suppose 47A. 2R. 16P. inform of a parallelogram, of which the length is to exceed the breadth by a given difference, for instance 80 perches, then add the square of half this difference to the area; and take the square-root of the sum; to which add half the difference for the greater side, and subtract it therefrom for the less; thus,

Any proposed quantity of ground may be laid out or included in the form

of a Square - - by prob. 2d. Parallelogram, I side giv. by pro. 4th. Triangle of a given base, by pro. 7th. Circle - by prob. 13th.

It is sometimes most convenient, when land is to be laid out adjacent to a creek, river, or other crooked boundary, to measure off-sets to the angles or bending thereof, from a right line or lines taken near such boundary, and to deduct the area of these off-sets from the given quantity, and then to lay off the remainder from the right-line or lines, in the desired form.

In laying out new lands, attention must be paid to the allowance for roads, as exemplified in prob. 14th.

EXAMPLE X.

It is required to divide off 30 acres, to the south east end of the tract, of which the field-notes are given in example 4th, by a right-line to run N. 20° E. See example 4th.

SECTION VIII.

of surveying harbours, shoals, sands, &c.

PL, 13. fig. 1.

HERE are three methods whereby this may be performed; for the observations may be made either on the water or on the land. Those made on the water are of two kinds, one by the log-line and compass (as in plane sailing measuring) the course and distance round the sand; and then to be plotted as a large wood, or any inclosure taken by the circumferentor.

This method I omit for two reasons; first, because it is to be deduced from the writers of navigation: and, secondly, because the distances thus measured are liable to the errors of currents, which generally attend shoals or sands near the shore.

The second method, where there are no distances to be measured on the water, though still there is one inconvenience, common also to the former, because the bearings or observations are to be taken on that unstable element (an error scarce mentioned by practical artists) I shall briefly hint at; and so rather choose a third, which is liable to neither of these imperfections.

 $0 \circ$

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Let a boat be manned out with a signal flag, a log and line, lead and line, and to observe the bearings of any land mark, a compass with sights.

Take two or more objects or places, as A, B, C, on the shore, from whence the boat may be seen on the several parts of this shoal, and determine their relative position by bearing and distances either before or after the other necessary observations are made.

One of the boat's crew is to sound till he finds himself on the edge of the sand, by the depth of water, and then to come to an anchor; which he is to signify to two persons on the shore, at B and C, by his signal. And then from those known land-marks, B and C, the observers are to take the bearings of the boat, and to register their observations; which, when done, they are to signify to the crew by waving a flag, or by some other signal.

And in the mean time, to prevent mistakes, let the crew take the bearings of each of these landmarks: then weigh anchor, which suppose at D.

Then by sounding, proceed to E, and make like observations. And so at E, F, G, &c. till you have surrounded your sand.

And if in this process, you are about to lose the sight of one of your land-marks, suppose C, let your assistant at C, or B, who at that time will also be about to lose the sight of the boat, by signals (before agreed on) remove to some other object before-hand agreed on, suppose to H, or K; and then to proceed as before.

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Lastly, if the sand runs so far out at sea, that the object cannot be seen by the boat, nor the boat by the observer on shore; there may be rockets fired by the boat's crew, and also by the observers on the shore in the night, whereby those bearings may be taken almost at as great a distance as the light can be seen. For supposing they rise but a quarter of a mile above the apparent horizon, its stay will be about 9 seconds, and its distance for this quarter of a mile will be visible about 44 miles.

But rockets rise much higher, and then the distances are much greater, whereby they are visible.

Or two boats may lay at anchor instead of the land marks, and then you may work as before.

Now, since the land-marks B and C are fixed, their position may be laid down in the draught, as in common surveying, by plotting the distance between B and C. And then by plotting the line BD, and the line DC, according to their position, their common intersection will give the point D. And in like manner E, F, G, &c. may be plotted; and so the shoals completed. And this from the bearings taken at B and C.

If this be a standing lake, environed by bogs, or other impediments, the observations at D, E, F, &c. by taking their opposites, may suffice to plot the same from the land-mark, A, B, C, &c. as well as those taken on the land: or, indeed, by the course and distance, as in navigation, if the water be smooth and without a current.

In sea shoals, it is convenient to note at each obmervation the depth of the water found by the lead, and the drift and setting of the current by the logand compass, while the heat is at anchor, which may be done with ease and expedition enough. For while the boat rides at an anchor, her stern points out the setting of the current, and the logand glass will measure its drift.

And these ought to be noted on the draught, which may be thus:

The currents may be shewn, by drawing a dart pointing out its setting, and its drift by the Roman capital letters, the depth of the water by the small figures, and rocks by little crosses, &c.

SECTION IX.

LEVELLING.

PL. 13. fg. 2.

LEVELLING is the art of ascertaining the perpendicular ascent or descent of one place (or more) above or below the horizontal level of another, for various intentions; and of marking out courses for conveyance of water, &c.

The true level is a curve conforming to the surface of the earth; as ABG.

The apparent level is a tangent to that curve; as ADE.

The correction, or allowance for the earth's curvature, is the difference between the apparent level and the true, as BD. The quantity of this correction may be known by having, in the right-angled triangle CAB, the two legs, AC=the semidiameter of the earth (=1267500 perches) and AD=the distance of the object, to find the hypothenuse CD, from which taking CB: (=CA) the remainder will be the correction BD; but it may be obtained more practically thus;

Square the distance in

(four-pole chains, and divide by \$00,)

or in perches, and divide by 12800, or in miles, and multiply by 8,)

for the correction in inches.

Example.

Required the correction for 20 four-pole chains =80 perches=1 mile.

800)20 × 20 = 400(.5 12800)80 × 80 = 6400(.5 1=.25, and .25 × 25 × 8=.5

that is, .5, or 1 inch, the correction required.

But, to save the trouble of calculation, we insert the following table of corrections.

A Table of Corrections:

The distances in four-pole chains.

1	Distar.	Correc.	Distar.	Corre	
1	Chains	inches	Chains.	nches	
F	l	,0012	27	U,9 1	
1	2	J,Q05	28	0,98	
1	3	0,01125	29	1,05	1
1		ს, 02	30	1,12	
L	5	0,03	31	,19	1
Γ	6	0,04	32	1,27	
1	7	J , 06	33	1,35	
1	8	,08	34	1,44	5
ł	9).10	35	1,53	.
L	10	J'13	36	1,62	
Г	11	J ₁ 15	37	:.71	
ı	12	U,18	-38	1,80	
I	13	0,21	39	1,91	
ł	14	0.24	40	2,00	
L	15	∂.28	45 -	2.28	
	16	J,32	50	3,12	2500 000
ı	17	0,36	55	8,78	
I	18	J ,4 0	60	4,50	
	19	0,45	65	5,31	
	20	∴.50	70	6,12	P № # # 19.
Γ	21	ı) .\$ 5	75	7,03	
1	22	0,60	80	8,00	
1	23	1.67	85	9,03	,
1	24	0.72	90	10,12	
ł	25	J,78	95	11,28	
•	26),84	100	12,50	•

The first thing necessary in levelling, is the adjusting of the level, which may be performed several ways; The following is very easy and practical.

Choose some ground which is not above 4 or 5 feet out of the level, for the distance of 8 or 10 chains length, and suppose it be AB (fig. 3.) and find the middle between A and B, which suppose to be C; plant the instrument at C: direct the tube to a station-staff, held up at A, and elevate or

depress the tube, till the bubble is exactly in the middle of the divisions; then by signals direct your assistant at A, to rise or depress the vane, which glass cuts the middle of that vane: then see how many feet, inches, and parts, are cut by the upper part of the vane, which suppose to be 3 feet 4 inches and 6 tenths.

In like manner direct to the other staff at B, and suppose the upper edge of that vane to cut at the height of 6 feet, 5 inches and two tenths, then will these two vanes be on a level.

From 6 feet 5.2 inches subtract 3 feet 4.6 inches, and reserve the remainder 3 feet 0.6 inches.

Now, remove the instrument as close to the higher station-staff as you can; so that the middle of the telescope may almost touch it. Then bring the telescope as near to a level as the judgment of the eye will direct.

Measure from the ground, the height of the top of the telescope; and also of the bottom, in feet, inches, and parts; suppose them to be 4 feet, 10.5 inches, and 5 feet 0.3 inches; then half the sum of the heights 4 feet 11.4 inches is the height of the centre of the glass; and to this add half the breadth of the vane, which suppose to be 1 inch and 5 tenths, and to the sum 5 feet 0.9 inches, add the preceding remainder 3 feet 0.6 inches; then let the person at B move his vane, till the upper edge cut 8 feet 1.5 inches, the sum of the preceding numbers.

Now, so elevate or depress the tair or the buleble, till the bair cut the middle of the vane at life, and at the same time the bubble stands at the middle of the divisions; and then will the instrument be duly adjusted.

If you have a mind to be more accurate, repeat the operation; but when you place the instrument at C, turn the tube at right angles to the line AB, and there set it level; then proceed with a repetition of the work. Only observe to cross-level it in this adjustment, and in all future uses whatsoever.

Or the level may be adjusted thus: As before, first plant the instrument in the middle between A and B (fig. 4.) and observe the heights on the station-staves, which suppose to be as above; and consequently their difference, as before, is 3 feet 0.6 inches. New measure from C towards the highest ground A. some distance that comes almost to A; suppose 4 chains to D; and DB will be & chains, and DA one chain: Then plant the instrument at D, direct the telescope to A, and setting the bubble to the middle of the division. direct your assistant to move the wane, till the hair cuts the middle of it; and note down the feet, inches, and parts cut by the upper edge of the vane; which suppose to be 3 feet 8.4 inches: To this add the difference 3 feet 0.6 inches, and the sum 6 feet 9 inches reserve.

Now direct the telescope to the staff at B, level it, and direct your assistant to move the vane, till the hair cuts the middle thereof; and then, if the upper edge of the vane cuts the foregoing sum 6 feet 9 inches, the hair and bubble are truly adjust-

cd. But if not, say, As BD less AD, is to the difference between the numbers cut by the upperctigs of the vane, and the number 6 feet 9 inches; so is the distance AD to a number, which added to that cut by the vane, when less than 6 feet 9, and subtracted from the number cut by the vane, when it is greater than 6 feet 9, will give a number to which let the assistant fix the vane; then so elevate or depress the hair or the bubble, till the hair cuts the middle of the vane at B, and the bubble stands in the middle of the divisions; for then the level will be adjusted. The operation may be again repeated, and at every station cross levelled, which will confirm the former adjustment.

Or it will be still better to set the station staves equally distant from the instrument (suppose about 16 or 20 perches each) at an angle of about 60°, or so as to form nearly an equilateral triangle therewith, and level the 2 vanes (A and B fig. 5.) as before, which will be then both in the same horizontal level, whether the instrument be right adjusted or not, because one will be as much above or below the true level of the instrument, as the other, being in the same distance from it; then remove the instrument as near as may be to one of them. suppose A, and raise or lower the vane A to the exact level of the visual ray in the instrument, noting precisely how much it is moved, and have the other vane B move just as much, in order to bring them again to a level, allowing for the correction of the apparent level if it be a sensible quantity; then adjust the instrument to the level of the vane at B. .

To adjust the rafter level (plate 13. fig. 6.) which may be 10, 12, or 14 feet in the span AB; set it on a plank or hard ground nearly level, and mark

where the plumb line cuts the beam mn, suppose at c, then invert the position by setting the foot A, in the place of B, and B in that of A, marking where the line now cuts, as at c; the middle point between c and c will be the true levelling mark.

To continue a level course with this instrument, set the foot A to the starting place, and move B upward or downward toward D or E, tilk the point B be determined and marked for a level, with A, then carry the instrument forward in the direction of C till the foot A rests at B, whence the point C is levelled as before, &c. Sights may be placed at r and s, and the instrument adjusted to them, as before, by reversing them in the direction of some distant object.

After the instrument is duly adjusted, you may proceed to use it. Let the example be this annexed (fig. 7.) where A every where represents the level, and B the station staves; and suppose the route be made from a to e; first plant the instrument between the staves a and b: at A direct the level to aB, bring the bubble to the middle of the divisions, and instruct your assistant so to place the vane, that the hair in the telescope cuts the middle of the vane, then in a book divide into two columns, the one entitled Back sights, the other Fore sights, enter the feet, inches, and parts cut by the upper edge of the vane at aB, in the column entitled Back sights.

Then look toward the other staff b B, bring the bubble to the middle of the divisions, and direct your assistant to place the vane so, that the hair cuts the middle of the vane; then enter the feet, inches, and parts cut by the upper edge of the vane, in the column of Fore sights.

Now, plant the instrument at A^s , still keeping the staff Bb exactly in the same place, and carry the staff aB forwards to the place cB; now look back to the staff bB, and enter the numbers cut by the vane there under the title Back sights; then look forwards to cB, and enter the observation under the title Fbre sights. Do the like when the instrument is planted at A^s , A^s , &c. always taking care to keep the staff in the same place when you looked at it for a Fore sight, till you have also taken with it a Back sight,

Having finished your level, add up the column of Back sights into one sum, and the column of Fore sights also into one sum; and the difference between these sums is the ascent or descent required. And if the sum of the Fore sights be greater than the sum of the Back sights, then e is lower than a; but if the sum of the Fore sights be less than the sum of the Back sights, e is higher than a. For example, let the numbers be as in the following table.

•	Back sights.					Fore sights.				
-	Feet.	~	nch.	-	Tenths.	Feet.	-	Inch.	Tenths.	
	3 '		· 7	٠,	5	. 6	•	4,	. 5	
١	4		6	٠	. 8	. 8	•	3,	, 3 1	
	. 6		. 0	,	2	5		4,	. 7.	
	9		- 5	٠.	0	8		7 ,	8	
	1	•	o	,	7	9		4,	. 8	
	24		8	,	2	38	•	1 .,	0	
						24		8,	2	
٠		•			:	13	•	4 .	8	
	Henc	e th	e de	306	nt is	15	٠.	4 ,	8	

Observations.

- 1. And if the distances thus taken are short, the curvature of the earth may be rejected. For, if the distance from the instrument be every where about 100 yards, all the curvatures in a mile's work will be less than half an inch.
- 2. If the distance from the instrument to the hindermost staff, be every where equal to the distance from the instrument to the corresponding staff; the curvature of the earth, and the minute errors of the instrument, will both be destroyed. Hence it will be much best to set the instrument as equally distant from both staves as may be.
- 3. If the distances of the instrument from the staves, be very unequal and very long, the curvatures must be accounted for, and the distances in order thereto, must be measured.
 - 4. Therefore it appears, that the best method to take a level is to measure the several distances from the instrument to the back and forward station staves; and enter them in the field-book, according to the titles of their several columns, as in the following example; and correct the heights from the table of allowances, which may be done at home when you are about to sum up the heights.

-	370 3,25 3.24 418 4,86 430 6,10 6,08 328 7,18 760 5,38 5,31 289 6,75 584 7,25 7,21 530 9,53 326 8,15 8,14 485 11,25 658 10,25 10,20 376 8,65		ds.		
Distan.	Height	Corrected.	Distan.	Height	Corrected.
Links.	Inches.	Inches.	Links.	Inches.	Inches.
370	3,25	3,24	418	4,86	4,34
480	6,10	6,08	328	7,18	7,17
	5,38	5,31	289	6,75	6.67
584	7,25	7,21	530	9,53	9,50
326	8,15	8,14	485	11,25	11,22
* · 658 ·	10,25	10,20	376	8,65	8,63 .
. 580	6,32	6,29	720		10,28
3658		46,47	31,46		57,81
3146	1				46,47
48,04	[]		1		11,34

So that the fall in 68 chains is about 11 inchestand it of an inch.

Lastly, Though hitherto we have considered the level with one telescope only, the same observations may be applied to a level with a double telescope; and I would advise those who use the double telescope, at every station to turn that end of the telescope forward, which before was the contrary way.

A nore general method of levelling, adupted to the surveying of roads and hilly ground, is exhibited in the following example, in which the measures are given in links.

Examples.

PL. 13. fig. 8.

Required the bearing and distance of the place B from A, and its perpendicular ascent or descent, above or below the horizontal level of A.

Stat.	Course or Bearing	Elev. or Depres.	Obl. Dist.	Hor. Dist.	Perpen. Ascent or desc.	Dil. Lat.	De- part.
2 3 4	NE79°15 NE75 Oc NE50 30 S E85 15 S E76 Oc	D 21 45 E 14 00 D 11 30	738 684 976 930 620	635 947 911	253.4 236.1 185.4	602 .75	613
		. 1	3948	3783	217.6 Desc.	622 N.	349 2 E.

As Dif. Lat. 622
Is to radius S. 20°,
So is Dep. 3492
To T. Bear. 79°54′.

As S. Bear. 79° 45′ Is to Dep. 3492, So is radius S. 90° To Dist. 3547.

As 100 links: 66 feet: 217.6 links: 143.6 feet, the descent B below the level of A.

Hence, B bears N. 79° 54' E. from A Nearest horiz. dist. 3547 links. Sum of obl. dist. 3948 links. Sum of horiz. dist. 3783 links. Perp. desc. 217.6L. = 143.6.F.

answer.

With the angular elevation or depression in the third column, and the oblique distance in the fourth (as course and distance) are found the horizontal distance in the fifth, and the perpendicular ascent or descent on the sixth, for each station (as difference of latitude and departure:) then, with the bearing and horizontal distance we get the difference of latitude and departure in the two last columns.

The ascents and descents in the sixth column are distinguished by the letters E and D in the third, signifying elevation or depression; and being added separately, the difference of their sums

is set at the bottom of the column with the name of the greater, and shews the perpendicular descent of B below the horizontal level of A.

In like manner the northings and southings in the seventh column are distinguished by the letters N and S in the second, &c.

PROMISCUOUS QUESTIONS.

The perambulator, or surveying wheel, is so contrived as to turn just twice in the length of a pole or 162 feet; what then is the diameter?

Answ. 2.626 feet.

2. Two sides of a triangle are respectively 20 and 40 perches; required the third, so that the content may be just an acre?

Answ. either 23.099 or 58.876 perches

3. I want the length of a line by which my gardener may strike out a round orangery that shall contain just half an acre of ground.

Answ. 27f yards:

4. What proportion does the arpent of France, which contains 100 square poles of 18 feet each, bear to the American acre, containing 160 square poles of 16.5 feet each, considering that the length of the French foot is to the American as 16 to 15?

Answ. as 512 to 605.

5. The ellipse in Grosvener square measures 840 links the longest way, and 612 the shortest, within the rails: now the wall being 14 inches thick, it is required to find what quantity of ground it incloses, and how much it stands upon.

Answ. it incloses 4A. 6P. and stands on 1760#

square feet.

6. Required the dimensions of an elliptical acre with the greatest and least diameters in the proportion of 3 to 2?

Answ. 17.479 by 11.653 perches..

7. The paving of a triangular court at 18d. per foot, came to 100l. The longest of the three sides was 88 feet: what then was the sum of the other two equal sides?

Answ. 106.85 feet.

8. In 110 acres of statute measure, in which the pole is 161 feet, how many Cheshire acres, where the customary pole is 6 yards, and how many of Ireland, where the pole in use is 7 yards?

Answ. 92A. 1R. 28P. Cheshire; 67P. 3R. 25P.

Irish.

- 9. The three sides of a triangle containing 6A. 1R. 12P. are in the ratio of the three numbers, 9, 3, 6, respectively; required the sides?

 Answ. 59.029, 52.47, and 39.353.
- 10. In a pentangular field, beginning with the south side, and measuring round towards the east, the first or south side is 2735 links, the second 3115, the third 2370, the fourth 2925, and the fifth 2220; also the diagonal from the first angle to the third is 3800 links, and that from the third to the fifth 4010; required the area of the field?

Answ. 117A. 2R. 28 P.

• 11. Required the dimensions of an oblong garden containing three acres, and bounded by 104 perches of pale fence?

Answ. 40 perches by 12.

12. How many acres are contained in a square meadow, the diagonal of which is 20 perches more than either of its sides?

Answ. 4A. 2R. 11P.

- 13. If a man six feet high travel round the earth, much greater will be the circumference described by the top of his head than by his feet?
- Answ. 37.69 feet. N. B. The required difference is equal to the circumference of a circle 6 feet radius, let the magnitude of the earth be what it may.
- 14. Required the dimensions of a parallelogram containing 200 acres, which is 40 perches longer than wide?

Answ. 200 perches by 160.

15. What difference is there between a lot 28 perches long by 20 broad, and two others, each of half the dimensions?

Ausw. 1A. 3R.

PART III.

containing the Astronomical methods of finding the Latitude, Vanation of the compass, &c. with a description of the instruments used in these operations.

SECTION I.

INTRODUCTORY PRINCIPLES.

AY and night arise from the circumsotation of the Earth. That imaginary line about which the rotation is performed, is called the Axis, and its extremeties are called Poles. That towards the most remote parts of Europe is called the North Pole, and its opposite the South Pole. The Earth's Axis being produced will point out the Celestial Poles.

The Equator is a great circle on the Earth, every point of which is equally distant from the Poles; it divides the Earth into two equal parts, called Hemispheres: that having the North Pole in its centre is called the Northern Hemisphere—and the other, the Southern Hemisphere. The plane of this circle being produced to the fixed stars, will point out the celestial Equator or Equinoctial. The Equator, as well as all other great circles of the sphere, is divided into 360 equal parts, called degrees; each degree is divided into 60 equal parts, called minutes; and the sexagesimal division is continued.

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Note. The ancients having no instruments by which they could make observations with any tolerable degree of accuracy, supposed the length of the year, or annual motion of the earth, to be completed in 360 days: and hence arose the division of the circumference of a circle into the same number of equal parts, which they called degrees.

The Meridian of any place, is a semi-circle passing through that place, and terminating at the Poles of the Equator. The other half of this circle is called the *opposite Meridian*.

The Latitude of any place, is that portion of the Meridian of that place, which is contained between the Equator and the given place; and is either North or South, according as the given place is in Northern or Southern Hemisphere, and therefore cannot exceed 90°.

The Parallel of Latitude of any place, is a circle passing through that place, parallel to the Equator.

The Difference of Latitude between any two places, is an arch of a meridian intercepted between the corresponding parallels of latitude of those places. Hence, if the places lie between the Equator and the same Pole, their difference of latitude is found by subtracting the less latitude from the greater: but if they are on opposite sides of the Equator, the difference of latitude is equal to the sum of the latitudes of both places.

The First Meridian is an imaginary semicircle, passing through any remarkable place, and is therefore arbitrary. Thus, the British esteem that

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to be the First Meridian which passes through the Royal Observatory at Greenwich; and the French reckon for their First Meridian, that which passes through the Royal Observatory at Paris.—Formerly many French geographers reckoned the meridian of the island of Ferro to be their First Meridian; and others, that which was exactly 20 degrees to the west of the Paris Observatory. The Germans, again, considered the meridian of the Peak of Teneriffe to be the First Meridian. this mode of reckoning, Europe, Asia, and Africa, are in east longitude; and North and South America, in west longitude. At present, the first meridian of any country is generally esteemed to be that which passes through the principal Observatory, or chief city of that country.

The Longitude of any place is that portion of the Equator which is contained between the first meridian, and the meridian of that place: and is usually reckoned either east or west, according as the given place is on the east or west side of the first meridian; and, therefore, cannot exceed 180°.

The Difference of Longitude between any two places is the intercepted arch of the Equator between the meridians of those places, and cannot exceed 180°.

There are three different Horizons, the apparent, the sensible, and the true. The apparent or visible Horizon is the utmost apparent view of the sea or land. The sensible is a plane passing through the eye of an observer, perpendicular to a plumbline harging freely; And the true or rational Horizon is a plane passing through the centre of the Earth, parallel to the sensible Horizon.

Altitudes observed at sea, are measured from the visible Horizon. At land, when an astronomical quadrant is used, or when observations are taken with a Hadley's quadrant by the method of reflection, the altitude is measured from the sensible Horizon; and in either case, the altitude must be reduced to the true Horizon.

The Zenith of any given place is the point inamediately above that place, and is, therefore, the elevated pole of the Horizon: The Nadir is the other pole, or point diametrically opposite.

A Vertical is a great circle passing through the Zenith and Nadir; and, therefore, intersecting the Horizon at right angles.

The Altitude of any celestial body in that portion of a Vertical, which is contained between its centre and the true Horizon. The Meridian Altitude is the distance of the object from the true Horizon, when on the Meridian of the place of observation. When the observed Altitude is corrected for the depression of the Horizon, and the errors arising from the instrument, it is called the apparent Altitude; and when reduced to the true, Horizon, by applying the parallax in Altitude, it is called the true Altitude. Altitudes are expressed in degrees, and parts of a degree.

The Zenith Distance of any object is its distance from the Zenith, or the complement of its Altitude.

The Declination of any object is that portion of its meridian which is contained between the equinoctial and the centre of the object; and is either north or south, according as the star is between the equinoctial and the north or south pole.

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The Ecliptic is that great circle, in which the annual revolution of the Earth round the Sun is performed. It is so named, because Eclipses cannot happen but when the moon is in or near that circle. The inclination of the Ecliptic and Equinoctial is at present about 23° 28°; and by comparing ancient with modern observations, the obliquity of the Ecliptic is found to be diminishing—which diminution, in the present century, is about half a second yearly.

The Ecliptic, like all other great circles of the sphere, is divided into 360°; and is further divided into twelve equal parts, called Signs: each Sign, therefore, contains 30°. The names and characters of these Signs are as follows:

Aries, & Cancer, & Libra, & Capricornus, & Taurus, & Leo, & Scorpio, & Aquarius, & Gemini, U Virgo, & Sagittarius, & Pisces, &

Since the Ecliptic and Equinoctial are great circles, they, therefore, bisect each other in two points, which are called the Equinoctial Points. The Sun is in one of these points in March, and in the other in September; hence, the first is called the Vernal, and the other the Autumnal Equinox—and that sign which begins at the Vernal Equinox is called Aries. Those points of the Ecliptic, which are equidistant from the equinoctial points, are called the Solstitial Points; the first the summer, and the second the winter solstice. That great circle which passes through the equinoctial points and the poles of the earth, is called the Equinoctial Colure: and the great circle which passes through the solstitial points and the poles of the earth, is called the Solstitial Colures -

When the Sun enters Aries, it is in the Equinoctial; and, therefore, has no declination. From thence it moves forward in the Ecliptic, according to the order of the signs, and advances towards the north pole, by a kind of retarded motion, till it enters Cancer, and is then most distant from the Equinoctial; and moving forward in the Ecliptic. the Sun apparently recedes from the north pole with an accelerated motion till it enters Libra, and being again in the Equinoctial, has no declination; the Sun moving through the signs Libra, Scorpio, and Sagittarius, enters Capricorn; and then its south declination is greatest, and is, therefore, most distant from the north pole; and moving forward through the signs Capricorn, Aquarius, and Pisces, again enters Aries: Hence, a period of the seasons is completed, and this period is called a Solar Year.

The signs Aries, Taurus, Gemini, Cancer, Leo, and Virgo, are called Northern Signs, because they are contained in that part of the Ecliptic which is between the Equinoctial and North Pole; and, therefore, while the Sun is in these signs, its. declination is north: the other six signs are called Southern Signs. The signs in the first and fourth quarters of the Ecliptic are called Ascending Signs. because, while the Sun is in these signs, it approaches the north pole—and, therefore, in the northern, temperate, and frigid zones, the Sun's meridian altitude daily increases; or, which is the same, the Sun ascends to a greater height above the horizon every day. The signs in the second. and third quarters of the Ecliptic are called Destending Signs,

The Tropics are circles parallel to the Equinoctial, whose distance therefrom, is equal to the

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obliquity of the Ecliptic. The Northern Tropic touches the Ecliptic at the beginning of Cancer, and is, therefore, called the *Tropic of Cancer*; and the Southern Tropic touches the Ecliptic at the beginning of Capricorn, and is hence called the *Tropic of Capricorn*.

Circles about the poles of the Equinoctial, and passing through the poles of the Ecliptic, are called Polar Circles; the distance, therefore, of each Polar Circle from its respective Pole, is equal to the inclination of the Ecliptic and Equinoctial. That Circle which circumscribes the North Pole is called the Artic, or North Polar Circle; and that towards the South Pole, the Antartic, or South Polar Circle.

That semicircle which passes through a star, or any given point of the heavens, and the Poles of the Ecliptic, is called a Circle of Latitude.

The Reduced Place of a Star is that point of the Ecliptic, which is intersected by the circle of latitude passing through that star.

The Latitude of a Star is that portion of the circle of latitude contained between the Star and its reduced place—and is either north or south, according as the Star is between the Ecliptic and the north or south pole thereof.

The Longitude of a Star is that portion of the Ecliptic, contained between the Vernal Equipox and the reduced place of the Star.

SECTION II.

Description of the Instruments requisite in Astronomica?

Observations.

THE QUADRANT.

T is generally allowed that we are indebted to John Hadley, Esq. for the invention, or at least for the first public account of that admirable instrument, commonly called Hadley's Quadrant, who in the year 1731, first communicated its principles to the Royal Society, which were by them published soon after in their Philosophical Transactions; before this period, the Cross Staff and Davis's Quadrant were the only instruments used for measuring altitudes at sea, both very imperfect, and liable to considerable error in rough weather; the superior excellence however of Had-: ley's Quadrant, soon obtained its general use among seamen, and the many improvements this instrument has received from ingenious men at various times, has rendered it so correct, that it is now applied, with the greatest success, to the important purposes of ascertaining both the latitude and longitude at sea, or land.

The Octant or Frame, is generally made of ebony, or other hard wood, and consists of an arch firmly attached to two radii, or bars, which are strengthened and bound by the two braces, in order to prevent it from warping.

Rr

The Arch, or Limb, although only the eighth part of a circle, is on account of the double reflection, divided into 90 degrees, numbered 0, 10, 20, 30, &c. from the right towards the left; these are subdivided into 3 parts, containing each 20 minutes, which are again subdivided into single minutes, by means of a scale at the end of the Index. The arch extending from 0 towards the right hand is called the arch of excess.

The Index is a flat brass bar, that turns on the centre of the instrument; at the lower end of the Index there is an oblong opening: to one side of this opening a Nonius scale is fixed to subdivide the divisions of the arch; at the bottom or end of the index, there is a piece of brass which bends under the arch, carrying a spring to make the Nonius scale lie close to the divisions; it is also furnished with a screw to fix the Index in any desired position.

Some instruments have an adjusting or tangentscrew, fitted to the Index, that it may be moved more slowly, and with greater regularity and accuracy than by the hand; it is proper, however, to observe, that the Index must be previously fixed near its right position by the above mentioned screw, before the adjusting screw is put in motion-

The Nonius is a scale fixed to the end of the Index for the purpose, as before observed, of dividing the subdivisions on the Arch into Minutes; it sometimes contains a space of 7 degrees, or 21 subdivisions of the limb, and is divided into 20 equal parts; hence each division on the Nonius will be one-twentieth part greater, that is, one minute longer than the divisions on the Arch; con-

sequently, if the first division of the Nonius marked 0, be set precisely opposite to any degree, the relative position of the Nonius and the Arch must be altered one minute before the next division on the Nonius will coincide with the next division on the Arch, the second division will require a change of 2 minutes, the third of 3 minutes, and so on, till the 20th stroke on the Nonius arrives at the next 20 minutes on the Arch; the 0 on the Nonius will then have moved exactly 20 minutes from the division whence it set out, and the intermediate divisions of each minute, have been regularly pointed out by the divisions of the Nonius.

The divisions of the Nonius scale are in the above case reckoned from the middle towards the right, and from the left towards the middle; therefore the first 10 minutes are contained on the right of the 0, and the other 10 on the left. But this method of reckoning the divisions being found inconvenient, they are more generally counted, beginning from the right-hand towards the left; and then 20 divisions on the Nonius are equal to 19 on the limb, consequently one division on the Arch will exceed one on the Nonius by one-twentieth part, that is, one minute.

The 0 on the Nonius, points out the entire degrees and odd twenty minutes subtended by the objects observed; and if it coincides with a division on the Arch, points out the required angle: thus, suppose the 0 on the Nonius stands at 25 degrees, then 25 degrees will be the measure of the angles observed; if it coincides with the next division on the left hand, 25 degrees 20 minutes is the angle; if with the second division beyond 25

degrees, then the angle will be 25 degrees 40 minutes; and so on in every instance where the 0 on the Nonius coincides with a division on the Arch: but if it does not coincide, then look for a division on the Nonius that stands directly opposite to one on the Arch, and that division on the Nonius gives the odd minutes to be added to that on the Arch nearest the right-hand of the 0 on the Nonius; for example, suppose the Index division does not coincide with 25 degrees, but that the next division to it on the Nonius is the first coincident division, then is the required Angle 25 degrees 1 minute; if it had been the second division. the Angle would have been 25 degrees 2 minutes,. and so on to 20 minutes, when the 0 on the Nonius would coincide with the first 20 minutes on the Arch from 25 degrees. Again, let us suppose the 0 on the Nonius to stand between 50 degrees and 50 degrees 20 minutes, and that the 15th division on the Nonius coincides with a division on the Arch, then is the angle 50 degrees 15 minutes. Further, let the 0 on the Nonius stand between. 45 degrees 20 minutes and 45 degrees 40 minutes, and at the same time the 14th division on the Nonius stands directly opposite to a division on the Arch, then will the Angle be 45 degrees 34 minutes.

The Index Glass is a plane speculum, or mirror of glass quicksilvered, set in a brass frame, and so placed that the face of it is perpendicular to the plane of the instrument, and immediately over the centre of motion of the Index. This mirror being fixed to the Index moves along with it, and has its direction changed by the motion thereof.

This glass is designed to reflect the image of the Sun, or any other object, upon either of the two horizon glasses, from whence it is reflected to the

eye of the observer. The brass frame, with the glass, is fixed to the Index by the screw; the other screw serves to place it in a perpendicular position, if by any accident it has been put out of order.

The Horizon Glasses are two small speculums on the radius of the Octant; the surface of the upper one is parallel to the Index glass when the O on the Nonius is at 0 on the Arch; these mirrors receive the rays of the object reflected from the Index glass, and transmit them to the observer. The fore Horizon glass is only silvered on its lower half, the upper half being transparent, in order that the direct object may be seen through it. back Horizon glass is silvered at both ends; in the middle there is a transparent slit, through which the Horizon may be seen. Each of these glasses is set in a brass frame, to which there is an axis; this axis passes through the wood work, and is fitted to a lever on the under side of the quadrant, by which the glass may be turned a few degrees on its axis, in order to set it parallel to the Index glass.

To set the glasses perpendicular to the plane of the quadrant, there are two sunk screws, one before and one behind each glass: these screws pass through the plate on which the frame is fixed into another plate, so that by loosening one and tightening the other of these screws, the direction of the frame, with its mirror, may be altered, and thus be set perpendicular to the plane of the instrument.

The Dark Glasses, or Shades, are used to prevent the bright rays of the Sun, or the glare of the Moon, from hurting the eye at the time of observation; there are generally three of them, two red, and one green. They are each set in a brass frame

which turn on a centre, so that they may be used separately or together, as the brightness of the object may require. The green glass may be used also alone, if the Sun be very faint; it is likewise used in taking observations of the Moon; when these glasses are used for the fore observation, they are set immediately before the fore Horizon glass, but in front of the other Horizon glass, when a back observation is made.

The Sight Vanes are pieces of brass, standing perpendicular to the plane of the instrument: that one which is opposite the fore horizon, is called the fore Sight Vane, the other the back Sight Vane. There are two holes in the fore Sight Vane, the lower of which, and the upper edge of the silvered part of the fore Horizon glass, are equidistant from the plane of the instrument, and the other is opposite to the middle of the transparent part of that glass; the back Sight Vane has only one hole, which is exactly opposite to the middle of the transparent slit in the Horizon glass to which it belongs: but as the back observations are liable to many inconveniences and errors, we shall not give any directions for their practice.

ADJUSTMENTS.

The several parts of the Quadrant being liable to be out of order from a variety of accidental circumstances, it is necessary to examine and adjust them, so that the instrument may be put into a proper state, previous to taking observations.

An instrument properly adjusted, must have the Index glass and Horizon glasses perpendicular to the plane of the Quadrant; the plane of the fore Horizon glass parallel, and that of the back Horizon

zon glass perpendicular to the plane of the Index glass, when the 0 on the Nonius is at 0 on the Arch; hence the Quadrant requires five adjustments, the first three of which being once made, are not so liable as the last two to be out of order; however they should all be occasionally examined in case of an accident.

I. To set the Plane of the Index Glass perpendicular to that of the Instrument,

Place the Index near to the middle of the Arch, and holding the Quadrant in a horizontal position, with the Index glass close to the eye, look obliquely down the glass, in such a manner that you may see the Arch of the Quadrant by direct view, and by reflection at the same time; if they join in one direct line, and the Arch seen by reflection forms an exact plane, or strait line, with the Arch seen by direct view, the glass is perpendicular to the plane of the Quadrant; if not, it must be restored to its right position by loosening the screw, or tightening it, or vice versa, by a contrary operation.

II. To set the Fore Horizon Glass parallel to the Index Glass, the Index being at 0.

Set the 0 on the Nonius exactly against 0 on the Arch, and fix it there by the screw at the under side. Then, holding the Quadrant vertically, with the Arch lowermost, look through the Sight Vane, at the edge of the sea, or any other well defined and distant object. Now, if the Horizon in the silvered part exactly meets, and forms one continued line with that seen through the unsilvered part, the Horizon glass is parallel to the Index glass. But if the Horizons do not coincide.

then loosen the button-screw in the middle of the lever, on the under side of the Quadrant, and move the Horizon glass on its axis, by turning the nut at the end of the adjusting lever, till you have made them perfectly coincide; then fix the lever firmly in this situation by tightening the buttonscrew. This adjustment ought to be repeated before and after every observation. Some observers adopt the following method, which is called finding the *Index error*. Let the Horizon glass remain fixed, and move the Index till the image and object coincide; then observe whether 0 on the Nonius agrees with 0 on the Arch, if it does not, the number of minutes by which they differ is to be added to the observed altitude or angle, if the 0 on the Nonius be to the right of the 0 on the Arch, but if to the left of the 0 on the limb, it is to be subtracted.

It has already been observed, that that part of the Arch beyond 0, towards the right hand, is called the Arch of excess: the Nonius, when the '0 on it is at that part, must be read the contrary way, or which is the same thing, you may read off the minutes in the usual way, and then their complement to 20 minutes will be the real number, to be added to the degrees and minutes pointed out by the 0 on the Nonius,

III. To set the Fore Horizon Glass perpendicular to the Plane of the Quadrant.

Having previously made the above adjustment, incline the Quadrant on one side as much as possible, provided the Horizon continues to be seen in both parts of the glass; if when the instrument is thus inclined, the edge of the sea seen through the lower hole of the Sight Vane continues to form

factly adjusted; but if the reflected Horizon be separated from that seen by direct vision, the speculum is not perpendicular to the plane of the Quadrant: then if the limb of the Quadrant is inclined towards the Horizon, with the face of the instrument upwards, and the reflected sea appears higher than the real sea, you must slacken the screw before the Horizon glass, and tighten that which is behind it; but if the reflected sea appears lower, the contrary must be performed. Care must be always taken in this adjustment to loosen one screw before the other is screwed up, and to leave the adjusting screws tight, or so as to draw with a moderate force against each other.

This adjustment may be also made by the Sun, Moon, or a Star; in this case the Quadrant is to be held in a vertical position; if the image seen by reflection appears to the right or left of the object seen directly, then the glass must be adjusted as before by the two screws.

It will be necessary, after having made this adjustment, to examine if the Horizon glass still continues to be parallel to the Index glass, as sometimes by turning the sunk screws the plane of the Horizon glass will have its position altered.

USE OF HADLEY'S QUADRANT.

The use of the Quadrant is to ascertain the Angle subtended by two distant objects at the eye of the observer; but principally to observe the altitude of a celestial object above the Horizon: this is pointed out by the Index when one of the

objects seen by reflection is made to coincide with the other, seen through the transparent part of the Horizon glass.

To take an Altitude of the Sun, Moon, or a Star, by a Fore
Observation

Having previously adjusted the instrument, place the 0 on the Nonius opposite to 0 on the Arch, and turn down one or more of the screens, according to the brightness of the Sun; then apply the eye to the upper hole in the fore Sight Vane, if the Sun's image be very bright, otherwise to the lower, and holding the Quadrant vertically, look directly towards the Sun so as to let it be behind the silvered part of the Horizon glass, then the coloured Sun's image will appear on the speculum; move the Index forward till the Sun's image, which will appear to descend, just touches the Horizon with its lower or upper limb; if the upper hole be looked through, the Sun's image must be made to appear in the middle of the transparent part of the Horizon, but if it be the lower hole, hold the Quadrant so that the Sun's image may be bisected by the line joining the silvered and transparent parts of the Horizon glass.

The Sun's limb ought to touch that part of the Horizon immediately under the Sun, but as this point cannot be exactly ascertained, it will be therefore necessary for the observer to give the Quadrant a slow motion from side to side, turning at the same time upon his heel, by which motion the Sun will appear to sweep the Horizon, and must be made just to touch it at the lowest part of the Arch; the degrees and minutes then pointed out by the Index on the Limb of the Quadrant will be the observed altitude of that limb which is brought in contact with the Horizon-

When the meridian or greatest altitude is required, the observation should be commenced a short time before the object comes to the meridian; being brought down to the Horizon, it will appear for a few minutes to rise slowly; when it is again to be made to coincide with the Horizon by moving the Index forward; this must be repeated until the object begins to descend, when the Index is to be secured, and the observation to be read off.

From this description of the Quadrant and its use, the manner of adjusting and using the Sextant will be readily apprehended. Our limits will not allow a particular description of this excellent instrument.

The Artificial Horizon.

In many cases it happens that altitudes are to be taken on land by the Quadrant or Sextant; which, for want of a natural horizon, can only be obtained by an artificial one. There have been a variety of these sorts of instruments made, but the kind now described is allowed to be the only one that can be depended upon. It consists of a wood or metal framed roof, containing two true parallel glasses of about 5 by 21 inches, fixed not too tight in the frames of the roof. This serves to shelter from the air a wooden trough filled with quicksilver. In making an observation by it with the Quadrant, or Sextant, the reflected image of the sun, moon, or other object, is brought to coincide with the same object reflected from the glasses of the Quadrant or Sextant: half the angle shown upon the limb is the altitude above the horizon or level required. It is necessary in a set of observations that the roof be always placed the same way. When done with, the roof folds up flatways, and, with the quicksilver in a bottle. &c. is packed into a portable flat case,

SECTION III.

To find the Latitude by the Meridian Altitude of the Sun.

The Latitude of a place is its distance from the equator, either North or South; and is measured by an arch of a Meridian contained between the Zenth and the equinoctial. Hence, if the distance of any heavenly body from the Zenith, when on the Meridian, and its declination, or the number of degrees and minutes it is to the Northward, or Southward of the equinoctial, be given, the Latitude may thence be tound.

The Altitude of the Sun, observed by a Quadrant, or Sextant, requires four corrections in order to obtain the true altitude; these are:

the Semidiameter, Dip, Refraction, and Parallax.

By the Semidiameter of the Sun is meant the angle subtended by the distance from its centre to its apparent circumference. The quartity of this angle is given for every sixthday in the year in table 10.

The Dip of the Horizon is a vertical angle contained between a Horizontal plane passing through the eye of an observer, and a line drawn from his eye to the visible Horizon. This Dip is found in Table 8, when the visible horizon is formed by the apparent junction of the water and sky; but in Table 9, when land intervenes. In this case, the line that separates the land and water is used as the Horizon, and its distance from the observer must be duly estimated.

The Refraction of any celestial body is the difference between its apparent place, and that wherein it would be seen, if the space between the observer and object, was either a void, or of a uniform

density. Table 6 contains this Refraction.

That part of the heavens, in which an object appears, when viewed from the surface of the earth, is called its apparent place; and the point, wherein it would be seen, at the same instant, if viewed from the centre of the earth, is called its true place; the difference between the true and apparent places, is called the Parallax. The Sun's Parallax in Altitude is found in Table 7.

RULE

For finding the Latitude from the Sun's Meridian Altitude.

Having observed with the Quadrant, or Sextant, the altitude of the Sun's lower limb above the visible horizon,—or the line of separation of the land from the water, when that horizon is obstructed by land—add thereto the semidiameter, taken from table 10 at the given day of the month, or he one nearest to it, and from this sum subtract the

Dip, from table 8 or 9, corresponding to the height of the observer's eye above the surface of the water; and this result will be the apparent altitude of the Sun's centre. Then take the refraction from table 6, and the parallax from table 7, corresponding to this altitude, and the difference of these quantities, called the correction, being subtracted from the apparent altitude, the remainder will be the Sun's true altitude; the complement of which will be its zenith distance, north or south, according as the Sun bears south or north, at the time of observation.

When the observation has been made by bringing the Sun's image in the Quadrant, or Sextant, to a just coincidence with its image in an artificial horizon, half the angle shown on the instrument is the Sun's apparent altitude, which must be corrected by the corresponding refraction and parallax only, in order to obtain the true altitude.

Take the Sun's declination from table 13, answering to the given year, month, and day, observing whether it be north or south, and reduce it, as there directed, by the help of table 14, to the longitude of the place of observation. Then the sum, or difference of the zenith distance, and declination, according as they are of the same, or of a contrary denomination, will be the latitude of the place of observation, of the same name with the greater of those two quantities.

EXAMPLES.

1st. March 10th, 1811, in longi- 2d, May 10th, 1811, in long 80° inde 70° W, the Mer. Alt of ⊙ L. W, at noon, the angular distance L. was observed to be 49° 50 between the ⊙ bearing such, and bearing south—height of the ob- its reflected image in the artificial server's eye 12 feet, required the horizon was found with a scattart latitude in to be 98° 30° 40° required the lati- Mer. Alt. ⊙ L. L. = 49° 50° 00° S. tade.

Mer. Alt. O L. L = 490 50 000 S. tude. 980 50' 40" + 2 - 490 15' 20" Semidiameter = + 16 08 Dip-table 8 -03 19 O Ap. Ait. Ap. Alt. = 50 02 49Correction True Alt. 50 02 07 True Alt. Zenith Dist. Reduced Dec. = \$9 57 53N. = 4 15 298. Zenith Dist. Reduced Dec. Latitude. 35 62 24N.

3d. July 24th, 1811, in long, 62° 4th, Ontober 11th, 1812, in length 30° W, the Mer. Alt of © L. L. 91° W, the Meridian Altitude of above the border of a lake was © L. L. above the visible horizon observed, by a person on the apwas observed to be 47° 13° bearpostic shore. We be 56° 32° bear-ing S, the height of the eye being leng S—the distance of that bor- 25 feet; required the latitude der of the lake beneath the sun Mer. Alt. © L. L. =47° 13 00° S, being 3 miles from the observer, Semidianneter = + 15 05° and the height of his eye above Dip from table 8 = -4 47° the sarriace of the water, 8 feet; required the latitude.

Mer. Alt. © L. L. =56° 32° 00° S. Correction = -46° Semidianneter = + 15 48° True Alt. =47° 23° 38° Dip from table 9 = -2 36° True Alt. =47° 23° 38° Dip from table 9 = -2 36° True Alt. =47° 23° 38° Dip from table 9 = -2 36° True Alt. =47° 23° 38° Dip from table 9 = -2 36° True Alt. =47° 23° 38° Dip from table 9 = -33° 15° 10° N. B. For the various other metalitude polymer of the latitude by the altitude of the north star, in the explanation of table 12, annexed to this treatise.

SECTION IV.

VARIATION OF THE COMPASS.

The variation of the compass is the deviation of the points of the mariner's compass from the corresponding points of the horizon, and is termed east or west variation, according as the magnetic needle, or north point of the compass, is inclined to the eastward or westward of the true north point of the horizon.

The true amplitude of any celestial object is an arch of the borison contained between the true east or west points thereof, and the centre of the object at the time of its rising or setting; or it is the degrees and minutes, the object rises or sets to the northward or southward of the true east or west points of the horizon.

The magnetic amplitude, is an arch contained between the east or west points of the compass and the centre of the object at rising or setting; or it is the bearing of the object, by compass, when in

the horizon.

The true azimuth of an object is an arch of the horizon contained between the true meridian and the azimuth circle passing through

the centre of the object.

The magnetic azimuth, is an arch contained between the magnetic meridian and the azimuth circle passing through the centre of the object; or it is the bearing of the object, by compass, at any time when it is above the horizon-

The true amplitude, or azimuth, is found by calculation, and the

magnetic amplitude, or azimuth, by an azimuth compass.

THE AZIMUTH COMPASS.

From the accounts of the compasses, heretofore given in the description of surveying instruments, it is presumed that the nature and properties of the azimuth compass will be readily conceived by a contemplative inspection; the directions for its uses are as follow:

To observe the Sun's amplitude.

Turn the compass-box until the vane containing the magnifying glass is directed towards the sun: and when the bright speck, or rays of the sun collected by the magnifying glass, falls upon the slit in the other vane, stop the card by means of the nonins, and read off the amplitude.

Without using the magnifying glass, the sight may be directed through the dark glass towards the sun; and in this case, the card is to be stopped when the sun is bisected by the thread in the other

ane.

The observation should be made when the sun's lower limb appears somewhat more than his semidiameter above the horizon, because his centre is really then in the horizon, although it is ap-

parently elevated on account of the refraction of the atmosphere: this is particularly to be noticed in high latitudes.

To observe the Sun's Azimuth.

Raise the magnifying-glass to the upper part of the vane, and move the box, as before directed, until the bright speck fall on the other vane, or on the line in the horizontal bar; the card is then to be stopped, and the divisions being read off, will be the sun's magnetic azimuth.

If the card vibrate considerably at the time of observation, it will be better to observe the extreme vibrations, and take their mean as the magnetic azimuth. When the magnetic azimuth is observed, the altitude of the object must be taken, in order to obtain the true

azimuth.

It will conduce much to accuracy if several azimuths be observed, with the corresponding altitudes, and the mean of the whole taken for the observation.

To find the variation of the Compass by an amplitude.

RULE—1. To the log. secant of the latitude, rejecting the index, add the log. sine of the sun's declination, corrected for the time and place of observation; their sum will be the log. sine of the true amplitude, to be reckoned from the east in the morning, or the west in the afternoon, towards the north or south, according to the declination.

2. Then if the true and magnetic amplitudes, be both north or both south, their difference is the variation; but if one be north and the other south, their sum is the variation; and to know whether it be easterly or westerly, suppose the observer looking towards that point of the compass representing the magnetic amplitude: then if the true amplitude be to the right hand of the magnetic amplitude, the variation is east, but if to the left hand, it is west.

EXAMPLE I.

July 3, 1812, in latitude 9° 86' S. the Sun was observed to rise E 32° 42' N: required the variation of the compass.

Latitude 9° 36′ S. - Secant 0.00613 Declination 22 59 N. - Sine 9.59158

True amplitude F. 23 20 N. - Sine 9.59771 Mag. amplitude E. 12 42 N.

Variation - 10 38 west, because the true amplitude is to the left of the magnetic

EXAMPLE II.

September 24, 1812, in latitude 26° 32′ N. and longitude 78° W. the Sun's centre was observed to set W. 6° 15′ S about 6h. P. M. required the variation of the compass.

0º 30' S-Sun's declination Corr. for long. 78° W. Corr. for time 6h. P. M. 6 Reduced declination 41 Sine 8.07650 26 Latitude 32 0.04834W. 0 46 S. 81.2484 True amplitude W. 6 158 Mag. amplitude

Variation 5 29 east, because the true amplitude is to the right hand of the magnetic.

To find the Variation of the Compass by an Azimuth

Rule. 1.—Reduce the Sun's declination to the time and place of observation, and compute the true altitude of the Sun's centre.

2. Subtract the Sun's declination from 90°, when the latitude and declination are of the same name, or add it to 90°, when they are of contrary names; and the sum, or remainder, will be the Sun's polar distance.

3. Add together the Sun's polar distance, the latitude of the place, and the altitude of the Sun; take the difference between half their sum and the

polar distance, and note the remainder.

4. Then add together the log. secant of the altitude rejecting their the log. secant of the latitude indices. the log. co. sine of the half sum,

and the log. co. sine of the remainder.

- 5. Half the sum of these four logarithms will be the sine of an arch, which doubled, will be the Sun's true azimuth; to be reckoned from the south in north latitude, and from the north in south latitude: towards the east in the morning, and towards the west in the afternoon.
- 6. Then if the true and observed azimuths be both on the east, or both on the west side of the meridian, their difference is the variation: but if one, be on the east, and the other on the west side of the meridian, their sum is the variation; and to know if it be east or west, suppose the observer looking towards that point of the compass representing the magnetic azimuth; then if the true azimuth be to the right of the magnetic, the variation is east, but if the true be to the left of the magnetic, the variation is west.

November 2, 1812, in latitude 25° 32′ N. and longitude 75° W. the altitude of the Sun's lower limb was observed to be 15° 36′, about 4h. 10m. P. M. his magnetic azimuth at that time being S. 58° 32′ W. and the height of the eye 18 feet; required the variation of the compass.

Sun's de. Nov. 2, at n. 140 48' S. Obs. alt. Sun's lower limb 150 68'
Cerr. for long. 750 W. + 4
Co. for ti. 4h. 10m. af. n. + 3
Dip + 4 + 12

CO. IOI D. Mr. IVIII- MI-	r s	- 4)	
Reduced declination	14 55 90 00	Refraction	15 48 3
Polar distance Altitude - Latitude -	104 55 15 45 25 32	True altitude - - Secant 0.01562 - Secant 0.04463	15 45
Sum Half Remainder	146 12 73 6 31 49	- Co. sine 9.46345 - Co. sine 9.92929	•
•	32 14	19.45399 - Sine 9.72699	

True azimuth S. 64 28 W. Mag. azimuth S. 58 32 W.

Variation - 5 56 east, because the true azimuth is to the right of the magnetic-

To draw a true meridian line to a map, having the variation and magnetical meridian given.

On any magnetical meridian or parallel, upon which the map is protracted, set off an angle from the north towardathe east, equal to the degrees or quantity of variation, if it be westerly, or from the north towards the west, if it be easterly, and the line which constitutes such an angle with the magnetical meridian, will be a true meridian line.

For if the variation be westerly, the magnetical meridian will be the quantity of variation of the west side of the true meridian, but if easterly, on the east side; therefore the true meridian must be a like quantity on the east side of the magnetical one, when the variation is westerly, and on the west side when it is easterly.

To lay out a true meridian line by the circumferentor.

If the variation be westerly, turn the box about till the north of the needle points as many degrees from the flower-de-luce towards the east of the box, or till the south of the needle points the like number of degrees from the south towards the west, as are the number of degrees contained in the variation, and the index will be then due north and south: therefore if a line be struck out in the direction thereof, it will be a true meridian line.

If the variation was easterly, let the north of the needle point as many degrees from the flower-de-luce towards the west of the box, or let the south of the needle point as many degrees towards the east, as are the number of degrees contained in the variation, and then the north and south of the box will coincide with the north and south points of the horizon, and consequently a line being laid out by the direction of the index, will be a true meridian line.

This will be found to be very useful in setting an horizontal dial, for if you lay the edge of the index by the base of the stile of the dial, and keep the angular point of the stile toward the south of the box, and allow the variation as before, the dial will then be due north and south, and in its proper situation, provided the plane upon which it is fixed be duly horizontal, and the sun be south at noon; but in places where it is north at noon, the angular point of the index must be turned to the north.

How maps may be traced by the help of a true meridian line.

If all maps had a true meridian line laid out upon them, it would be easy by producing it, and drawing parallels, to make out fieldnotes; and by knowing the variation, and allowing it upon every bearing, and having the distances, you would have notes sufficient for a trace. But a true meridian line is seldom to be met with, therefore we are obliged to have recourse to the foregoing method. It is therefore advised to lay out a true meridian line upon every map.

To find the difference between the present variation, and that at a time when a tract was formerly surveyed, in order to trace or run out the original lines.

If the old variation be specified in the map or writings, and the present be known, by calculation or otherwise, then the difference is immediately seen by inspection; but as it more frequently happens; that neither is certainly known, and as the variation of different instruments is not always alike at the same time, the following prac-

tical method will be found to answer every purpose.

Go to any part of the premises where any two adjacent corners are known; and, if one can be seen from the other, take their bearing; which, compared with that of the same line in the former survey, shows the difference. But if trees, hills, &c. obstruct the view of the object, run the line according to the given bearing, and observe the nearest distance between the line so run and the corner, then.

As the length of the whole line
Is to 57.3 degrees,
So is the said distance
To the difference of variation required.

EXAMPLE.

Suppose it be required to run a line which some years ago bone NE. 45°, distance 80 perches, and in running this line by the given bearing, the sorner is found 20 links to the left hand; what allowance must be made on each bearing to trace the old lines, and what is the present bearing of this particular line by the compass?

Answer, 34 minutes; or a little better than half a degree to the left hand, is the allowance required, and the line in question bears N. 440 26. E.

Note. The different variations do not affect the area in the calculation, as they are similar in every part of the survey.

* 57.3 Is the radius of a circle (nearly) in such parts as the circumference contains 360.

TABLE L

LOGARITHMS OF NUMBERS.

EXPLANATION.

of the Logarithms of any two numbers, is the logarithm of the product of these numbers. Hence it is inferred, that if a rank, or series of numbers in arithmetical progression, be adapted to a series of numbers in geometrical progression, any term in the arithmetical progression will be the logarithm of the corresponding term in the geometrical progression.

This table contains the common logarithms of all the natural numbers from 0 to 10000, calculated to six decimal places; such, on account of their superior accuracy, being preferable to those, that are

computed only to five places of decimals.

In this form, the logarithm of 1 is 0, of 10, 1; of 100, 2; of 1000, 3 &c. Whence the logarithm of any term between 1 and 10, being greater than 0, but less than 1, is a proper fraction, and is expressed decimally. The logarithm of each term between 10 and 100, is 1, with a decimal fraction annexed; the logarithm of each term between 100 and 1000 is 2, with a decimal annexed, and so on. The integral part of the logarithm is called the Index, and the other the decimal part.—Except in the first hundred logarithms of this Table, the Indexes are not printed, being so readily supplied by the operator from this general rule; the Index of a Logarithm is always one less than the number of figures contained in its corresponding natural number—exclusive of fractions, when there are any in that number.

The Index of the logarithm of a number, consisting in whole, or in parts, of integers, is affirmative; but when the value of a number is less than unity, or 1, the index is negative, and is usually marked by the sign, —, placed either before, or above the index. If the first significant figure of the decimal fraction be adjacent to the decimal point, the index is 1,— or its arithmetical complement 9; if there is one cipher between the decimal point and the first significant figure in the decimal, the index is — 2, or its arith. comp. 8; if two ciphers, the index is — 3, or 7, and so on; but the arithmetical complements, 9, 8, 7 &c. are rather more conveniently used in trigonometrical calculations.

The decimal parts of the logarithms of numbers, consisting of the same figures, are the same, whether the number be integral, fractional, or mixed: thus,

of the natural number	23450 2345.0 234.50 23.450 2.3450 2.3450 .02345	4.370143 3.370143 2.370143 1.370143 0.370143 1.370143 2.370143 3.370143	9.370143 or 8.370143 7.370143
	C.002040	C0.010140	£

N. B. The arithmetical complement of the logarithm of any number, is found by subtracting the given logarithm from that of the radius, or by subtracting each of its figures from 9, except the last, or right-hand figure, which is to be taken from 10. The arithmetical complement of an index is found by subtracting it from 10.

PROBLEM I.

To find the logarithm of any given number.

RULES.

1. If the number is under 100, its logarithm is found in the first page of the table, immediately opposite thereto.

Thus the Log. of 53, is 1.724276.

2. If the number consists of three figures, find it in the first column of the following part of the table, opposite to which, and under 0, is its logarithm.

Thus the Log, of 384 is 2.584331—prefixing the index 2, because

the natural number contains 3 figures.

Again the log. of 65.7 is 1.817565—prefixing the index 1, because there are two figures only in the integral part of the given number.

3. If the given number contains four figures, the three first are to be found, as before, in the side column, and under the fourth at the top of

the table is the logarithm required.

Thus the log. of 8735 is 3.941263—for against 873, the three first figures found in the left side column, and under 5, the fourth figure found at the top, stands the decimal part of the logarithm, viz .941263, to which prefixing the index, 3, because there are four figures in the natural number, the proper logarithm is obtained.

Again the logarithm of 37.68 is 1.576111—Here the decimal part of the logarithm is found, as before, for the four figures; but the index is 1, because there are two integral places only in the natural number.

4. If the given number exceeds four figures, find the difference between the logarithms answering to the first four figures of the given number, and the next following logarithm; multiply this difference by the remaining figures in the given number, point off as many figures to the right-hand as there are in the multiplier, and the remainder, add-

ed to the logarithm, answering to the first four figures, will be the required logarithm, nearly.

Thus; to find the logarithm of 738582; the log. of the first four figures, viz. 7385 .868350 the next greater logarithm = 868409

to be multiplied by the remaining figures = 82

118
472

then to .868350 add 48

the sum 5.868398, with the proper index prefixed, is the required logarithm.

5. The logarithm of a vulgar-fraction is found by subtracting the logarithm of the denominator from that of the numerator; and that of a mixed quantity is found by reducing it to an improper fraction, and proceeding as before.

Thus to find the Logarithm of 7; from the log. of 7 = 0.845098 subtract the log. of 8 = 0.903090

Remainder = 9.942008 = the required log.

PROBLEM II.

To find the number answering to any given logarithm.

RULES.

1. Find the next less logarithm to that given in the column marked o at the top, and continue the sight along that horizontal line, and a logarithm the same as that given, or very near it, will be found; then the three first figures of the corresponding natural number will be found opposite thereto in the side column, and the fourth figure immediately above it, at the top of the page. If the index of the given logarithm is 3, the four figures thus found are integers; if the index is 2, the three first figures are integers, and the fourth is a decimal, and so on.

Thus the log. 3.132580 gives the Nat. Numb. 1357
2.132580 gives 135.7
1.132680 gives 13.57
0.132580 gives 1.357
9.132580 gives 1.357
4.1357 &c.

2. If the given logarithm cannot be exactly found in the table, and if more than four figures be wanted in the corresponding natural number; then find the difference between the given and the next less loga-

rithms, to which annex as many ciphers as there are figures required above four in the natural number; which—divide by the difference between the next less, and next greater logarithms, and the quotient annexed to the four figures formerly found, will give the required natural number.

Thus to find the natural number of the log. 4.828991; the next less log. is .828982 which gives 6735; the next greater log. is 829046

Dif. = 64 next less log. = 828982 given log. = 828991

Dif. with one e annexed = 90 then 64) 90 (1.4

260 256

therefore 1.4 being annexed to 6735, the required natural number, 67351.4, is now obtained.

LOGARITHMS OF NUMBERS.

TABLE I.

No.	Log.	No.	Log.	No.	Log.	No.	Log.	No.	Lo .
1	0.000000	21	4.322219	,41	1.612784	61	1.785350	81	1.908485
3	0.301030	22	1.342423	42	1.623249	62	1.792392	82	1.913814
3 4	0.477121	23 24	1.361728	43	1.633468 1.643453	63	1.799341	83	1.919078 · 1.924279
5	0.698970	25	1.397940	44 45	1.653213	65	1.812913	84	1.929419
6	0.778151.	26	1.414973	46	1.662758	66	1.819544	86	I-934498
7	0.845098.	27	1.431364	47	1.672098	67	1.826075	87	L939519
8	0.903090	28	1-447158	48	1.681241	68	1.832509	88	1.944483
9	0.954243	29	1.462398	49	1.690196	69	1.838849	89	1.949390
10	1.000000	30	1.477121	şo	1.698970	70	1.845098	90	1.954243
31	1-041393	31	1.491362	51	1.707570	71	1.851258	16.	1.959041
12	1.079181	32	1.505150	52	1.716003	72	1.857332	92	1.963788
13	1.113943	33	1.518514	53	1.724276	73	1.863323	93	1.968483
24	1.146128	34	1.531479	54	1.732394	74	1.869232	94	1.973128
25	1.176091	35	1.544068	55	1.740363	75	1.875061	95	1.977724
16	1.204120	36	1.556302	.56	1.748188	76	1.880814	96.	1.982271
17	1.230449	37	1.568202	57	1.755875	77	1.886491	97	1.986772
18	1.255273	38	1.579784	. 58	1.763428	78	1.892095	98	1.991226
19	1.278754	39	1.591065	59	1.770852	79	1.897627	99	1-995635
20	1.303030	40	1.602060	60	1.778151	1 80	1.903090	100	2.000000

•	No.	0	1	2	3	. 4	5 .	6	7	8	9
-	100	000000	000434	000868	001301	001734	002166	002598	003029	003460	003891
	101	004321	004751	,005180	005609	006038	006466	006894	007321	007748	008174
	103	008600	009200	009451	009876	010300	010724	011147	011570	011993	01241
	104	017011	017451	013868	018284	018700	014940	015360 019532	019047	020161	02077
	105	021189	021603	022016	022428	022841	013252	023664	024075	024486	02489t
	106	025306	025715	026124	026533	026942	027760	027757	028164	028571	028078
	107	029384	029789	030195	030600	031004	031408	031812	032216	032619	033021
	109	037426	037825	038227	038620	039017	035430	039811	040207	040602	040008
-	110							043755			
	111	045323	045714	046105	046495	046885	047275	047664	048053	048442	048830
	112	049218	049606	049993	050380	050766	051152	047664 051538	051924	05-309	052694
	113	053078	953403	053840	054230	:054013	054996	055378	055760	050142	050524
	115	060608	061076	057000	106 t 8 Za	050420	050005	059185 062958	062122	062700	064081
	116	064458	064832	065206	065580	065953	066326	066699	067071	067443	067814
	117	98:860	068,557	068928	069298	069668	070038	070407	070776	071145	071514
	118	071882	072250	072617	072985	073352	073718	074085	074451	074816	075182
-	119	075547	075912	076170	070040	077004	077368	077731	078094	078457	078815
	120 121	079181	079543	079904	082861	084310	080987	081347	081707	082067	086201
	122	086360	086716	087071	087426	087781	088136	088490	088845	089198	089552
•	123	089905	090258	090611	090963	091315	091667	092018	792370	092721	093071
	124	093422	093772	094122	094471	,094820	1095169	095518	095866	096215	096562
	125	100270	1007257	097804	1097951	098297	098644	098990	099335	099681	100026
	127	103804	104146	104487	104828	100160	105510	102434	106191	106(31	106870
	128	107210	107549	107888	108227	108565	108903	105851	109578	109916	110253
-	129	110590	110926	111262	111598	111934	112270	112605	112940	113275	11360g
	130							115943			
	131	117271	117003	117934	118265	118595	118926	119256	119586	119915	120245
	133	122842	124178	124504	124830	125156	122210	122543 125806	126131	126456	126781
i	134	127105	127429	127752	128076	128399	128722	129045	129368	129690	130012
ì	135	130334	130655	130977	131298	131619	131939	132260	132580	132900	133219
	136	133539	133858	134177	134490	134814	135133	135451	135768	136086	136403
	138	139879	140194	140508	140822	141116	141450	13861 ⁸ 141763	142076	142389	142702
	139	149015	143327	143639	143951	144263	144574	144885	145196	145507	145818
_	140	146128	146438	146748	147058	147367	147676	147985	148294	148603	148911
	141	149219	149527	149835	150142	1 50449	150756	151063	151370	151676	151982
	143	152288						154119			
	144	158362	158664	168066	150266	1150549	150852	157154	160468	160760	161068
1	145	161368	161667	161967	162266	162564	162863	163161 163161	163460	163757	164053
	146	104353	164650	164947	165244	165541	165838	166134	166430	166726	167022
	147	1107317	107613	167908	108203	168497	168792	169086	109380	109074	109961
i	149	173186	173478	172760	174060	174761	174641	172019 174932	175222	175612	17:801
j	150	176001	176281	176670	176050	177248	177526	177825	178112	178401	178680
	151							180699			
1	152	181844	182129	182415	182700	182085	187270	183554	188830	184127	184407
	153	184691	184975	185259	185542	185825	186108	186391	186674	186956	187239
	154 155							189209			
	156	193125	193405	193681	193950	194237	194514	194792	195069	195346	195621
	157	1195900	196176	196452	196729	197005	197281	197556	197832	198107	198381
	158	1199057	198932	199206	199481	199755	200029	200303	200577	200850	201124
-	159							203033			
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İ	No.	0	1	2	3	4	5	6	7	8	9
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1	161	206826	207095	207365	207634	207903	208172	20844 I	208710	208978	209247
1	162	209515	209783	210051	210318	210586	210853	211120	211388	211054	211921
	163	1212188	212454	212720	212080	21121	411110	445/05	214049	1~~+3.4	214579 217221
1	164	214044	215109	218010	218277	218525	218708	210060	210722	210:81	219846
1	165	220108	220370	220621	220802	221153	221414	221675	221936	222196	222456
	167	222716	222976	223236	223496	223755	224015	224274	224533	224792	225054
1	168	225309	225568	225826	226084	226342	226600	226858	227115	227372	225051 227630
1	169	227887	228144	228400	228657	228913	229170	229426	229082	229938	230193
1	170	230449	230704	230960	231215	231470	231724	231979	232233	232488	232742
	171	222006	227250	222504	234757	234011	234204	1234517	1234770	235023	235270
	172	235528	235781	236033	236285	230537	230789	237041	237292	37544	237795 240300
	173	238040	238297	238548	238799	239049	239299	239550	242202	242541	242700
	174	242028	242286	241048 243534	242782	244020	244277	244524	244773	245010	245266
	175 176	246612	245750	246006	246252	124640 0	246746	240001	1247230	247482	247728
į	177	247971	248219	248464	248700	248954	249198	249443	249687	249932	250176
	178	250420	250664	250908	251151	251395	251638	251881	252125	252367	250176 252610
1	179	252853	253090	253338	253580	253822	254004	254300	254548	254790	255031
1	180	255273	255514	255755	255996	256236	256477	256718	256958	257198	257439
	181	1257679	257918	258158	258398	1258637	258877	259116	259355	595941	259833
j	r82	260071	260310	260548	260787	261025	261263	261501	261738	261976	262214 264582
ı	183	262451	262688	262925	263162	263399	263636	203873	204109	204345	264582
Ì	184	204818	205054	265290	205525	205701	265990	268 - 78	268812	260046	260220
1	185 186	2605172	2607400	260080	270212	270446	270670	270012	27 1144	271227	269279
	187	271842	272074	269980 272306	272538	272770	273001	273233	273464	273696	273927
	188	274158	274389	274620	274850	27 (08 t	275311	275542	275772	276002	276232
	189	276462	276691	276921	277151	277380	277609	277838	278067	278206	278525
1	190	278754	278982	279210	279439	279667	279895	280123	280351	280578	280806
1	191	281033	281261	281488	281715	281942	282169	282395	282622	282849	283075
1	192	283301	283527	281488 283753	283979	284205	284431	284656	284882	285107	285332
	193	285557	285782	286007	286232	286456	286681	280905	287130	287354	287578
-	194	287802	288025	288249	288473	288696	288920	289143	289300	269589	289812
1	195	290035	290257	290480 292699	290702	290925	291147	291309	291591	201013	292034
	196	204466	204687	294907	205127	205747	205567	205787	206007	206226	206446
	198	206665	296884	297104	297323	297542	297761	207070	298198	298416	298636
	199	298853	299071	299289	299507	299725	299943	300161	300378	300595	300813
-	200	301230	301247	301464	301681	301808	302114	302221	302547	302764	302080
	201	303196	303412	301464 303628	303844	304050	304275	304491	304706	30492!	305136
4	202	1305351	1305566	305781	305996	306211	306425	306639	300854	1307068	307282
į	203	307496	307710	307924 310056	308137	308351	308564	308778	308991	309204	309417
	204	309630	309843	310056	310268	310481	310693	310906	311118	311330	311542
	205			312177							
	206 207	215070	216180	314289	314499	314710	217019	315130	217426	21764	217854
	207	318062	318272	316390 318481	318680	318808	31/016	810214	310022	310720	310058
1	209	320146	320354	320562	320760	320077	321184	321391	321598	321804	322012
1	210			322633							
i	211	324282	324488	324694	324899	325105	1325310	325516	325721	325926	326131
1	212	326336	326541	326745	326950	327155	327359	327563	327767	327972	328176
١	213	328380	328583	328787	328991	329194	329398	329601	329805	330008	328176 330211
	214	330414	1330017	330819	331022	331225	331427	331630	331832	332034	≀332230
	215	1332438	1332640	332842	333044	1333246	333447	333649	3 3 3 8 50	1334051	334253
	216	334454	334055	334856	335056	335257	335458	335058	35059	1330059	336260 338257
	217	228456	228676	2288	337000	33/200	35/459	220670	220840	240047	340246
1	219	34044	340642	240841	341020	341227	341425	341622	341830	342028	342225
ł		0							7	8	9
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1	No.	0	ì	2	3	4	5	.6	7	8	9
.1	220	242429	342620	742817	242014	242212	242400		242802	343999	344106
1	221	344392	344580	344785	344981	345178	345374	345570	345766	345962	346157
1	232	346353	346549	346744	346030	347135	347330	347525	347720	347915	348110
1	223	348305	348500	348694	348889	349083	349278	349472	349666	349860	350054
4	224	350248	350442	350636	350829	351023	351216	351410	321603	351796	351989
1	225	352182	352375	352568	352761	352954	353147	353339	353532	353724	353916
4	226	354108	354301	354493	354085	354870	355008	355200	355452	355643 357554 359456	355054
1	227 228	350020	350217	350400	350599	258666	248886	250076	250266	35/554	250646
1	229	35/933	360026	360215	360404	350000	260782	360072	359260	361350	361539
1	230	261728	261019	262105	262204	262482	262671	262810	262048	262226	262424
ı	231	262612	262800	262088	264176	264262	264551	264720	264026	363236 365113 366983	365301
1	232	365438	265675	365862	366040	366236	366423	366610	366796	366083	367169
·	233	13073501	307542	307729	307915	308101	308287	300473	1300059	300044	309030
1	234	169216	260401	360587	360772	360048	370143	370328	370513	370608	370883
1	235	371068	371253	371437	371622	371806	371991	372175	372360	372544 374382	372728
I	236	372912	373096	373280	373464	373647	373831	374015	374198	374382	374505
1	237	374748	374932	375115	375298	375481	375004	375840	370029	376212	370394
ı	338	370577	379759	370942	377124	377300	370306	277070	377052	378034	380020
1	239	3/0390	3/0500	3/0/01	3/0943	3/9124	3/9300	3/940/	3/9000	379849	28.86
ı	240 241	380211 382017 383815	38210	38227	380754	282727	282017	18200	382277	282456	282626
1	243	282815	182005	284174	284252	284522	3847 E2	284801	385070	285240	285428
ł	243	385606	385786	38 5064	786142	386321	386499	186677	386846	387034	387212
ı	244	387390	387568	387746	387923	388101	388279	388456	388634	388811	388989
l	245	389166	389343	389520	389697	389875	390051	390228	390405	387034 388811 390582	390759
ı	246	1390935	391112	391200	[391404	391041	391017	391993	392109	392345	392521
ı	247	392697	392873	393048	393224	393400	393575	393751	393926	394101	394277
ł	248	394452	394027	394802	394977	395152	395320	395501	395070	395850	390025
1	249	390199	390374	390540	390722	390090	39/0/0	39/245	39/410	397592	39//00
ı	250	397940	398114	398287	398461	398634	398808	398981	399154	399327	399501
ł	251	399074	399047	400020	1400192	402080	400530	403422	40260	401056 402777	402040
ı	252 253	403120	402202	402464	403625	402807	402078	404 140	404 320	404492	404663
ı	254	404834	40,000	405175	405346	405517	405688	405858	406020	406100	406370
ł	255	1400 (40	400710	1400001	1407051	1407221	407391	407501	407731	407000	400070
ı	256	408240	408410	408579	408749	408918	409087	409257	409426	409595	409764
1	257	409933	410102	410271	410440	410608	410777	410946	411114	411283	411451
ı		411620	411788	411956	412124	412292	412400	412028	412790	412964	413132
ŀ	259	413300	413407	413035	413802	413970	414137	414305	414474	414639 416308	414800
ł	260	4.14973	415140	415307	415474	415641	415808	415974	410141	410308	410474
1	261	410040	410807	410973	417139	417306	417472	417038	417404	417970 419625 421275	410735
ı	262 263	410056	410407	420286	410/90	420616	420781	A2004	421110	421276	421420
I	264	421604	421768	421922	422007	422261	422426	422500	422754	422918	423082
1	265	423246	423410	423573	423737	423901	424064	424228	424392	424555	424718
ı	266	424882	425045	425208	425371	425534	425697	425860	426023	424555 426186	426349
ı	267	426511	426674	126836	426999	427101	427324	427480	427048	427811	427973
1	268	428135	428297	428459	428621	428782	428944	429106	429268	429429	429591
l-	269	429752	429914	430075	430236	430398	430559	430720	430881	431042	431203
ı	270	431364	431525	431685	431846	432007	432167	432328	432488	432649	432809
ı	271	432969	433129	433290	433450	433010	433770	433930	434090	434249	434409
1	272	434509	434728	434888	435048	435207	435300	435520	435005	435844 437433	437 502
l	273	4277	430322	42806	428226	438284	438542	428700	438860	437433	43017
1	274 275	430222	430401	430648	430806	439064	440122	440270	440437	440594	440752
	276	440000	441066	441224	441281	441538	441605	441852	442009	442100	442323
ľ	277	442480	442626	1442702	1442050	443106	443203	443419	443570	443732	443888
ĺ	278	444045	1444201	444357	444413	444009	1444825	444981	1445137	445293	445448
L	279	445604	445760	445915	446071	440226	440382	440537	440092	440848	447003
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280					447778		448088	448242	448397	448552
281	LAAXTON	AAXXOI	AAOO I C	440170	440724	440478	440073	444707	44994	145~45
282	1460240	4.60402	450557	460711	145080C	451018	451172	451320	145:4/9	145.435
283	461786	457040	452007	462247	452400	453563	452700	452850	453013	PAS 3 1 0 3
284	453318	453471	453624	453777	453930	454082	454235	454387	454540	454692 456214
285	454845	454997	455149	455302	455454	455606	455758	455910	456002	450214
286	456366	456518	456670	456821	456973	457125	457276	457428	457579	457730
287	457882	458033	458184	458330	458487	458038	458709	450940	459091	459243
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291 292	465282	465522	466680	466820	465077	466126	466274	466423	466571	466719
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298	1474210	474702	1474508	474053	1474799	474044	147 (OGO	1475235	475301	4/55-4
299	475971	475010	475902	470107	470252	470397	470542	4/0007	4/0032	476976
300	477121	477266	477411	477555	477700	477844	477989	478133	470278	478423
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302	481142	481286	481720	481874	1482016	1482150	482202	482445	482688	482731
303 304	482874	1482016	1482150	1482302	148344c	A82 (87	1483730	483872	484015	484157
305	484300	484442	484584	484727	484860	48011	485153	485295	485437	485579
306	485721	485863	486005	486147	486289	486430	486572	486714	486855	48557 9 486997
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315	1406711	1408448	1408580	1408724	1485502	1408000	1400177	1200275	1400413	
316	499687	499824	499962	500000	500236	500 274	500511	500548	500785	5009 22 502290 5036 54
317	501059	501196	501333	501470	501607	501744	501880	501017	502154	502290
318	502427	502564	502700	502837	502973	503 109	503246	503382	503518	503654
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323	1509202	509337	509471	509006	509740	509874	5 10008	510143	510277	SIGHT
324 325	1510545	1510079	1510013	510947	511081	511215	511348	512818	5130ET	511750 513084 514415
325	613218	51:361	1512484	512617	512750	C12882	514016	CIAIAO	S14282	514415
327	1514540	1514000	1514013	1514940	1515079	515211	5 4 5 3 4 4	1515470	13:3009	13.3/4.9
328	1515874	516006	516139	516271	516403	516535	516668	516800	516931	517004
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332	1521138	142120Q	(21400	(21530	< 21661	C21702	C21022	 {2,20	[522183	582314
333	522444	522575	522705	522835	522966	523096	523226	523356	523486	523616 524915
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1	340	531479	531607	531734	531862	531990	532117	532245	532372	532500	532627 533899
1	341	532754	532882	533009	533136	533263	533391	533518	533645	533772	533899
ı	342	2402b	1534153	1574280	1534407	534534	534001	5347071	5349141	333041))).v/
1	343	F25204	C 2 C A 2 1	C2CC47	C26674	£ 3 £ 800	[C Z C D 2 7]	C 3 PO C 3	\$3017Q	530300	5304321
I	344	536558	536685	536811	536937	537063	537189 538448	537315	537441	537507	537093
ı	345	537819	537945	538071	538197	538322	539703	538574	530099	530025	530931
1	346	539070	539202	540680	539454	540820	540055	541080	541205	241330	541454
ı	347	540329	541704	541820	CALOCT	542078	540955 542203	542327	542452	542576	542701
ł	348	542825	543050	543074	543199	543323	543447	543571	543696	543820	543944
ŀ	349	-44069	*****	C44216	CAAAAO	EAREGA	EAA688	544812	544026	€4 €060	545183
ı	350										
1	351 352	546543	546666	546789	546913	547036	\$45925 \$47159 \$48389 \$49616	547282	547405	547529	547652
ł	353	547775	547898	548021	548144	548266	548389	548512	548635	548758	548881
1	354	549003	549126	549249	549371	549494	549616	549739	549861	549984	550100
ł	355	550228	550351	550473	550595	550717	550840 552059	550962	551084	551200	551320
1	356	551450	551572	551094	551810	551938	552059	552181	552303	652640	662762
ł	357	552668	552790	552911	553033	553154	553276 554489	553390	554721	554852	534973
ı	358	553883	554004	554120	55424/	555578	556600	555820	555040	556061	556182
1.	359	255094	333413	3330	23343/	2000	555699	7,7006	557146	557267	557387
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	361		1 XX 7 A	I E E XOAX	I C COORS	' C CO I A A	1 5 60 70 8	6 60420	1 5 5 G 5 A G I	33400/	339/5/
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ı	364	561101	561221	561340	561459	561578	561698 562887	561817	56:936	562055	562174
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ı	367	564666	564784	564903	565021	565139	565257 566437	565376	505494	505012	565730
ı	368	565848	565966	566084	566202	500320	500437	500555	567840	567067	568084
L	369	507020	150/144	150/202	154/5/9	34/49/	134/014	34//34	74,	, , , , ,	
	370	568202	568319	568436	568554	568671	568788	508905	509023	509140	50925/
1	37 E	569374	569491	509008	509725	509842	469959	570070	571250	571476	571502
ı	372	570543	570000	570770	1570093	572174	572201	572407	572522	572630	571 592 57 2 755 573945
	373	571709	C72088	572104	572220	573336	573453	573568	573684	573800	5739 - 5
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	376		C7 6702	C7 54 10	67 C C 2A	1775050	575705	575000	15759901	5/0111	5/00
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	378	277469	C77007	[7772]	1577820	1577051	\$7.0000	570101	1570295	5/0410	3/43-3
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	381	580925	581039	281123	581267	581381	581495	581008	581722	501030	282085
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	383	583199	583312	503420	1503539	.584787	584896	\$ \$ \$ \$ \$ \$	585122	585236	585348
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	387	587711	587822	587935	588047	588160	588272 589391	588384	588496	588608	588720
	388	588832	588944	589056	589167	589279	589391	589503	589615	589726	589838
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-	390			1000087	501200	501510	601621	501722	1501843	591955	592000
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	393		404601	1:04DT2	1004774	1004014	COAUAC	1401011	1141141	1797-/~	137331
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	3 97 3 98	500882	(99002	600101	600210	600319	600428	600537	600646	600755	600864
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460	662758	662852	662947	663041	663135	663230	663324 664266 665206	663418	963512	663607
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462	664642	664736	664830	664924	665018	666040	665206	065299	1665393	60,437
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47 I 472	673942	674024	674126	074218	674310	674402	671101	671586	671677	67.1760
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477 478	678518 679428	670610	670610	670700	670701	670882	670072	630062	6801.4	079337
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519	715167	/15251								
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520	716303 716838	710087	710170	710254	710337	710421	710504	717421	717504	710754
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605	781755	781827	781800	781071	782042	782114	782186	782258	782320	782401
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626	796674	796644	706712	796782	706852	706021	796990	797060	707120	707108
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١	717	855510	855580	855640	855701	855761	855822	855882	855043	8:6003	8 56064
ł	718	856124	856185	856245	856306	856366	856427	856487	856548	855398 856003 856608	·· 56668
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ľ	720	357332	857393	857453	857513	857574	857634	857604	857754	857815	857875
1	721	857935	857995	858056	858116	858176	858236	858297	858357	858417	858477
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1	724	859739	959799	859858	859918	859978	860038	860098	860158	860218	860278
I	725	860338	860398	860458	860518	860578	860637	860697	860757	860 8 17 861415	860877
1	726	860937	86.0990	801050	861110	86.	801230	86.8.	861355	861415	861475
1	727 728	862121	862101	862251	862210	862270	862420	862480	862540	862012 862608	862668
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ŀ										863798	
1	730 731	862017	862077	864026	864006	18641	864214	864274	864222	864202	864450
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1	742	870404	8710402	871106	870579	871222	87128	107U755	821209	870872 871456 872040	870930
1	7 43 744	871572	871621	871600	871744	871806	87186	871022	871081	872010	872002
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ı	748	873902	873960	874018	874076	874134	874192	874250	874308	874366	874424
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١	752	876218	876276	876333	876391	876449	876507	876564	876622	876680	876737
1	753	187670C	876XC2	876010	876068	`877026	1 X 7 7 0 X 2	. Xマフミム レ	X77IOX	377250	877211
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ł	755 756	878522	87822	8-26-	27860-	87875	878800	9782 92	878349	878981	870000
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Į	759	880242	880299	880356	880413	880471	885528	880585	880642	880699	880756
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789			897187							
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813	909556	910144	10197	10251	10304	10358	10411	10464	10518	10571
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843	02(828	925879	925031	925982	926034	92608	926137	925673	926239	926291
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847 848	028206	92/935	92/900	928640	928601	028652	028702	928754	928806	028856
849								929266		
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860	024408	24540	221500	0346:0	024700	024751	024801	934852	024002	024053
861	035002	25054	2343991	035154	934/00	934/31	934301	935356	937496	01(762
862	93550719	35558	335608	935658	935709	935759	935809	935860	935910	935960
863	936011	36061	36111	936162	936212	936262	936313	936363	936413	936463
864 865	930514 9	36564	30014	930064	930715	930705	930015	936865	930916	930966
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882	945460	945518	945074	945616	94:66	945715	1945764	1945813	945862	9450
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889	048000	94800	1948999	946048	94000	910146	94010-	940244	940202	ومموا
893	949390	949439	949488	949536	949585	949034	949083	949731	949780	94982
891	949878	949926	949975	950024	950073	950121	950170	950219	950267	95031
892	950365	950413	950462	950511	950560	950608	950657	950705	950754	95080
893	950851	950000	950949	950997	951046	951095	951143	951192	951240	95128
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895	951822	1951872	951435	1951960	1952017	952066	952114	1952163	952211	95320
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916	961895	51961943	3†961 99 0	0 962038	3 962085	1962132	2 962 180	962227	962275	196212
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925	0661	3 066 19	3:06620£	066-0-	066	1066	10664	1066	0665-	066.4
925	0666	1.0666	9 966236 8 966705	10667	066	0669	0668	066-	066004	lo6
920 927	06700	7:067	7 06~	0677	106706	06	1066	106	0674	06-
927 928	997080	0.907127	7 907173	3;907220	0 907207	7 907314	41007301	11907408	1.9 0 7454	1907 CC
	10600	5 0600	5 967642	1069-	1069	907782	1907829	1907875	yu7922	y0796
929	968016	968062	2 968109	968156	968203	968249	91968296	968343	968389	95843
930	968483	3.968530	0;968576	968623	968670	968716	6-968763	968810	968856	96890
931	968950	o 968996	6'969043	3¦969090	o 9 69 136	969183	11969229	969276	969323	196936
932	909410	b, 969462	2 969509	9 969556	5 969602	2'969 6 49	9:969695	969742	2i969788	196983
933	909882	3 ;969928	81969975	970021	1970068	31070114	1 070161	1970207	970254	197030
933	979347	7 970393	3,970440	1970486	51070522	1070670	a ∙070626	1070672	070710	107076
	1970812	2,970851	81970g04	11970951	11070007	' 07 IO44	11071000	0 071127	. 041185	167122
	7, -017	\$ 07 1 22	1'071-6	1071	1077-57	10/1044	1971090	9/1137	7/1103	7/12:
935	100		2 97 1 3 0 9	1197 (415	1971401	1 971508	971554	1 g71600	971047	197160
935 936	971740	J1971780	0 071812		11071026		1 A7901X	いっててのわき		10721
935 936 937	971740	J1971780	0 071812		11071026		1 A7901X	いっててのわき		10721
935 936 937 938	971740	J1971780	0 071812		11071026		1 A7901X	いっててのわき		10721
935 936 937	971740	J1971780	6 971832 9 972295 2 972758		11071026		1 A7901X	いっててのわき		10721

No.	0	l i	2	3	1 4	5	6	7	8	9
940	072128	073174	073220	973266	973313	973359	973405	973451	973497	97354
941	973590	973174 973636	973682	973728	973774	973820	973866	973913	973959	97400
942	1074061	1074007	1974143	Q7418Q	1974235	974281	974337	1974373	1974420	197440
943	974512	974558	974604	974650	974696	974742	974788	974834	97488c	97492
944	974972	975018	975064	975110	975156	975202	975248	975294	975340	97538
945	975432	975478 97 59 37	975524	975570	975010	076121	975707	975753	975799	07620
946 947	975350	976396	076442	076487	976533	976170	076625	076671	976717	47676
948	9768c8	976854	976900	976946	976991	977037	977083	977129	977175	97722
949	977266	977312	977358	977403	977449	977495	977541	977586	977632	97707
950	977724	977760	977815	977861	977906	977952	977998	978043	978089	97813
. 951	1078 280	078226	078272	078217	078262	078400	0784C4	978 (00)	078646	9784
952	978637	978683 979138 979594	978728	978774	978819	978865	978911	978956	979002	97904
953	979093	979138	979184	979230	979275	979321	979300	979412	979457	97950
954	979548	979594 980049	979039 0 800 04	979005	080184	979770	080276	080222	080267	9/995
955 956	080458	080502	480540	080 044	080640	080685	980730	980776	080821	98086
957	980912	980957	981003	981048	981093	981139	981184	981229	951275	98132
958	1081304	981411	981456	981501	981547	981592	981037	981083	981728	98177
959	981819	981864	981909	981954	982000	982045	982090	982135	982181	98222
960	081271	082216	082262	082407	082452	082407	982543	982488	482622	98267
961	982723	982769 983220	982814	982859	982904	982949	982994	983040	983085	98313
962	983175	983220	983265	983310	983356	983401	983446	983491	983536	98358
963	983020	983671	983710	983702	903807	903052	983897	983 94 2	084427	08448
964 965	084527	984122 984572	084617	084662	084707	084752	084707	084842	084887	08403
966	1084077	08 (022	08(067	OXCIIZ	1006167	08 (202)	9852471	08 (202	985337	98538
967	1985426	985471	985516	985561	985606	985051	985090	9×5743	985780	985831
968	1086876	08 (020	300780	.080010	10860551	080100	980144	981089	900234	98027
969	986324	 986369	986413	986453	986503	980548	980593	980037	980082	98072
970	986772	986816	986861	986906	986951	986995	987040	987085	987130	98,17
971	10×7210	0X7364	087200	1087767	1987798	087447	0074071	987672	1407577	40104
972	987000	987711	987750	987800	088201	088226	088281	985426	088470	98851
973	088440	987711 988157 988603	088648	088603	908737	u88782	988826	088871	988915	98896
975	980005	989049 989494	989094	989138	989183	989227	989272	989316	989361	98940
976	989450	989494	989539	989583	989628	989672	989717	989761	989806	989850
977	989895	989939 989383	989983	990028	990072	990117	990161	990206	990250	990294
978	990339	990383	990428	990472	990510	990501	990005	990050	990094	990731
979	990783	990827	990871	990910	990900	991004	991049	991093	99113/	99.10.
980	991226	991270	991315	991359	991403	991448	991492	991530	991580	99102
981 982	1991009	991713	991757	002244	991040	991890	991934	991979	99246:	99250
983	903563	992156	992642	992686	992710	992774	992818	992863	992007	99295
984	1002006	002020	002032	002127	10021721	001210.	00 22001	00 2 2 0 4 1	001140	99339
985	1002426	002480	002524	003508	003013	993047	9937011	9937451	993789	99303.
986	1002877	002021	001000	004000	0040(3	994097	9941411	QQ4 1 8 S I	994229	99427:
987	994317	994361 994801	994405	994449	994493	994537	994501	994025	994009	99471
988	1994757	994801	006284	00 5 228	994953	995416	995460	995404	995547	33.3.
	277.70	995679	777204	23,320	2237	00.5854	005808	00504	00 5486	006024
990	006074	1006117	1016161	loo620c	006240	000202	000220	000 1801	000424	99040
991	006412	996117	996500	996642	996687	996730	996774	996818	996802	99690
993	996440	996555 996993 997430	997037	997080	997124	997168	997212	997255	997299	99734.
994	997386	997430	997474	997517	997561	997605	997648	997691	997736	99777
995	100-X72	こののマギのマ	'007010	1007054	1007008	COSUAI	44606	1440140	4401/6	199021
996	998259	998303	998346	1998390	998434	990477	0080521	990504	9900042	99908
997	1998095	998303 998739 999174	990702	000261	330300	32-313	999302	999435	999478	99952
779	999565	999609	999652	999696	999739	999783	999826	999870	499913	99995
	0	333.5	2	3	4	5	6.	7	8	9
1		·								

Logarithmic Sines, Tangents, and Secants:

This table contains the logarithmic, or, as they are sometimes called, the artificial sines, tangents, and secants, to each degree and minute of the quadrant, with their complements or co-sines, co-tangents, and co-secants, to six places of figures besides the index.

To find the Logarithmic Sine, Co-Sine, &c. of any Number of Degrees and Minutes.

If the given degrees be under 45, they are to be taken from the top, and the minutes f om the left side column, opposite to which in that column with the name of the legarithm at the top, will be found the required logarithm. But if the degrees be more than 45, they will be found at the bottom of the page, and the minutes in the right side dolumn; likewise the name of the logarithm is to be taken from the bottom of the page.

When the given degrees exceed 90, they are to be subtracted from 180 degrees, and the logarithm of the remainder taken out as before. Or the logarithmic sine, tangent, &c. of degrees more than 90, is the logarithmic co-sine, co-tangent, &c. of their excess above 90 degrees.

BXAMPLES.

		•	•		logarithm:
Required	the log. sine of	36	32	-	9.774729
· •	co-sine of	61	18	-	9.681443
	tangent of	54	17	-	10 143263
	co-tang. of	42	50	-	10.032877
	secant of	19	27	•	10.025519
	co-secant of	70	33	-	10.025519
	sine of	108	36		•
4	or sine of	71	24	•	9.976702
•	or co-sine of	18	36		

To find the Degrees and Minutes nearest corresponding to a gives Logical rithmic Sine, Co-sine, Gr.

Look in the column marked at the top or bottom with the name of the given logarithm, and when the nearest to it is found, the corresponding degrees and minutes will be those required, observing that when the name is at the top of the column, the degrees are to be taken from the top and the minutes from the left side column, but if the name is at the bottom, the corresponding degrees will be there likeness, and the minutes in the right side column.

EXAMPLES.

The degrees and minutes corresponding to the

log. sine	9.265390	are	100	37'
co-sine			70	
tangent	9.70156		26	42
•	10.25413		5 6	9

The logarithmic sines, &c. taken out to degrees and minutes only are in general sufficiently accurate, but in some of the more rigid astronomical calculations, it is frequently necessary to take them out to the nearest second; when this is the case they are to be found in the following manner:

To find the sine, tangent, &c. of an arch expressed in degrees, minutes and seconds.

RULE.

Find the sine, tangent, &c. answering to the given degree and minute, and also that answering to the next greater minute; multiply the difference between them by the given number of seconds, and divide the product by 60; then, the quotient added to the sine, tangent, &c. of the given degree and minute, or subtracted from the co-sine, co-tangent, &c. will give the quantity required, nearly.

If the arch be less than three degrees, it will be necessary to use the

following rule ---

To the arithmetical complement of the given degrees and minutes reduced to seconds, add the logarithm of the given degrees, minutes, and seconds, reduced to seconds, and the log.-sine, tangent, &c. of the given degrees and minutes, the sum, rejecting 10 from the index, will be the log.-sine, tangent, &c. of the proposed number of degrees, minutes, and seconds.

To find the degrees, minutes, and seconds, answering to a given logarithmic sine, tangent, &c.

RULE.

Find the degrees minutes and seconds answering to the next less logarithmic sine, tangent, &c. which subtract from that given; multiply the remainder by 60, and divide the product by the difference between the next less and next greater logarithms, and the quotient will be the seconds to be annexed to the degrees and minutes before found.

If the given logarithm is that of the sine or tangent of a small arch—then, to the arithmetical complement of the next less logarithm in the tables, add the given logarithm, and the logarithm of the degrees and minutes, in seconds, answering to the next less logarithm, the sum, rejecting radius, will be the logarithm of the number of seconds in the required arch.

		.	Sine 0	Degree.		-	
M	0"	10"	20"	30"	40"	50"	
0		5.685575	5.986605	6.162696	6.287635	6.384545	59
1	6.463726	6.530673	6.488665	6.639817	6.685575	6.726967	58
2	6.764756	6.799518	6.831703	6.861666	6.889695	6.916024	57
3	6.940847	6.964328	6.986605 7.100548	7.007794	7.027997	7.047303	56
4	7.065786 7.1626 96	7.083515	7.190725	7.204089	7.217054	7.147973	55
5	7.241877	7.253776	7.265358	7.276639	7.287635	7.298358	53
I 7	7.308824	7.319043	7.329027	7.338787	7-348332	7.357672	52
8	7.366816	7-375770	7.384544	7-393145	7.401578	7.409850	51
9	7.417968	7.425937	7.433762	7-441449	7.449002	7-456426	_50
10	7.463725	7.470904	7.477966	7.484915	7-491754	7.498487	49
11	7.505118	7.511649	7.518083	7.524423	7.530672 7.566387	7.536832	48
12	7.54290 6 7.577668	7.548897 7.583201	7.55480 6 7.5886 64	7.560635	7.599388	7.572065 7.604652	47 46
14	7.609853	7.614993	7.620072	7.625093	7.630056	7.634963	45
16	7.639816	7.644615	7.649361	7.654056	7.658701	7.663297	44
15	7.607844	7.672345	. 7.676799	7.681208	7.685573	7.689894	43
17	7.694173	7.698410	7.702606	7.706762	7.710879	7.714957	43
18	7.718997	7. 722999 7.746270	7.726965 7.750031	7.730896 7.753758	7.734791 7.757454	7.738651	41 40
-	7.742477						-
20 21	7.764754 7.785943	7.768358 7.789376	7.771932	7.775477 7.796162	7.778994 7.799515	7.782482	39 38
22	7.806146	7.809423	7.812677	7.815905	7.819111	7.822293	37
23	7.825451	7.828586	7.831700	7.834791	7.837860	7.840907	36
24	7.843934	7.846939	7.849924	7.852888	7.855833	7.858757	35
25	7.861662	7.864548	7.867414	7.870262	7.873092	7.875902	34
26 27	7.878695 7.895085	7.881470 7.89775 8	7.884228	7.886968 7.903054	7.889690 7.905678	7.89239 6 6.908287	33
28	7.910879	7.913457	7.900414	7.918566	7.921098	7.923616	32 31
29	7 926119	7 928608	7.931082	7-933543	7.935989	7.938422	30
30	7.940842	7.943248	7.945641	7.948020	7.950387	7.952741	29
31	7.955082	7.957410	7.959727	7.962031	7.964322	7.966602	28
32	7.968870	7.971126	7.973370	7.975603	7.977824	7.980034	27
33	7.982233	7.984421	7.986598	7.988764	7.990919	7.993064	26
34	7.995198 8.00778 7	7.997322 8.009850	7.999435 8.011903	8.001538 8.013947	8.003631 8.015981	8.005714 8.018005	25
35 36	8.020021	8.022027	8.014023	8.026011	8.027989	8.029959	24 23
37	8.031919	8.033871	8.035814	8.037749	8.039675	8 041592	23.
38	8 043501	8.045401	8.047294	8.049178	8.051054	8052922	21
39	8.054781	8.056633	8.058477	8.060314	8.062142	8.063963	20
40	8.065776	8.067582	8.069380	8,071171	8.072955	8.074731	19
41	8.076500	8.078261	8.080016	8.081764	8.083504	8.085238	18
42	8.086965	8.088684	8.090398 8.100537	8.092104	8.093804 8.103864	8.095497	17
43 44	8.097183 8.107167	8.098863 8.10880g	8.110444	8.102204 8.112074	8.113697	8.105519 8.115315	16
45	8.116926	8.118532	8.120131	8.121725	8.123313	8.124895	14
46	8.126471	8.128042	8.129606	8.131166	8.132720	8.134268	13
47	8.135810	8.137348	8.138879	8.140406	8.141927	8.143443	12
48	8.144953	8.146458	8.147959	8-149453	8.150943	8.152428	1.1
49	8.153907	8.155382	8.156852	8.158316	8.159776	8.161231	10
50	8.162681	8.164126	8 165566	8.167002	8.168433	8.169859	9
5°.	8.171280	8.172697 8.181102	8.174109 8.182488	8.175517 8.183868	8.176920	8.178319 8.186617	1
52 53	8.179713	8.189348	8.190707	8.192062	8.185245	8.194760	6
54	8.196102	8.197440	8.198774	8.200104	8.201430	8.202752	
55	8.204070	8.205384	8.206694	8.208000	8.209302	8.210601	5
56	8.211895	8.213185	8.214472	8.215755	8.217034	8.218309	3
57 58	8.219581	8.220849 8.228380	8.222113 8.229622	8.223374 8.230861	8.224631	8.225884 8.233328	2 I
59	8.227133 8.234557	8.235782	8.437003	8.238221	8.232096 8.239436	8.240647	0
	6011	50'	40''	30"	20//	10"	M
	721	30	Resine 10		AU.		

Ge-sine \$9 Degrees.

LOGARITHMIC TANGENTS.

Tangent O'Degree,

			Tangent (Degree,			
м	0"	10"	20'	30.,	40"	50"	
0		5.685575	5.986605	6.162696	6.287635	6.384545	59
I r	6.463726	6.530673	6.588665	6.639817	6.685575	6.726968	58
2	6.764756	6.799518	6.831703	6.861666	6.889695	6.916024	57
3	6.940847	6.964329	6.686605	7.007794	7.027998	7.047303	56
4	7.065786	7.083515	7.100548	7.116939	7.132733	7-147973	55
5 6	7.162696	7.176937	7.190725	7.204089	7.217054	7.229643	54
	7.241878 7.308825	7.253777 7.319044	7.265359 7.329028	7.276640 7.338788	7.287635 7.348333	7.298359 7.357673	53 52
7	7.366817	7.375772	7.384546	7.393146	7.401579	7.409852	51
9	7.417970	7.425939	7.433764	7.441451	7.449004	7.456428	50
10	7.463727	7.470906	7.477968	7.484917	7.491756	7.498490	49
111	7.505120	7.511651	7.518085	7.524426	7.530675	7.536835	48
12	7.542909	7.548900	7.554808	7.560638	7.566390	7.572068	47
13	7.577671	7.583204	7.588667	7.594062	7.599391	7.604655	46
14	7.609857	7.614996	7.620076	7.625097	7.630060	7.634968	45
. 15	7.639820	7.644619	7.649366	7.654061	7.658706	7,663301	44
16	7.667849	7.672350	7.676804	7.681213	7.685578	7.689900	43
17	7.694179	7.698416	7.702612	7.706768	7.710885	7.714962	42
. 18	7.719003	7.723005	7.726972	7.730902	7.734797	7.738658	41
19	7.742484	7.746277	7.750037	7.753765	7.757462	7.761127	40
20	7.764761	7.768365	7.771940	7-775485	7.779002	7.782490	39
21	7.785951	7.789384	7.792790	7.796170	7.799524	7.802852	38
22	7.806155	7.809432	7.812686	7.815915	7.819120	7.822302	37
23 24	7.825460	7.828596	7.831710	7.834801	7.837870	7.840918	36
25	7.843944	7.846950 7.864560 .	7.849935 7.867426	7.870274	7.855844	7.875915	35
26	7.878708	7.881483	7.884240	7.886981	7.889704	7.892410	1.33
27	7.895099	7.897771	7.900428	7.903068	7.905692	7.908301	32
28	7.910894	7.913471	7.916034	7.918581	7.921113	7-923631	31
29	7.926134	7.928623	7.931098	7 933559	7.936006	7.938439	30
30	7.940858	7.943265	7-945657	7.948037	7.950404	7:952758	29
31	7.955100	7.957428	7.959745	7.902049	7.964341	7.966621	28
32	7.968889	7.971145	7.973389	7.975622	7.977844	7.980054	27
33	7.982253	7.984441	7.986618	7.988785	7.990940	7.993085	26
34	7.995219	7.997343	7.999456	8.001560	8 003653	8.005736	25
35	8.007809	8.009872	8.011926	8.013970	8.016004	8.017029	24
36	8.020044	8.022051	8.024047	8.026035	8.028014	8.029984	23
37 38	8 031945	8.033897 8.045428	8.035840	8.037775	8.039701	8.041618	22
39	8.043527	8.056661	8.058506	8.049205 8.060342	8.062171	8.052949 8.063992	20
40	8.065806	8.078293	8.069410	8.071201	8.072985 8.083536	8.074761	19
1 42	8.086997	8.088717	8.090430	8.092137	8.093837	8.095530	17
43	8.097217	8 098897	8.100571	8.102239	8.103899	8.105554	16
1 44	8.107202	8.108845	8.110481	8 112110	8.113734	8.115352	15
45	8.116963	8.118569	8.120169	8.121763	8.123351	8.124933	14
46	8.126510	8.128081	8.129646	8.131206	8.132760	8.134308	13
47	8.135851	8.137389	8.138921	8.140447	8.141969	8.143485	12
48	8.144996	8.146501	8.148001	8.149497	8.150987	8.152472	11
49	8.153952	8.155426	8.156896	8.158361	8.159821	8.161276	10
50	8.162727	8.164172	8.165613	8.167049	8.168480	8.169906	9
51	8.171328	8.172745	8.174158	8.175566	8.176969	8.178368	
52	8.179763	8.181152	8.182538	8.183919	8.185296	8.186568	7 6
53	8.188036 8.196156	8.189400	8.190760	8.192115	8.193466	8.194813	
54	8.204126	8.197494 8.205440	8.206750	8.200159	8.201485 R 200250	8.202808 8.210658	5
55 56	8.211953	8.213243	8.214530	8.215814	8.209359	8.218369	4
57	8.219641	8.220909	8.222174	8.223434	8.224692	8.225945	3 2
58	8.227195	8.228442	8.229685	8.230924	8.232160	8.233392	i
59	8.234621	8.235846	8.237068	8.238286	8.239501	8.240713	0
	60"	50"	40"	30"	20"	10"	м
]	1 55	. 55	1 37	1 00	1 20	1 10	1 20

Co-Cugent 89 Begrees-

Sine 1 Degree

,			Sine 1 I	egree			
м	0′′	10"	20"	3077	40"	50"_	·
0	8.241855	8.243060	8.244261	8.245459	8.246654	8.247845	59
1	8.249033	8.250218	8.251400	8.252578	8.253753	8.254925	58
2	8.256094	8.157260	8.258423	8.259582	8.260739	8.261892	57
3	8.263042 8.269881	8.264190 8.271010	8.265334 8 272137	8.266475	8 267613 8.274381	8.268749 8.275499	56
4	8.276614	8.277726	8.278835	8.273260 8.279941	8.281045	8.282145	55
5 6	8.283243	8.284339	8.285431	8.286521	8.287608	8.288692	53
7	8.289773	8.292852	8 29 1928	8 293002	8.294073	8.295141	52
8	8.296207	8.297270	8.298330	8.299388	8.300443	8 301496	51
9	8.302546	8.303594	8.334639	8.30,681	8.306711	8.327759	50
10	8.308794	8.304827	8.310857	8.311885	8.312910	8.313933	49
11	8.314954	8.315972	8.316987	8.318001	8.319012	8.320020	48
12	8.321027	8.322031	8.323033	8.324032	8.325029 8.330964	8.326024	47 46
13	8.327016	8.328007 8.333901	8.328995 8.334876	8.329980 8.335848	8.336819	8 331945 8.337787	45
15	8.332924 8.338753	8.339717	8 3406-8	8.341638	8.342596	8.343551	44
16	8.344504	8.345455	8.346405	8.347352	8.348297	8 349240	43
17	8.350180	8.351119	8.352056	8.352991	8.353924	8 354855	42
18	8.355783	8.356710	8.357635	8.358558	8.359479	8.360398	41
19	8.361315	8.362230	8.363143	8.3640;4	8.364964	8.365871	40
20	8.366777	8.367681	8.368582	8.369482	8.370380	8.371277	39
21	8.372171	8.373063	8.373954	8 374843	8.375730	8.376615	38
22	8.377499	8.378380	8.379260	8.380138	8.381015	8.381889	37
23 24	8.382762 8.387962	8.383633 8.388823	8.384502 8.389682	8.385370	8.386236 8.391395	8 392249	36 35
25	8.393101	8.393951	8.394800	8.390539 8.347	8.396493	8.397337	34
26	8.398179	8.399020	8.399859	8.40696	8.401532	8.402366	33
27	8.403199	8.404030	8.404859	8.405687	8 406513	8.407338	32
28	8.408161	8.408983	8.409803	8.410621	8.411438	8.412254	31
29	8.413068	8.413880	8.414691	8.415500	8.416308	8.417114	30
30	8.417919	8.418722	8.419524	8.420324	8.421123	8.421921	29
31	8.432717	8.423511	8.427304	8.425396	8.425886	8.426675	28
32	.8.427462	8.428248	8.429032	8.429815	8 430597	8.431377	27 26
33	8.432156 8.436800	. 8 432933 8.437569	8.433709 8.438337	8.434484 8.439103	8.435257 8.439868	8.436029 8.440632	25
35	8.441394	8.442155	8.442915	8.443674	8.444431	8.445186	4
36	8.445941	8.446694	8.447446	8.448196	8.448946	8.449694	23
37	8.450440	8.451186	8.451930	8.452672	8.453414	8.454154	22
38	8.454893	8.455631	8.456368	8.457103	8.457837	8.458570	21
39	8.459301	8.460032	8.460761	8.461489	8.462215	8.462941	20
40.	8.463665	8.464388	8.465110	8.465830	8.466 -50	8.467268	39
41	8.467985	8.468701	8.469416		8.470841	8 471553	18
42	8 472263 8.476498	8.472971	8.473679	8.474386	8.475091	8.475795	17 16
43 44	8.480693	8.477200 8.481388	8.477901 8.482082	8.478601 8.482775	8.479299 8.483467	8 479997 8.484158	15
45	8.484848	8.485536	8.486224	8.486910	8.487596	8.488180	14
46	8.488963	8.489645	8.490326	8.491006	8.491685	8-492363	13
47	8.493040	8.493715	8.494390	8.495064	8.495736	8.496408	12
48	8.497078	8.497748	8.498416	8.499084	8.499750	8.500415	11
49	8.501080	8.501743	8.502405	8.503067	8.503727	8.504386	10
50	8.505045	8.505702	8.506358	8.507014	8.507668	8 508321	9
50	8.508974	8.509625	8.510275	8.510925	8.511573	8.512221	8
52 52	8.512867 8.516726	8.513513 8.517366	8.514157 8.518005	8.514801	8.515444	8.516086	7
53 54	8.520551	8.521186	8.521819	8.518643 8.522451	8 519280 8.523083	8.519916	5
55	8.524343	8.524972	8.525599	8.526226	8.526852	8-527477	4
56	8.528102	8.528725	8.529347	8.529969	8.530589	8.531209	3
57	8.531828	8.532446	8.533063	8.533679	8.534295	8.534909	2
58	8.535523	8.536136	8.536747	8.537358	8.537969	8.538578	1
59	8.539186	8.539794	8.540401	8.541007	8.54.612	8.542216	0
	60''	50".	40"	30"	·20·'	10"	M
			Co-sine 88	1)0,,,,,,,,,,			-

Co-sine 88 Degrees.

Tangent 1 Degree.

	0"	10"	20"	30"	40*	50"	
×							
٥	8.241921	8.243126	8.244328	8.245526	8.340721	8.247913 8.254996	59
1 2	8.249101	8.250287	8 251409	8.25040	8 260811	8.261965	58
3	8.256165 8.263115	8 264262	8.265408	8.266540	8.267688	8.268824	57, 56
4	8.269956		8.272213				55
	8.276691	8.277804	8.278913	8.280020	8.281124	8 282225	54
5	8.283923	8.284419	8:285512	8.286602	8.287689	8.288774	53
7 8	8.289856	8.290935	8.292012	8.293086	8.294157	8.295226	52
	8.296292	8.297355	8.298416	8.299474	8 300530	8.301583	
9	8.302633		8.304727			8.307849	50
10	8.308884	8.309917	8.310948	8.311976	8.313002	8.314025	49
41	8.315046	8.316065	8.317081	8.318095	8.319100	8.320115	48
12	8.321122		8.323129 8.329093				47 46
13 14	8.327114 8.333025	8 424002	8.224077	8.225050	8.226021	8.337890	
15	8.338856		8.340783				44
16	8.344610	8.145562	8.346512	8.347459	8.348405	8.349348	+3
17	8.350289	8.351229	8.352166	8.353101	8.354035	8.354966	42
18	8.355895	8.356823	8.357748	8.358671	8 359593	8.360512	41
19	8.361430		8.363259			8.365988	40
20	8.366894	8.367799	8.368701	8.369601	8.370500	8.371397	39
21	8.372291	8. 273184	8 374076	8.374965	8.375853	8.376738	38
22	8.377622	8.278604	18.7707861	8. 180203	8.381140	8.382015	37
23	8.382889	8.383760	8.384630	8.385498	8.386364	8.387229	36
24	8.388092	8.388953	8:389812	8.390070	8 206628	8 0074701	35
25 26	8.393234	8:394085	8.394934	8 400824	8 401670	8.402505	34
27	8.398315 8.403338	8 404170	8.405000	8.406828	8.406655	8.407480	33
28	8.408304	8.400126	8.409946	8 410765	8.411682	8.412399	31
29	8.413213	8 414026	8.414837	8.415647	8 416456	8 417262	30
30	8.418068	8.418872		8.420475		8.422072	
31	8.412869	8422664	8.424458	8.425250	8.426C40	8.426830	28
32	8.427618	8.428404	8.429180	8.429973	8.430755	8.431536	27
33	8.432315	8.422003	8.433870	8.434645	8.435419	436191	26
34	8.436962	8.437733	8.438500	8.439267	8.440033	8.440797	25
35	8.441560	8.442322	8.443082	8,443841	8-444599	8.445355	24
36	8.446110	8.440804	8.447616 8.452104	8.448507	8 452580	8 454220	23
37 38	8.450613	8 45 6808	8.456545	8 467281	8.448016	8.458749	21
39	8.455070 8.459481	8 460212	8.460942	8.461670	8.462308	8.463124	20
				8.466016			
40 41	8.463849 8.468172	8.464572	8.469604	8.470318	8.471021	8.471742	19.
42	8.472454	8.472162	8.473871	8.474570	8.475285	8.47 (000	17
43	8.476693	8.477206	8.478007	8.478798	8.479497	8.480195	16
44	8.480892	8.481588	8.482283	8.482976	8.483669	8.484360	15
45	8.485050	8.485740	8.486428	8.487115	8.487801	8.488486	14
46	8.489170	8.489852	8.490534	8 491215	8.491894	8-492573	13
47	8.493250	×-493927	8.494602 8.498632	8 400000	8 40004	8 1005	12
48	8 497 493	8 407060	8.502625	8.503287	8.503948	8.504608	10
49	8.501298						
50	8.505267	8.505925	8.506582 8.510503	8 511150	8.507893	8 51245	8
51 52	8.509200 8.513098	8 #12744	8.514389	8.515024	8.512677	8.516319	7
52 53	8.516961	8. (17602	8.<18241	8.518880	8.519517	8.520154	6
54	8.520790	8	8.522059	8.522692	8.523324	8.523956	5
55	8.524586	8.626216	8. 525844	8.526472	8.527048	8.527724	4
56	8.528349	8.528971	8.529596	8.530218	8.530340	8.531460	3
57	8.532080	8. 5 22608	8. 222216	8.533933	8.534549	8.535164	2
58	8.535779	8.536392	8/437005	8.537616	0 538227	3 538837	I
59	8.539447		8.540662	0.541209			
. !	60"	50"	40"	30	20"	10"	M

				-				
	0''	-	-	•		, Secant.	Co-se (M
M		_			1alig		Infinite.	60
0	8.24185				builte.	10.000000	13.536274	
1	8.24903					10.000000	13.235244	
2	8.2560g.	:				10.000000		5
3	8.26304			·			12.934214	
4	8.26988			V 3	12 837304		12 837 304	
5	8.2766 8.2832						12.758123	
7	8.28g-		•				12.691176	
8	8.296			. ,06817	12.633183	10 000001	12.633184)
9	8.302			1,970			12.582032	5
10	8.30				12.536273	10.000002	12.536274	5
11	8 31			505120	12.494880	10.000002	12.494882	4
12	8.32		40.00	7.542909	12.457091	10.000003	12.457094	4
13	8.3			7 577672		10.000003	12.422332	
14	8.3			7.609857	12.390143		12.390147	
15	8.3		999وورده د	7.0 39820	12.360180		12.360184	4
16	8.		3 99995	7 007849	12.332151			4
17	8.	•	. 2999995	7.094179	12 305821		12.305827	
18	8.		1.999994	7.719003	12.280997	10.000006		
19	8			7.742484	12.257516		12.257522	4
20	-8		9.999993	7.764761	12.235239	10.000007	12.235246	4
21	٤	3 -3.4		7.785951	12.214049		13.214057	3
22	1	20110	9.9999 <u>9</u> 1		12.193845		12.193854	
23	t	85443		7.825460				3
24		2 - 501934		7.843944		10.000011		
25	1	191562	9.999989		12.138326		12.138338	3
26		5-8695	9.999987	7.878708	12.121292		12.121365	3
27 28	6	- 195085		7.910894	12.089106	-	12.089121	3
- 1	53	- 926119	9 999985	7.926134	12.073866		12.073881	3
29	84	- 040842	9.999983		12.059142	-	12.059158	3
30		7.955082	9.999982			10.000018	12.044918	2
31	F 1	7.968870	9.999981		12.031111			2
32 33	4 1	7.982233		7.982253			12.017767	2
34		7.995198	9 9 9 9 9 7 9					
35		8.007787	9.999977	8.007809	11.992191		11 992213	2
3	36	8 020021	9.999976	8.020045	11.979955		11.979979	2
-	137	8.031919	9.999975		11.968055	10.000025	11.968081	2
	38	8.043501	9.999973	8.043527	11.956473		11.956499	2
	39	8.054781	9.999972		11.945191	10.000028	11 945219	2
	40	8.065776	9 999971	8.065806	11.934194	10.000029	11.934224	2
	1 1	8 076500	9.999664	8 076531	11.923469	10.00031	11.923500	1
		8.086965	9.999968	8.086997	11.913003	10.000032	11 913235	1
	43	8.097183	9.999966					1
		8.10716-		8.107202		10.000036		1
		8.116926	9.999963		11.883037		11 883074	
		8.126471	9.999961			10.000039	11.873529	
		8.135810	9 999959			10.000041	11.864190	1
		8.144953 8.153907	9 999958			10.000042 10.000044	11.855047 11.846093	1
	1	8.162681	9.999956 9.999954		11.840048		11.840093	1
			7.777714	0	11 828672			-
		8.171280	9 999952	8 17076	11 020072	10.000048	11.020720	
	1 1	8.179713	9.999450	8 128014	11.820237	10.000050	11.81201	
		8. 18798 5 8. 196 102	0.000046	8 106176	11.803844	10.000052	11.803898	
	11''	8.204070	3.339940	8.20/1126	11.795874	10.000016	11.79:010	
		8.211895	0.000041	8.211052	11.788047	10.000018	11.788104	
		8.219581		8.219641		10.000060	11.780410	ı
		8.227134		8.227195		10.000062		
	59	8.234557			11.765379			
		8.241855	9.999934	8.241922	11.7 (8078	10.000066		1

1 Degree.

				Degree.			
M	Sine.	Co-sine.	Tang.	Co-tang	Secant.	Co-sec.	K
-0	8.241855	9-999934	8.241021	11.758079	10.000066	11.758145	60
1	8.240077	0.000032		11.750898		11750967	59
2				11.743835		11.743906	58
3	10 2			11.736885		11.736958	
4		9.999925		11.730044		11.730119	56
5	8.276614	9.999922		11.723309		11.723386	55
				11.716677		11.716757	54
7				11.710144	10.000082	11.710227	53
8	8.296207	9.999915	8.296292	11.703708	10.000085	11.703793	52
9	8.302546		8.302634	11.697366	10.000087	11.697454	51
10	8.308794	9.999910	8.308884	11.691116	10.000090	11.691206	50
12	8.314954	0.000007	8.215046	11.684954	10.000093	11.685046	49
				11.678878	10.000095	11678973	48
	8.327016	0.000002	8 327114	11.672886	10.000098	11.672984	47
14	8.372924	9 949899	8 333025	11.666975	10 000 101	11.667076	46
15	8.338753	9.999897	8.338856	11.661144	10.000103	11.661247	45
16	8.344504			11.653390	10.000106	11.655496	
17	8 350181	9.999891	8.350289	11.649711	10.000109	11.649819	43
18	8.355783			11.644105	10.000112	11.644217	42
19	8.361315			11.638570		11.638685	41
20	8.366777	9.999882	8.366895	11 633105	10.000118	11.633223	40
21	8.372171	9.999879	8.372292	11.627708	10.000121	11.627829	39
22	8.377499	9.999876	8.377622	11.622378	10.000124	11.622501	38
23	8.382762	9.999873	8.382889	11.617111	10.000127	11.617238	37
24	8.387962	9.999870	8.388092	11.611908	10.000130	11 612038	36
25				11 606766		11.606899	35
26	8.398179	9.999864	8.398315	11.601685	10.000136	11.601821	34
27					10 000139	11.596801	33
28		9.999858			10 000 142		32
29		9 999854	8.413213	11.580787	10.000146	11.580932	31
_30	8.417910			11.581932	10.000149	11.582081	30
31				11.577,131	10.000152	11.577283	29
32				11.572382			28
33	8 432156			11.567685	10.000159	11.567844	27
34				11.563038	10.000162	11.563200	26
35				11.558440	10.000166	11 558606	25
36		9 999831		11.553890		11.554059	24
37 38	8 154803	9.999817	8 455070	11.549387	10.000173		23
39	8.459301	0 000820	8.459481	11.540519	081000.01		21.
40			8.463849		10.000184	11.536335	20
_							
41			8.468172	11.531828	10.000187	11.532015	19
42			8 472454 8.476693		10.000191	11.527737	
43				11.523307	10.000199	11.519307	17
44 45	8 484848	9.999801		11.514950	10.000199	11.515152	15
	ا نہ ذر ما	9.999794		11.510830	10.000206		14
47	8.493040			11.506750	10 000210		13
48		9.999786	8.497293		10.000214	11.502922	12
49	8.501080		8.501298		10.000218		
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51		-		11.490800	10.000226	11.491026	9
1 2	8.512862	0.000760	8.512008	11.486902	10.000271	11.487133	
22	8.516726	0.00076	8.51606	11.483039	10.000235	11.483274	7
				11 479210		11.479449	
				11.475414			5
	8.528102			11.471651		11.471898	
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60	8.542819	9-999735	8.543084	11.456916	10.000265	11.457181	٥
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LOGARITHMS OF NUMBERS:

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760	880814	880871	88092	S0989	881012	881099	881156	881213	881270	881328
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762	881955	882012	88206y	862126	882183	882240	882297	882354	882411	882468
763		1882581	382630	882695	882752	882809	882866	882923	882980	883037
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766 7 6 7	88 705	884863	884000	88406	884022	881078	885125	884102	884682 885248	884706
768	886261	885418	885474	885531	885587	885644	88 4700	885757	885813	886870
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773	888179	888230	888292	888348	888404	888460	888516	888573	888629	888685
774	888741	888707	888853	888909	388g6;	889021	889077	889134	889190	889246
775	889302	889358	889414	889470	889526	889582	889638	889694	889750	889806
776	889862	889918	889974	890030	890086	890141	890197	890253	890309	890365
777	890421	890477	890533	80589	890044	801050	890750	890812	890868	890924
778 779	801627	801503	801640	801705	801460	801816	801872	801028	891426 391983	803030
	109133	91393	2 2226	0,705	8, 1700	0-22	910/2	091920	39.903	8-2019
780 781	802095	802702	802762	802818	1802317	802020	802085	8020404	892540 893096	092595
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784	894316	894371	894427	894482	1894538	894593	894648	894704	894759	894814
785	894870	804925	894980	895036	895091	895146	895201	895257	895312	895367
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787	895975	896030	896085	896140	896195	896251	896306	896361	896416 896967	896471
788	890526	896581	890030	890092	896747	896892	896857	896912	890907	897022
789									897517	
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792 793	800272	800228	800282	800127	800402	800547	800603	800666	8991 6 4 89 9 711	800766
794	800820	800475	800030	844085	000010	000004	000140	000203	900258	000212
795	900367	900422	900476	900531	900586	900640	900695	900749	900258 900804	878000
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797	901458	901513	901567	901622	901676	901731	901785	901840	901894	846106
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802 803	1904174	904228	904283	904337	904391	904445	904499	904553	904607	04001
804	1904715	904/70	005261	9040/0	005472	001126	905040	005624	905148	205202
805									906227	
806	906335	906389	906443	906497	906550	906604	906658	906712	906766	06820
807	1906873	906927	906981	927095	907089	907142	907196	907250	907304 9	207358
808	907411	907465	907519	907573	927626,	907680	907734	78770	907841 9	07895
809	907948	908002	908056	908109	908163	908217	908270	908324	908378 9	08431
810	908485	908539	908592	908646	908699	908753	908807	08860	908914 9	08967
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816	911600	911743	911797	11800	011005	11106	01200010	12062	12116 9	12160
817	912222	912275	912328 9	12381	912435 0	12488	912541 9	12594	1264719	12700
818	912753	12806	12859	12913	912966	13019	13072	13125	13178 9	13231
819	913284	13337	13390	13443	913496 9	13549	13602	13655	13708 9	13761
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820	913814	913867	913920	913973	914026	914079	914131	914184	914237	914290
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822	014872	014025	014077	1016030	101 (08 5	1915130	912199	915241	1915294	9153471
823	915400	915453	915505	91555	915011	016101	016242	915769	016240	916401
824	0164:4	n16507	016550	016612	0 L6664	016717	916770	916822	910875	9109271
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828	0 1 8 2 2 2	018082	018126	DIXIXX	0.13240	1018202	018745	918397	910450	81020K
829	918555	918607	918659	918712	918704	918810	918809	918921	910973	919020
830	914078	919130	919183	919235	919287	919340	919392	919444	919496	919549
831	919601	919653	919705	919758	919810	020284	020426	919967 920489	020641	020502
832	920123	020607	020240	92020U	020852	020006	920058	921010	921062	921114
833 834	10211661	021218	921270	021222	021374	921420	921478	1921530	921502	9210341
835	921686	921738	921790	921842	921894	921946	921998	922050	922102	922154
836	922206	922258	922310	922362	922414	922466	923518	922570	922622	922674
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838	933244	923290	923348	923399	923451	923503	943333	923607	924176	024228
839	¥45702)	y-5014	725005	20391/	224485	024530	034585	924124	024602	024744
840	1004006	A 9 4 8 4 A	A 2 4 X A A I	0340511	0.2.500.2	1025054	1426100	924641 925157	424204	44 4001
841 842	025212	026264	025415	025467	925618	1925570	925021	9250731	925724	9257701
843										
844	026242	026204	02644 C	026407	020(48	1920000	1020041	920702	940754	9300051
845										
846	927370	927422	927473	987524	927570	927927	92/074	927730 928242	028202	92/032
847 848	028206	927935	927900	928540	928601	028652	928702	928754	428805	928856
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850	020410	929479	020521	020572	929623	020674	929725	929776	929827	929878
851	020020	029981	930032	930083	930134	930185	930236	929776 930287	930338	930389
852	102044O	0.704011	010(41	1030493	930043	1930094	195-/45	1930/90	93004/	220000
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857	932981 933487	933031	933082	933133	933183	933234	933285	933335	933386	933437
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859	19139931	9340441	9340941	934145	934195	934240	934290	93454/	93439	y3444 •
860	024408	024540	02.1500	024650	934700	934761	934801	934852	934902	9349 (3)
861	ina consi	025054	025104	026164	025206	026266	10 1 2 200	10353501	0111400	0167671
862 863	In that I	0260BI	020111	0201021	020212	0 70 202	1940616	935860 936363	4 404 4	4 6 9 4 0 4 8
864	1026554	026661	026614	0.26664	026716	020766	1030015	9308041	910910	030000
865	1027016	027006	937110	037107	937217	937207	1937347	9373071	93/410	93/4091
866	1027518	022-68	027618	0276681	027718	(a 27790)	1037810	0170001	977919	@ 2 7 Q O Q I
867	DIOXXOIA	0.13000	018110	0 28 100	918210	938209	938319	930370	930410	930470
868								939369		
859	939020	9394/0	939120	3391/0	739220	9397/5	030810	020868	020018	030069
870 871	939519	939509	939019	939009	040218	040267	939019	939868 940367	040417	949467
872	740516	0.40 : 66	910616	040666	940716	040765	010812	940865	940915	940904
873	041014	041064	041114	041161	041213	941263	941313	941302	941412	941402
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87.7 87.8	043000	013144	943099	043642	943602	943742	943791	943841	943890	943939
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880	944483	044532	044681	044621	044680	044720	044770	044828	944877	
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894	951337	951386	951435	951483	951532	951580	951620	951677	951240 951726	951774
895	1951823	1961872	1051020	1061000	1052017	0.52066	062114	1052162	0 (2 2 1 1	A CRACOL
896	952308	952356	952405	952453	952502	952550	952599	952647	95 2696 953180 953663	952744
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906	1957140	917170	1957224	1957272	1057720	1957708	1057410	1007404	1057661	0
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909	1958564	958611	958659	958707	958755	958803	958850	958898	958946	958994
910	959041	9 (908)	050137	050184	050232	050280	050228	050276	0 504 12	000478
911	040418	0.50.66	0.0614	0 00661	1050700	050767	0.00804	laca8ca	la conco	100000
912	959995	960042	960090	1960138	960185	1960233	960281	960328	.960376	960423
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917.	1992309	1902417	1903404	1902511	1902559	1902606	1062662	1062701	062748	charack
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923	1905202	905*49	.905290	1905343	1905390	006477	00 (484	1000011	1005178	on:62cl
924	1905072	-905719	∵905700	1905813	1905860	196 (907	:06<954	106600 I	966048	a660ac
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932	909410	,9094 0 2	909509	1909556	909602	'060640	ahabas	060742	060788	nank z c
933	303007	, 909920	909975	970021	1970008	1070114	970161	070207	0702CA	070700
934	17/434/	9/0393	9/044"	1970400	1970577	(070(70	070020	020072	070710	070766
935	9,0012	,9/0050	9/0404	970951	1070007	07 1044	1000	071127	071189	071776
936	17// 4	77.3	9/1309	147 (415)	1971401	'07 I COX	071554	071 BOO	071647	0216001
937 938	. 7/ -/4~(9/1/00	9/1054	97 4079	1971025	071071	072018	072004	072110	073166
939										
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f	940		973174								
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1	951	978180	978226 978683	978272	978317	978363	978409	978454	978500	978546	978591
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1	953	979093	979138	979184	979230	979275	979321	979396	979412	979457	979503
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1	961	082722	108276a	082814	082850	982904	9829491	982994	983040	983085	983130
1	962	983175	983220	983265	983310	983356	983401	983446	983491	983536	983581
ł	963	983626	1983671	983716	983762	983807	983852	983897	983942	983987	984032
I	964	984077	984122	984167	984212	984257	984302	984347	984392	964437	904402
1	965	984527	984572 985022	984017	984002	904707	084752	084797	086202	085227	085282
1	966 967	9°49/7	086471	985516	085561	985606	98,601	98(666	085741	985786	985830
ł	968	085876	985471 985920	985066	086010	986055	986100	986144	986180	986234	986270
1	969	986324	986369	986413	986458	986503	986548	986593	986637	986682	986727
ŀ	970	086772	086816	198986	a86906	986951	986995	987040	987085	987130	987174
1	971	087210	087264	987309	987353	987398	987443	987487	987532	987577	987622
1	972	987666	987711 988157	987756	987800	987845	987890	987934	987979	988024	988068
ł	973	988113	988157	988202	988247	988291	988336	988381	988425	988470	988514
1	974	1088cca	lo886021	988648	088603	908737	(988782)	988820	9888711	988915	988900
ı	975	1084450	989049 989494	OXO E 20	OXOZX2	OXODAX	080072	0807171	OXOTALI	ONGNO	000000
1	976	OZOZOE	IAXAA2A.	. 680083	000028	000072	900117:	9901911	0002001	990250	9902941
ł	977 978	1000110	10001831	990428	990472	990510	1990501	990005	990050	990094	770/30
1	979	990783	990827	990871	990916	990960	991004	991049	991093	991137	991182
Į.	980	001226	991370	215100	991360	991403	991448	991492	991536	991580	991625
1	186	991660	991270	991757	991802	991846	991890	991934	991970	992023	992067
ı	982	002111	002166	902200	002244	QQ2288	1992333.	9923771	992421	992405	19925091
1	983	1002557	002508	992042	1002080	992730	1992774'	992010	9920031	992907	992951
ł	984	1002006	002020	001081	001127	993172	1993210,	993200	0933041	993348	99339#1
1	985	993436	993480	993524	993508	993013	993057	993701	995745	993709	993033
I	986 987	993877	993921 994361	993905	994009	994453	39409/	224.41	00462	994660	994712
1	988	004757	994801	004844	084880	004033	994077	90 (021	995064	995168	995152
1	989	994196	995240	995284	995328	995372	99 416	995460	995504	995547	995591
ŀ	990	00.662	995679	00 5722	095767	00 (811	995854	995898	995042	995086	996030
1	991	1006074	006117	101000	1000205	990249	990293	990230	990380	990424	990400
1	992	1006612	996555	996599	1996643	996687	996730	996774	996818	996862	990905
1	993	laafaaa	aanaa 2	1997037	1007080	007124	QQ7 I 98	997212	9972551	997299	19973431
I	994	007286	097430	997474	997517	497461	1997005	997048	997692	997730	1997? 79 1
1	995		997867								
1	996	998259	998303	1993346	1998390	990434	990477	oognes	000000	000042	000087
1	997	99095	990739	990/02	000261	330000	000378	999302	999435	999478	999522
I	9 98 22 9	999130	999600	999642	999696	999730	999783	999826	999870	499913	999087 999521 999957
ŀ	<u>, A</u>	1227	1999009	2	3	4	5	6.	7	8	9
1		0	1 I	1 4	1 3	1 49	1 3	<u> </u>			

	Sine.	Co-sine.	Tang.	Co-tang.	Secant	Co-sec.	м
м		-	-		-	-	_
0			9.021620			10.980765	60
1				10.977166			59
2				10.975956			58
3				10.974749	10,002426	The second second	57
4			9.026455			10.975984	56
5			9.027655		10.002453	10.974797	55
6			9.028852			10.973614	54
7			9 030046			10.972433	53
8			9.031237			10.971250	5
9			9.032425			10.970082	51
10	9.031089	9-997480	9.033609	10.966391	10.002520	10.968911	50
11	9.032257	9.997466	9.034791	10.965209	10.002534	10.967743	49
12	9.033421	9.997452	9.035969	10.964031	10.002548	10.966579	48
13	9.034582	9-997439	9 037144	10.962856	10.002561	10.965418	47
14	9.035741	9.997425	9.038316	10.961684	10.002575	10.964259	46
15	9.036896	9.997411	9.039485	10.960515	10.002589	10.963104	4
16	9.038048	9.997397	9.040651	10.959349	10.002603	10 961952	44
17		9.997383		10.958187		10.960803	43
18		9.997369		10.957027	10.002631	10.959658	42
19		9.997355		10.955870	10.002645	10.958515	41
20		9-997341		10.954716	10.002659	10.957375	40
21						10.956238	35
		9.997327		2202		- CC - C - C - C - C - C - C - C - C -	38
22		9.997313		10.952418		10.955105	
23			9.048727		10.002701	10.953974	37
24		9.997285				10.952846	36
25			9.051008			10.951721	35
26		9-997257		10.947856	10.002743	10,950600	34
27		9.997242		10.946723			33
28		9.997228		10.945593	10.002772		3
29		9.997214	1 2220	10.944465	10.002786		31
30	9 053859	9.997199	9.056659	10.943341	10.002801	10.946141	30
31	9.054966	9.997185	9.057781	10.942219	10.002815	10.945034	29
32		9.997170			10.002830	10.943929	28
33		9.997156		10.939984		10.942828	27
34		9.997141				10.941729	26
35		9.997127		10.937760		10.940633	2
36		9.997112		10.936652		10.939540	24
37		9.997098		10.935547		10.938449	2
38		9.997083		10.934444	TO COLLA MARKET	10.937361	2.2
39		9.997068		10.933345		10.936276	21
40		9.997053		10.932248	10.002947	10.935194	20
_		-	-00	-			
41	9.065885					10.934115	19
42		9.997024				10.933038	IS
43			9.071027				17
44		9.996994		10.927887	1 A . C. A. C.	10.930893	16
45		9.996979		10.926803			1
46		9.996964		10.925722		10.928758	12
47			9.075356				
48		9.996934		10.923568		10.926634	
49	9.074424		9.077505		10.003081	10.925576	11
50	9.075480	9.996904	9.078576	10.921424	10.003096	10.924520	10
51	9.076533	9-996889	9.079644	10.020350	10.003111	10.923467	9
52			9.080710		10.003126		8
53		9.996858		10.918227		10.921369	7
54			9.082833				7
55		9.996828		10.016100	10.003172		5
56		9.996812		10.015053	10.003188	10.018241	4
	9.082797		9.086000			10.917203	3
C7						10.916168	2
57	0.082822	0.000784	O.OXTOCOL				
58	9.083832			10.912950			
57 58 59			9.087050 9.088098 9.089144	10.911902	10.003234	10.915136	1

7 Degrees.

ī	м	Sine.	Co-sine.	Tang.	Co-tang.	Secant	Co-sec.	· · ·
ŀ	_							- M
1		0 086033	0 006776	LA COOTEST	10 000812	10.003249	10 01-0-8	60
ł	2	0.087047	0.006720	0.001228	10.008772	10.003280	10.013076	59 58
ł	3	0.088070	0.006701	0.042266	10.007734	10.003296	10.01 1070	57
ı	4					10.003312		56
l	- 5	9.00 1008	4.046673	9.044336	10.905664	10.003327	10.008002	55
ı	6	9.092024	9 996657	9.095367	10 904633	10.003343	10.9279761	54
ı	7	9.093037	9.996641	9.096395	10.903605	10.003359	10.906963	53
1	8	9.094047	9.996625	9.097422	10.902578	10.003375	10.905953	52
ŀ	9	9.095056	9.996610	9.098446	10.901554	10.003390	10.904944	51
1	10				10.900532	10.003406	10 903938	50
ľ	11	9.097065	9.996578	9.100487	10.899513		10.902935	49
ı	12	9.098066	9.996562	9.101504	10.898498	10.003438	10.901934	48
1	13	9.099065	9.996546	9.102519	10 897481	10.003454	10.900935	47
ł	14	9.100062	9.996530	9.103532	10.890408	10 003470	10.899938	46
1	15	9.101056	9.996514	9-104542	10.895458	10.003486	10.898944	45
ł	16	9.102048	9.990498	9.105550	10.894450	10.003502	10.897952	44
1			9-996482			10.003518 10.003535	10.896963	43
1	18	0.104025	9.996465 9.996449	9.108560		10.0035351	10.895975	41
ł	:3	0.100002	9.996433	9 100550	10.890441	10.003567	10.894990	40
1-	_							
1			9.996417			10.003583	10.893027	39
ł			9.996384			10.003616	10.891073	38
1	2.5	9.100001	0.006268	0.113522	10.886467		10.890099	37 36
l	25		9.995363	0.114(21	10.885479	10.003649	10.889127	35
ł	26	9:11842	0.006135	9.115507	10.884493		10.888158	34
l	27		9.096318	9.116491	10.883509		10.88719:	33
1	28	9.113774	0.006202	9-117472	10.882528	10.003698	10.886226	32
1	29	9.114737	9.996185	9.118452	10.881548	10.003715	10.885263	31
ł	30	9.115698	9.996269	6.119429	10.881548	10.003731	10.884302	30
ŀ	31	9.116656	9.996252	9.120404	10.879596	10.003748	10.883344	24
ŧ	22	0.117612	9.996235	9.121.377	10.878623	10.003765	10.882387	28
ŧ	22	0.118667	0.006210	9. 122348	10.877652	10.202781	10.881433	27
1	24	9.119519	9.996202	9-123317	10.875583	10.003798	10.280481	26
1	35	9-120469	9.996185	9.124284	10.875716	10 003815		25
ł		9.121417	9.996168	9.125249	10.874751	10.003833		24
l	37	9.122302	9.996151	9 120211	10.873789	10.003849	10.877638	23
I	38	9 123300	9.990134	9.12/1/2	10.872828	10.003866		22
ł		0.124240	0.006100	0.120087	10.870913	10.003883	10.874813	21 20
1-	40							
1	41	9.120125	9.996083	9.130041	10.869959	10.003917	10.873875	19
1	42	9.127000	9.990000	9-130994	10.869006	10.003934	10.872940	18
I	43	0.122024	2.330049	9.132802	10.868056	10.003968	10.871075	17 16
1	44	9.120864	9.996014	9.133830	10.866161	10.003985	10.870146	15
1	46	9.13078	9 99 5008	9.134784	10.865216	10.001002	10 869219	14
1	47	9.131706	9.99;980	9 - 1 3 5 7 2 6	10.864274	10.004020		13
1	48	9.132630	9.995963	9.136667	10.863333	10.004037	10.867370	12
ł	49	9.133551	9.995946	9.137005	10,802395	10.004054		11
1	50	9.134470	9.995928	9.138542	10.861458	17.00.1071	10.865530	10
1	51	9.135387	9.995911	9.139476	10.860524	10.001089		9
1	62	0.126202	.0.00:804	9.110409	10.859591	10.001106		Ý.
ı	53	9.137216	9.995876	9.141340	10.858600	10.001124	10.862784	7 .
ł	54	9.138128	9.995859	9.142209	[10.857731]	10.004141	10.861872	6
1	55	9.139037	9.995841	9.143196	10 856804	10.00+159	10.860963	5
1	56	9-139944	9.995823	9.144121	30.855879	10.004174	10.850056	4.
1	57	9-43850	9.995806	9.145044	10.854955	10.004194	10.859150	3
1	58	9-141754	9.995788	9.145900	.10.054034	10.001212	10.050240	2.
4	59	9.142055	9.995771	0.147802	10.852107	10.004229	10.8:644	1
1.	60							
1	М	Cosinc	5m.	i Ootang.	Tang.	· Co-sec.	Secant.	М

			8 1	Degrees.			
м	Sine.	Co-sine.	Tang.	Co-tang.	Sccant.	Co-sec.	м
-0	9-143555	9.995753	9-147803	10.852197	10.004247	10.856445	60
ì	9.144453		9.148716		10.004265	10.855547	59
2				10.850368	10.004283	10.854651	58
3		9.995699	9.150544			10.853757	57
4		9.995681		10.848546		10.852864	56
5		9.995664	9.152363		10.004336	10.851974	55
6			9.153269			10.850198	54 53
8	9.149802		9.155077	10.844923	10.004390	10.849314	52
و		9.995591	9.155978	10.844022		10.848431	51
τó		9.995573	9.156877	10.843123	10.004427	10.847549	50
11	9.153330	9.995555	9-157775	10.842225	10.004445	10.846670	49
12	1	9.995537	9.158671	10.841329		10 845792	48
13	9.155083		9.159565	10.840435	10.004481	10.844917	47
14			9.160457	10.839543 10.838653	10.004499 10-004518	10.844043	46
15		9.995482	9.161347 9.162236	10.837764		10.842300	45
•	9.157700	0.005446	9.163123	10 836877	10.004554	10.841431	43
17			9.164008		10.004573	10.840565	43
19	17 75 15 5		9.164892	10.835108	10.004591	10.839699	41
20	1		9.165774	10.834226	10.004610	10.838836	40
21	9.162025	9.995372	9.166654	10.833346	10.004628		39
	9.162885	9.995353	9.167532	10.832468		10.837115	38
23	9 163743	9.995334	9.168409	10.831591	10.004666		37
24		9.995316	9.169284	10.830716	10.004684	10.835400	36
25			9.170157	10.829843	10.004703	10.833693	35
26	1	0.005260	9.171899		10.004740		34
27 28	1	9.995241	9.172767		10.004759	10.831992	32
29	1	9.995222	9.173634	10.826366	10.004778	10.831144	31
30	1 -		9.174499	10.825501	10.004797	10.830298	30
31	9 170547	9.995184	9 175362	10 824638			29
32	0.171380	9.995165	9.176224	10.823776		10 828611	28
33		19.995146	,9.177084	10.022910			27
	9.173070	9.995127	9.177942	10.82205E	10.004873	10.826930	26
35			9.178799 9.1796 55	10.820345		10.825256	25
	9.174744	0.005070	9.180508			10.824422	23
37 28	9.176411	9.995051	9.181360			10.823589	22
	9.177242	9.995032	9 182211	10.817789	10.004968		21
	9.178072	9 995013	9.183059	10.816941	10.504987	10.821928	20
41	9.178900	9.994993	9.183907	10.816093	10.005007	10.821100	19
42	9.179726	9.994974	9.184752	10.815248			18
	9.180551	9.994955	9.185597	10.314403			17
44	9.181374	9-994935	9.186439	10.813561	10.005065		16
45	9.182196 9.183016	9.994910	9.187280	10.811880			15
1 40	9.183834	9.994890	9.188958	1	10.005123	10.816166	13
48	9.184651	9.994857	9.189794	10.810206	10.005143		12
1 40	0.185466	9.994838	9.140629		10.005162	10.814534	11
50	9.186280	9.994818	9.191462	10.808538	10.005182		10
51	9.187092	9.994798	9. 192 294		10.005202	10.812908	9
	'A 187001	0 00 1770	0.103124	10.806876	10.005221	10.812097	8
53	9.188712	9-994759	9.193953	10.806047	10.005241	10.811288	7
54	9.189519	9-994739	0.104780	10.805220	10.005281	10.809675	6
55	9.190325	9.994720	0.105120	10.803394	10.00 (100	10.808870	5
67	0.101022	0.004680	0.197253	10.862747	10.005320	10.808067	3
-8	0.102721	0.00.1660	0.108074	10.801926	10.005340	10.807266	2
e n	0.102534	0.004640	0.108804	10.801106	10.00 (300)	10.800466	1
60	9.194732	9.994620	9.199713	10.800287	10.005380	10.805668	٥.
и	Co sine.	Sine.	Co-tang.	Tang.	Co-sec.	Secant.	M
,				legrees			

9 Degrees.

4,	4 'Sine.	Co-sine		, Co-tang	. Secant.	Co-sec.	, м
17	0.104223	0.004620	0.10071	3 10.80028	7 10.00538	10.805668	60
	7.77733	0.004600	0.200 62	10.70047	110.00540	10.804871	59
1 3	10.10.025	0.004580	0 20124	10.70866	10.00542	10.80407	58
						10.803281	
3	9.190719	9.994500	9.20215	79/04	10.005440	10.803281	57
1 4	19.197511	9.994540	9.20297	1110.79702	9 10.00546	10.802489	56
1 5				10.79621		10.801698	,
16	12					10.800909	
7		9.994479	9.205400	o; 10.794600	10.005521	10.800121	53
8	9.200666	9.994459	9.206207	10.79379	3 10.005541	10.799334	52
19	9.201451	9.994438	9.207013	10.792987	10.005562	10.798549	51
10	9.202234	9.94418	9.207817	10.79218	10.00 5 582	10.797766	50
1-							
11						10.796983	49
12	9.203797	9-994377	9.209420	10.790580	10 005623	10.796203	48
113	9.204577	9.994357	9.210320	10 789780	10.005643	10.795423	47
14	9.205354	9.994336	9.211018	10.788982	10.005664	10.794646	46
15	9.206131	9.994316	9.211815	10.788185	10.005684	10.793869	45
16	9.206906	9.994295	9.212611	10.787389	10.005705	10.793094	44
117	9.207679	9.994274	9.213405	10.786595	10.005726	10.792321	43
118	0 2084 52	0.004254	0.214108	10.78 (802	10 00 5746	10.701548	42
19	0.200222	0.004222	0 214080	10.785011	10.005767	10 700778	41
20			0 21 6780	10.784220	10.005788	10.790778	
1					-		40
21	9.210760	9.994191	9 216568	10.783432	10.005809	10.789240	39
22	9.211526	9.994171	9.217356	10.782644	10.005829	10.788474	38
23	9.212291	9.994150	9.218142	10 781858	10 005850	10.787700	37
24	9.213055	9.994120	9.218026	10.781074	10.005871	10.786945	36
25	0.217818	0.004108	9.210710	10.780200	10.005892	10.786182	35
26	9.214579				10.005913	10.785421	34
27				10.778728			
28							33
				10.777948			32
29					10.005976		31
30	9.217609	9 994003	9.223607	10.776393	10.005997	10.782391	30
31	9.218363	9.993982	9.224382	10.77 5618	10 006018	10.781637	20
32	9.219116	0.003060	0.225166	10.774844	10.006040		28
33	9.219868	0.002020	0.225030	10.774071	10 006061		27
					10.006082		26
34							
35				10.772529		10.778633	25
36				10.771761		10.777885	24
37	9.222861					10 777139	23
38	9.223606	9.993832	9.229773	10.770227	10.006168	10.776394	22
39	9.224349	9.993811	9.230539	10.769461	10.006189	10.775651	21
40	9.225092	9.993789	9.231302	10.768698	10.006211	10.774908	20
			9.232065		10.006000		
41				10.767935		10.774167	19
42					10.006254	10.773427	18
43				10.766414		10.772689	17
44					10.006297		16
45					10.006319		15
46					10.006340		14
47	9.230252 9	.993638	9.236614	10.763386	10.006362	10.769748	13
48	9.230984 9	.993616	9.237368	10.762632		10.769016	12
49	1			10.761880	10.006406	10.768285	11
50					10.006428	10.767556	10
51	9.233172 9			10.760378	10.006450	10.766828	2
52				10.759629			8
53	9.234625 9					10.765375	7 6
54	9.235349 9				10.006 5 16	10.764651	6
55	9.23607319			10.757390		10.763927	5
56				10.756646		10.763205	4
57	9.237515 9			:0.755903		10.762485	3
	9.238235 9			10.755161		10.761765	2
					10.006626		i
59 60	9.238953 9			10 25368.			6
	9.239670 9					20.760330	
M	Co sine.'	Sine.	Co-tang	Tang.	Co-sec.	Secant '	ж

M	Sine.	Co-sine.	Tang	Co-tang.	Secant.	Co-sec.	M
	0.220670	2.002251				10.260220	60
0	9.239070	9.993331	9.240319	10.753681	10.000049	10.700330	
1	9.240,30	9.993329	9.24/05/	10.752943	10 036671	10 759014	59
2	19.241121	9.993307	9 -47794	10.752206	10.000093		58
3	9.241814	.Ģ.993285	9. 248 530	10.751470	10.006715	10.758186	57
4	19.242520	9.993252	9.249264	10.750736	10.006738	10.757474	56
	9.343237	9.993240	9.249998	10.750002	10.006760	10 756763	55
				10 749270			54
,	0.211656	0.003:05	6.251461	10.748539	10.006801	10.755344	53
8	10.24:262	0.002172	0.252101	10.747809	10.006828	10.75.1627	52
1 .	19.245353	9.9931/2	3.252.30	10.747080	10.000020	10.754037	5-
	19.240.009	9.995149	9.252920	10.747080	10.0000831		51
10	9.240775	9.993127	9.253046	10.746352	10.006873	10.753225	50
11	0.247478	9.993104	9.254374	10.745626	10.006896	10.752522	49
12				10.744900			48
13	4 248882	0.002060	0.255824	10.744176	10 006041	10.751117	47
123	9.240003	9.993039	9.235024	10.744176 10 743453	10.000941	10.7501.7	46
14	9.249503	9 993030	9.250547	10 743453	10.000904	10.750417	•
115	9.250282	9.993013	9 257209	10.742731	10.000987	10.749718	45
16	19.250980	9.992990	9.257990	10.742010	10.007010	10.749020	44
17	19.251677	9.992967	9.258710	10.741290	10.007033	10.748323	43
18	9.252373	9.992944	9.259429	10.740571	10.007056	10.747627	42
19	9.253067	9.992921	9.260146	10.740571	10.007074	10.746933	41
20	10.253761	9.992808	U-260862	10.739137	10.007102	10.746239	40
							_
21				10.738422			39
22	9.255144	9.992852	9.262292	10.737708	10.007148	10.744856	38
23	9.255834	9.992829	9.263005	10.736995	10.007171	10.744166	37
24	9.256523	9.992806	9.263717	10.736283	10.007104	10.743477	36
25	0 257211	0.002782	0.264428	10.735572	10.007217	10.742780	35
26				10.734862			34
27	0.258682	0 002726	0.265042	10.734162	10.007264	10 741417	37
	9.250503	9.992/30	9.205847	10.734153 10.733445 10.732739	10.00/204	10.741417	33
28	9.259208	19.992713	9.200555	10.733445	10.007287	10.740732	32
29	9.259951	9.992090	9.207261	10.732739	10.007311	10.740049	31
30	9 260633	9.992666	9 267967	10.732033	10 007334	10.739367	30
31				10.731329			20
32				10.730625			28
	9.201994	0.002506	9.209375	10.730025	10.00/301	10.730000	
33	9.2020/3	9.992590	9.270077	10.729923 10.729221	10.007404	10.737327	27
34	9.203351	9.992572	9.270779	10.729221	10.007428	10.730049	26
35	9.264027	19 992549	9-271479	10.728521	10.007451	10.735973	25
36	19.264703	19.992525	19.272178	10.727821	110.007476	10.725207	24
37	9.265377	9.992501	9.272876	10.727124	10.007400	10.734623	23
38	9.2660:1	9.992478	9.272572	10.726427	10.007522	10.72 2040	22
39	0.266722	0.002454	0.274260	10.725731	10.007546	10.733277	21
40				10.725036			20
41	9.268065	9.992406	9 275658	10.724342	10.007504	10.731935	19
42	9.268724	9.992382	9.276351	10.721040	10.007618	10.731266	18
43	9.260402	9.992368	0.277042	10.723649	10.007642	10.730508	17
44	9.270060	0.00222	0.277724	10.722266	10 00766	10.72002	16
45	9.2/0/35	3.994311	9.2/0424	10.721576	10.007009	10.729205	15
46	9.271400	9.992287	19.279113	10.720887	10.007713	10.728000	14
47	9.272064	9.992263	19.279801	10.720199	10.007737	10.727936	13
48	9.272720	9.992239	19.280488	10.719512	10.007761	10.727274	12
49	9.273388	9.992214	9.281174	10.718826	10.007786	10.7266:2	11
50	9.274044	9.992190	9.281858	10.718142	10.007810	10.725051	10
51	19.4/4/08	9 992100	19.202542	10.717458	10.007834	10.725292	9
52	9.275307	9.992142	9.283225	10.716775	10 007858	10.724633	8
53	9.270025	.9.992118	' 9.2 83907	10.710003	110.007882	10.723975	7
54	9.276681	9.992093	9.284588	10.715412	10.007907	10.723319	6
55	·Q.277337	9.992060	·0.28 < 268	10.714772	10.007021	10.722662	5.
56	9.277001	9.992014	9.28 (047	10.714053	10.007016	10.722000	4
57	0.278645	0.002020	0.286624	10.713376	10.007490	10.721265	
58	0.270207	0.001006	0 282201	10 71 252	10.00/980	10 22020	3
	0.270049	7.77.790	0.08707	10.712699	10.008004	10. / 20703	8
59	9-2/9940	9.991971	9.207977	10.712023	10.008029	10.720052	1
60	9.200599	9.991947	9.288052	10.711348	10.008053	10.719401	_ 0
	Co-sine.	Sine.	Catana	Tang.	Co-sec.	Secant.	
M	CO-sinc.	DINC.	CO-tang.	Tans.	CO-acc.	SECHIL.	M

				Degrees.			
M	Sine.	Co-sine.	Tang.	Co-tang	Secant.	Co-sec.	м
-	9.280599	0.001047	0.288652	10.711348	10.008053	10.719401	60
Ĭ				10.710674		10.718752	59
1 2	0.281897	9.991897	9.189999	10.710001		10.718103	58
3	9.282544	9.991873	9.290671	10.709329		10.717456	57
4		9.991848	9.291342	10.708658	10.008152	10.716810	56
5	9.283836	9.991823	9.292013	10.707987	10.008177	10.716164	55
6	9.284480	9.991799	9.292682	10.707318	10.008201	10.715520	54
7			9.293350			10.714876	53
8		9.991749		10.705983	10.008251	10.714234	52
9			9.294684	10.705316		10.713592	51
10		9.991699		10.704651	10.008301		50
71		9.991674		10.703987		10.712312	49
12	9.288326			10.703323		10.711674	48
13				10.702661		10.711036	
	9.289600	9.991599	9.298001	10.701999		10.710400	46
. 15			9.298662	10.701338		10.709764	45
	9.290870			10.700678		10.709130	44
17	9.291504	9.991524	9.299980	10.700020	10.000470	10.708496	43 42
19	9.292768	0.001477	0.30120	10.698705		10.707232	41
20		9.991448		10.698049	10.008552	10.70660	40
 							
21	9.294029	9.991422	9,302007	10.697393 10. 6 96739		10.705971 10.705342	39 38
22	9.294658	0.001272	9.303261	10.696086	10.008629	10.704714	37
24	0.205012	0.001246	0.204567	10.695433	10.00864	10.70408~	36
				10.694782	10.008679	10.701461	35
				10.694131	10.008705	10.702836	34
27	9.297788	9.991270	0.306510	10.603481	10.008720	10.702212	33
28		9.991244	9.307168	10.692832	10.008756	10.701588	32
29	9.299034	9.991218	9.307815	10.692185	10 008782	10.700966	31
30	9.299655	9.991193	9.308463	10.691537	10.008807	10.700345	30
31	9.300276	9 991167	9.309109	10.690891	10.008833	10.699724	29
32	9.300895	9.991141	9.309754	10.690246		10.699105	28
33	9.301514	9.991115	9.310398	10.689602	10.00888	10.698486	27
34	9.302132	9.991090	9.311042	10.688958	10.008910	10.697868	26
				10 688315		10.697252	25
36	9.303364			10.687673	10.008962	10.696636	24
37		9.991012		10.687033	10.008988	10.696021	23
38			9.313608	10.686392	10.009014	10.695407	22
39			9.314247	10.685753		10.694793	20
40		9-990934		10.685115	10.009066	10.694181	
41				10.684477	10.009092	10 693570	19
	9.307041		9.316159		10.009118	10.692959	18
	9.307650			10.683205		10.692350	17
	9.308259			10.681936	10.009171	10.691741	
45			9.318064 9.318697	10.681303		10.691133 10.690526	15 14
46 47		9-99C777		10.680671	10.009223	10.680020	13
48				10.680039	10.009236	10.689315	12
49	9.311289	9.990697			10.009305	10.688711	11
50			9.321222	10.678778			10
		9.990645	9.321851	10 678140	10.009355	10 682:0:	
51 52	9.312495		9.322479	10.677521	10.009382	10.686001	8
53	9.313698	9.990591			10.009382		7
54 54	9.314297	9.000:65	0.323732	10.676267	10.000425	10.68 5703	6
55	9.314897	0.00018	9. 3243 68	10.67 (642	10.009462	10.68 (102	5
1 66	9.315495	9 990511	9.324982	10.675017	10.009489	10.68.1504	4
					10.009515		3
₹8	9.316689	9.990458	9.326231	10.673769	10.000 542	10 683311	2
59	9.317284	9.990431	9.326853	10.673147	10.009569	10.682716	1
60	9.317879	9.990404	9.327475	10.672525	10.009596	10.682121	0
N	Co-sine.		Co-tang.	Tang.	Co-sec.	Secant.	M
•——							

12 Degrees.

				Degrees.			
М	Sine.	Co-sine	Tang.	Co-tang.	Secant.	Co-nec.	М
1	9.317879	9.990404	9.327474	10.672526	10.009596	10.682121	60
	9.318473	9 490378	9.328095	10.671905	10.009622	10.681527	59
				10 671285			58
3	5 9.319658	9.990324	9.329334	, 1 0.6 70666	10.009676	10.680342	57
				10.670047			56
1 9	5/9-320840	9.990270	9.330570	; 10 669430	10.009730	10.679160	55
1 9	5;9.321430	19.990243	9.331187	10.668813	10 004757	10.678570	54
1 7	7 9.322019	9.440215	9.331803	10.668197	10.000785	10.077981	53
1 8	9.322607	19.990188	9.332418	10.667582	. 10.00 j 81 2	10.677393	52
9	9.323194	19.990161	19.333033	, 10.666967	10.009839	10.676800	51
10	9 323780	9.990134	9 333646	10.666354	10.004866	10.676220	50
11	19.324366	9.990107	9.334250	10.665741	·10.00u8a	10.675634	49
1 12	2 0.224050	0.000070	0.224871	10.66 (120	10.000021	10.67:000	48
1 13	3 4.325534	9.990052	0. 225482	10.664518	10.000048	10.674466	47
1 1	0.326117	14.000025	0.336503	10.662007	10.00007	10.67 388 3	46
1 1	4. 126700	9.989997	19.336702	10.663298	10.010003	10.673300	45
				10.662689			44
1 ,	0.327862	0.080012	0.337010	10.662081	10.010048	10.672178	43
1	9 328112	9.980015	9.338627	10.661473	10.01008	10.671 568	42
1 10	0.720021	0.080887	0. 330133	10.660867	10.010113	10 670070	41
2	9.329599	0.980860	9.334720	10.660261	10.010140	10.670401	40
				10.659656			39
				10.659052			38
				10 658448			37
				10.657845			36
				10.657243			35
20	9.333051	9.989093	19.343358	10.656642	10.010307	10.000949	34
2	9.333024	9.989665	9.343958	10.656042	10.010335	10.000370	33
33	5,9.334195	9.989037	9.344558	10.655442	10.010363	10.005805	32
29	9.334707	9.989010	9 345 157	10.654843	10.010390	10.665233	31
1				10.654245			30
31	19.335906	9.989553	9.346353	10.653647	10.010447	10.664094	29
32	9.336475	9.989525	9.346949	10 653051	10.010475	10 663525	28
33	9.337043	9.989497	9.347545	10.652455	10.010503	10.662957	27
34	9.337610	9.989469	9.348141	10.651859	10.010531	10.662390	26
				10.651265			25
36	9.338742	9.989413	9.349329	10.650671	10.010587	10.661258	24
37	9.339307	9.989385	9.349922	10.650078	10.010615	10.660693	23
				10.649486			22
39	9.340434	9.989328	9.351106	10.648894	10 010672	10.659566	21
40	9.340996	9.989300	9.351697	10.648303	10.010700	10.659004	20
1-	9.341558			10.647713			19
				10.647124			18
1 77	0.242620	2.3080314	0.35246	10.646535	10.010786	10.657221	17
				10.645947			16
				10.645360			15
				10.644773			14
1 47	0.344012	0.080100	0.255812	10 644187	10.010072	10.61.088	13
1 76	0.345460	0.080071	0.256208	10.643602	10.010030	10.664621	12
40	0.246024	0.080042	0.256082	10.643018	10.010029	10.662076	11
1 70	0.346570	9.080014	0.357666	10.642434	10.010086	10.652421	10
F	2377779		3 3 7 7 3 0	10.641851		234	
151	19.347134	9.900985	9.358140	10.041851	10.011015	10.052800	9
52	9.347087	9.933950	9.358731	10 641269	10.011044	10.052313	8
53	9.348240	9.988927	9.359313	10.040687	10.011073	10.051760	7
54	9.348792	9.958898	9.359893	10.640687	10.011102	10.051208	6
1 55	9.3493431	gigoonug,	9.300474	10.039520	10.011131	10.0500571	5
56	9-349893	9.988840	9.301053	10.638947	10.011160	10.050107	4
- 57	9.350443	9 988811	9.301032	10.638368	10.011189	10.049557	3
158	9.350992	9.988782	9.302210	10.637790	10.011218	10.049008	2
				10.637213	10.011247	10.648460	1
100				10.636636		10.647912	
ы	Co-sine	Sinc.	Co-tang.	Tang.	Co-sec.	Secant. 1	M
			77	Degrees.			
•			* *	- 0	•		

13 Degrees.

			131	Degrees.			
м	Sine.	Co-sine.	Tang.	Co-tang.	Secant.	Co-sec.	м
	9 352088	9.988724	.363364	10.6 166 16		<u> </u>	60
0		9.988695				10.647365	59
1	9.352635	9 988666	9.364515		10.011334	10.646819	-58
2	9.353181	9 988636				10.646274	57
3 4	9.354271	9.988607			10 01 1393	10.645729	56
	9.354815	9.988578	1.366237		10.011422	10.645185	55
5	9.355358				10.011452	10 644642	54
	9.355901	9.988519				10.644099	53
7 8	9 356443	9.988489	9.367953	10.632047	10.011511	10.643557	52
9	9.356984	9.988460	9.368524	10.631476	10.011540	10.643016	51
10	9.357524	9.988430	9.369094	10.630906	10.011570	10.642476	50
_					10.011599	10.641936	49
111	9.358064	9.988401		10.629768		10.641397	48
12	9.358603	9.988371		10.629700	10.011658	10.640859	47
13	9.359141		9.370799		10.011688	10.640322	46
14	9.359678		9.371367			10.639785	45
15 16	9.360215	9.900202	9.371933 9.372499			10.639248	44
	9.360752	9.988223				10.638713	43
17	9.361287 9.361822		9.373064 9.373629		10.011807	10.638178	42
•	9.362356		9.373029		10.01 1837	10.637644	41
19	9.362889	9.988133	9.374756	10.625244	10.011867	10.637111	40
1-							
21	9.363422	9.988103		10.624681	10.011897	10.636578	39
22	9 363954	9.988073	9.375881		10.011927	10.636046	38
23	9.364485	9.988043	9.376442		10.011957	10.634984	37 36
24	19 305010	9.988013	9.377003	10.622997		10.634454	35
25		9.987983	9.377563	10.622437	10.012017	10.633925	34
26	9.366075	9.987953	9.378122		10.012047	10.633396	33
27	9.366604	9.987922	9.378681	10.621319	10.0120/8	10.632869	32
28	9.367131	9.987892				10.632341	31
29	9.367659	9.987862		10.619646		10.631815	30
30	9.368185	9.987832	9.380354			,	
31	9.368711	9.987801			10.012199	10.631289	29
32	9.369236	9.987771	9.381466		10.012229	10.630764	28
33	9 369761	9.987740			10.012260	10.630239	27
34	9.370285	9.987710	9.382575	10.617425	10.012290	10.629715	26
35	9 370808	9.987679	9.383129	10 616871	10.012321	10.629192	25
36	9.371330	9.987649	9 383682		10.012351	10.628670	24
37		9.987618	9.384234	10.615766	10.012382	10.628148	23
38	9-372373		9.384786				21
39	9.372894	9.987557	9.385337	10.614663	10.012443	10.627106	20
40	9-373414	9.987526	9 385888	10.614112	10.012474	10.626586	
41	9-373933	9.987496		10.613562	10.012504	10.626067	19
42	9.374452	9.987465	9 386987	10.613013	10.012535	10.625548	18
43	9 374970	9.987434	9.387536	10.612464	10.012566	10.625030	17
44	9-375487	9.987403	9 388084			10 624513	16
45	9.376003	9.987372	9.388631	10.611369	10.012628	10.623997	15
46	9.376519		9.389178	10.610822	10.012659	10.623481	14
47	9-377035	9.987310			10 012690	10.622965	13
48	9.377549	9.987279	9.390270		10.012721	10.622451	12
49	9.378063	9.987248	9.390815	10.609185	10.012752	10.621937	11
50	9.378577	9.987217	9.391360	10.608640	10.012783	10.621423	10
51	9.379089	9.987186	9.391903	10.608097	10.012814	10.620911	9
52	9.379601		9.392447	10.607553	10.012845	10.620399	8
53	9.380113	9.987124	9.392989	10.607011	10.012876	10.619887	7
54	9.380624	9.987092	9.393531	10.506469		10.619376	6
55	9.381134	9.98706 t	9.394073		10.012939	10.618866	5
56	9.381643	, 9.987030	9.394614	10.605386		10.618357	4
157	0.282152	:g.g86gg8	9.395154	10.604846	10.013002	10.617848	3
58	0. 282661	a.a86a67	0.305604	: 10.604306	10.013033	10.017339	2
59	9. 282168	4.486936	9 396233	10.603767	10.013064	10.616832	1
60	9.383675	9.986904	9.396771	10.003229	10.013096	10.616325	
M	Co-sine.		Co.tang.		Co-sec.	Secant.	M

16 Degree

		and the same		- 10	Degree.		_	_
ĸ	34	Sine-	Co-sine	Tang.	Co-tang	Secant	Co-sec-	Man
В	0	0.383675	9.986904	9-396771	10.603829	10,013096	10.610126	66
B		9.384182			10.602601	10,013117	10.615818	50
и			9.986873	9.397846	10.602144	10/013750	10.615315	58
в	2	9.384687			10.601617	10/013191	10.614808	57
п	3	9.385192	9.986809		10.601081	10.013232	10.614301	\$6
P	4	9.385697	CARLO SERVICE CO.	DOM: NO.			10,613709	
r	5	9.386201	9.986746	9-399459	AD.600545	10,013254		55
в	6	9.186704	9-986714	9-399990	10.600010	10-013256	10.613396	54
п	7 8	9.387107	9-985583	9.400934	10.599470	10:013317	10.611793	53
	_	4.387709	9-986651	9.401058	10.598942	10.013349	10.610301	59
	9	9.385210	9.986619	9.401591	10.598409	10.015381	10.011700	51
в	10	9.388711	9-986587	9-402424	10.597876	10.013413	10.611289	10
W	11	9.389211	9.986555	9.402656	10-597344	10,013445	10,610789	49
п	12	9.389711	9 986523	9,403187	10.596813	10.013477	10.010189	48
к	13	9.390210	9.986491	9.403718	10.595282	10,013509	10-600700	477
в	14	9.390708	9.086450	9.404249	10.595751	10.013547	10,609392	46
в	15	9.391206	9.986427	91404778	10.595222	10.013573	10.008794	42
ı	16	9.191701	0.086305		10.594692	10,013604	10:608467	44
	17	9.392199	4.986363	9.405816	10.594164	10.013637	10.609801	100
	12	9.192695	9.986;31	9.406364	10.593636	10.013660	10.607305	15
	19	9.593191	9.986299	9.406892	10.593108	10.013701	10.606810	45
	20	0.393685	9.986266	9-407419	10.592581	10.013734	10.606314	40
						10.013766	10.604821	
я	21	9-394179	9.986234	9-407945	10.591055	10.013708	10.60 (327	39
к	22	9.394073	9:986202	9.408471	10.591529	10.013831	10.004324	37
в	23	9.395166	9.986169	9 408997	10.591003	10.011361	10.604343	36
В	24	9.395658	0.986137	9-409531	10.590479	10.011300	10:5038:0	35
и	25	9.396150	9-986104	9/41/00/45	10.589955	10.013928	10:003359	
п	26	9.396641	9.980072	9-410509	10.589431	10.013961	10,602868	34
в	27	9.397132	9.986039	9.411092	10.558908	Mary or other party and the	10,602370	23
и	28	9.397621	9.980007	9-411615	10.588385	10.015093	10.601550	30
и	29	9.398111	9-985974	9-519137	10.587863	10.014068	10.601400	10
в	30	9 31)8600	2-985942	9-412658	10.587342	-	NA COLUMN	
п	31	9.399088	9:985909	9:413179	10.586821	10,014091	10,600912	20
	32	9-399575	9-985876	9 413099	10.586301	10.014124	10:600425	28
п	33	9.400062	9.985843	9.414219		10.014157	10.599938	27
п	34	9.400549	9.985811	9-414738	10.585262	10.014189	10.59945	26
п	35	9.401035	9-985778	9-415257	10.584743	10.014121	10.598965	75
п	56	9.401520	9.985745	9.415775	10.584225	10.014255	10.598480	74
в	37	9 402005	9:985712	9-415293	10.583707	10/01/1288	10.597995	20
п	38	9.402489	9.985679	9.416810	10.583190	10.014321	10.597512	20
п	39	4.402972	9.985646	9-417326	10.582674	10.014354	10.597015	21
	40	9.403455	9.985613	9 417842	10.582158	10.014187	10.500.585	10
В	41	9.403938	91685580	9.418358	10.581642	10.014420	10.596662	14
1	42	9.404420	9 985547	9.418873	10 581127	10.014453	10-595580	18
1	43	9.404901	91985514	9.419387	10.580613	10.014486	10-105099	187
	44	9.405382	9.985480	9.419901	10:580099	10.014530	101504618	th.
	45	9.405863	9:985447	9.420415	101579586	10.014553	10.104138	15
	40	9.406741	9.985414	9,420927	40.579073	10.014586	10,593059	14
	47	0.406810	9.985381	9.431440	10.578560	10.014619	10.593180	10
	48	9.407299	9-985347	9.421952	10.578048	10.014653	10.592703	12
	49	9-407777	9-985314	9.422463	1C.577537	10.014686	10.592223	12
	90	9.408254	9.985280	9.422974	10:577026	10.014720	10.591745	10
	51	9-408731	9.985247	9.423484	10.576516	10.014753	rm.co.sóa	9
	52		9.985213	9.423992	10.576007	10,014187	10.500793	8
		9.409682		9.424503	10.575497	10.014830	10-600118	-
	55	4.410157	9.985146	9.425011	10.574989	10:014854	10.589 143	R.
	55		91985113	9-425519	10.574481	10.014887	10.589368	1
	26	9.411106	9-985079	9.416027	10.573973	10.014933	10 581504	100
1	27	9.411570	9-985045	9.425534	10.575466	10.014955	101588433	100
1	ES	9.412052	9 085011	9.427041	10.572959	10.014969	10,587948	3
	50	9.412524	9:984978		10.572453	10.015021	10.587470	12
	54 55 50 57 58 59 60	9.412995	9.984944		10,571948	10.013056	10.587004	0 - 0 10 4
1		-		Co-tang.	Tang.	Co-sec.	Second	11 1
1	M	Co-sine-	Sinc.	CO-TAINE.	- mile	and the same of	The same of	

15 Degrees.

				Degrees.			
M	Sine.	Co-sine.	Tang.	Co-tang.	Secant.	Co-sec.	M
-	9.412006	0.084044	0.428052	10.571948	10.015056	10.587004	60
	9.413467						59
1 2	9.413938	0.084876	429062	10.570938			58
1 2	9.414408	0.084842	9.429566	10.570434			57
1 4	9.414878	0 084808	0.430070	10.569930			56
	9.415347					10.584653	55
	9.415815					10.584185	54
	9.416283						53
	9.416751						
٥	9.417217	0.984638	0.432580	10.567420			51
ıó	0.417684	0.084602	9.433080	10.566920	10.015397	10.582316	50
_							
111	9.418150	9.984509	9.433580	10.566420	10.015431		49
	9 418615						- 1
13	9.419079	9.984500	9.434579	10 565421			
1 14	9 419544	9.984400	9.435078	10.564922			46
	9.420007						45
	9.420470						
	9.420933			10.563430	10.015637		
	9.421395			10.562933	10.015672		42
	9.421857			10.562437	10.015706		41
				10.561941	10.015741	10.577682	40
21	19.422778	9.984224	9.438554	10.561446	10.015776	10.577222	39
22	19.423238	9.984190	9.439048	10 560952	10.015810		38
23	9.423697	9.984155	9-439543	10.560457	10.015845	10.576303	.37
				10.559964	10.015880		36
				10.559471	10.015915	10.575385	35
	9.425073				10.01 5950		
27	9.425530	9.984015	9.441514	10.558486	10 01 5985		33
28	9.425987	9.983981	9.442006	10.557994	10.016019		
29	9.426443	9.983946	9.442497	10.557503	10.016054		31 6
	9 426899				10.016089		30
r	9.427354			10.556521	10.016125		29
1 ::	9.44/334	0.9030/3	9.4434/9			10.572191	28
3.2	9.42/009	9.983840	9.44.5908	10.556032			
33	9.428717	9 983770	9.44443	10.555542	10.016195	10.571737	26
34	9.420717	9 903//0	9-44494/	10.555053			
35	9.429170	9.903/35	9-445435	10.554565		10.570830	25
30	9.429623	9.983/00	9.445943	10.554077			24
37	9 430075	9.903004	3.440411	10.553589			23
30	9.430527	0.08222	9.440098	10.553102			21
39	9.430978	9.903594	9-447304	10.552616	10.016406		
				10.552130			20
41	9.431879	9.983523	9.448356	10.551644	10.016477		19
42	9.432329	9 983487	9.448841	10.551159	10.016513		18
43	9.432778	9.983452	9.449326	10.550674	10.016548		17
44	9.433226	9.983416	9.449810	10.550190	10.016584	10.566774	16
45	9.433675	9.983381	9.450294	10.549705	10.016619	10.566325	15
46	9 434122	9.983345	9-450777	10.549223	10.016655	10.565878	14
47	9.434560	9 983309	9.451260	10.548740	10.016691		
48	19.435016	9.983273	9.451743	10 548257	10.016727	10.564984	12
49	9.435462	9.983238	9.452225	10.547775	10.016762		
_50	9.435908	9.983202	9.452706	10.547294	10.016798	10.564092	10
17	9.436262	9.982166	9.452187	10.546812	10.016834	10.563647	9
1 (2	la.436798	9.984116	19.453668	10.546332	10 016870	10.563202	8
62	0.437242	9.983094	9.454148	10.545852	10.016906	10.562758	7
1 64	9.437686	9.98 20 68	9.454628	10.545772	10.016942	10.562314	6
1 6	9.438120	9.983022	9.455107	10.544802	10.016978	10.561871	5
1 26	0.438572	4.082086	0.455686	10.544414	10.017014	10.561428	4
1 27	0.430014	9.0820 0	0.456264	10.542026	10.017050	10.560086	3
28	9.430466	9.982014	0.456642	10.542468	10.017086	10.560544	2
50	0.430807	9.982878	0.457010	10.542081	10.017122	10.560102	1
60					, , , , , , ,		
	0.440118	9.982842	9.457406	10.542504	10.017168	10.559662	0
1-	9-439897 9-440338 Co-sine.	9.982842 Sine.	9.457496 Co-tang.		Co-sec.	10.559662	<u>0</u>

16 Degrees.

		-	-	Of the latest section in		-	_
1 .	n Silie.	Co-sine	Tang.	Co-tang.	Secunt	Co-sec.	- 11
-		T. P. Pura		40 242404	10.017158	10.559662	100
0		9,982842	9-457496	10.543504			100
1	9+40778	9.982805	9 457975	10.542027	10/01/195	10.559222	59
2	9.441218	9.982769	9.458449	10.541551	10.017231	10.558780	58
3	0.441658	9.982733	9-458935	10.541075	10.017267	10-558341	57
4	0.44 2046	9.982090	9.459400	10.540600	10.017304	10.557604	5%
	0.442525	9.982660	9.459875	10.540125	10.017340	10.557465	35
5 6	9 44-555	0.083634	9.460349	10.539651	10.017376	10.557027	54
	4-44-6/2	9.982624		10.539177	10.017413	10.556590	
7 8		9.982587	9.460823				53
8	9.443847		9.461197	10.538703	10.017449	10.556153	52
9	9.414284	9 982514	9.461770	10.538230	10.017486	10.555716	31
10	9.414 20	9.982477	9 462242	10.537758	10.017523	10 555280	50
-	W 100 100	9 982441	9.462714	10.537286	10.017559	10.554845	49
102	9 445155			10 406814	to our cont	10.554410	
1/2		9.982404	9.463186	10.536814	10.017596		42
13	THE RESERVE OF THE PERSON NAMED IN	9.982367	9.463658	10.536342	10.017633	10.553975	177
14	19-446459	9.982331	9.464128	10.535872	10.017669	101555541	40
15	9.446893	9.982294	9.464599	10.535401	10.017706	10.553107	45
16	9 447326	9.982257	9.465069	10.534931	10.017743	10 151074	44
17		9 982220	9.465539	10.53446x	10.017780	10.152221	43
18	9.448191	9.982183	9.466008	10.533992	10.017817	10.551809	42
		9.982146	9.466416	10.533524	10.017854	10.551377	41
19	9.448623				10.017891	10.550010	_
20	9.449054	9.982109	9.466945	10.533055		-	40
21	9 449485	9.982072	9.467413	10.532587	10,017928	10.550515	39
22	9 440016	9.982035	9.467880	10.532120	10.017905	10.550085	38
23	9.450345	9.981998		10.531653	10.018003	TO CAUGET	37
		9.981961			10.018039	10.049335	36
24	9.450775			the same of the same of the	10.018075	10 (48796	
	9.451204		9.469280	10.530720	The second second		15
26		9.981886		10.530254	10.018114	ML 548 368	34
27	9.452060		9-470211	10.529789	10.018151	10.542040	33
28	9-452488	9.981812	9.470676	10.529324	10.018188	10/507510	52
29	9.452915	9.981774	9-471141	10.528859	10 018225	10-547085	31
30.	9.453342	9.981737	9 471605	10.528395	10.018263	10-546058	30
		-			-		_
31	9-453768	9.981700	9-472068	10.527932	10.018300	10.546999	2.9
32	9-454194	9.981602	9-47=53=	10.527468	10.018338	10.545800	28
33	9.454619		9-471995	10.527005	10.018375	10.545381	47
34	9.455044	9.981587	9-473407	10.526543	10.018413	10.544950	16
35	9.455409			10.526081		10.544531	25.
	9.455893			10.525019	10.018488	10-544107	34
37	9.456316			10.525158	10.018426		22
		9.981436					1 56
1000			9-47 5303	10.524697	10.018504	10.543201	
10000	9.457162		9-475763		10.018601	10.542838	21
49	9.457584	9.981361	9.476223	10.523777	10.018639	10/542416	20
	9-458006		9.476683	10.523317	10.018619	10/541994	19
	9.458427		9-477142	10.522858	10.018715	10.541171	18
43	9.458848	9.981247	9-477601	10.522399	10:018753	10.541152	17
44	9 459268	9.981109	9 478050	10,521941	10.018791	10.500033	16
	9.459688	9.98:171	9-478517	10,521483	10.018829	10.540314	15
	9.460108		9-478975	10:521025	10.018867	10.539892	13
47	9 450527	4 981095	9-479432	10.520568	10.018905	10:539473	13
48	9 460946	9.981057	9-479889	10.520111	10.013943	10.539054	12
	9.461364		9.480345	10.519655	10.018981	10.138636	27
	9.461782		9.480801	10.519199	10.019019	10.538218	10
		-	-			-	
	9.462199		9 481257		10.019058	10.537801	9
		9.980904	9-481712		10 019096	10 537 384	8
53		9 980866	9.482167	10.517833	10 019134	10 935068	7
54	9.463448	9.980827	9.482521	10.517379	10,019173	10.536552	6
		9.980789	9 483075	10 516925	10.019311	10.515116	5
	9.464279				10.019350	STOCK AND RESIDENCE	1
				10.516018	10.019288	10.515306	2
					The second second		3
	9.465108		9-484435	10 515565	10.019327	10.534898	4 3 3 1 1
	9.465522				10.010365	10.514418	
60	9.465935	9.980596	9-485339	10.514661	10.019404	10.514065	0
24	Co sine		Co-tang-	Tang.	Co-sec.	Secunt.	BR
-		COLUMN TO A	America Pro-	a ming.	OF BUD	The second second	THE REAL PROPERTY.

17 Degrees.

-				Hagrees.			
M	Sine.	, Co-sine.	Tang.	Co-tang.	Secant.	Co-sec.	x 1
	45.000	0.00006	0.485220	10 (1466)	10.019404	10 524065	60
0	19.405935	19.980590	9.405339	10.514001	10.019442	10.534005	59
1	0.400340	9.900558	9.485791	10.514209	10.019481	10 533034	58
1 2	9.400701	19 980519	9.480242	10 513750	10.019461		
3	9.407173	9 980460	9.480093	10.513307	10.019520	10.532827	57
4	9 407585	9.980442	9.487143	10.512857	10.019558		56
5	9.407990	9.980403	9.487593	10.512407	10.019597	10.532004	55
6	9.468407	9.980364	9.488043	10.511957	10.019636		54
7	9 468817	9.980325	9.488492	10 511508	10.019675	10.531183	53
8	9.469227	9 980286	9.488941	10.511059	10.019714	10.530773	52
9	9.469637	9.980247	9.489390	10.510010	10.019753	10.530363	51
10	9.470046	9.980208	9-489838	10.510162	10.019792	10.529954	50
11	9.470455	0.080160	'p 400286	10.509714	10.019831	10.529545	49
12	9 470863	0.080120	0.400733	10.500267	10.019870		48
13	0.471271	1.080001	0.401180	10 (08820)	10.010000	10 (28730	47
14	0.471670	0 080052	0.401627	10 (08373	10.019948	10.528321.	46
15	0.472086	0.080012	0.402077	10 507027	10.019988	10.527914	45
16	0.472402	0.070072	0.402610	10.507481	10.020027		
17	0 472808	2-27-22/3	0 402065	10.507025	10.020066	10.527102	43
18	0.472204	77/3934	0.402410	10.507035	10.020105		42
19	0 477710	7.7.707)	0.402814	10.606146	10.020145	10.526290,	41
20	0.47411	7.8/303)	0.404200	10.505701	10.020184	10.525885	40
	9.4/4113	9 9/9010	3.494499	-55,51			_
21	9.474519	9.979776	9 494743	10.505257	10.020224	10.525481	39
22	9 474923	9-979737	9.495186	10.504814	10.020263	10.525077	38
23	9.475327	9.979697	9.49 5630	10.504370	10.020303	10.524073	37
24	9.475730	9.979658	9.496073	10 503927	10.020342	10.524270	36
25	9.476133	9 979618	9.496515	10.503485	10.020382	10.523007	35
26	Ma.476 c 261	0.070470	Q.AQDECT	, 10. 503043	10.020421	10.523404	34
27	19.4749361	10.474.634	19 497 (99	110.302001	10.020401	10 123002	33
28	10.47.73 <i>4</i> 01	0 070490	10.407841	10.502159	10.020501	10.522000.	32
29	16.477741	la 070450	0.408282	10 (01718)	10.020541	10.522259	31
30	9.478142	9.979420	9 498722	10.501278	10.020580	10.521858	30
31	9.478542	9.979380	9.499163	10 500837	10.020620	10.521458	29
32	0.478942	9 979340	9.499603	10.500397	10.020660	10.521058	28
33	0 470 242	0.070300	io (00042	10 4000 (8)	10.020700	10.520658	27
34	9 479741	0.070260	9 500481	10.499519	10.020740	10.520259	26
3.5	9.480140	9.979220	9 500920	10.499080	10.020780	10.519860!	25
35 36	9.4405 19	9.979180	19.501359	10.498041	10.020820	10 519401	24
37	0.480027	0.070140	0.501707	: 10.4982071	10.020860	10.010001	23
38	0.481224	0.070100	0 502235	10.497765	10.020000	10.518666	2.2
39	9.481731	9.979059	9.502672	10.497328	10.020941	10.518269	21
40	9.482128	9.979019	9.502100	19.496891	10.020900 10.020941 10.020981	10.517872	20
41	0.480	0.078070	0.000046	10.496454	10.021021	10.517475	19
42	9.402525	7 9/09/9	9.303340	10 406018	10.021051	10.517070	18
	0.4810.4	7 7/4939	0 (04418	10.405582	10.021102	10.516684	17
48	0 48 27 10	2.3/0030	9.504410	10.405146	10.021142	10.516288	16
	9.405/12	9.9/0050	3.304034	10.494711	10.021183	10.515802	15
45	9.404107	9 9/0017	9.303409	10.404276	10.021223	10.515400	14
46 47	9.494541	3.9/9/17	0 505/24	10.402841	10.021263	10.515105	13
48	7404045	2.3/0/5/	9.300139	10.402407	10.021304	10.514711	12.
	9-407209	3.9/0090	9.500593	10.493407	10.02134	10.514318	11
49 50				.10 492973		10.513925	10
-				10 492540			
51	9 486467	9-978574	9 507893	10.492107	10.021426		9
52	9 486860	9-97 533	19.508326	10.491074	10.021467	10.513140	
53	9.487251	9.978493	9.508759	10.491247	10.021507	10 512749	7
54	9 487643	9 978452	9,509191	10.490809	10.021548	10.512357	
55	0.488024	0.078411	10.00022	10.490378	10.021589	10.5119001	5
56	0.488424	0 078270	0-610064	10.480040	10.021630	10 511576	4
57	9.488814	9.978329	9 510485	10.489 51 5	10.021571	10.511186	3.
58	9.489204	9.978288	9.510916	10.489084	10.021671	10.510796	2:
59	0.480602	0 078747	O PRIZAD	· 10.455054	110.021753	10.51040/	I
60	9 489982	9.978206	9.511-76	10.488224	10.021794	10.510018	<u> </u>
M	Co-sine	nine.	Co-tang.	Tang.	Co-sec	Secant	M

			10 1	regrees.			
M 1	Sine.	Ca-sine.	Tang.	Co-tang.	Secant	Co-sec.	34
-		-			TO DEVEND		60
0	9.489982	9.978206	9:511776	10,488124	10.011794	10.510018	
X	9.490371	9.978165	9.512206	10.487794	10.021835	10 509629	59
2	9.490759	9.978124	9.512635	10.487165	10.021816	10:509241	55
3	9.491147	9.978083	9-513004	10.486936	10.021917	10.508853	53
4	9-491535	9.978042	9-513403	10.486507	10.021958	10.508405	56
5	9.491911	9.978001	9.513921	10.486079	10.021999	10.508078	. 55
	9-492308	9.977959	9-514349	10.485651	10.022041	10.507691	54
7	9.442095	9.977918	9.514777	10,485223	10.022082	10.507305	33
	9.493081	9.977877	9-515204	10.484796	10.022123	ro gabyig	52
9	9 49 3466	9 977835	9.515631	10.484169	10.022165	10.506.534	51
10	9.493851	9-977794	9.516057	10.483943	10.022206	10-500 189	50
11	9.494236	9.977752	9.516484	10.483510	10,022248	10 (05764	49
12	9.494621	9.977711	9.516910	10.483090	10.022289	10.505379	48
13	9.49 5005	9.977660		10.482665	10.022331	10.504095	47.
14	9.495388	9.977628	9.517701	10.483230	10.022372	10.504612	46
15	9-495772			10.481815	10.022414	10.504228	45
16	9.496154	9.977544	The second second	10.481390	10.022456	10.503846	44
17	9.496537	9.977593	9.519034	10.480966	10.022407	10 copefit	43
18	9.496919	9 977461	9.519458	10.480542	10.022520	10.000081	42
119	9-497301	9 977419		10 480118	10.022681	10.502000	41
20	9.497682	0.977377	9.520305	10.479695	10.022623	10.502318	40
					10.022665	200	
3E	9.498064	9 977335		10.479272	THE PARTY OF THE PARTY.	10.501936	39
22	9-498444		The second second	10.478849	10.022701	10.501556	38
23	9-498825	9.977251	9.521573	10.478427	10.022749	10.501175	37
24	9-499204		A STATE OF THE PARTY OF	10.478005	10.012791	10.500796	30
25	9-499584			10 477583	10 022833	10.500416	35
26	9-499963		ACCUPATION OF THE PARTY OF THE	10.477162		10.500037	30
27	9.500343			10-476741	10.022917	10.499658	33
#8	9 500721	I be to the second		10.476320	10.022959	10-499279	32
29	9.501099		9.534100	10.475900	10.023001	10.498901	32
30	19.501476	9-976957	9.524520	10.475480	10.023043	10.498524	30
31	9.501854	9.976914	9-524939	10.475061	10.023086	10.408146	10
32	9.502231			10.474641	10.023128	10.497769	28
3.3	9.501607	9.9768 10		10.474222	10.022170	10.497393	27
34	9.502984			10 47 3803	10 02 3213	10.497016	26
35	9.503360	A CONTRACTOR OF THE PARTY OF TH		10 473385	10.018165	10.496640	25
36	9.503735		The second second	10.472967	FO:08 7208	10-405265	24
37	9.504110			10.472549	10.021340	10.494890	27
18	9.504485	9.976617		10.472132	10.013383	10.495515	20
139	9.504860			10.471713	10.023426	10.485140	22
	9.505234			10.471208	10.023468	10.494765	30
40			-	-			
41	9 505608		1000000	10.470881	10.023511	10 494392	19
42	9.505981			10-470465	10.023554	10.494010	18
15	9.506354	9.976404		10.470050	10.023596	10-493646	12
44	9.506727	9 976361		10 469634	10.023639	10,493273	10
45	9.507099			10.469219	10.023682	10.492931	18
46	9.507471			10.468804	10.023725	10.492529	14
47	9.507843		The second second	10 468 389	10 023768	10.492157	13
48	9.508214		1	10 467975	10.023811	10:491786	12
49	9.508585		10.00	10.467561	10.023854	10.491415	1.1
50	9.508956	9-976103	9.532853	10.467147	10.023897	10.491044	10
51	9.500326	9,976060	9 533266	10.466734	10.023940	10.490574	9
52	9.509696	The second second	9-533079	10.466321	10.023983	10.400304	8-
153	9.510065	9.975974	THE RESERVE TO	10.465908	10.024026	10.489935	1 3
54	9.510434			10.465496	10.014070	10.489566	6
55	9.510803			10.465084	10.024111	10.489197	35
56	9.511172	9.975844		10 464672	10.024156	10:488813	
57	9.511540		9 535739	10.464161	10.024200	10.488460	1
58	9.511007	9.975757	Contract of the Contract of th	10.461840	10,024241	10.485001	4000
59	9-512275		THE RESERVE	10 46 74 79	10.024286	10.487725	-
60	9 512642			10.467028	10.024330	10.487348	0
-			The Person Name of Street, or other Persons Name of Street, or oth			_	-
1 M	Co-sine.	Sine.	Co-tang.	Tang.	Co-sec.	Secant.	28

19 Degrees.

				Jegrees.			
<u> </u>	Sine	Co-sine.		Co-tang.	Secant.	Co-sec.	M
0	9.512642	9.975670	9.536972	10.463028	10.024330	10.487358	60
1	9.513009	9.975627	9.537382	10 46 26 18	10 024373	10.486991	59
2	9.513375	9.975583	9-537792	10.462208	10.024417	10.486625	58
3				10.461798			57
14				10:461389			56
5				10.460 9 80 10.460571			55
7	9.516202	9.975366	9 530827	10.460571	10.024592	10.484708	54
8				10.459755	10.024670	10.484434	52
9	9.515930	9.975277	9.540653	10.450247	10.024723	10.184070	51
10	9.516294	9.975233	9 541061	10.458939	10 024767	10.484070 10.483706	50
11	9.516657	9.975189	9.541468	10.458532	10.024811	10.483343	49
12	9.517020	9.975145	9 54 1875	10 458125	10.024855	10.482980	48
13				10.457719	10.024899	10.482618	47
14	9.517745	9.975057	9.542688	10.457312	10.024943	10.482255	46
15	9.518107	9.975013	9-543094	10.456906	10.024987	10.481893	45
16				10.456501			44
18			9.543905			10.484171	43
19	9.519561	9.974826	9.544715	10.455285	10.025164		42
20	9.519911	9.974792	9.545119	10.454881		10.480089	40
21		9.974748		10.454476			39
22				10.454072		10.479369	38
23			9.546331		10.025341		37
24	9.521349	9.974614	9.546735	10.453265	10.025386		36
25	19.521707	9.974570	9.547138	10.452862		10.478293	35
26	9.522066	9.974525	9.547540	10.452460	10.025475		34
27			9.547943				33
28				10 451655	10 025564		32
29 30		9-974391 9-974347		10.451253			31
1							30
31		9.974302					29
32 33	0.524564	0.074212	0.550252	10.450049 10.449648	10.025743		28 27
33				10.449048			26
35				10.448848			25
36				10.448448			24
37	9-525984	9.974032	9.551952	10.448048	10.025968	10.474016	23
38			9.552351		10.026013	10.473661	22
39				10.447250			21
40				10.446851	10.026103		20
41			9.553548		10.026148		19
42			9 553946				18
43			9-554344	10.445656			17
44			9.554741	10.445259 10.444861			16
45			9.555536				14
47			9.555933			10.470487	13
48			9.556329				12
49			9.556725			10.469785	11
50			9.557121	10.442879	10.026556		10
51		~~~	9-557517	10.442483	10.026602	10.469085	9
52		9.973352	9.557913	10.442087			9
53		9.973307	9.558308	10.441692	10.026693	10.468386	7 6
54		9.973261		10.441298	10.026739	10.468037	
55			9.559097				5
56			9.559491				4
57 58		9.973124	9.559885		10.026876	10.466991 10.466 6 43	3 2
59		9.973078	9.560279 9.560673				1
160		9.972986	9.561066	10.438934	10.027014	10.465948	0
W	Co-sine	Sine.			Co-sec.	Secant.	-M
1 24	CO-8111G	JIIR.	Co-tang.	Tang.	CO-sec.	JENKIII.	PL

			20 1	Degrees.	R CHA	21 1003	LA
1 16	Sine.	Co-sine.	Tapg.	Co-tang	Secant	Corner	31 (
-			9.561066	10.438934	10,017014	10.45 (048	60
1 3	9.534052		9.561459	10.438541	10.027060	10.454601	LL POST
1 3	9-534399	9.972990	9.501851	10.438149	10.027106	10.465255	59
1 0	9-534745	0.077848	9.502244	10-437756	10-017152	10.464908	58
3	9.535098		9.561636	10.437364	10-027198	10.464562	57
14	9 535438	9-972755		10.436972	10,027245	10.464217	
6	9.535129		9.565419	10.436 (8)	10.027291	10.463871	355
1 .	9.536474		9.563811	10.435189	10.027337	10 463526	3
1 8	9.536818		9.564202	10.435798	10.017383	10.462184	52
	9.537163	9.972570		10.435408	10.027410	10.462837	51
10	9.537507	9.972524	F D -	10.435017	10.027476	10.452442	50
				10,434627	10.027533	10.462440	
12	9.537851	9.972478	9.565373	100000000000000000000000000000000000000	10.017569	10.451806	49
12	9.538194	9.972431	9.565763	10.434237	10.027615	10,451461	48
13	9.538538	9.972385	9.566542	10.433458	10.027662	10.451110	45
14	9.538880	9.972338	9.566932	10.433068	10.027709	10 460777	1000
35	9.539223	9.972291	9.567320	10.432680	10.027755	10.450435	45
16	9.539505	9-972245	9-567709	10 432291	10.017801	10.460093	44
17	9.539907	9.972198	9.568098	10 431902	10.027849	10.450754	43
18	9.540249	9.972105	3.568486	10:431514	10.027895	10.459410	41
19	9.540590	9.972058	9-568873	10.431127	10,027942	10.419066	
20							49
21	9.541272	9.972011	9.509201	10.430739	10.017989	10.465725	32
22	9,541613	9.971964	9.569648	10 430352	10.028036	10.458387	33
23	9-541953	9.971917	9.570035	10.429905	Marie Company of the Company	10.458047	37
24	9.542293	9.971870	9.570422	10.429578	10.028130	10 457707	36
25	9.542632	9.971823	9.570809	10.429191	10.028224	10.417508	35
26		9.971776	9.571195	10.428805	10.028271	10.457029	34
27	9.543310	9.971729	9-571581		10.028318	10.456351	33
28	9-543049	9.971682	9-571967	10.428033	10.028365	10.456013	35
29	9:543987	9-971635	9.572352	10.427648	10.028412	10.455675	31
30	9.544325	9.971588	9-572738	10.427262		-	39
31	91544663	9-971540	9-573123	10.426877	10.028460	10.455337	2.9
32	9.545000	9-97/493	9-573507	10.426493	10.028507	10.455000	28
33	9.545338	9.971446	9.573892	10.426108	10.028554	10-454002	27
34	9-545674	9.971398	9.574270	10.425724	10.028602	10-121350	20
35	9.540011	9-971351	9.5"4660	10.425340	10,028649	10 45 5989	25
36		9.971303	9-575044	10.424956	10.018697	10.453655	14
37	9.546683	9-971256	9-575427	10.424573	10.028744	3D-453317	43
38	9.547019	9-971208	9.575810	10.424190	10.028792	10.452981	==
39	9-547354	9.971161		10.423807	10.028839	10.452040	21
40	9-547089	9.971113	9.576376	10.423424	10.028887	10-452311	20
41	9.548024	9.971066	9.576958	10.423042	10.018934	10.451976	19
42	9.548359	9.971018	9-577341	10.422659	10.028982		28
43	9.548693	9.970970	9-577723	10.422277		10.451307	15
44		9.970922	9-578104	10.421896	10 029078	The second second	16
45	9.549360	9.970874	9-578486	10.421514	10.029126	CORPORATION AND ADDRESS OF THE PARTY AND ADDRE	23
46		9.970827	9.578867	10.421133	10.029173		14
47	9.550026	9-970779	9.579248	10.420752	10.029221	3P-449974	15
48	9.550359	9.970731	9.579629	10.420371	10.029269	10-449041	32
49	9.550692	9.970683	9.580000	10.419991	10.029317	10.449308	21
50	9,551024	9.970035	9.580389	10.419611	10.029365	10.448976	10
51	9.551356	9-970586	9.580769	10.419231	10.029414		8
52	9.551687	9.970538	9.581149	10.418851	10.029462	10.448313	(3)
52	0.002018	9.070490	9, 581 528	10.418472	10.010510	10.447982	7
54	9.552349	9.970442	9.581907	10.418093	10.029558	10 4476SE	6
55	9.552680	9.970394	9.582280	10-417744	10.020000	10447330	5
56	9-553010	9.970345	9.582665		10.029655		4
57	9.553341	9.970297	9-583043		10.029703		3
58	9.553070	9-970249			10.029751		1 2
59	9.554000				10.029800		543010
	9-554329	9.970152	9.584177	10.415823	10.029848	10.445071	_0
M	Co-sine.	Sine.	Co-tang	Tang	Co-sec.	Secant.	34
-			Industry and J. R.	Degraps.		-	

21 Degrees.

, M	Sine.	Co-sing.	Tang.	Co-tang.	Secant.	Co-sec.	м
1			9.584177		10.029848	10.445671	60
1	0. 5 5 4 5 6 8	0.070102	0.584555	10.415445	10.029848		59
2	0.454087	0.070055	0.584032	10.415068	10.010046	10.445012	58
2	0.556536	la.070006	la. 48 4 200	10 414601	10.020004	10.4446851	57
4	9.555643	9.969957	9 585686	10.414314 10.413938	10.020043	10.444357	56
5	9.555971	9.959909	9,586062	10.413938	10.030001	10.444029	55
6	9.556299	9.909860	9.586439	10.413561	10.030140	10.443701	54
2	9.556626	9.969811	9.586815	10.4131 45	10.030189	10.443374	53
8	9.556953	9 969762	9.587190	10.412810	10.030298	10.443047	52
9	9.557280	9.969714	9.587566	10.412434	10 030286	10.442720	51
10	9.557626	9.409005	9.507941	10.412059	10.030335	10.442394	50
	9 557932			10.411684		10.442068	49
12	9.558258	9.969567	9.588691	10.411309	10.030433	10.441742	48
13	9.558583	9.969518	9.589066	10.410934	10.030482	10.441417	47
				10.410560			46
				10.410186			45
				10.409812			44
17 18				10.409438		10.440117	43
				10.409065 10.408692		10.439793	42
				10.408319		10.439469	41 40
							_
21 22	9.501178	9.909124	9.592054	10.407946 1 0.4 07574	10.030076	10.438822	39 38
22	0.501501	0.909075	0.592420	10.407574	10.030925	10.438499	37
				10.406829			36
25	0.562468	9.968976	0. CO2 CA2	10.406458	10.031024	10.437532	35
26	9 562790	0.068877	0 (01014	10.406086	10.031122	10.437210	34
27	9.563112	9.968827	9.594285	10.405715	10.031173	10.436888	33
28	9.563433	9.968777	9.594656	10.405344	10.031223	10.436567	32
				10.404973			31
30	9.564075	9.968678	9.595398	10.404602	10.031322	10.43 5925	30
31	9.564396	9.968628	9.595768	10.404232	10.031372	10.435604	29
32	9.564716	9.968578	9.546138	10.403862	10.03 1422	10.435284	28
33	9.565036	9.968528	9 596508	10.403492	10.031472	10.434964	27
34	9.565356	9.968479	9.5 96 878	10.403122	10.031521	10.434644	26
35	9.565676	9.968429	9.597247	10.402753 10.402384	10.031571	10.434324	25
30	9.565995	9.968379	9.597616	10.402384	10.031621		24
57	9.500314	9.908329	9.597985	10.402015			23
30	9 500032	9.908278	9-590354	10.401646	10.031723	10.433368	22
40	9.500951	0.068178	0.590742	10.401278 10.400909	10.031772	10.433049	20
	9.30/209	3.9001/0	3.299091				-
41	9.567587	9.908128	9-599459	10.400541		10.432413	19
				10.400173		10.432096	17
7.5	0 568 522	o obzazz	0.600262	10.399806 10.399438	10.0319/3	10.431778	16
46	0.668866	0.067427	0.600020	10.399438	10.072072	10.431144	15
46	9.560172	9.967876	9.601006	10.398704	10.032124	10.430828	14
				10.398338	10.032174	10.430512	13
748	9.569804	9 967775	9.602029	10.397971	10.02222	10.420106	12
49	9.570120	9.967725	9.602395	10.397605	10.032275	10.429880	11
50	9.570120 9.570435	9.967674	9.602761	10.397239		10.429565	10
	9.570751			10.396873		10.429249	9
52	9.571066	9.967573	9.603493	10.396507	10.032427	10.428934	8
53	9.571380	9.967522	9.603858	10.396142	10.032478	10.428620	7
54	9.571695	'9.96747 L	9.604223	10.395777	10.032529	10.428305	6
55	9.572009	9.967421	9.604588	10.395412	10.032579	10.427991	5
	9.572323			10.395047	10.032630	10.427677	4
	9.572636		9.605317	10.394683	10.032681	10.427364	3
58	9.572950	9.907168	9.005682	10.394318	10.032732	10.427050	2
59	9.573203	0.907217	9.000046	10.393954	10.032783	10.426737	0
	Co sine.	9.907100		10.393590			
×	Co sine.	Sine.	Co-tang	Tang.	Co-sec.	becant	K I

			. 22	Degrees.			
1 M	Sine.	Co-sine.	Tang.	Co-tang	Secant.	Co-sec.	M
1	9-573575	9 967166	9.606410	10.393590	10.032834	10.426425	60
	1		9.606773		10.032885	10.426112	59
] :		9.967064			10.032936		58
] :	1 0			10.392500	10.032987	10.425488	57
1 4	1		9.607863	10.392137	10.033039	10.425176	56
1	9.575130		9.608225 9.608588	10.391775	10.03 (090 10.033 141	10-424864	55
		9.966808	9.608950			10.424242	54
1 1		9.966756	9 609312	10.390688	10.033244	10.423931	52
			9.609674	10.390326	10.033295	10.423621	51
	9.576689		9.610036	10.389964		10.423311	50
1	9.576949	9.966602	9 610397	10.389603	10.033398	10.423001	49
12		9.966550		10.389241		10.422691	48
13	9.577618		9.611120	10.388880		10.422382	47
12				10.388520		10.422073	46
			9.611841	10.388159		10.421764	45
15		9.966344 9.966292	9.612261	10.387799			44
17		9.966240	9.612921	10.387079	10.033708	10.421147	‡3 42
lig		9 966188		10.386719	10 03 38 12	10.420530	41
20	9.579777	9.966136	9.613641		10.033864	10.420223	40
21		9.966085	9.614000			10.419915	39
	9.580392			10 385641			38
23	1 0.2		9.614718				37
2.			9 615077	10.384923			36
	9.581312		9.615435	10.384565	10.034124	10.418688	35
26	9.581618			10.384207	10.034176		34
27			9.616151	10.383849		10.418076	33
28		9.965720	9.616509	10.383491		10.417771	32
29		9.965668		10.383133	10.034332	10.417465	31
30	9.582840		9.617224			10.417160	30
31	9.583145	9.965563	9.617582	10.382418	10.034437	10.416855	29
32	9.583449	9.905511	9.017939	10.382061	10.034489		28
33	9 503754	9.905458	9.018295	10.381705	10.034542	10.416246	27
1 34	0.584261	0.065262	0.610008	10.380992	10.034594	10.415942	26
26	0 584666	9.965301	9.619364	10.280626	10.034600	10.415335	24
37	9 584968	9.965248	9.619721	10.380279	10.034752	10.415032	23
38						10.414728	22
						10.414426	21
40	9 585877	9.965090	9.620787	10.379213	10.034910	10.414123	20
41	91586179	9.965037	9.621142	10.378858	10.034963	10.413821	19
42	9 586482	9.964984	9.621497	10.378503	10.035016	10.413518	18
43	9.586783	9.964931	9.621852	10.378148	10.035069	10.413217	17
44	9.587085!	9.9648791	9.622207	10.377703	10.0351211	10.412016	16
45	9.587386	9.964826	9.622561	10.377439	10.035174	10.412614	
						10.412312	14
47 48				10.376731		10.412011	13
40	9.588.00	9.964612	0 622076	10.276024	10.035354	10.411410	11
50	9.588800	9.964660	9.624330	10.37 (670	10 03 (440	10.411110	10
51					-	10.410810	. 9
	9.309190	0.064121	0.621026	10.274064	10.0255493	10.410511	8
				10.374612			7
54	9.590088	9.964347	9.625741	10.374259	10 03 26 25	10.400012	6
55	9.590387	9.96.1294	626093	10.373907	10.035706	10.400613	5
56	9.590686	9.964240	9.626445	10.373555	10.035760	10.409314	4
57	9.590984	9.964187	9.626797	10.373203	10.035813	10.409016	3
58	9 591282	9.964133	9.627149	10.372851	10.035867	10.408718	. 2
59	9.591580 9	964080	0.027501	10.372499	10.035920	10.408420	
				10.372148			
M	Co-sine.	Sine.	Co-tang	Tang	Co-sec.	Secant.	м
			C= 33	eurcest			

			23	Degrees.			
1	Sine	Co sine	Tang	Co-tang.	Secant.	Co-sec.	M
1		0.064026	0.627852	10.372148	10.035074	10.408122	60
2	9.592176	0.062073	0.628203	10.371797			59
	9-592473	0.963010	0.628554	10.371446	10.036081		58
1 3	9.592770	0.062866	0 628000	10.371005	10.036135		57
3	9.593067	0:062811	9.629255	10.370745			56.
1 7	9.593363	0.062757	0.620606	10.170194	10.036243		55
1 8	7.3933-3	0.062704	0.620056	10.370044	10.036296	10.406341	54
1	9.333433	0.062650	0.630306	10.369694	10.036350	10.406045	53
8	9.594251	0.063506	0.630656	10.360344	10.036404	10.405749	52
	9-594547	0.063642	0.631006				Śŧ
10	9.594842	0.063488	0.631355	10.368645	10.036512	10.405158	50
					10 036566		49
111	9.595137	9.903434	0.622022		10.036621		48
12	9.595432	9.9033/9	0.622401	10.267500	10.036675	10.404273	47
13	9.595727	9.903323	0 622250		10.036729		46
14	9.596021 9.596315	9.9032/1	0 622008		10.036783		45
1.5	9.596609	9.903217	0.622447	10.366553			44
1	9.596903	0.062108	0.622705		10.036892		43
17	9.59 09 03 9.5 9 7196	2.302100	0.624142	10.365857			42
18	9.597490	0.062000	0.584100		10.037001	10.402510	41
20	9-597783	0.062045	0.634828	10.365162	10.037055	10.402217	40
	3. 33/ 103	2:27-273	5 6 3 4 3 4				
21	9.598075	9.902890	9.035105		10.037110		39 38
22	9.598368	9.902830	9.035532		10.037219		
23	9.598660	9.902701	9.0350/9		10.037273		37 36
24	9.598952	9.902727	9.030220	10.363//4	10.037328		35
7.5	9-599244	9.902072	9.0305/2		10.037383		34
20	9-599536	9.902017	0.622266		10.037438		33
27	9.599827	9.902502	0.627611	10.262280	10.037492		32
20	9.600118	9.902500	0 627016	10 362044	10.037547	10.399591	31
29	9.600409	9.902453	0 628202	10.261608	10.037602	10.399300	30
30	9.600700	9.902390	9.030302				
31	9.600990	9.962343	9.038047	10.301353	10.037657	10.399010	29
32	9,601280	9.962288	9.038992	10.361008	10.037/12	10.398720	28
33	9.601570	9.902233	9.039337		10.037767		27
34	9.601860	9.902178	9.039082		10.037822	10,397850	26
35	9.602150	9.902123	9.040027		10.037933	10.397561	25
30	9.602439	9.902007	9.040371		10.037988	10.397272	24
37	9.602728	9.902012	9.040710	10.358940		10.396983	22
30	9.603017	9.901957	0.641404	10.358596	10.038008	10.396695	21
39	9 603305	9 901902	0.641747	10.358253	10.038154	10.396406	20
140	9.603594	y.yo. 040	3.541/4/	*******			
41	9.603882	9.961791	9.042091	10.357909	10.038209	10.396118	19
42	9.604170	9.901735	9.042434		10.038265		18
43	9-604457	9-901080	9.042777		10.038320		17
44	9.604745	9.901034	9.043120	10.350000	10.038376	10.395255	
45	9.005032	9.901509	9.043403	10.356537	10.038487	10.3949881	15
46	9 625319	9.901513	9.043800	10.550194	10.038487	10 204204	14
47	9.605606	9.901458	9.044148	10.355510	10.030542	10.204108	13
48	9-005092	9,901402	0.644822	10.755168	10.038664	10.302821	11
49	9-000179	9.901340	0 645174	10.355168	10.028710	10.202626	10
	9.606.165						
1 51	9.606751	9.961235	9 045516	10.354484	10.088765	19.393249	9
52	9.607036	9.901179	9.045857	10.354143	10.038821	10.392904	-
53	9.607322	9.901123	9.040199	10.353801	10.038877	10.392078	7
54	9.607607	9.961067	9.040540	10.353460	10.038933	10.392393	6
55	9.607892	9.901011	9.040881	10.353119	10.038989	10.392108	5
56	9.008177	9.900955	9.047222	10.352778	10 039045	10.391023	4
57	9.002401	9.900899	9.047502	10.352438	10.039101	10.201266	3 2
58	9.008745	9.900843	9.047903	10.352097	10.039137	10.200071	1
59	9.009029	9.900780	0612-23	10.351757	10.039214	10.300687	ò
00	9.609313 Co-sine.	9.950730	3.440303				
	/ h	Sine.	Co-tang	Tang.	Co-sec.	: Secant. ¹	M

M. Sine. Co-sine Tang. Co-tang. Secant. Co-sec. M.				24	Degrees.			- 5
0 9.609313 9.960730 9.628583 10.351417 10.039270 10.39087 60 2 9.609370 9.96074 9.628333 10.351077 10.039281 10.39087 3 9.610164 9.960361 9.649602 10.350938 10.039489 10.389886 57 4.9610749 9.960362 9.649602 10.350938 10.039489 10.389886 57 9.610749 9.960323 9.630620 10.349380 10.039489 10.389881 57 9.611074 9.960323 9.630620 10.349380 10.039691 10.38971 10.389	130	/ Sine.	Co-sine.	Tang.	Co-tang:	Secant.	Collec:	34
1 9.609507 9.960074 9.648937 10.350077 10.039324 10.360103 59 2 9.610164 9.960505 9.649942 10.350038 10.039439 10.380505 57 4 9.610747 9.960505 9.649942 10.350038 10.039439 10.380505 57 6 9.611074 9.960392 9.649042 10.350038 10.039439 10.380505 56 9 9.611074 9.960392 9.649042 10.349074 10.039658 10.380505 56 9 9.611074 9.960392 9.650200 10.349074 10.039658 10.388705 57 9 9.611858 9.960279 9.651297 10.348703 10.039668 10.388705 57 9 9.611858 9.960279 9.651297 10.348703 10.039671 10.388424 51 10 9.61240 9.960165 9.651297 10.348703 10.039718 10.388565 50 11 9.61240 9.960165 9.651297 10.348703 10.039718 10.388565 50 11 9.61240 9.960165 9.651297 10.348703 10.039718 10.388565 50 11 9.61240 9.960165 9.651297 10.348703 10.039718 10.388565 50 11 9.61240 9.950165 9.6512400 10.347688 10.039831 10.388565 50 11 9.61240 9.950165 9.6512400 10.347688 10.039831 10.388565 50 11 9.61240 9.950165 9.6512400 10.347688 10.039831 10.388529 48 12 9.61240 9.95088 29.953863 10.347688 10.039831 10.388529 48 13 9.61381 9.959988 29.953863 10.346034 10.000001 10.388517 47 14 9.61240 9.95088 9.653288 10.34603 10.00001 10.388517 47 15 9.61240 9.95088 9.65337 10.346049 10.00001 10.386173 41 19 9.614169 9.55054 9.65311 10.346049 10.00001 10.388615 45 10 9.61382 9.95988 9.653010 10.345089 10.00001 10.388615 41 10 9.61438 9.95993 9.655348 10.34361 10.00001 10.388617 41 10 9.61408 9.95080 9.65318 10.34508 10.00001 10.388617 41 10 9.61408 9.95080 9.65318 10.34508 10.00001 10.388617 41 10 9.61808 9.95080 9.65308 10.34080 10.00001 10.388617 41 10 9.61808 9.95080 9.65808 10.34080 10.00001 10.388617 10.000		-	_		The state of the s		-	40
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39 9.620213 9.958503 9.661710 10.338290 10.041497 10.279787 21 40 9.620488 9.958445 9.662043 10.237957 10.041555 10.379512 20 42 9.620488 9.958387 9.662043 10.337524 10.041613 10.376213 12 42 9.61038 9.958329 9.662709 10.337524 10.041671 10.378651 18 42 9.611038 9.958321 9.663042 10.335958 10.041671 10.378657 17 44 9.621687 9.958313 9.663042 10.335958 10.041671 10.378687 17 49 9.621687 9.95813 9.663375 10.335958 10.041787 10.378687 17 49 9.621689 9.95805 9.664039 10.355933 10.041846 10.378131 16 46 9.621339 9.958056 9.664039 10.335961 10.041904 10.377853 14 9.622662 9.957979 9.664703 10.335927 10.041904 10.377853 11 9.62266 9.95797 9.665035 10.335927 10.042021 10.377318 12 9.622956 9.95797 9.665035 10.335957 10.042021 10.377318 12 9.623501 9.957863 9.665366 10.334595 10.042079 10.377044 11 9.9623501 9.957863 9.665366 10.334595 10.042079 10.377044 11 9.623501 9.957863 9.665366 10.334595 10.042079 10.377044 11 9.9623501 9.957863 9.665366 10.334595 10.042177 10.376771 10.356771 10.623577 49.957746 9.665062 10.334595 10.042196 10.376498 9 9.623774 9.957746 9.666002 10.334595 10.042196 10.376498 9 9.623774 9.957746 9.666002 10.334595 10.042196 10.376498 9 9.623774 9.957746 9.666002 10.3335977 10.042196 10.376498 9 9.623774 9.957746 9.666002 10.3335977 10.042196 10.376498 9 9.623774 9.957746 9.666002 10.3335977 10.042196 10.376498 9 9.623774 9.957746 9.666002 10.3335977 10.042196 10.376498	37	I TO THE OWNER OF THE PARTY OF			A STATE OF THE PARTY OF THE PAR		CONTRACTOR AND ADDRESS OF THE PARTY AND ADDRES	
40 9.620488 9.958445 9.662043 10.337957 10.041575 10.379512 20 41 9.620763 9.958387 9.662376 10.337624 10.041613 10.376137 10 42 9.621038 9.958329 9.662709 10.337301 10.041671 10.378661 18 43 9.621513 9.95827 9.663042 10.336958 10.041791 10.378687 17 44 9.621587 9.958213 9.663375 10.336958 10.041787 10.378887 17 45 9.621861 9.958154 9.663757 10.356203 10.041787 10.378413 16 46 9.621233 9.95806 9.664039 10.335961 10.041904 10.377863 14 47 9.621409 9.958038 9.664371 10.335629 10.041904 10.377863 14 48 9.622682 9.957979 9.664703 10.335529 10.041904 10.377801 13 48 9.622682 9.957979 9.664703 10.335529 10.041904 10.377801 13 49 9.621936 9.957979 9.665035 10.335529 10.04201 10.377044 15 50 9.623529 9.957863 9.6656507 10.334303 10.042079 10.377044 11 51 9.623501 9.957864 9.665607 10.334303 10.042137 10.376498 9 52 9.623774 9.957746 9.666002 10.334303 10.042134 10.376498 9 52 9.623774 9.957746 9.666002 10.334303 10.042154 10.376498 9						No. of the last of	-	
41 9.620763 9.958387 9.662376 10.337624 10.041613 10.376137 10 42 9.621038 9.958329 9.662709 10.337301 10.041671 10.378661 1E 43 9.621513 9.958271 9.663042 10.336958 10.041791 10.378687 17 44 9.621587 9.958213 9.663375 10.336955 10.041787 10.378687 17 45 9.621861 9.958154 9.663707 10.356203 10.041846 10.378139 15 46 9.622133 9.958096 9.664039 10.335961 10.041904 10.377863 14 47 9.621409 9.958038 9.664391 10.335629 10.041904 10.377863 14 48 9.622682 9.957979 9.664703 10.335629 10.041904 10.377801 13 48 9.622682 9.957979 9.665035 10.335629 10.04201 10.377318 11 49 9.621926 9.957863 9.665051 10.334985 10.042079 10.377044 11 50 9.623252 9.957864 9.665667 10.334303 10.042137 10.37624 11 51 9.623501 9.957864 9.665607 10.334303 10.042137 10.376498 9 52 9.623774 9.957746 9.666002 10.334303 10.042134 10.376498 9					THE RESERVE AND ADDRESS OF THE PARTY OF THE	The second second second		
42 9.621038 9.958329 9.662709 10.337291 10.041671 10.378462 18 43 9.521313 9.958271 9.6650421 10.335958 10.041739 10.378687 17 44 9.621861 9.958154 9.665042 10.335632 10.041787 10.378413 16 45 9.621861 9.958154 9.665707 10.356303 10.041787 10.378413 16 46 9.621335 9.958096 9.664039 10.335961 10.041962 10.377865 14 47 9.621409 9.958088 9.664371 10.335921 10.041962 10.277591 13 48 9.622652 9.957979 9.664703 10.335829 10.041962 10.277318 15 49 9.621036 9.957979 9.665035 10.334985 10.042079 10.377044 15 50 9.621229 9.95863 9.665366 10.334634 10.042137 10.37624 11 51 9.623501 9.957804 9.665697 10.334303 10.042196 10.376498 9 52 9.623774 9.957746 9.666602 10.334303 10.042154 10.376498 9 52 9.623774 9.957746 9.666602 10.334303 10.042154 10.376498 9				2000		-	-	=
43 9.621383 9.958271 9.6652042 10.336958 10.041729 10.378687 17 44 9.621387 9.958213 9.6653707 10.336958 10.041787 10.3788413 16 45 9.6212861 9.95838 9.6653707 10.356233 10.041787 10.3788413 16 46 9.6212409 9.958038 9.664371 10.335961 10.041962 10.377505 14 47 9.6212409 9.958038 9.664371 10.335629 10.041962 10.377505 14 48 9.622652 9.957979 9.664703 10.335997 10.042071 10.377318 12 49 9.621229 9.957863 9.665035 10.334965 10.042079 10.377044 11 50 9.623229 9.957863 9.665667 10.334303 10.042171 10.376771 10 51 9.623502 9.957864 9.665067 10.334303 10.042196 10.376498 9 52 9.623774 9.957746 9.666002 10.334303 10.042196 10.376498 9		The second second				ALCOHOLD STREET, STREE	The second second	
44 9.621887 9.95813 9.663375 (0.336025 10.041787 10.378413 16 45 9.621861 9.95814 9.663375 (0.336025 10.041846 10.378133 15 46 9.621833 9.958096 9.664039 (0.335026 10.041964 10.37833 15 47 9.621409 9.958038 9.664371 (0.335026 10.041964 10.377865 14 48 9.622686 9.957979 9.664703 (0.335297 10.042041 10.377318 12 49 9.622696 9.957921 9.665035 (0.334965 10.042079 10.377044 11 50 9.623601 9.957864 9.665087 (0.334303 10.042196 10.376498 9 51 9.623601 9.957864 9.665087 (0.334303 10.042196 10.376498 9 52 9.623774 9.957746 9.666002 (0.3333971 10.042196 10.376498 9		The second second				THE REAL PROPERTY.		
45 9.621861 9.958154 9.663707 10.356293 10.041846 10.378139 15 46 9.622136 9.958096 9.666039 10.335961 10.041904 10.377865 14 47 9.622409 9.958038 9.664371 10.335629 10.041904 10.377865 13 48 9.622682 9.9577979 9.665703 10.335297 10.042021 10.377318 12 49 9.622936 9.957921 9.665035 10.334965 10.042021 10.377044 11 50 9.623501 9.957863 9.665366 10.334965 10.042137 10.376771 10 51 9.623501 9.957864 9.665697 10.334303 10.042196 10.376498 9 52 9.623774 9.957746 9.6660029 10.3333971 10.042136 10.376498 9								
46 9.621133 9.958036 9.664039 10.335961 10.041904 10.377863 14 47 9.621409 9.958038 9.664371 10.335829 10.041962 10.277802 13 48 9.622682 9.957979 9.664703 10.335297 10.042021 10.377388 14 49 9.621936 9.957921 9.665035 10.334965 10.042079 10.377044 11 50 9.621229 9.957863 9.665366 10.334965 10.042137 10.376771 10 51 9.623501 9.957804 9.665697 10.334303 10.042196 10.376498 9 52 9.623774 9.957746 9.666002 10.334303 10.042134 10.376498 9						Contract of the Contract of th	the second second	
47 9.621409 9.958038 9.664371 10.335629 10.041962 10.277591 13 48 9.622622 9.957979 9.664703 10.335629 10.042021 10.377318 12 49 9.621936 9.957921 9.665035 10.334965 10.042079 10.377044 11 50 9.621229 9.957863 9.665366 10.334034 10.042137 10.376241 11 51 9.623501 9.957804 9.665697 10.334303 10.042196 10.376498 9 52 9.623774 9.957746 9.666029 10.334303 10.042196 10.376498 9			A THE STATE OF					
48 9.622682 9.957979 9.664703 10.335297 10.042011 10.377318 12 49 9.622936 9.957921 9.665035 10.334965 10.042079 10.377044 11 50 9.623202 9.957863 9.665366 10.334634 10.042137 10.376771 10 51 9.623501 9.957804 9.665697 10.334303 10.042196 10.376498 9 52 9.623774 9.957746 9.666029 10.333971 10.042196 10.376498 8		The Street Street					THE RESERVE TO THE RE	
49 9.622936 9.937921 9.665035 10.334965 10.042079 10.377044 11 50 9.623229 9.957863 9.665366 10.334634 10.042137 10.376771 10 51 9.623501 9.957804 9.665697 10.334303 10.042196 10.376498 9 2 9.623774 9.957746 9.666029 10.333977 10.042196 10.376498 8	176		Mark Committee					
\$0 9.623229 9 957863 9.665366 10.334634 10.042137 10.376771 1D \$1 9.623501 9.957804 9.665697 10.334303 10.042196 10.376498 9 \$2 9.623774 9.957746 9.666029 10.333971 10.042244 10.376226 8					MARKET AND ADDRESS OF THE PARK			
1 9.623501 9.957804 9.665697 10.334303 10.042195 10.378498 9 52 9.623774 9.957746 9.666029 10.3333971 10.042244 10.376226 8								
52 9.623774 9.957746 9.666029 10.333971 10.042254 10.376226 8	Name of	-	THE RESERVE OF THE PERSON NAMED IN	1000	-	-	The same of	
								9
\$\frac{9}{.924\sqrt{9}}\frac{9}{.957\sqrt{628}}\frac{9}{.966\sqrt{6069}\text{s}}\frac{10.333304}{10.043373}\frac{10.37\sqrt{953}}{10.37\sqrt{628}}\frac{7}{65}\frac{9}{.952\sqrt{628}}\frac{9}{9}\frac{66609\text{s}}{10.333320}\frac{10.043371}{10.04371}\frac{10.37\sqrt{628}}{10.37\sqrt{603}}\frac{5}{10.043430}\frac{10.37\sqrt{603}}{10.37\sqrt{603}}\frac{5}{10.042430}\frac{10.37\sqrt{603}}{10.37\sqrt{603}}\frac{5}{10.0425\sqrt{603}}\frac{10.37\sqrt{603}}{10.37\sqrt{603}}\frac{10.0425\sqrt{603}}{10.042607}\frac{10.042607}{10.042607}\frac{10.37\sqrt{603}}{10.042607}\frac{10.042607}{10.042607}\frac{10.37\sqrt{603}}{10.042607}\								. 8
65 9.624891 9.9577570 9.667621 10.333309 10.042430 10.375409 10.624863 9.957511 9.667352 10.322048 10.042489 10.375409 10.667352 10.322048 10.042489 10.375409 10.375439 10.325448 10.042489 10.375439 10.375439 10.625439 10.375439 10.625439 10.375439 10.625439 10.375439 10.625439 10.625439 10.625439 10.625439 10.62563	153							7
16 9.624863 9.957511 9.667632 10.332504 10.642436 10.375409 4 17 9.625135 9.957452 9.667682 10.332548 10.642489 10.375439 4 18 9.625406 9.957393 9.668613 10.33198 10.642607 10.374394 2 19 9.625677 9.957335 9.668613 10.331657 10.642665 10.374322 1 10 9.625677 9.957336 9.668672 10.331328 10.64265 10.374322 1 10 9.625648 9.957376 9.668672 10.331328 10.642714 10.374052 1 10 Consider view Contains. Tang. Consecutive security	10+							
7 9.625436 9.9573452 9.667682 10.332318 10.042548 10.374865 2 58 9.625406 9.957393 9.668633 10.331657 10.042665 10.374394 2 9.625406 9.957396 9.668343 10.331657 10.042665 10.374392 2 10.042648 9.957376 9.668672 10.331328 10.042714 10.374052 10.042665 10.374322 10.042665 10.374322 10.042665 10.374322 10.042665 10.374322 10.042665 10.374052 10.042665 10.042665 10.374052 10.042665 10.04	155							5
79 9.625406 9.957393 9.668613 10.321987 10.042607 10.374894 2 59 9.625406 9.957335 9.668633 10.321657 10.042667 10.374894 2 60 9.675948 9.957376 9.668672 10.331328 10.042714 10.374051 0 60 9.675948 9.957376 0.068672 10.331328 10.042714 10.374051 0 60 9.675948 9.957376 0.068672 10.331328 10.042714 10.374051 0 60 9.05867 10.042714 10.374051 0 60 9.05867 10.042714 10.374051 0 60 9.05867 10.042714 10.374051 0 60 9.05867 10.042714 10.374051 0 60 9.05867 10.042714 10.042	150							4
19 9.625977 9.957335 9.668343 10.331657 10.042665 10.374322 10.00 10.042665 10.374322 10.00 10.042665 10.374322 10.00 10.042665 10.374322 10.00 10.042665 10.374051 10.042665 10.042665 10.374051 10.042665 10	157							3
160 9 675945 9.957276 9.668672 10.331328 10.042724 10.374052 10.374052 10.042724 10.374052 10.042724 10.374052 10.042724 10.374052 10.042724 10.374052 10.042724 10.374052 10.042724 10.374052 10.042724 10.374052 10.042724 10.374052 10.042724 10.374052 10.042724 10.374052 10.042724 10.374052 10.042724 10.374052 10.042724 10.374052 10.042724 10.374052 10.042724 10.374052 10.042724 10.04	130							7
M Casin Sine Cottang, Tang Cosen, Secont in	160					10.042005	10.374322	
M County Sine Costing, Tang, Coston Second in	-		-					
	1 74	Country	anne .	Co-tang.	Tank.	00.800	Secant	21

			23 .	Degrees.			>
M	, Sine.	Co-sine.	Tang.	Co-tang.	Secant.	Co-sec.	М
0	9.625948	9.957276	9.668673	10.331327	10.042724	10.374052	60
1	9.626219			10.330998	10.042783	10.373781	59
2	9.626490	9.957158	9.669332	10.330668	10.042842	10.3735101	
3		9.957099				10.373240	57
4		9.957040	9.669991		10.042960	10.372970	56
Ş		9 956981		10.329680	10.043019	10.372700	55
6		9.956921		10.329351	10.043079	10.372430	54
7				10.329023 10.328694	10.043138	- ·	53
ŷ		9.956744		10.328366	10.043197	10.371891	52
10	9 628647	9.956684	9.671963		10.043316	10.371353	5 E 50
11	9.628916	9 956625	9.672291				
12		9.956566		10.327709	10.043375 10.043434	10.371084	49 48
13		9.956506			10.043494		
14				10.326726	10.043553	10.370279	47 46
15				10.326398	10.043613	10.370011	45
61				10.326071	10.043673		44
17	9 630524	9.956268	9.674257	10.325743	10.043732		43
18	9.630792	9.956208	9.674584	10.325416	10 043792	10.369208	43
19	9.631059			10.325090		10.368941	41
20	9.631326	9.956089	9.675237	10.324763	10.043911	10.368674	40
21		9.956029			10.043971	10.368407	39
22				10.324110	10.044031	10.368141	38
23				10.323783	10 244091	10.367875	37
24				10.323457		10.367608	36
25 26				10.323131	10.044211	10.367342	35
27				10.322806		10.367077	34
28		9.955609		10.322450	10.044391	10.366546	33 32
29				10.321829			31
3ó		9.955488		10.321504		10.366016	30
31		9.955428	9.678821	10.321170			29
32		9.955368		10.320854			28
33	9.634778	9.955307	9.679471			10.365222	27
34	9.635042		9.679795	10.320205	10.044753	10.364958	26
35		9.455186		10.319880		10.364694	25
36		9.955126	9.680444			10.364430	24
37		9.955065	9.680768		10.044935	1	23
38	9.636097	9.955005	9.681092	10.318908 10.318584	10.044995	10.363903	22
39 40	9.636623	9-954944 9-954883	9.681740		10.045056	10.363640	21
41	9.636886	9 954823	9.682063			10.363114	19
42 43	9.637148	9.954762 9.954701	0.682710	10.317613	10,045238	10.362852	17
44		9.954640				10.362327	16
55			9.683356		10.045421	10.362065	15
46	9.638197	9.954518				10.361803	14
47		9.954457	9.684001	10.315999	10.045543	10.361542	13
48		9.954396	9.684324	10.315676	10.045604	10.361280	12
49	9.638981	9-954335		10.315354	10.045665	10.361019	11
50	9.639242	9.954274	9.684968	10.315032	10.045726	10.365758	10
١٠	9.639503	9.954213	9.685290	10.314710	10.045787	10.360497	9
				10.314388			8
53				10.314066			6
54	0.640644	9.954029	0.686	10.313745	10.045971	10.359716	
55 56	0.642804	9.953908	0.686808	10.313423		10.359450	5 4
57		9.953845				10.358936	3
58				10.312460		10.358676	2
59		9 953722			10.046278	10.358417	1
69		9.953660		10.311818	10.046340	10.358158	0
м	Co-sine.	Sine.	Co-tang	Tang.	Co-sec	Secant.	M
				7.			

	A STATE OF	-	201	Degrees-	2200	-	
M	, Sine,	Co-sine.	Tung	Co-tang.	Secant.	Co-sec.	26
	The same of					_	60
0	9.641842	9 953660	9.005152	10.311818	10.046340	10.358158	
1 1	9.642101	9-953599	9.688502	10.311498	10 046401	10 357899	59
12	9.642360	9-953537	9 688823	10.341177	10-046463	10.357640	58
	9.642618	9.953475	9.689143	10.310857	10.046525	10.357382	57
13	9.642877	9 953413	9 689463	10.310537	10.046587	10.357123	56
14	A THE REST LAND		9.689783	10.310217	10,046648	10 356865	
1 5	9.643135	9 953352					55
6	9.643393	9.953190	9.690103	10 309897	10.046710	10.356607	54
7 8	19.643050	9.953228	6.690423	10-309577	10.046772	10.356350	53
8	9.643908	9.953100	9.690742	10-309258	10.046854	10.356091	52
9	9.644165	9.953104	9.691062	10.308938	10.046896	1D.555835	51
10	9.644423	9.953042	9.691381	10.308619	10.045958	10.355577	60
		-			-	10.155320	
21	9.644680	9.952980	9.691700	10.308300	10.047020	SHEET AND ADDRESS OF THE PARTY	42
12	9.644936	9.952918	9.692019	10-307981	10.047082	10,355064	48
13	19.645193	9.952055	9.092338	10.307661	10.047145	ID-354BOY	47
14	9.645450	9.952793	9.692656	10 307344	10.047307	ED.354550	46
25	9.645706		9-692975	10-307025	10.047269	10.354164	45
16	9.645962	9.952669	9.693293	10-300707	10.047331	10.354038	44
	9.646218	9.952600	9.693612	10-306388	10.047394	ID-353782	43
17		San Street Company of the Company of					
13	9 646474		9.693930	10-306070	10.047456	10.353526	100
19	9-640729	9.952481	9.694248	10.305752	10.047519	20.352171	#
20	9.646984	9.952419	9 694566	10.305434	10.047581	10.353016	40
21	9.647240	9.952356	9.694883	10.305117	10.047644	10.352760	39
23		The second second	9.095201	10.304799	10.047706	10.352406	38
1000	9.047494	No. of Participation,		10.304482	No. of Concession, Name of Street, or other Persons, Name of Street, Name of S	10.352251	32
23	19-647749	9.951131	9.695518	The second second	10.047769		
24	9.648004		9.695836	10-304164	10.047833	10.351096	30
25	9.648258	9.952106	9.696153	10 303847	10.047894	10.351743	35
26	9.648512	9 952043	9.696470	10.303530	10-047957	10.351488	34
27	9.648766	9.951980	9 696787	10.303213	10.048020	10.351234	33
28	9 644020	9.951917	9 697103	10.301897	10.048081	10.350980	32
29	0 649274	9.951854	9.697420	10.302580	10.048146	10.350716	31
	The second second		Annual Control of the Control	10.301164	10 048209	10.950473	
30	9.649527	9.951791	9.697736	101301104	-		30
34	9.649781	9 951728	9.098053	10.301947	10,048271	10.550219	20
32	9 650034	9.951665	9.698369	10.301631	10.048334	10-349966	28
33	9.650287	9.951602	9.698685	10-301315	10.048398	10.349713	27
34	9.650539	COMPANIES OF STREET	9.699001	10.300999	10.048461	10.340461	26
35	9.650792	A COMPANY OF THE PARTY OF	9.699316	10.300684	10.048523	10-349208	25
					10.048538		
36	9.651044	9-951412	9 099632	10.300368	A STATE OF THE PARTY OF THE PAR	10.348946	181
37	9.651297	9.951349	9.699947	10.300053	10.048551	10.348703	#5
38	19.05 \$ 549	9.951286	9.700263	10.299737	10.048714	10.348451	22
139	9.651800	9.951222	9.700578	10.299422	10.048778	10.348200	21
40	19.652052	9.951159	9.700893	10.299107	10.048841	10.347948	20
			-	10.298792	-		$\overline{}$
41	9 652304		9 701208		10.048904	10,347696	10
42	9.652555	A COLUMN TWO IS NOT THE OWNER.	9.701523	10.298477	10.048968	10.347445	18
43	9.652806	9.950968	9.701837	10.298163	10.049032	10.347494	17
44	9.653057	9.950905		10.297848	10.049095	10.340943	10
45	9.653308	9.950841	9.702466	10.297534	10.049159	10.346692	15
46	9.653558	9.950778	9.702780	10.297220	10.049222	10.345441	14
47	9.653808		9.703005	10.296905	10.049280	10.346192	13
48	9.654059	9.950650	9.703400	10.296591	10.049350	10-345941	12
	9.654309	9.950586	9.703723	10.296277	10.049414	10-345691	22
49	THE RESIDENCE OF THE PARTY OF T	DATE OF THE PARTY AND ADDRESS OF THE PARTY AND	THE RESERVE OF THE PARTY OF THE		State of the last	The second secon	-
50	9.054558	9-950522	9.704036	10.295964	10.049478	10.345442	10
51	9.654808	9.950458	9.704350	10.295650	10.049541	10.345192	9
52	19.655068	9.950394		10.295337	The second second	10.244942	8
153				10.295023	10.049670	10.344693	17
				10. 2947 10	10.049734		6
54					Contraction of the last of the		
155				10.294397		10.344195	2
150				10.294084	10.049863	10.343946	
55 56 57 58				16.293772	10.049926	10.345698	3
158		9.950010	9.706541	10.293459	10 029990	10.343449	
59	9.056799		9.706854		10.050055	10.343201	100
160	9.657047	9.949881	9 707166	10.292834	10.050119	10.342953	0
N	Co-sine.	Sine.	Co-tang.	Tang.			
100	Co anic.	Diffe.	Co-tang.	rang.	Co-sec.	Secant.	31

27 Degrees.

N Sine Co-sine Tage Co-tang Secant Co-sec N				21	Degrees.			
1	м	, Sine.	Co-sine.	, Tang.	Co-tang	Secant.	Co-sec.	M
1	0	0.657047	0.040881	0.707166		10.060110		60
2 9.657742 9.949688 9.708102 10.291898 10.250312 10.34210 57 69 658037 9.949688 9.708102 10.291886 10.250312 10.342210 57 69 65878 9.949528 9.708726 10.291274: 10.050442 10.341716 55 69 658531 9.9494949 9.709349 10.290651 10.2050571 10.341292 53 10.290631 10.290631 10.341249 53 9.9659271 9.949300 9.709971 10.290239 10.250700 10.340248 59 9.9659271 9.949325 9.710282 10.289407 10.050570 10.340248 50 10.290571 10.965971 9.949300 9.709971 10.280296 10.050570 10.340248 50 10.290571 10.965976 10.340248 50 10.28026 10.050570 10.340248 50 10.28026 10.28026 10.050570 10.340248 50 10.28026 10.050570 10.340248 50 10.28026 10.28026 10.050570 10.340248 50 10.28026 10.050570 10.340248 50 10.28026 10.050570 10.340248 50 10.28026 10.28026 10.050570 10.340248 50 10.28026 10.050570 10.340248 50 10.28026 10.28026 10.050570 10.340248 50 10.28026 10.050570 10.340248 50 10.28026 10.28026 10.280274 47 10.28026 10.28026 10.280274 47 10.28026 10.28026 10.280274 47 10.28026 10.28026 10.280274 47 10.28026 10.28026 10.280274 47 10.28026 10.28026 10.280274 47 10.28026 10.28026 10.280274 47 10.28026 10.28026 10.280274 47 10.28026 10.28026 10.280274 47 10.28026 10.28026 10.280274 47 10.28026 10.28026 10.280274 47 10.28026 10.28026 10.280274 47 10.28026 10.28026 10.28026 10.33024 47 10.28026 10.28026 10.28026 10.33024 47 10.28026 10.28026 10.28026 10.33024 40 10.28026 10.28026 10.28026 10.33026 10.33026 10.28026 10.28026 10.28026 10.33026 10.33026 10.28026 10.28026 10.28026 10.28026 10.33026 10.33026 10.28026 10.28026 10.28026 10.28026 10.33026 10.28026 10.28026 10.28026 10.33026 10.33026 10.28026 10.28026 10.28026 10.33026 10.33026 10.28026 10.28026 10.28026 10.33026 10.33026 10.28026 10.28026 10.28026 10.33026 10.33026 10.28026 10.28026 10.28026 10.33026 10.33026 10.33026 10.28026 10.28026 10.28026 10.33026 10.33026 10.33026 10.28026 10.28026 10.28026 10.33026 10.33026 10.28026 10.28026 10.28026 10.33026 10.33026 10.28026 10.28026 10.28026 10.28026 10.33026 10.33026 10.28026 10.28026 10.28026 10.28026 10.28026 10.28026 10.28026 10.28026 10.	1		0.040816					1
3 9.667790 0.949688 9.708102								
4 9.65837 9.949633 9.708414 10.291586 10.050377 10.341963 56 9.658384 9.949558 9.708726 10.291274 10.050442 10.341716 55 56 9.965878 9.949499 9.709349 10.290651 10.050571 10.341465 54 56 56 56 56 56 56								
5 96;8884 994958 9.708726 0.201274; 10.050452 10.341716 55 6 96;8778 9.949494 9.709037 10.29065; 10.050506 10.341040 5 9.96;9878 9.949439 9.709349 10.29065; 10.050506 10.340483 5 9.96;9878 9.949305 9.70934 10.29065; 10.050506 10.340483 5 10.96;9763 9.949305 9.710593 10.28906 10.050765 10.340483 5 10.96;9763 9.949105 9.710593 10.28906 10.050765 10.340483 5 10.96;9763 9.949404 9.711215 10.288735 10.050765 10.339991 48 15 9.660506 9.948975 9.711545 10.288735 10.050765 10.339949 46 17 9.660506 9.94876 9.711215 10.288735 10.050765 10.339949 46 17 9.660506 9.94876 9.711246 10.287834 10.051025 10.339949 46 17 9.66136 9.94876 9.711246 10.28784 10.051025 10.339949 46 17 9.66136 9.94854 9.711246 10.28784 10.05115 10.33900 44 19.9661726 9.94854 9.711266 10.287834 10.05115 10.33900 44 19.9661726 9.94854 9.711266 10.287834 10.05115 10.338274 41 19.660234 9.94854 9.711266 10.28624 10.05116 10.338030 10.2866149 9.948388 9.714314 10.28595 10.051646 10.338734 32 9.662319 9.948259 9.71658 10.285686 10.051646 10.337741 38 9.66390 9.948333 9.71454 10.28595 10.051646 10.337741 38 9.66390 9.948329 9.716471 10.28595 10.051677 10.330580 31 9.666406 9.947919 9.716675 10.285976 10.051743 10.336380 32 9.664406 9.947919 9.716675 10.285976 10.05137 10.335594 30 9.666807 9.948000 9.71860 10.28565 10.05137 10.335594 30 9.666807 9.948739 9.716687 10.28597 10.052337 10.333508 31 9.666517 9.947031 9.716675 10.28597 10.052337 10.33568 32 9.666807 9.94733 9.716675 10.28567 10.052337 10.33568 32 9.666807 9.94733 9.716675 10.28597 10.052337 10.33368 32 9.666869 9.94733 9.716675 10.28597 10.052337 10.33368 32 9.666869 9.946040 9.71876 10.28598 10.052361 10.33141								
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7 9-658778 9-949429 9-709349 10.290651 10.050571 10.341222 53 9-659371 9-949300 9-709971 10.29029 10.050505 10.340795 51 10 9-659517 9-949325 9-710282 10.289407 10.050530 10.340729 51 11 9-65009 9-949105 9-710593 10.289407 10.050830 10.340237 49 11 9-660050 9-949105 9-711215 10.288735 10.050505 10.340237 49 11 9-660050 9-949040 9-711215 10.288735 10.050505 10.339914 48 11 9-66050 9-949040 9-711215 10.288735 10.050505 10.339919 48 11 9-66050 9-948845 9-711215 10.288735 10.051025 10.339349 45 11 9-66050 9-94885 9-711215 10.288735 10.051025 10.339349 45 11 9-660746 9-94885 9-711246 10.28734 10.051125 10.339309 44 12 9-661726 9-94885 9-71246 10.28734 10.051125 10.339300 44 13 9-661726 9-94885 9-71246 10.28734 10.051125 10.338300 44 14 9-661726 9-94885 9-71246 10.28734 10.051125 10.338374 47 14 9-661726 9-94885 9-71246 10.28734 10.051125 10.338374 47 14 9-66214 9-948849 9-71306 10.28634 10.051126 10.338374 47 14 9-66224 9-948849 9-71306 10.28634 10.051126 10.338374 47 14 9-66234 9-948838 9-714313 10.285995 10.05148 10.337785 39 12 9-66317 9-948250 9-714933 10.285995 10.05148 10.337781 38 12 9-66317 9-94826 9-714933 10.285995 10.05146 10.337541 38 13 9-66406 9-947999 9-714933 10.285905 10.05146 10.337541 38 13 9-66406 9-947999 9-716578 10.285231 10.05128 10.33551 35 14 9-665379 9-94826 9-714536 10.285231 10.05128 10.33551 35 15 9-665879 9-947803 9-71658 10.285231 10.05128 10.33551 33 15 9-665879 9-947695 9-716979 10.283231 10.052337 10.335502 32 15 9-665879 9-947695 9-716979 10.283231 10.052337 10.333532 32 15 9-666824 9-947797 9-717091 10.283233 10.052071 10.335534 32 15 9-665879 9-947695 9-71678 10.283231 10.052335 10.333517 31 15 9-666824 9-947760 9-718791 10.283231 10.052335 10.333367 32 16 9-66824 9-947760 9-718791 10.283231 10.052335 10.333367 32 17 9-66600 9-947979 9-716477 10.283331 10.052335 10.333367 32 18 9-669468 9-947979 9-716477 10.283331 10.052361 10.333558 32 18 9-669469 9-94880 9-94880 10.28988 10.053356 10.333658 32 18 9-669469 9-94880 9-94880 10.28988 10.053356 10.333658 32 18 9-669468 9-94680 9-9	6							
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	9.671609	0.045026		10 274326			60
ĭ	0.671817	9.945868		10.274021		10.328153	
2				10 273716		10.327916	59 58
3		9.945733		10.273412		10.327679	57
4		9.945660		10.273108		10.327442	56
5				10.272803		10.327205	55
6	9.673032		9.727501			10.326968	54
7		9 945464	9.727805			10.326732	53
ક			9.728109	10.271891		1	52
9		9.945328		10.271588	10.054672		51
10	9.673977	9.945261	9.728716	10.271284	10.054739	10.3 26023	50
11	9.674213	9.915193	9.729020	10,270980	10.054807	10.325787	49
12		9.945125		10.270677		10 325552	48
13	9.674684	9 945058	9.729626	10.270374	10.054942	10.325316	47
14	9.674919	9.944990	9.729929	10.270071	10.055010	10.325081	46
15	9.675155	9.944922	9.730233	10.269767	10.055078	10.324845	45
16	1 , , , , , ,	9.944854		10.269465		10.324613	44
17			9-730838				43
18		9.944718		10.268859	* * *		42
19		9.944650		10.268556			41
20			9-731746	10.208254	10.055418	10 323672	40
21			9.732048	10.267952	10.055486	10.323438	39
			9.732351				38
	9 677030			10.267347			37
			9.732955			10.322736	36
25			9.733257	10.266743		10.322502	35
27			9.733558	10.266442			34
			19.734162	10.265838		10.322036	33 32
	9.678430			10.265537		10.321570	31
30			9.734764	10.265236		10.321337	30
1			9.735066				
31				10.264934		10.321105	29 28
				10.264332			27
				10.264031		10.320408	26
				10.263731		10.320176	25
36	9.680056	9.943486	9.736570	10 263430	10.056514	10.319944	24
37	9.680288	9.943417	9.736871	10.263129	10.056583	10.319712	23
38	9.680519	9.943348	9.737171	10.262829	10 056652	10 319481	22
39	9.680750	9.943279	9 737471	10.262529	10.056721	10.319250	21
40	9.680982	9.913210	9.737771		10.056790		20
41	9.681213	9.943141	9.738071	10.261929	10.056859	10.318787	19
			9.738371	10.261629	10.056928	10.318557	18
43				10.261329			17
44	9.681905	9-942934	9.738971		10.057066		16
45	9.082135	9.942864	9.739271	10.200729	10.057136	10.317865	15
40				10.260430			14
				10.260130 10.259831			13
10	9.682025	0.042289	9.740168	10.250622	10.057344		12 11
50	9.683284	9.94-34/	9.740767	10.259233		10.316716	10
				10.258934			
52	0.682712	y.y+4++0	0.74126	10.258634	10.057552	10.316486	8
53	9.682072	0.042208	9.74166	10.258336	10.057602	10.216028	7
54	9.68.1201	9.942220	9.741062	10.2580:8	10.057761	10.315799	6
55	9.684433	9.942160	9.742261	10.257739	10.057821	10.315570	5
56	9.684658	9.942099	9.742559	10.2574411	10.057901	10.315342	4
57	9.6848\$7	9.942029	9.742858	10.257142	10.057971	10 315113	3
58	9.085115	9.941959	9.743156	10.256844	10.058041	10.3148851	2
591	9.685343	9.941889	9.743454	10.256546	10.058111	10.314657	1
60	9.6855-1	9.941819	9.743752	10.256248	10.058181	10.314429	_ 0
M (Co-sine.	Sine.	Co-tang.	Fang.	Co-sec.	Secant.	м
							

29 Degrees.

			29 1	Degrees.			
м	Sine.	Co-sine.	Tang	Co-tang	Secant.	Co-sec.	м
O.	9.685571	9.9418:9	9.743752	10 256248	10.058181		<u>(iii</u>
1	9.685799	9.941749	9.744050	10.255950	10.058251	10.314201	59
2	9.686027	9 941679	9-744348	10.255652	10.058321	10.313973	58
3	9.686254	9.941609	9.744645	10.255355	10.058391	10.313746	57
14	9.080482	9.941539	9.744943	10.255057	10.058461	10.313518	56
5	0.686026	0.041208	0.745240	10.254760	10.058531	10.313291	55
7	9.687163	0.041728	0.745825	10.254165		10.313004	54 53
8	9.687389	9.941258		10.253868		10.312611	52
9	9 687616	9.941187		10.253571		10.312384	ςι
10	y.687843	9.941117	9.746726	10.253274		10.312157	50
11	9.688069		9.747023	10.252977	10.058454	10.311931	49
12	9.688295	9.940975	3-747319	10.252681	10.059725	10.311705	
13	9.688521	9.940905	9.747616	10.252384		10.311479	
14	9.688747	9.940834	9.747913	10.252087		10.311253	46
16	9.688972 9.689198			10.251791		10.31 1028	45
17	9.689423	9.940693		10.251495		10.310802	44
18	9 689648		9.749097	10.250903	10.059449		43
19	9.689873	9.940480		10.250607	10.059520	10.310332	41
20	9.690098	9.940409		10.250311	10.059591	10.309902	40
21	9.690323	9.940338		10.250015	10.059662	10.309677	39
22		9.940267		10.249719	10.059733		38
23	9.690772	9.940196	9.750576	10.249424		10.309228	
24		9.940125			10.059875	10.309004	36
25	9.691220	9.940054	9.751167	10.248833		10.308780	35
26 27	0.601668	9.939982	9.751402	10.248538	10.060018	10.308556	34
28	0.601802	9.939911 9.939840	9.751757	10.248243	10.060089	10.308332	33
29		9.939048		10.247948 10.247653	10.000103	10.308168	32 31
30		9.939697	9.752642	10.247358		10.307661	30
31		9 939625		10.247063			
32	9.692785	9.939554	0.753231	10.246769		10.307438	29 28
33	9 693008	9.939482	9.753526	10 246474	10.060518	10.306992	27
34	9.693231	9.939410	9.753820			10.306769	26
35		9.939339		10 245885	10.060651	10 306547	25
36	9.693676	9.939267	9.754409	10.245591	10.060733	10.30632.1	24
37 38	9.093098	9.939195	9.754703	10.245297	10.060805	10.306102	23
39		9.939123 9.939052		10.245003	10.060877	10.305880	2,2 2,1
40	9.694564	9.938980	9.755585	10.244415	10.060948	10.305658	20
41		9.938908					
42		9.938836		10.244122	10.061092	10.305214	18
43	9.695229	9.938761	9.756465	10.243535	10.061237	10.304993	17
44	9.695450	9.938691	9.756759	10.243241		10.304550	36
45	9.695671	9.938619	9.757052	10.242948	10.061381	10.304329	15
46	9.6 15892	9.938547	9.757345	10.242655	10.061453	10.304108	14
47	9.090113	9.938475	9.757638	10.242362		10.303887	13
48 49	9.696554	9.938402	9.757931	10.242069	10.061598	10.303666	12
50	9.696775	9.938258	9.758517	10.241776	10.061670		10
51				10.241190		10.303225	
52	9.090995	0.028112	9.75010	10.241190	10.061815	10.303005	9
53	9.697435	0.038010	0.750305	10.240605		10.302785	
54	9.697654	9.937967	9.759687			10.302346	7
55	9.097874	9.937895	9.759979	10.240021		10,302126	5
56	9.698094	9.937822	9.760272	10.239728	10.062178	10.301906	4
57	9.698313	9.937749	9.760564	10.239436	10.062251		3 2
58	0.098532	9.937676	9.760856	10.239144	10.062324	10.301468	
59	0.608070	9.93/004	9.701148	10.238852	10.062396	10.301249	1
						10.301030	
N,	Co-sinc.	Sine.	Co-tang, l	Tang.	Co-sec.	Secant.	м

Sine. Co-sine. Tang. Co-tang. Secant. Co-sec. 31	4			-	- 30 1	Degreea.	-	_	
0 9.698970	T	M	Sine.	Co-sine.	Tang.	Co-tang.	, Secant.	Co-sec.	- 36
1 9.699189 9.93738 9.761731 10.218869 10.06242 10.100513 59 9.969940 9.93738 9.76260 10.237394 10.062615 10.30037 57 9.96002 9.97703 9.76260 10.237394 10.06208 10.30037 57 9.700040 9.937019 9.76237 10.20210 10.06208 10.299720 58 9.700716 9.936940 9.76237 10.20210 10.06208 10.299720 58 9.700716 9.936940 9.76237 10.20210 10.06208 10.299720 58 10.970115 9.926799 9.76237 10.23621 10.06208 10.299720 58 10.970115 9.926799 9.76238 10.23523 10.06238 10.299607 51 10.970115 9.92679 9.76238 10.235207 10.05238 10.05238 10.299607 51 10.970180 9.99575 9.76234 10.335207 10.05231 10.05231 10.06208 10.299607 51 10.970180 9.99575 9.76234 10.33507 10.063348 10.299608 47 47 47 47 47 47 47 4	1	-	o Sallann			TO VARIET	In obserte	-	
2 9.699407 (9.937315 9.768031 10.237686 10.066688 10.30373 57 9.769069 9.937315 9.768071 10.23738 10.066388 10.30373 57 9.700669 9.937016 9.768071 10.23731 10.066381 10.30373 56 9.9700380 9.937002 9.761479 10.23631 10.066381 10.39993 54 9.700716 9.936946 9.763770 10.23631 10.066381 10.29993 54 9.700716 9.936946 9.763771 10.23631 10.066381 10.239938 51 10.99038 10.99938 51 10.970115 19.996799 9.764351 10.23631 10.066381 10.239938 51 10.99038 10.99938 51 10.970185 9.936725 9.764441 10.23532 10.066381 10.23638 10.239038 11 13.9701808 9.936725 9.764441 10.23532 10.065328 10.236634 10.236631 12.99039 9.96558 9.76524 10.23533 10.063388 10.23908 12.99738 12.99038 9.96575 9.76524 10.23531 10.06338 10.05908 10.23663 12.99038 12.99038 9.96575 9.76524 10.23531 10.063369 10.239638 10.239	п				the second second	The second second	THE RESERVE AND ADDRESS OF THE PERSON NAMED IN COLUMN 1	The second second	
3 9.699086 9.937312 9.763214 10.237686 10.06288 10.300314 56 9.909844 9.937089 9.763269 10.237733 10.062835 10.39938 55 9.702060 9.936940 9.76388 10.237733 10.062835 10.39938 55 9.702060 9.936942 9.76388 10.235733 10.062835 10.39938 55 10.9702151 9.936942 9.76370 10.35337 10.06283 10.39938 55 10.9702151 9.936942 9.76373 10.35337 10.06333 10.39938 55 10.9702151 9.936942 9.76333 10.35307 10.063348 10.399052 51 10.970318 9.93672 9.76393 10.35307 10.063348 10.399063 11 19.70368 9.93672 9.76393 10.35307 10.063348 10.399663 14 19.70369 9.95657 9.76574 10.33507 10.063348 10.399684 10.39663 15 9.70215 9.93641 9.76585 10.33305 10.063348 10.39968 10.39968 10.39968 10.39306 10.39368 10.39368 10.39968 10.393	н		The second second	DESCRIPTION OF THE PARTY NAMED IN	Laboratory Company	The second second	I DOMESTIC POST - DUTCH		
9, 6998.4 9, 97728 9, 76260 10.277394 10.062761 10.29978 5 9, 700000 9, 937019 9, 76387 10.276210 10.06285 10.29978 5 9, 700716 9, 93646 9, 763770 10.26211 10.06285 10.29972 5 9, 700716 9, 93646 9, 763770 10.26210 10.06298 10.29972 5 10.970171 9, 93679 9, 764971 10.25210 10.06297 10.296210 10.06297 10.296210 10.06297 10.296210 10.06297 10.296210 10.29621	и		SAMPLE AND SECTION	Company of the Control of				the second second	
\$ 9,70006a [9,937019] 9,76388] 10.236812 10.060908 10.299720 53	н	3		9.937312		10.237686	The second second second	10,300374	57
6 9,700380 9,937003 9,763479 10.236321 10.06098 10.29930 54 7 9,700498 9,937019 9,763479 10.236321 10.06098 10.29930 53 9,700151 9,926799 9,764351 10.236321 10.060308 10.299308 53 11 9,701508 9,936724 9,76461 10.236327 10.063028 10.299308 53 12 9,701508 9,93652 9,763461 10.236327 10.063328 10.299308 13 13 9,701801 9,93652 9,763441 10.236327 10.063338 10.296321 40 14 9,702019 9,93657 9,765214 10.236307 10.063348 10.296321 40 15 9,702216 9,93641 9,76380 10.233305 10.063348 10.29632 40 17 9,70266 9,93648 9,76838 10.23306 10.063638 10.29938 46 17 9,70269 9,93618 9,76638 10.23306 10.063638 10.29938 46 19 9,70249 9,93514 9,76838 10.23301 10.063790 10.29731 43 10 9,70317 9,936060 9,76734 10.23301 10.063790 10.29731 43 10 9,70317 9,936060 9,76734 10.23301 10.063639 10.29731 43 10 9,70317 9,936060 9,76734 10.23301 10.063038 10.29668 40 12 9,70419 9,93514 9,76784 10.23301 10.063038 10.29668 40 12 9,70419 9,93564 9,76890 10.23301 10.063038 10.29668 40 12 9,70419 9,93568 9,76890 10.23301 10.06400 10.29630 17 12 9,70482 9,93584 9,76890 10.23120 10.06400 10.29630 17 13 9,70504 9,935309 9,76890 10.23079 10.06400 10.29600 37 14 9,70508 9,935300 9,76890 10.23079 10.06400 10.29600 37 14 9,70508 9,935300 9,708500 10.23079 10.06400 10.29600 37 14 9,70508 9,935300 9,707040 10.20662 10.29631 10.20630 10.29630	н	4	9.699844	9.937238	9.762000	10-237394	10.062762		56
6 9,700380 9,937002 9,763783 10.236321 10.06308 10.29930 54 7 9,700163 9,936046 9,763779 10.236321 10.06308 10.29930 53 9,700151 9,936799 9,763651 10.235321 10.06308 10.29930 53 11 9,701531 9,936792 9,763651 10.235327 10.063318 10.296302 11 13 9,70153 9,93652 9,76343 10.235307 10.053318 10.296302 11 13 9,70180 9,936578 9,765314 10.235307 10.053318 10.296302 10.266312 10.266		5	9.700062	9.937105	9.762897	10.237103	10.062835	10.199918	35
7 9-700498 9-937019 9-764547 10.236211 10.06398 10.299202 52 9-760933 8-936872 9-764061 10.236210 10.063928 10.299202 52 10.9701351 9-936799 9-764521 10.235327 10.063273 10.298631 12.9701365 9-936792 9-764643 10.235327 10.063273 10.288631 13.9701363 9-93672 9-764643 10.235327 10.063273 10.288631 14.97013019 9-936752 9-764643 10.235067 10.063243 10.288631 14.97013019 9-936752 9-76524 10.23486 10.063243 10.28863 12.970130 14.97013019 9-936753 9-76524 10.23486 10.063243 10.28863 12.970130 9-93632 9-766575 10.23485 10.063263 10.29764 15.9702452 9-95677 9-766695 10.233025 10.063633 10.29764 15.9702452 9-95677 9-766695 10.233025 10.063633 10.29764 15.9702452 9-95677 9-766695 10.233025 10.063633 10.29764 15.9702452 9-936663 9-766765 10.233025 10.063633 10.29764 15.9702452 9-936663 9-766765 10.233025 10.063633 10.29764 15.9702461 9-936663 9-766765 10.233025 10.063633 10.29764 15.9702461 9-93564 9-766875 10.233025 10.063633 10.29764 15.9702461 9-93564 9-766875 10.233025 10.064676 10.296829 10.290317 9-936663 9-767524 10.233025 10.064676 10.296829 10.290317 9-936663 9-767524 10.233025 10.064676 10.296829 10.290314 9-935849 9-768703 10.233025 10.064676 10.296829 10.290314 9-935849 9-768924 10.231265 10.064676 10.29631 37.970314 9-935669 9-768703 10.231265 10.064676 10.29631 37.970314 9-935669 9-768703 10.231265 10.064676 10.29631 37.970450 9-935669 9-768703 10.231265 10.064676 10.29631 37.970450 9-935669 9-768703 10.231267 10.064676 10.29631 37.970450 9-935669 9-768703 10.231267 10.064676 10.29631 37.970450 9-935669 9-768949 9-776896 9-768949 9-776896 9-768949 9-776896 9-768949 9-776969 10.29638 10.064477 10.29631 37.970450 9-93569 9-776986 10.29638 10.064477 10.29631 37.970450 9-93569 9-777045 10.22963 10.064477 10.29631 37.970450 9-934798 9-777105 10.22963 10.064477 10.29631 32.970410 9-934429 9-777308 10.22967 10.066670 10.29632 10.29632 10.29632 10.29632 10.29632 10.29632 10.29632 10.29632 10.29632 10.29632 10.29632 10.29632 10.29632 10.29632 10.29632 10.29632 10.29632 10.29632 10.29634 10.29634 10.29634 10.29634 10.2	и	6	9.700180	9.937092	9.763188	10.236812	10.062908	10,299710	34
8 9,700716 9,936946 9,762770 10.252310 10.063188 10.299067 10.9701151 9,930799 9,764521 10.253377 10.063188 10.299067 11 9,701368 9,936725 9,764643 10.235357 10.063120 10.288643 50 129067 11 9,701368 9,936725 9,764643 10.235357 10.063120 10.288643 50 12 9,701368 9,936725 9,764643 10.235357 10.063120 10.288643 14 9,701368 9,936725 9,764643 10.235367 10.063121 10.268613 14 9,70136 9,936735 9,764514 10.23346 10.063121 10.268613 14 9,70136 9,936735 9,764514 10.234466 10.063431 10.26768 17 9,702669 9,936310 9,766095 10.233295 10.063569 10.297764 17 9,702669 9,936210 9,766095 10.23329 10.065769 10.297764 17 9,702669 9,936210 9,766095 10.23325 10.065769 10.297543 18 9,702386 9,936210 9,766095 10.23325 10.063564 10.297543 12 9,703533 9,93526 9,767545 10.23323 10.063564 10.29689 10.2973317 9,936062 9,767545 10.23323 10.063564 10.29689 10.2973317 9,936062 9,767545 10.233245 10.063564 10.29689 10.296713 12 9,703533 9,935840 9,767545 10.23245 10.064074 10.296407 12 9,93764 9,935840 9,768124 10.23145 10.064074 10.296407 10.	п	7	9.700498	9-917019	9.763479	10.236car	10.062981	10,200 (02	
9 9-700933	п	8	Marie Company of the	Military and the last	The second second	The second second	The second second second		
10 9-701 15 9-936799 9-764352 10.235648 10.063200 10.268632 12 9-701808 9-936728 9-764933 10.235677 10.063278 10.268632 13 9-701808 9-93678 9-763804 10.235677 10.063278 10.268632 14 9-702019 9-93695 9-763804 10.234488 10.063493 10.29762 15 9-702452 9-93683 9-763805 10.233057 10.063569 10.29762 17 9-702669 9-936838 9-76695 10.23305 10.063569 10.29764 17 9-702069 9-936136 9-766854 10.233015 10.063716 10.297524 18 9-703883 9-936136 9-76695 10.233035 10.063716 10.297524 19 9-703573 9-936988 9-767595 10.233035 10.063716 10.296807 12 9-703573 9-935808 9-767595 10.233035 10.064012 10.296807 12 9-703573 9-935808 9-767595 10.233035 10.064012 10.206407 1	ı	0	ACCRECATE VALUE OF THE PARTY OF		AND DESCRIPTION OF THE PERSON NAMED IN	THE RESERVE OF THE PERSON NAMED IN			
11 9-701368 9-936725 9-764643 10-23537 10.063475 10.266631 12 9-701580 9-96778 9-767244 10.263486 10.063488 10.268413 12 13-270602 9-936305 9-767344 10.23486 10.063495 10.29764 15 9-702459 9-936305 9-765805 10.234195 10.063596 10.29764 15 9-702459 9-93638 9-766835 10.234195 10.063596 10.29764 14 9-702101 9-936136 9-766875 10.233315 10.063760 10.29764 14 9-702101 9-936136 9-766875 10.233315 10.063760 10.29731 14 9-702101 9-936136 9-766875 10.233315 10.063760 10.29731 13 9-703517 9-936062 9-767845 10.233745 10.063864 10.26689 12 12 12 12 12 12 12 1	п	-		THE RESERVE AND ADDRESS OF THE PERSON NAMED IN	The second second second				
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6 9.713098 9 932609 9.780489 10.219211 10 067391*10.286902 5 8 9.713308 9 932533 9.78075 10.219215 10.067467 10.286922 5 8 9.713376 9.932380 9.781366 10.218340 10.067543 10.2286483 5 9 9.713726 9.932380 9.781366 10.218340 10.067520 10.286474 5 10 9.713935 9.931304 9.781631 10.218369 10.067620 10.286474 5 12 9.714351 9.932075 9.782481 10.217799 10.067849 10.285856 4 12 9.714352 9.932075 9.782486 10.217791 10.067972 10.285856 4 13 9.714461 9.932075 9.782486 10.217791 10.067925 10.285439 4 14 9.714769 9.931984 9.78371 10.21694 10.068079 10.28522 10.28521 19 9.715869 9.931845 9.783361 10.21694 10.068079 10.28522 10.28521 19 9.715809 9.931614 9.784195 10.216940 10.068379 10.28338 19 9.715629 9.931614 9.784195 10.216940 10.068363 10.284398 4 19 9.716329 9.931614 9.784195 10.21530 10.068363 10.284398 4 20 9.716617 9.931537 9.784479 10.21530 10.068363 10.284398 4 21 9.716329 9.931306 9.785321 10.21530 10.068651 10.283383 4 22 9.716349 9.931306 9.785321 10.21530 10.068651 10.283363 3 23 9.716629 9.931306 9.785321 10.21530 10.068651 10.283363 3 24 9.716846 9.931289 9.785616 10.214952 10.068648 10.283363 3 24 9.716846 9.931299 9.785616 10.214381 10.068771 10.283568 3 23 9.717953 9.931075 9.786184 10.214381 10.06871 10.283568 3 24 9.718497 9.930843 9.787603 10.214362 10.068648 10.283361 3 24 9.718497 9.930843 9.787603 10.214361 10.068521 10.283163 3 25 9.718793 9.930843 9.787603 10.214362 10.066925 10.282474 3 26 9.718909 9.930760 9.787886 10.214361 10.069381 10.2831915 3 27 9.718793 9.930843 9.787603 10.214361 10.069380 10.284593 3 29 9.718793 9.930843 9.787603 10.214361 10.069380 10.283608 3 29 9.718909 9.930450 9.788786 10.21214 10.069380 10.281503 3 29 9.718793 9.930843 9.787603 10.212164 10.069380 10.281503 3 29 9.718793 9.930843 9.787603 10.212164 10.069381 10.281693 10.280605 3 29 9.718793 9.930849 9.789586 10.212964 10.06938 10.280605 3 29 9.718793 9.930849 9.789586 10.212964 10.006933 10.280605 3 29 9.718793 9.930849 9.790151 10.209364 10.007076 10.279461 10.279605 3 29 9.72188 9.92989 9.79151 10.209384 10.007076	58			10.220082	9.779918	9-932702	9.712079	
7 9.713368 9.32533 9.780775 10.219215 10.067467 10.286692 5 9.713517 9.932457 9.781660 10.218940 10.067543 10.286483 5 9.713726 9.932380 9.781631 10.218940 10.067630 10.286665 10.9713935 9.932151 9.781631 10.218369 10.067696 10.286665 10.9713935 9.932151 9.782301 10.217799 10.067931 10.285483 10.217799 10.067831 10.285483 10.217799 10.067831 10.285483 10.217514 10.067931 10.285483 10.217514 10.067931 10.285483 10.217514 10.067931 10.285483 10.217514 10.067931 10.285439 10.217514 10.067807 10.285439 10.217514 10.068079 10.285439 10.217514 10.068079 10.285439 10.217514 10.068079 10.285431 10.217514 10.068079 10.285431 10.217514 10.068079 10.285431 10.217514 10.068079 10.285431 10.217514 10.068079 10.285431 10.217514 10.068079 10.285431 10.217514 10.068079 10.285431 10.217514 10.068079 10.285431 10.217514 10.068079 10.285431 10.217514 10.068079 10.285431 10.217514 10.068079 10.285431 10.217514 10.068079 10.285405 10	55 54			10.219/9/	0.780180	0.032600	0.7 12009	8
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44 9-720958 9.929677 9.791281 10.2087:9 10.070323 10.279042 1 45 9-721162 9.929599 9.791563 10.208437 10.070401 10.278838 1 46 9.721570 9.92942 9.791846 10.208154 10.070479 10.278634 1 47 9-721570 9.929442 9.792128 10.207372 10.070558 10.278430 1 48 9-721774 9.929364 9.792410 10.207590 10.070536 10.278430 1 49 9-721978 9-929286 9.792692 10.207590 10.070714 10.278022 1 50 9-72238 9 929207 9.792974 10.207026 10.070793 10.277819 1 51 9-72238 9 929050 9.793356 10.20644 10.070871 10.277615 52 9-72258 9 929050 9.79338 10.20642 10.070950 10.277412 53 9.722791 9.928972 9.793819 10.206181 10.071028 10.277429	18							42
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46 9 721366 9.929521 9.791846 10.208154 10.070479 10.278634 1 47 9.721570 9.929442 9.792128 10.207872 10.070558 10.278430 1 48 9.721774 9.929364 9.792410 10.207590 10.070636 10.278226 1 49 9.721978 9.929287 9.792692 10.207308 10.070714 10.278022 1 50 9.722181 9.929207 9.792974 10.207026 10.070793 10.277819 1 51 9.722385 9.929129 9.793256 10.206462 10.070950 10.277615 1 52 9.72258 9.92950 9.793538 10.206462 10.070950 10.277412 1 53 9.722791 9.928972 9.793819 10.206181 10.071028 10.277209	16							
47 9.721570 9.929442 9.792128 10.207872 10.070558 10.278230 1 48 9.721774 9.929364 9.792410 10.207590 10.070536 10.278226 1 9.721978 9.929286 9.792692 10.207508 10.070714 10.278022 1 50 9.722181 9.92907 9.792974 10.207026 10.070793 10.277819 1 51 9.722385 9.929129 9.792576 10.206262 10.070950 10.277615 1 52 9.722588 9.929050 9.793538 10.206262 10.070950 10.277412 1 53 9.722791 9.928972 9.793819 10.206181 10.071028 10.277209	15 14							76
48 9.721774 9.929364 9.7924 10 10.207590 10.070536 10.278226 1 9.721978 9.929286 9.792692 10.207308 10.070714 10.278022 1 50 9.722181 9.929207 9.792974 10.207026 10.070793 10.277819 1 51 9.722385 9.929129 9.793256 10.206462 10.070871 10.277615 1 52 9.722588 9.939050 9.793538 10.206462 10.070950 10.277412 1 53 9.722791 9.928972 9.793819 10.206181 10.071028 10.277209	13							
49 9.721978 9.929286 9.792692 10.207308 10.070714 10.278022 1 50 9.722181 9.929207 9.792974 10.207026 10.070793 10.277819 1 51 9.722385 9.929129 9.792356 10.206744 10.070871 10.277615 52 9.722588 9.929050 9.793538 10.206462 10.070950 10.277412 53 9.722791 9.928972 9.793819 10.206181 10.071028 10.277412	12				9.792410			48
51 9-722385 9-929129 9-793256 10.206744 10.070871 10.277615 52 9-722588 9-929050 9-793538 10.206462 10.070950 10.277412 53 9-722791 9-928972 9-793819 10-206181 10.071028 10.277209	11			10.207308	9.792692	9.929286		49
52 9.722588 9.929050 9.793538 10.206462 10.070950 10.277412	10	10.277819	10.070793	10.207026	9.792974	9 929207	9.722181	
52 9.722588 9.929050 9.793538 10.206462 10.070950 10.277412	9					9 929129		51
	8							52
#54 9-/44944 9 428893 9-794101 10 20(899 10.071 t07 10-277006	7							
	6							
55 9.723197 9.928815 9.794383 10.205617 10.071185 10.276803 56 9.723400 9.928736 9.794664 10.205336 10.071264 10.276600	5 4							136
57 9.723623 9.928657 9.794945 10.205055 10.071343 10.276397	3							57
58 9.723805 9.928 578 9.795227 10.204773 10.071422 10.276195	2							58
[59 9.724007 9.928499 9.795508 10.204492 10.071501 10.275993	I	10.275993	10.071501		9.795508	9.928499		59
60 9.724210 9.928423 9.795789 10.204211 10.071580 10.275790	0	10.27 5790	10.071580	10.204211	9.795789		9.724210	160
	M	Secant.	Co-sec.	Tang.	Co-tang.	Sine.	Co-sine.	ж

58 LOGARITHMIC SINES, TANGENTS, AND SECANTS.

32 Degrees.

				ægrees.			
М	Sine.	Co-sine.	Tang.	Co-tang.	Secant.	Co-sec.	м
-0	0.724210	u-028420	9.795789	10.204211	10.071580	10.275790	60
ĭ	0.724112	0.028142	9.796070	10.203930	10.071658	10.275588	59
2	0.724614	9.928263	9.796351	10.203649	10.071737	10.275386	58
3	0.724816	9.928183	9.796632	10.203368	10.071817	10.275184	57
4	0.725017	9.928104	9.796913	10.203087	10.071896		56
5	0.725219	9.928025	9.797194	10.202806	10.071975	10.274781	
6	0.725420	9.927946	9-797475	10.202525	10.072054		54.
7	0.725622	9.927867	9-797755	10.202245	10.072133	10.274378	
8	0.725823	9.927787	19.798036	10.201964	10.072213	10.274177	52
9	0.726024	9.927708	9.798316	10.201684	10.072292	10.273976	51
10	9.726225	9.927629	9.798596	10,201404	10.072371	10.273775	50
17	0.726426	0.027540	9.798877	10.201123	10.072451	10.273574	49
12	0.726626	9.927470	9.799157	10.200843	10.072530	10.273374	
1	10 726827	0.027200	0 700437	10.200662	10.072610	10 273173	47
14	9.727027	19.927310	9.799717	10.200283	10.072690	10.272973	46
	9.727228	9.927231	9.799997	10.200003	10.072769	10.272772	45
16	9.727428	9.927151	19.800277	10.199723	10.072849	10 272572	44
17	9.727628	9.927071	9.800557	10.199443	10.072929	10.272372	43
18	9.727828	9.926991	9.800836	. 10. 199 164	10.073009	10.272172	42
19	9.728027	.9.926911	9.801116	10.198884	10.073089	10.271973	41
20				10.198604			
21	9.728427	9.926751	9.801675	10.198325	10 07 3249	10.271573	39
22	9.728626	4.926671	9.801955	10.198045	10.073329	10.271374	
23	9 728825	9 926591	9.802234	10.197766	10.0-3409	10.271175	37
24	9.729024	19.926511	9.802513	10.197487	10.073489	10.270976	36
25	9.729223	9.926431	9.802792	10.197208	10.073569	10 270777	35
				10.196928			34
						10.270379	
28	9.729820	9.926190	19.803630	10.196370	10.073810	10.270180	- 1
29	9.730018	9.926110	9.803908	10.196092	10.073890		31
				10.195813		10.269783	30
31	19.730415	9.925949	9 804466	10.195534	10.074051	10.269585	
. 32	9.730613	9.925868	9.804745	10.195255	10.074132	10.269387	28
				10 194977			5. 1
				10.194698		10 268991	
	9.731200	9.925020	9.805580	10.194420	10 074374		
36	9.731404	9.925545	9.805859	10 194141	10.074455	10.268596	
37	9.731002	9.925405	9.800137	10 193863	10.074535	10.268398,	- 1
38	9.731799	9.945304	9.806693	10.193585	10.074697	10.268201	22
	9.731990	9.925222	0.806071	10.193307		10.267807	21
40							
41	9.732390	9.925141	9 807 249	10.192751		10.267619	19
42	9.732587	9.925000	9.807527	10.192473	10.074940		18
) · · · · ·			10.192195			17
44				10.191917			16
45 46				10.191639			15
40	9.733373			10.191302			14
				10.190807			13
49		9.924491		10.190529		10.266039	11
50			9.809748		10.075591	10.265843	10
_			9.810025	10.189975			
51	9.734353			10.189698	10.075672	10.265647	8
52	0.724744	10.024164	9.810302	10.189420			~
33	0.734070	0.024082	9.810847	10.189420	10.075836	10.205250	6
34	0.736126	0.024001	9.811124	10.188866	10.075917	10.20,001	
26	0.735330	0.023010	0.811410	10.188590	10.076081	10.204605	\$ 4
57	0.735626	9.923877	9 811687	10.188313	10.076163		3
58		9.923755	9.811064	10.188036	10.076245		2
				10.187759			7
66		9.923591	9.812517	10-187483	10.076409		0
M	Co-sine.	Sine.	Co-tang.	Tang.	Co-sec.	Secant.	м
ستبلإ				Domoge.	. 00-300.	. Decam. I	

Sine Co-sine Tang. Co-tang. Secant Co-sec №				ردن	Degrees.			
1 9,736303 9,923309 9,812794 10.187206 10.076491 10.262697 5 2 19,736498 9,923427 9,813070 10.186530 10.076673 10.263303 57 3 9,736886 9,923263 9,813632 10.186537 10.076573 10.263203 57 5 9,737274 9,923068 9,814175 10.185637 10.076902 10.262203 57 7 9,73767 9,923016 9,844451 10.185637 10.076902 10.26223 54 8 9,737661 9,922931 9,81475 10.185638 10.0766902 10.262726 54 7 9,738498 9,922686 9,815555 10.18445 10.077691 10.263239 52 9 9,737855 9,922851 9,815904 10.18596 10.077694 10.262339 52 11 9,73841 9,922686 9,815555 10.184445 10.077314 10.261759 49 12 9,73841 9,922686 9,815555 10.184445 10.077314 10.261759 49 13 9,73862 9,922428 9,816781 10.18569 10.077397 10.261166 48 13 9,73964 9,922729 9,816678 10.183618 10.077314 10.260794 44 14 9,73820 9,922319 9,816681 10.183618 10.077645 10.260987 45 15 9,739073 9,922372 9,816678 10.183791 10.077645 10.260987 45 16 9,739078 9,922729 9,816931 10.183691 10.077645 10.260987 45 17 9,73938 9,922189 9,817209 10.182791 10.077645 10.260987 45 18 9,74959 0,921707 9,81850 10.18169 10.077811 10.260002 43 19 9,740167 9,221697 9,818510 10.181690 10.078141 10.260002 43 19 9,740167 9,221697 9,818510 10.181690 10.078431 10.259833 39 1,74150 9,921190 9,821739 9,816999 10.185241 10.079870 10.259358 30 19 9,741699 9,921190 9,82032 10.181415 10.078893 10.259358 33 19 9,744609 9,921190 9,82030 10.181690 10.078843 10.259884 33 19 9,744609 9,921190 9,82030 10.181690 10.078860 10.259853 31 19 9,74380 9,921697 9,828730 10.187941 10.079820 10.259450 37 19 9,74373 9,920368 9,821739 10.179491 10.079880 10.259358 32 19 9,741699 9,921190 9,820368 10.18169 10.079880 10.259363 31 19 9,744679 9,921694 9,820368 9,821730 10.179491 10.079880 10.259363 31 19 9,744787 9,920486 9,823703 10.179491 10.079880 10.259363 31 19 9,744797 9,92088 9,823703 10.179491 10.079881 10.25938 21 19 9,743791 9,920368 9,823703 10.179491 10.079881 10.25938 21 19 9,743791 9,920368 9,823703 10.179491 10.079881 10.255638 20 10 9,744787 9,919339 9,826733 10.179491 10.080691 10.255638 10.179491 10.080671 10.255639 10.179491 10.080671	×	, Sine.	Co-sine.	Tang.	Co-tang.	Secant.	Co-sec	M ·
1	1-	0.736100	0.023501	0.812517	10.187483	10.076400	10.263891	60
2 9,736498 9,923427 9,813070 10.1869301 10.076673 10.263303 5 3 9.736686 9.923263 9,813623 10.186377 10.076673 10.263200 5 6 9.737274 9.923098 8,813899 10.186101 10.076819 10.262220 5 7 9.737667 9.923105 9,814453 10.185548 10.076920 10.263233 53 8 9.737667 9.923268 9,815279 10.185548 10.076984 10.263233 53 9.737855 9.922868 9,815279 10.18496 10.077149 10.262145 51 10 9.738434 9.922668 9,815279 10.184721 10.07732 10.261166 48 13 9.738637 9.922639 9,815951 10.18469 10.07737 10.261166 48 14 9.73883 9,923748 9,815931 10.18469 10.07737 10.261166 48 15 9.739013 9.92355 9,816678 10.18496 10.07737 10.261166 48 15 9.73906 9.923272 9,81697 10.183291 10.077645 10.261303 47 9.739398 9.923278 9,81693 10.183667 10.077645 10.261303 47 9.739398 9.923278 9,81693 10.182667 10.077645 10.26003 43 18 9.739500 9.923169 9,817484 10.182516 10.077681 10.260603 43 19 9.73973 9,922069 9,817484 10.182516 10.077684 10.260603 43 19 9.73973 9,922169 9,81730 10.18291 10.077681 10.260603 43 19 9.73973 9,921607 9,818310 10.181690 10.078876 10.260603 43 29 9.74059 9.92169 9,818310 10.181690 10.078843 10.259833 39 11 9.74067 9,921877 9,818310 10.181690 10.078843 10.259833 39 12 9.74059 9.921244 9,81931 10.180865 10.078876 10.259833 39 13 9.74150 9,921244 9,820234 10.17964 10.078893 10.259838 39 13 9.74150 9,921274 9,82031 10.180865 10.078876 10.25983 37 13 9.74262 9,920123 9,82038 10.17940 10.078810 10.259873 31 19 9.743789 9,92107 9,82038 10.17940 10.079841 10.259538 10 9.743793 9,920088 9,82133 10.17940 10.079841 10.259538 10 9.744509 9,921107 9,82058 10.179491 10.079881 10.25960 13.25971 13 9.74280 9,921049 9,828580 10.179491 10.079881 10.25960 13.45971 1 14 9.74360 9,921079 9,82058 10.179491 10.079881 10.25960 13.45971 1 15 9.74360 9,921099 9,88269 10.179491 10.079881 10.25960 1 15 9.746849 9,91950 9,82769 10.17949 10.079881 10.25960 1 16 9.74479 9,91939 9,82679 10.17949 10.079881 10.25960 1 17 9,74450 9,91939 9,82679 1 18 9,74450 9,91939 9,82679 10.17949 10.00009 10.259374 1		0.736303	0.022600	0.812704				5
3 9.73669a 9.93345 9.81347 10.186673 10.076675 10.263308 5 9.7378069.933181 9.81389 10.186101 10.076819 10.263114 56 9.737274 9.932088 9.814775 10.185825 10.076902 12.26726 54 9.737867 9.92393 9.814775 10.185825 10.0706902 12.26726 54 9.737867 9.92393 9.814775 10.185825 10.0706902 12.26726 54 9.73861 9.92393 9.815004 10.184961 10.0707149 10.262139 52 9.737875 9.922858 9.815004 10.184961 10.077314 10.261759 49 9.73841 9.922686 9.815555 10.184445 10.077314 10.261759 49 9.73841 9.922686 9.815831 10.18469 10.077397 10.261766 48 13 9.738627 9.923357 9.816678 10.183618 10.077521 10.261759 49 9.73930 9.923357 9.816678 10.183618 10.077561 10.260779 44 9.738820 9.923759 9.816678 10.183618 10.077561 10.260797 44 9.739308 9.923727 9.816678 10.183618 10.077561 10.260797 44 9.739509 9.92303 9.817729 10.182791 10.077678 10.260707 44 9.739509 9.92303 9.81709 10.182791 10.077678 10.260707 44 9.739509 9.92303 9.817759 10.18241 10.077661 10.26002 43 9.739509 9.92303 9.817759 10.18241 10.077861 10.260017 41 9.73978 9.921857 9.818505 10.18169 10.078661 10.260017 41 9.740509 9.921691 9.818361 10.18169 10.078661 10.250015 43 9.744550 9.921691 9.818360 10.18169 10.078661 10.259641 38 9.741508 9.921724 9.81856 10.18169 10.078661 10.259661 39 9.741889 9.921724 9.82034 10.18061 10.078663 10.259687 37 9.74181 9.920399 9.821739 10.18061 10.078643 10.259887 39 9.741609 9.92169 9.821880 10.18061 10.078643 10.259845 33 9.741508 9.921679 9.821850 10.17934 10.079361 10.257888 33 9.741508 9.921679 9.821860 10.179374 10.079361 10.25738 32 9.744509 9.92169 9.821860 10.179374 10.079361 10.25738 32 9.744509 9.920309 9.821606 10.179374 10.079361 10.255687 22 9.74659 9.919319 9.82160 9.82179 10.177374 10.080607 1	-	0.716408	0.021427	0.812070	10.1860 20	10.076572	10.263502	
4 9.736886 9.93263 9.813623 10.186377 10.076737 10.263114 56 9.737474 9.932088 9.814175 10.185835 10.076902 10.262026 54 7 9.737467 9.932016 9.844451 10.18548 10.076902 10.262026 54 8 9.737661 9.932931 9.814748 10.18548 10.076902 10.263236 53 9 9.737855 9.932851 9.815004 10.18496 10.077149 10.26333 53 9 9.738088 9.932768 9.815004 10.18496 10.077149 10.262145 51 10 9.738434 9.932686 9.81555 10.184444 10.07734 10.261373 47 11 9.73830 9.932380 9.81608 10.183618 10.077367 10.261373 47 12 9.73803 9.93235 9.816658 10.183444 10.077374 10.261373 47 13 9.739308 9.932389 9.817209 10.18321 10.077630 10.261373 47 15 9.739308 9.932189 9.817484 10.18326 10.077645 10.260373 47 17 9.739308 9.932169 9.817484 10.18276 10.07784 10.260373 47 18 9.73950 9.932169 9.817484 10.18276 10.07784 10.260417 41 19 9.73973 9.922033 9.817484 10.18261 10.077841 10.260603 43 19 9.73975 9.921940 9.818035 10.18196 10.077841 10.260217 41 20 9.73975 9.921940 9.818301 10.18261 10.077894 10.260217 41 21 9.74074 9.921677 9.81836 10.18146 10.07826 10.250833 39 21 9.74050 9.92167 9.818360 10.18196 10.07846 10.250833 39 21 9.74074 9.92167 9.81836 10.18196 10.07836 10.25983 37 22 9.74074 9.92167 9.81836 10.18196 10.07836 10.25983 37 23 9.741508 9.92124 9.81836 10.18196 10.07836 10.25983 37 24 9.74074 9.92167 9.81836 10.18036 10.07836 10.25986 33 25 9.740934 9.92154 9.818360 10.18196 10.07837 10.25983 37 25 9.740934 9.92154 9.82033 10.1908 10.07836 10.25987 34 25 9.74074 9.92167 9.82836 10.18031 10.07887 10.25988 32 25 9.740934 9.92154 9.82373 10.17921 10.07880 10.25987 34 25 9.74074 9.92169 9.82836 10.17921 10.07887 10.25980 10.25987 34 26 9.74169 9.92169 9.82836 10.17921 10.07886 10.25987 34 27 9.74171 9.920099 9.82038 9.82133 10.17921 10.07887 10.25980 10.25987 34 28 9.74450 9.92031 9.82836 10.17921 10.07986 10.25587 34 29 9.74869 9.92109 9.82689 9.82139 10.17931 10.07986 10.25587 22 20 9.74988 9.92109 9.82869 9.82139 10.17931 10.07986 10.25587 22 20 9.74988 9.92109 9.82869 9.82139 10.17939 10.07986 10.25587 22 20 9.74988 9.9208 9.8288 10.17899 10.07986	2	0.736602	0.027746	0.813347				5-
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22	21	9.740167	9.921857	9.818310				
23		9.740359	9.921774	9.818585	10.181415	10.078226	10.259641	38
24 9.740742 9.921627 9.819135 10.180805 10.078393 10.259368 35 9.74074125 9.921441 9.819684 10.180310 10.078559 10.258875 34 27 9.741508 9.921374 9.820324 10.179401 10.078543 10.258842 32 9.741508 9.921190 9.820583 10.179402 10.078810 10.258301 31 30 9.741889 9.921107 9.820783 10.179402 10.078810 10.258301 31 30 9.742462 9.92086 9.821607 9.82132 10.178648 10.078893 10.258311 30 9.742462 9.920782 9.821666 10.178120 10.078803 10.257328 27 49.742842 9.920782 9.821880 10.178120 10.079821 10.257328 27 49.742622 9.920782 9.821826 10.178120 10.079221 10.257348 29 9.742873 9.920649 9.822237 10.177846 10.079221 10.257348 29 9.743813 9.920649 9.822377 10.177846 10.079328 10.256378 22 9.743602 9.920520 9.822703 10.177891 10.079328 10.256587 22 9.743602 9.920520 9.822703 10.177891 10.079326 10.256587 22 9.743792 9.920268 9.822370 10.1776376 10.079326 10.256687 22 9.743792 9.920268 9.823352 10.176500 10.079328 10.256687 22 9.743792 9.920268 9.823352 10.176500 10.079328 10.256638 21 9.744739 9.920019 9.824345 10.176505 10.079326 10.256638 21 9.744739 9.920019 9.824345 10.176526 10.079328 10.25638 21 9.744739 9.91931 9.824619 10.17551 10.079328 10.256389 18 9.744739 9.91931 9.824619 10.17551 10.079328 10.25638 10.25638 20 9.744560 9.919339 9.825713 10.176376 10.080054 10.255639 17 9.744789 9.919379 9.82566 10.174834 10.080492 10.255639 17 9.745494 9.919508 9.825713 10.174834 10.080492 10.256509 11 9.745894 9.919508 9.825986 10.174874 10.080492 10.254831 10.256687 10.774594 9.919508 9.825781 10.174887 10.080561 10.254831 10.256575 10.746989 9.919508 9.825786 10.174874 10.080492 10.254530 11 9.745894 9.919508 9.825786 10.174874 10.080492 10.254530 11 9.746848 9.919689 9.82778 10.174887 10.080561 10.254337 10.254590 9.745684 9.919689 9.82778 10.174887 10.080576 10.254337 10.254590 9.745684 9.919689 9.82778 10.174887 10.080576 10.253376 10.253376 9.746848 9.919689 9.82778 10.174880 10.080576 10.253376 10.253376 9.746848 9.919685 9.82778 10.174880 10.080576 10.253376 5 9.746848 9.919859 9.82778 10.17203 10.080571 10.253376 5 9.746	123	9.740550	9.921691	9.818860	10.181140	10.078309	10.259450	
26 9.740934 9.921524 9.819410 10.180590 10.078876 10.259666 3 3 4 9.74156 9.921457 9.819959 10 180041 10.078559 10.258875 3 4 9.741508 9.921377 9.819959 10 180041 10.078643 10.258808 3 2 9.741508 9.921190 9.820508 10.179412 10.078810 10.258301 3 1 9.741889 9.921107 9.820783 10.179217 10.078893 10.258301 3 1 9.742871 9.920939 9.821332 10.178688 10.079861 10.257920 2 9 9.742871 9.920939 9.821332 10.178688 10.079961 10.257920 2 9 9.742871 9.920939 9.821332 10.178688 10.079961 10.257538 2 7 9.74362 9.920768 9.821800 10.178394 10.079144 10.257538 2 7 9.74362 9.920762 9.821323 10.178688 10.079961 10.257538 2 7 9.74362 9.920604 9.822409 10.177571 10.079328 10.257158 2 7 9.743502 9.920504 9.822403 10.177571 10.079326 10.257158 2 9 9.743703 9.920436 9.822470 10.177571 10.079386 10.256687 2 9 9.743702 9.920368 9.822403 10.176703 10.079361 10.256687 2 9 9.743702 9.920368 9.823270 10.17603 10.079361 10.256388 2 2 9 9.743602 9.920368 9.823521 10.17650 10.079328 10.256388 2 2 1 0.744739 9.920468 9.82370 10.17602 10.079364 10.256388 2 2 1 0.744739 9.920468 9.823521 10.17650 10.079328 10.256388 2 2 1 0.744739 9.919931 9.824619 10.17518 10.080369 10.256388 1 9 9.744739 9.919931 9.824619 10.17518 10.080369 10.25638 1 9 9.744739 9.919931 9.824619 10.175181 10.080407 10.256398 1 9 9.744739 9.919931 9.824619 10.175181 10.080407 10.25638 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		9.740742	9.921667	9.810135	10.180865	10.078393		36
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6	9.747562	9.918574	9.828987	10.171013	10.081426	10.252438	60
1	9-747749	9.918489	9.829260	10.170740	10.081511	10.252251	59
2	9.747936	9.918404	[9.829532	10.170468	10.081596	10.252064	58
3	9.748123	9.918318	9.829805	10 170195	10.081682	10.251877	57
4	9.748310	9.918233	9 830077	10.169923	10 081767	10.251690	56
5		9.918147		10.169651		10.251503	55
6		9.918062		10.169379		10.251317	54
7		9 917976		10.169107	10.082024	10.251130	53
8		9 917891	9.831165		10.082109	10.250944	52
9	1	9.917805		10.168563		10.250757	51
10	9 749429	9.917719	9.831709		10.082281	10.250571	50
11		9.917634	9.831981	10.168019		10.250385	49
12		9.917548	9.832253	10.167747	10.082452	10.250199	48
13		9.917462		10.167475	10.082538		47
14		9.917376					46
15				10.166932			45
16	9.750543	9 917204	9.833339				44
17	19.750729	9.917118	9.833611		10.082882		43
18	9.750914	9.917032	9.833882		10.082968		42
19		9.916946					41
20	9.751284		9.834425		10.083141	10.248716	40
21		9.916773			10.083227	10 248531	39
22	9.751654			10.165033		10.248346	38
73			9.835238		10.083400		37
24				10.164491	10.083486		36
25			9.835780				35
26	9.752392		9 836051		10.083659		34
27	9.752576	9.910254	9.836322	10.163678	10.083746	10.247424	33
28	1		9.836593		10.083919	10.247240	32
29	9.752944		1			10.247056	31 30
30	9.753128						
31	9.753312				10.084093		29
32		9.915820				10.246505	28
33	19.753079	9.915733	9.837946	10.162054	10.084267		27
34				10.161513		10.246138	26
35 36	9.754229		9.838757			10.245954	25
	9.754412		9.839027	10.160973		10.245771	24
37 38			9.839297				22
39	9.754778	0.015210	9.839568	10.160432			21
40	9.754960				10.084877	10.245040	20
_							_
41	9.755143		9.840108 9.840378			10.244857	19
42	9.755326		9.840647			10.244674	
43		9.914800	9.840017	10.159353	10.085140		17
44		9.914685			10.085315	10.244310	15
45 46		9.914598	9.841457	10.158543	10.085402	10.244128	14
47		9 914510		10.158274	10.085490	10.243764	13
48		9.914422	9.841996	10.158004		10.243582	12
49		9.914334	9.842266		10.085666	10.243400	11
50	9.756782	9.914246	l - a ·	10.157465	10.085754	10.243218	10
-	9.756963	9.914158	_	10.157195	10.085842		
51			9.843074				9
52 53			9.843343			10.242856	7
	9.757507	9.913804	0.843612	10.156288	10.086106	10 242402	6
54 55	9.757688	9.913806	9.84 2882	10.156118	10.086194	10.242212	5
36	9.757860	9.912718	9 844161	10-156840	10.086282	10.242522	4
57	9.758050	9.913630	9.844420	10.155580	10.086370		3
58	9.758230	9.913541	9.844689	10.155311	10.086450	10.241770	2
59	9.758411	6.913453	9.844958	10 155042	10.086547	10.241 580	٠, ١
60	9.758591	9.913365	9.845227	10.154773		10.241409	0
M	Co sine.	Sine.	Co-tang	Tang.	Co-sec	Secant	¥
-							

Sine. Co-sine. Tang. Co-tang. Secant. Co-se 9.758591 9.913365 9.845227 10.154773 10.086635 10.241 19.758772 9.913276 9.845496 10.154504 10.086724 10.241	
0 9.758591 9.913365 9 845227 10.154773 10.086635 10.241. 1 9.758772 9.913376 9.845496 10.154504 10.086724 10.241	109 60
1 9.758772 9.913276 9.845496 10.154504 10.086724 10.241	
	228 59
2 9-758952 9-913187 9-845764 10-154236 10-086813 10-2410	
3 9-759132 9.913099 9.846033:10.153967.10.086901 10.240 4 9-759312 9.913010 9.846302 10.153698 10.086990 10.240	
4 9.759312 9.913010 9.846302 10.153698 10.086990 10.240 5 9.759492 9.912922 9.846570 10.153430 10.087078 10.240	
6 9-7 59672 9.912833 9-846839 10.153161 10.087167 10.240	508 55 128 54
7 9-759852 9-912744 9-847107-10.152893 10.087256 10.240	148 52
8 9.760031 9.912655 9.847376 10.152624 10.087345 10.230	60 52
1 9/9.760211 9.012566 9 847644 10.152356 10.087434 10.220	Soi ET
10 9.700390 9.912477 9.847913 10.152087 10.087523110.239	50 50
1 110 760(60)0 012 288 0 848 181 10 1518 10 10 087612 10 000	
12 9.760748 9.912299 9.848449 10.151551 10.087701 10.239	52 48
# 1319.70002719.01321019.848717110.151283110.087700110.22nd	721 A7
14 9.761 106 9.912121 9.848986 10.151014 10.087879 10.238 15 9.761285 9.912031 9.849254 10.150746 10.087969 10.238	94 46
16 9.761464 9.911942 9.849522 10.150478 :0.088058 10.238	15 45
17 9.761642 9.911853 9.849790 10.150210 10.088147 10.238	36 44
18 9.761821 9.911763 9.850058 10.149942 10.088237 10.238	79 42
19 9.761999 9.91 1674 9.850325 10.149675 10.088326 10.2380	01 41
19 9.761999 9.911674 9.850325 10.149675 10.088326 10.2386 20 9.762177 9.911584 9.850593 10.149407 10.088416 10.2376	23 40
21 9.762356 9.911495 9.850861 10.149139 10.088605 10.237. 22 9.762534 9.911405 9.851129 10.148871 10.088595 10.237.	44 39
22 9.762534 9.91 1405 9. 851 129 10. 14887 1 10.088595 10.237	66 38
1 23/9-702712/9-911315/9-851390/10.148004/10.088085/10.237	188 37
24 9.762889 9.911226 9.851664 10.148336 10.088774 10.237	11 26
25 9.763267 9.911136 9.851931 10.148069 10.088664 10.236 26 9.763245 9.911046 9.852199 10.147801 10.088954 10.236	33 35
26 9.763245 9.91 1046 9.852 199 10.147801 10.088954 10.236	
27 9.763422 9.910956 9.852466 10.147534 10.089044 10.236 28 9.763600 9.910866 9.852733 10.147267 10.080134 10.226	78 33
	32
29 9.763777 9.910776 9.853001 10.146999 10 089224 10.236 30 9.763954 9.910686 9.853268 10.146732 10.089314 10.236	123 31
35 97 93934 97 97 97 97 97 97 97 97 97 97 97 97 97	30
31 9.764131 9.910596 9.853535 10.146465 10.089404 10.2351 32 9.764308 9.910506 9.853802 10.146198 10.089494 10.2351	69 29
33 9.764485 9.919415 9.854069 10.14593 1 10.089585 10.235	92 28
34 9.764662 9.910325 9.854336 10.145664 10.089675 10.235	38 26
35 9.764838 9.910235 9.854603 10.145397 10.089765 10.225	62 25
35 9.764838 9.910235 9.854603 10.145397 10.089765 10.235 36 9.765015 9.910144 9.854870 10.145130 10.089856 10.234	85 24
4 37 9.705 P9 1 9.91005 + 19.055137 10.1448 0 3 1 10.08 9 9 4 6 10.224	00' 27
38 9.765367 9.909963 9.855404 10.144596 10.090037 10.234	22 22
39 9.765544 9.909873 9.85567 10.144329 10.090127 10.2344 40 9.765720 9.909782 9.855938 10.144062 10.090218 10.234	56: 21
41 9.765896 9.909691 9.856204 10.143796 10.090309 10.234	04 19
42 9.766072 9.909601 9.856471 10.143529 10.090399 10.233	28 18
43 9.766247 9.909510 9.856737 10.143263 10.090490 10.233	53 17
44 9.766423 9.909419 9.857004 10.142996 10.090581 10.233	77 16
45 9.766598 9.909328 9.857270 10.142730 10.090672 10.2333 46 9.766774 9.909237 9.857537 10.142463 10.090763 10.2333	02 15
47 9.766949 9.909146 9.857803 10.142197 10.090854 10.2330	51 13
48 9.767124 9.909055 9.858069 10.141931 10.090945 10.232	76 12
49 9.767300 9.908964 9.858336 10.141664 10.001036 10.232	00 11
50 9.767475 9.908873 9.858602 10.141398 10.091127 10.232	
51 9-767649 9-908781 9-858868 10-141132 10-091219 10-232	
52 9 767824 9.908690 9.859134 10.140866 10.091310 10.232	76 8
53 9 767999 9-908599 9-859400 10.140600 10.091401 10.2320	01 7
1 54 9.768 173 9.908 507 9 8 50666 10.140224 10.501402 110.221	27 6
\$ 5519.70834819.90841619.859932110.140068110.001584110.2211	(2 E
56 9.768522 9.908324 9.860198 10.139802 10.091676 10.231	78 4
57 9.768697 9.908233 9.860464 10.139536 10.091767 10.231	
58 9-76887 1 9-908 141 9-860730 10-139270 10-091859 10-231	
59 9.769045 9.908049 9.860995 10.139005 10.091951 10.230 60 9 769219 9.907958 9.861261 10.138739 10.092042 10.230	
M Co-sine Sine. Co-tang Tang. Co-sec. Secar	_
M Co-sine. Sine. Co-tang. Tang. Co-sec. Secar	t x

36 Degrees.

				Jegrees.			
M	Sine.	Co-sine.	Tang.	Co-tang	Secant.	Co-sec.	_X
0	9.769219	9.907958	9.861261	10.138739	10.092042	19.230781	60
1	9.769393	9.927866	9.861527	10.138473	10,092134	10.230607	59
2	9.769566	9.907774	9.861792	10.138208	10.092226	10.230434	58
3	9.769740	9.407682	9 862058	10.137942	10.092318	10.230260	57
4	9.769913	9.907590	9.862323	10.137677	10.092410	10.230087	56
-	~ ~~~~	9.907498	9.862589	19.137411	10.092502	10.2299131	55 4
6	9.770260			10.137146	10.002594	10.229740	54
7	9.770433	9.907314	9.863119	10.136881	10.092686		53
				10.136615		10.229394	52
				10.136350		10.229221	5 t
10	9.770952	9.907037	9.863915	10.136085	10.092963	10.129048	_50
1:	9.771125	9.406945	9.864180	10.135820	10.093055	10.228875	49
12	9.771298	9.906852	9 864445	10.135555	10.093148	10.228702	48
13	9.771470	9.906760	9.864710		10.093240	10,228530	47
14	9 771643	9.906667	9.864975	10.135025	10.093333	10.228357	46
15	9 77 1815	9.906575	9.865240	10.134760	10.007425	10.228185	45
16	9.771987	9.906482	19 865505	10.134495	10 093518	10.228013	44
17	9.772159	9.906389	19.865770	10.134230	10.093611	10.227841	43
			9.866035			10.227669	42
	9.772503	9.906204	9.866300		10.093796		41
20	9.772675	9.906111	9.866564		10.093889		40
	9.772847			10.133171	10.093982	10.227153	39
22	9.773018	9.905925	9.867094		10.094075		38 1
23	9.773190	9 905832	9.867358	10.132642		10.226810	37
					10.094261		36
25	9.773533	9.905645	9.867687	10.132113	10.094355	10.226467	35
26	9.773704	9.905552	9.868152	10.131848	10.094448	10.226296	34
	9.773875	9.905459	9.868416		10.094547		33
28					10.094634		32
29			9.868945	10.131055	10.094728		31
30	9.774388	9.905179	3.869209	10.130791	10.094821	10.225612	30
31	9.774558	9.905085	9.869473	10.130527	10.094915	10.225442	29
32	9.774729	9.904992			10.095008	10.225271	28
33	9.774899	9.904898	9.870001		10 095102		27
34	9.775070	9.904804	9.870265		10.095196		26
35	9.775240	9.904711	9.870529	10.129471	10.095289	10.224760	25
	9.775410			10-129207	10.095383	10.224590	24
37	9.775580	9.904523	9.871057	10 128943	10.095477	10.224420	23
38	9.775750	9.904429	9.871321	10.128679	10.095571	10.224250	32
	9.77 5920		9.871585	10.128415	10.095665		31
40	9.776090	9.904241	9.0/1049	10.120151	10.095/39		20
41	9.776259	9.904147	9.872112	10.127888	10.095853	10.223741	19
42			9.872376	10.127624	10.095947	10.223571	18
43	9.776598	9.903959	9.872640	10.127360	10.096041	10 223402	17
44	9.776768	9.903864	9.872903	10.127097	10 096136	10.223232	16
45	9.776937	9.903770	9.873167	10.126833	10.096230	10.223063	15
	9.777106	9.903676	9.073430	10.120570	10 090324	10.2228941	14
47	9.777275	9.903581	9.873094	10.126306	10.096419	10.222725	13
48	9-777444	9.903487	9-873957	10.126043	10.096513	10.222556	13
		9.903392			10.096608		11
_	9-777781	9 903298	9.874484		10.096702		10
		9.903203	9.874747	10.125253	10.096797	10.222050	9
52	9.778119	9.903108	9.875010	10.124990	10.096892	10.221881	8
53	9.778287	9.903014	9.875273	10.124727	10.096986	10.321713	7
54	9.778455	9.902019	9.875530	10 124464	10.007081	10 221545	6
	9.778624	9.902824	9 758co	10.124200	10.097176	10.221376	5 :
	9.7/0/92	9.902720	3.0 0003	10.123937	10.0972711	10.221206	4.
	9.778960	9 902034	0.876326	10.121674	10.007766	10,2210401	3
	9.779128	9.902539	9.876589	10 123411	10.097461	10 220872	2 .
		9 902444	9.870851	13.123149	10.097556	10.220705	1
-	9 779463				10.097651	10.220537	
M	Co-sine.	Sine.	Co-tang	lang	Co-s c	Secant	м

37 Degrees.

			37	Degrees.			
M	Sine.	Co-sine.	Tang.	Co-tang.	Secant.	Co-sec_	М
10	0.770461	0.003240	9.877114	10.122886	10.097651	10.220537	60
i	9.779631			10.122623		1	4
					10.097747	10. 220369	59
2				10.122360		10.220202	58
3	9.779966			10.122097	10.097937	10.220034	57
4		9.901967		10.121835	10.098033	10.219867	56
5	9.780300			10.121572	10.098128	10.219700	55
6	9.780467			10.121309	10.098224	10.219533	· 54
7	9.780634			10-121047	10.098319	10.219366	53
1 8	9.780801	9.901585		10-120784		10.219199	52
9	9.780968	9.901490	9.879478	10.120522	10.098510	10.219032	51
10	9.781134	9.901394	9.879741	10.120259	10.098606	10.218866	50
111	9.781301	0.001208	0.880002	10.119997	10.098702	10.218699	49
12	9.781468	0.001202	9.880265	10.119735	10.098798		48
13	9.781634	0.001106	9.880528	10.119472	10.098894		47
						10.218200	46
15		8.0000 IA	0.8810162	10.118948	10.000086	10.218034	45
16				10.118686		10.217868	
17	9.782298			10.118424		10.217802	44
18						1	+3
	0.782620	0.000120	0.88***	10.118161	10.099374	10.217536	42
19		9.900329	9.002101	10.117899		10.217370	41
20	9.782796			10.117637		10.217204	40
				10.117375	10.099663	10.217039	39
	9.783127			10.117113		10.216873	38
23	9.783292	9.900144	9.883149	10.116852	10.094856	10.246708	37
24	9.783458	9.900047	9 883410	10.116590	10.099953	10.216542	36
25	9.783623	9.899951	9.883672	10.116328	10.100049	10.216377	35
26	9.783788	9.899854	9.883934	10.116066	10.100146	10.216212	
27	9.783953	9.899757	9.884196	10.115804	10.100243	10-216047	
28		9.899660		10.115543	10-100:40	10.21 5882	32
20				10.115281	10.100436		31
30	9.784447	9.899467	9.884980		10.100533	10.215553	
I	9.784612	0 800270					
				1 1/2		10.215388	29
32	9.784776			10.114497	10.100727	10.215224	28
33	9.784941			10.114235	10.100824		27
	9.785105			10 113974	10.100922	, , , , ,	26
35			9.886288	3,	10.101019		25
	9 785433			10.113451		10.214567	24
37		9.898787		10.113190	10.101213		23
1 -	9.785761			10.112928	10.101311		22
39		9.898592		10.112667		10.214075	2 1
42	9.700009	9.898494	9.887594	10.112406	10.101506	10.213911	20
41	9.786252	9.898397	9.887855	10.112145	10.101603	10.213748	19
42	17 00 00		9.888116	10.111884	10.101701	10.213584	18
43	1 '0-	9.898202		10.111623	10.101798	10.213421	17
44		9.898104	9.888639	10.111361	10.101896	10.213258	16
45	1 04 -	9.898006			10.101994	10.213094	15
	9.787069				10.102092	10.212931	14
47		9.897810		10.110579	10.102190	10.212768	13
	9.787395			10.110318	10.102288	10.212605	12
49	9.787557		9.889943	10.110057	10.102386	10.212443	11
	9.787720			10.109796	10.102484	10.212280	
51		9.897418		10 109535	10.102582	10.212117	9
						10.211955	8
53	9-788208	9.897222	9.890986	10.109014	10.102778	10.211792	7
54	9.755370	9.897123	9-891247	10.108753	10 102877	10.211630	6
55	9.788532	9.897025	9 891507	10.108493	10-102975	10.211468	5
56	9.788694	9.896926	9.891768	10.108232	10.103074	10.211306	4
57	9.788856	9.896828	9.892028	10.107972	10.103172	10.211144	3
58	9.789018	9.896729	9.892289	10.107711	10.103271	10.210982	2
59	9.789180	9 896631		10.107451		10.210828	1
60	9.789342	9.896532	9.892810	10.107190	10.103468	10.210650	0
м	Co-sine.	Sine.	Co-tang	Tang.	Co-sec.	Secant.	м
1							

38 Degrees.

_			38	Degrees.			
M	Sine.	Co-sine.	Tang.	Co-tang.	Secant.	Co-sec.	×
0	9.789342	9.896532	9.892810	10.107100	10.103468	10.210658	60
ĭ	9.789504		9.893070			10.210496	59
2	9.789665	9.896335	9.893331				58
3	9.789827	9.896236		10.106409			57
4	9.789988	9.896137	9.893851	10.106149		10.210012	56
5	9.790149		9.894111	10.105889		10.209851	55
6	9.790310		9.894371	10.105629	10.104061	10.209690	54
7	9-790471		9 894632				53
8	9.790632		9.894892		10.104259	10.209368	52
9	9-799793		9.895152	10.104848		10.209207	51
10	9.790954		9 895412	10.104588			50
11	9.791115	9.895443	9.895672	10.104328		10.208885	49
12	9.791275	9.895343	9.895932	10.104068		10.208725	48
13	9.791436		9.896192	10.103808		10.208564 10.208404	47
14			9.896452 9.896712		10.104855	10.208243	46
15 16	9.791757 9.791917		9.896971	10.103288	10.105055	10.208083	45
17		9.894846		10.103769	10.105154		43
18	9.792237		9.897491	10.102509	10.105254	, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	42
19	9.792397		9.897751	10.102249	10.105354	10 207603	41
20	9.792557		9.898010	10.101990	10.105454	10.207443	40
21	9.792716	9.894446			10.105554	10.207284	39
22	9.792876		9.898530		10.105654		38
23	9.793035		9.898789		10.105754		37
24	9.793195	9.894146	9.899049	10.100951	10.105854	10.206805	36
25			9.899308		10.105954		35
26		9.893946			10.106054		34
27		9.893846		10.100173	10.106154	10.206327	33
28	9.793832		9.900086	10.099914	10.106255	10.206168	32
29	9.793991	9.893645			10.106355	10.206009	31
30	9.794150			10.099395	10.106456	10.205850	30
31	9.794308					10.205692	29
32		9.893343					28
33		9.893243			10.106757	10.205374	27
34 35	9.794942	1		10.098099	10.106959	10.205216	25
36	9.795101	1					24
37	9.795259	1 4 4			10.107161	10.204741	23
38	9.795417	1. ~.	1 : -		10.107261	10.204 583	22
139	9.795575	1 0 6 6			10.107362	10.204425	21
40	9-795733	9.892536	9.903197	10.096803	10.107464	10.204267	20
41	9.795891	9.892435	9.903455	10.096545	10.107565	10.204109	19
42		9.892334		1	10. 107666		18
43	9.796206	9.892233	9.903973	10 096027	10.107767	10.203794	17
44		9.892132			10.107868	10.203636	16
45	9.796521				10.107970	10.203479	15
46	9.796679		9.904750			10.203321	14
47		9 891827	1	1	10.108173	10.203164	13
48	9.796993	1 6 6	1 :	10.094733	10.108274	10.203007	12
49 50	9.797150	1 0 .	19.905526 19.905784	10.0944/4	10.108370	10.202693	10
,—							_
51		9.891421			10.108579		9
52				10.093698		10.202379	,
53 54	9.707024	0.801115	0.006810	10.093440	10.10888 6	10.202066	6
55	9.798001	0.801012	0.007077	10.002022	10.108087	10.201909	5
36	9.798247	9.890011	9.907336	10.092664	10.100080	10.201753	4
57				10.092406			3
58				10.092148	10.109293	10.201440	2
59	9.798716	9.890605	9.908111	10.091889	10.109395	10.201284	1
60		9.890503	9.908369	10.091631	10.109497	10 201 128	
M	Co-sine.	Sine.	Co-tang.	Tang	Co-sec.	Secant	M

39 Degrees.

v	, Sine.	Co-sine.		Co-tang.	Secant	Co-sec.	ж
×				10.091631			60
0	9.798072	9 890503 9.8904 0 0		10.091031			59
2	0.700184	0.800248	9 908886	10.091114	10.109702	10 200816	58
-3	0.700170	0.800105	9.000144	10.000856	10 100805	10.200661	57
4	9 799495	9.890093	9.909402	10.090598	10.109907	10.200505	56
6	9.799651	9.889990	9 909660	10.090340	10.110010	10 200349	55
	9.799806	9 889888	9 909918	10.090082		10.200194	54
8	9.799902	9 889785 9 889682	9.910435	10.089565		10.199883	53 52
9		9.889579	9.910693	10 089307		10.199728	51
10	9.800427		9.910951	10.089049		10.199573	50
11	9.800 (82	9.889374	9.911209	10.088791	10.110626	10.199418	49
12	9.800737		9.911467	10.088533		10.199263	48
13		9.889168		10.088276		10.199108	47
14	9 801047	9.889064	9.911982	10.088018		10.198953	46
16		9.888858 9.888858		10.087502		10.198644	45 - 44
17			9.912756	10.087 244		10 198489	43
18	9.801665		9.913014	10.086986	10.111349	10.198335	42
19	9.801819	9.888548	9.913271	10.086729		10.198181	41
20				10.086471		10.198027	40
21			9.913787	10.086213		10.197872	39
2.2			9.914044	10.085956		10.197718	38 37
23			9 914302	10.085440		10.197411	36
25	0.802743	0.887926	9914817	10.085183		10.197257	35
26	0.802807	0.887821	9.915075	10.084925		10.197103	34
27				10.084668		10.196950	33
28	9.803204	9.887614	9.915590	10.084410		10 196796	32
29 30			9.915104	10 084153	10.112594	10.196489	30
-	9.803664		9.916362	10.083638		10.196336	29
31	9.803817			10.083331		10 196183	28
33	9.803970			10.083123	10.112907	10.196030	27
34	9.804123	9.886989	9.917134	10.082866	10.113011	10.195877	26
35			9.917391		10.113115	10.195724	25
36			9 917648		10.113220	10.195572	2.4
37 38		9.886571	9.917905 9.918163		10.113429	10.195266	22
39			9.918420		10.113534	10.195114	2.1
40	9.805039	9.886362	9.918677	10.081323	10.113638	10.194961	20
41	9.805191	9.886257	9.918934	10.081966		10 194809	19
42		9.886152		10.080809		10-194657	18
43	9.805495	9 886047	9.919448	10.080552	10.113953	10.194505	16
44. 45	9.805047	0.885822	0.010062	10.080295 10.080038		10.194201	15
46		9.885732		10.079781		10.194049	14
47			9 920476	10.079524	10-114373	10.193897	13
48	9.806254			10.079267	10.114478	10-193746	12
49	9.806406			10.079010	10.114584	10.193594	10
50	9-806557		9.921247	10.078753	10.114609	10.193443	-
51	9.806709	9.885205	9.921503		10.114795	10.193291	8
52	0.807011	0.884004	0.022017	10.078240	10.115006	10.192989	7
53 54	9.807161	9.884889	9.922274	10.077726	10.115111	10.192837	6
55	9.807314	9 884783	9.922530	10.077470	10 115217	10.192686	5
56	9.807465	9 884677	9.922787	10.077213	10.115323	10.192535	4
57	9.807015	9.884572	9.923044	10.076956	10.115428	10.192385	3
58	0.807617	0.884260	0.027557	10.076700	10.115640	10.192083	1
50	9.808067	9.884254	9 923813	10.076187	10.115746	10.191933	0.
_	Co-sine		Cirtang.	Tang.	Co-sec.	Secant.	ж

66 LOGARITHMIC SINES, TANCEN'IS, AND SECANTS.

40 Degrees. Secant. Co-sec. M Co-tang. Sine. Co-sine. Tang. 0 9.808067 9.884254 9.923813 10.076187 10.115746 10.191933 1 9.808218 9.884148 9.924070 10.075930 10.115852 10.191782 59 2 9.808 368 9.884042 9.924327 10.075673 10.115958 10.191632 58 3 9.808519 9.883936 9.924583 10.075417 10.116064 10.191481 4 9.808669 9.883829 9.924840 10.075160 10.116171 10.191331 56 9.808819 9.883723 9.925096 10.074904 10.116277 10.191181 55 9.808969 9.883617 9.925352 10 074648 10.116383 10.191031 9.809119 9 883510 9.925609 10.074391 10.116490 10.190881 53 9.809269 9.883404 9.925865 10.074135 10.116596 10.190731 52 9 9.809419 9.883297 9 926122 10.073878 10.116703 10.190581 51 10 9.809569 9.883191 9.926378 10.073622 10.116809 10 190431 50 9.809718 9.883084 9.926634 10.073366 10.116916 10.190282 9.809868 9.882977 9.926890 10.073110 10.117023 10.190132 13 9.810017 9.882871 9.927147 10.072853 10.117129 10.189983 47 14 9.810167 9.882764 9.927403 10.072597 10.117236 10.189833 46 15 9 810316 9 882657 9.927659 10.072341 10.117343 10.189684 45 16 9.810465 9.882550 9.927915 10.072085 10.117450 10.189535, 17 9.810614 9.882443 9.928171 10.071829 10.117557 10.189386 18 9.810763 9.882336 9.928427 10.071573 10.117664 10.189237 43 19 9.810912 9.882229 9.928683 10.071317 10.117771 10.189088 20 9.811061 9.882121 9.928940 10.071060 10.117879 10.188939 40 21 9.811210 9.882014 9.929196 10.070804 10.147986 10.188790 39 22 9.811358 9.881907 9.929452 10.070548 10.118093 10.188642 38 23 9.811507 9.881799 9.929708 10.070292 10.118201 10.188493 37 24 9.811655 9.881692 9.929964 10.070036 10.118308 10.188345 36 25 9.811804 9.881584 9.930220 10.069780 10.118416 10.188196 26 9.811952 9.881477 9.930475 10.069525 10.118523 10.188048 27 9.812100 9.881369 9.930731 10.069269 10.118631 10.187900 33 28 9.812248 9.881261 9.930987 10.069013 10.118739 10.187752 32 29 9.812396 9.881153 9.931243 10.068757 10.118847 10.187604 31 30 9 812544 9.881046 9.931499 10.068501 10.118954 10.189456 31 9.812692 9.880938 9.931755 10.068245 10.119062 10.187308 32 9.812840 9.880830 9.932010 10.067990 10.119170 10.187160 29 28 33 9.812988 9 880722 9.932266 10.067734 10.119278 10.187012 34 9.813135 9.880613 9.932522 10 067478 10 119387 10.186865 35 9 813283 9.880505 9.932778 10.067222 10.119495 10.186717 25 24 36 9.813430 9.880397 9.933033 10 066967 10 : 19603 10 186570 37 9.813578 9.880289 9.933289 10.066711 10.119711 10.186422 23 38 9.813725 9 880180 9.933545 10.066455 10.119820 10.186275 39 9.813872 9.880072 9 933800 10.066200 10.119928 10.186128 22 21 40 9.814019 9.879963 9.934056 10.065944 10.120037 10.185981 41 9.814166 9 879855 9.934311 10.065689 10.120145 10.185834 19 42 9.814313 9.879746 9.934567 10.065433 10.120254 10.185687 43 9.814460 9.879637 9.934823 10.065177 10.120363 10.185540 44 9.814607 9.879529 9.935078 10.064922 10.120471 10.185393 18 17 **E6** 45 9.814753 9.879420 9.935333 10.064667 10.120580 10.185247 15 46 9.814900 9 879311 9.935589 10.064411 10.120689 10.185100 14 47 9.815046 9.879202 9.935844 10 064156 10.120798 10.184954 13 48 9.815193 9 879093 9.936100 10.063900 10.120907 10.184807 12 49 9.815339 9.878984 9.936355 10.063645 10.121016 10.184661 50 9.815485 9.878875 9.936610 10.063390 10.121125 10.184515 11 10 51 9.815632 9.878766 9.936866 10.063134 10.121234 10 184368 98 52 9.815778 9.878656 9.937121 10.062879 10.121344 10.184222 53 9.815924 9.878547 9.937376 10.062624 10.121453 10.184976 54 9.816069 9.878438 9.937632 10.062368 10.121562 10.183931 76 55 9.816215 9.878328 9.937887 10.062113 10.121672 10.183785 5 56 9.816361 9.878219 9.938142 10.061858 10.121781 10.183639 57 9.816507 9.878109 9.938398 10.061602 10 121891 10.183493 3 58 9.816652 9.877999 9.938653 10.061347 10.122001 10.183348 59 9.816798 9.877890 9.938908 10.061092 10.122110 10.183202 I 9.816943 9.877780 9.939163 10.060837 10.122220 10.183057 Co-sine. Co-tang. Sine. Tang. Co-sec. Secant.

49 Degrees.

1

41 Degrees.

			41 1	begrees.			
I' M	Sine.	Go-sine.	Tang.	Co-tang.	, Secant.	Co-sec.	M
-		·			10 122220		60
Į. °	JA-10943	9.077700	2.232.03	10.060.27	10.122220	10.103037	
1 .	9.847088	9-377670	9.939410	10.000502	10.122330	10.182912	59
1 =	19.517233	9.877500	9.939073	10.000327	10.122440	10.102707	58
41 3	9.817379	9.877450	9.939920	10.000072	10.122550	10.182021	57
£ 4	9.817524	9 877340	9.940183	10.059847	10.132000	10.182470	56
1. 5	9.817668	9-877230	9-940438	10.059502	10.122660 10-122776	10.182332	55
6	9.817811	9-877120	9.940094	10.059300	10.122580	10.182187	54
. 7	9.817958	9.877010	9.940949	10.059051	10 122990	10.182042	53
8	9.818103	9.876899	9.941204	10.058796	10.123101	10.181897	52
9	9.818247	9-876789	9.941458	10.058542	10.123211	10.181753	51
10	9.818392	9. 8 76678	9.941714	10.058286	10.123322	10.181608	50
14	0.818596	0.876568	9.941968	10.058012	10.123432	10.181464	49
72					10.123543		48
1 33	0.8:222	0.876247	0.042478	10 057682	10.123653	10.181176	47
1.3	218060	0.876276	0.042722	10.057267	10.122764	10.181021	46
1:3	0.810112	0.876126	0.042088	10.257012	10.122876	10.180887	45
13	0 8 10 2 4 7	9.876044	9.042242	\$8.0667.57	10.123764 10.123875 10.123986	10.180742	44
	0 8 0 407	0.875004	0-042408	10.056502	10.124006	10.180500	43.
1 17	0 810545	0.875702	0.042772	10.066248	10.124096	10.180455	42
1 ::	2 2 1 2 6 2 A	287:68	0.044007	10.00000	10.124318	10.180211	41
1 .9	2 8 10800	0.87777	0.044964	10.064729	10.124429	10.180168	497
							_
	9.819976	9-875459	9-944517	10.055483	10.124541	10.180034	39
32	19.820120	9.875348	9-944771	10 055229	10.124652	10.179880	38
1 23	9.820263	9-875337	9-945020	10.054974	10.124703	10.179737 10.179594 10.179450	37
1 24	19. \$ 20406	9.875136	9-945281	10.054719	10.124874	(0.179594	36
25	9.820550	9.875014	9-945535	10.054405	10.1249	10.179450	. 35
3 20	10. 520 0a 2	10:874001	10.045700	10,054210	10.125097	140.1793071	. 34,2
\$ 27	9-820836	9.874791	9.940045	10.053955	10 125209	10.179164 10.179021 10.178878	33.
j 28	9.820979	9.874680	9.946299	10.053701	10.136320	10.179024	32
1 29	9.821122	9.874568	9-940554	10.053446	10.125432	10.178878	31
30	9 821205	9.874450	9.940808	10.053192	10.135544	10.178735	30
31	9.821407	9.874344	9.947063	10.052937	10.125656	10.178593	29
B 22	.0.824 6 60	0.874222	10-047218	I IC.OC2682	10.12(768	10.1784(0)	28
4 22	.a.8216a+	10.874121	10.047471	10.0 (2428	10.12(870	10.1782071	27
T 24	A.821826	9,874000	9.947826	10.052174	110.12599 L	10.178106	26
3 3 4	19.821977	9,873896	9.948081	10.051919	10.120104	40.178023	25
1 16	0.822120	Q. 87 278A	0.018226	10.051664	10.124216	10.177880	24
1 27	0.822262	9.873672	9.948590	10.051410	10.125328	10.177738	23.
38	9.822404	9.873560	9.948844	10.051156	10.126440	10.177596	22
1 39	g.822546	9.873448	9-949099	10.050901	10.126552	10.177454	3:
1 40	9.822688	9.873334	9-949353	10.050647	10.126665	10.177312	20
T	o Reaken	0.872222	0-040607	10.00202	10.126777	10.177170	14
1 7	0.822070	0.872110	0.040862	10.060128	10.126890	10.177022	18
1 33	0.842114	9,872008	0.000116	10.040884	10.127002	10.176886	17
12	0.822255	0.87288	0.050270	10,040620	10.127002 10.1271.15	10.176746	16
1 48	0.822707	0.872772	0.060625	10 044 27 5	10.127228	10.170003	1-5
122	0.822690	872660	0.050870	10-040121	10.127341	10.176461	14
177	0.822680	0.872547	0.061122	10.048867	10.127462	19.176120	13
1 %	0.821841	0.872424	0.0(1188	10 048612	10.127453	10.176170	12
1 40	A \$22062	0.872221	0.051642	10.048248	10.127679	19.176017	11
				10-048104			10
1 51	9.034245	9.072095	9,957150	10.047850	10.127905	10.175755	8
1 52	y.024300	9-071901	9,952405	10.047595	10.12914	10.175614 10.175473 10.175332	7
53	y.024527	9.07 1005	y-#5 2059	10.047341	10 1050175	10 170222	6
1 54	9.024000	y 0/1755	9.952913	10.047087	10 128220	10.175102	5
1 55	9.034000	3.0/1041	9-953107	10.04647	10.128424	10.175193	3
1 50	y-04949	A 82 444	y. y) 5421	10.046444	10.128686	10.174010	3
1 57	0.825090	D.871704	7.773475	10.04607	10.128600	10.174910 10.174776	2
50	9.745230	0.871.9-	3.773929	10.0400/1	10.708814	10.174629	1
1 29	9 0 25 5 7 1	0.87:07	3.934103	10.04566	10.128027	10.174480	0
	2.02),,	70,10/3	9-93443/		0-	13.174489	
М	Co-sine.	Sino.	Co-tang.	Tang.	Co-sec.	Secunt	M

42 Degrees.

			74	Degrees.			
M	Sine.	Co-sine.	Tang.	Co-tang	Secant.	Co-sec	×
6					10.128927		60
	9.025511	9 870060	9 954437	10.045563	10.129040		
I	9.025051	9.870900	9.954691				59
	9.825791	9.070040	9 954945	10 045055	10.129154	10.174209	58
3				10.044800	16.129268	10.174069	
	9 826071	9.870018	9 95 54 54		10.129382	10.173929	_
5	9.826211	9 870504	9 955707		10. 129496		55
6			9.955961		10 129610		54
7			9.956215		10.129724		53
8			9.956469		10.129839		52
9.	9.826770	9.870047	9.956723	10.043277	10.129953		51
10			9.956977	10.043023	10.130067	10.173090	50
11	9.827049	9.869818	9 957231	10.042769	10.130182	10.172951	49
12	9.827189	9.869704	9.957485	10.042515	10.130296	10.172811	48
13	9.827328	9.869589	9-957739	10.042261	10.130411	10.172672	47
14	9.827467	9.869474		10.042007	10. 130526	10.172533	46
15	9.827606	9 869360	9.958246	10.041754	10.130640	10.172394	45
16	9.827745	9.009243	19.958500	10.041500	10.130755	10.172355	44
17	0.827884	9.809130	19.958754	10.041246	10.130870	10.172116	43
18	9 828023	9.869015	9.959008	10.040002	: 10. 130985	10.171977	42
19	0.828162	0.868000	0.000262	10.040738	10.131100	10.171838	41
20	9.828301	9.868785	9.959516	1.0040484	10.131215	10.171699	40
31		9.868670				10.171561	39
22	0.828678	0.868	0.060022	10.030077		10.171422	38
23						10.171284	37
24	0.828855	9.868324	9.960531	10.039469	10-131676	10.171145	36
25	0.828003	0.368200	0.060784	10.020216	10.131791	10.171007	35
26	9.829131	0.868003	0.061028	10.038062	10.131007	10.170869	34
27		9 867978	0.061201			10.170731	33
28		9 867862			10.132138		32
29	9 829545	0.867747		10 0:8201	10.132253	10.170455	31
30	0.824683	9.867631	9.962052	10.037048	10.132369		30
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31		9.867515			10.132485	10.170179	29
32				10 037440		10.170041	28
33		9.867167	9.902813	10.037187	10.132717	10.169903	27
34	9.830372		9.903007	10.030933	10.132833	10 160628	
35	0.820100	0.866025	9.963574	10.030080		10.169628	25
37	0.830500	9.866819	9.903574	10.030420	10.133065		24
38		9.866703			10.133181		23
	9.030704	9.866586	9.904551			10.169216	22
39	0.8310	0.866470	9.964335		10.133414		20
40	-		-		10.133530		20
41		9.866353				10.168805	19
42	9.831332	9.866237	9 965095	10.034905	10.133763	10.168668	18
43	9.831469	9.866120	9.965349	10.034651	10.133880	10.168531	17
44	9.831606	9.866004	9.965602	10.034398	10.133996	10.168394	16
45		9.865887				10.168258	15
46			9 966 109	10.033%91	10.134230	10.168121	14
47	9.832015	9 865653	9.966362	10.033638	10.134347	10.167985	13
48	9.832152	9.805536	9.966616	10.033384	10.134464	10.167848	12
49	9.832288	9.805419	9 900369	10.033131	10.134581	10.167712	11
50	9.032425	9.805302	9.967123	10 032877	10.134698	10.167575	10
51		9.865185	9 967376	10.032624	10.134815	10.167439	9
52	9.832697	9.865068	9.967620	10.012171	10.174072	10.167303	8
53	9.832833	9.86;950	9.967883	10.032117	10.135050	10.167167	7
54	9.832969	9.864833	9.968136	10.031864	10.135167	10.167031	6
55	9 833105	9.864716	9.968380	10.031611	10.135284	10.106895	5
56	9-833241	9.864598	9.968643	10.031357	10.135402	10 166759	4
57	9.833377	9.864481	9.968896	10.031104	10.135519	10.166623	3
58	9.833512	9.864363	9.969149	10.030851	10.135637		1
59	9.833648	9.864245	9.969403	10.030607	10 125766		1
60	9.833783	9 864127	9.969656	10.030344	10.135873	10.166217	0
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0 9.833783 9.864127 9.96955 10.030344 10.135873 10.166217 0 9.833919 9.863010 9.970162 10.030381 10.135030 10.165946 5 9.834489 9.863574 9.970162 10.029381 10.136324 10.16575 5 9.834489 9.86358 9.970629 10.030381 10.136324 10.16575 5 9.834450 9.86358 9.970629 10.029331 10.136344 10.16575 5 9.834450 9.86358 9.97022 10.030885 10.136692 10.165270 5 9.834499 9.863301 9.971429 10.028851 10.136692 10.165270 5 9.834999 9.863004 9.97135 10.028655 10.136936 10.165270 5 9.835434 9.862347 9.97188 10.027582 10.136936 10.16735 5 9.835433 9.862370 9.972441 10.027559 10.137054 10.164731 4 12.835403 9.862370 9.97248 10.027592 10.13772 10.164731 4 12.835403 9.862470 9.97248 10.027592 10.13772 10.164731 4 12.835403 9.862471 9.973301 10.026792 10.13729 10.164386 5 12.835403 9.862471 9.973301 10.026792 10.13729 10.16438 4 9.835672 9.862334 9.97370 10.026040 10.13729 10.16438 4 9.836075 9.862334 9.97370 10.026040 10.13785 10.164059 4 9.836347 9.861870 9.97446 10.025534 10.138481 10.163573 4 10.83647 9.861870 9.97447 10.025281 10.13842 10.163573 4 10.83647 9.861870 9.97446 10.025534 10.138481 10.163523 4 10.83647 9.861870 9.97526 10.024774 10.138481 10.163523 4 10.83647 9.86180 9.97536 10.024071 10.138481 10.163523 4 10.83647 9.86180 9.97536 10.024771 10.138481 10.163523 3 9.836878 9.861400 9.97536 10.024771 10.138481 10.163523 3 10.83781 9.86082 9.97536 10.024771 10.138481 10.163523 3 10.83781 9.86082 9.97536 10.024771 10.13859 10.162383 3 9.837842 9.86082 9.97536 10.024771 10.13859 10.162383 3 9.837842 9.86082 9.97638 10.02475 10.13958 10.162383 3 9.83874 9.86082 9.97638 10.02475 10.13958 10.162383 3 9.83874 9.86082 9.97638 10.02475 1	_	01-			Degrees.	Commit	0	-
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0, 83,4054 9,563892 9,97062 10.029381 10.136281 10.165811 5 9,834450 9,863573 9,97069 10.029381 10.136381 10.165811 5 9,834450 9,863538 9,970922 10.029381 10.136381 10.165815 5 9,834450 9,863301 9,971429 10.028051 10.136699 10.165270 5 9,83450 9,863301 9,971429 10.028051 10.136699 10.165270 5 9,83451 9,863618 9,971935 10.028051 10.136699 10.16501 5 10.16581 10.	0							60
3 9.834189 9.863774 9.970416 10.029381 10.136246 10.165574 5	1	9.833919			10.030091	10.135990	10.166081	59
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5 9.834450 9.863439 9.971032 10.029078 10.136862 10.165405 5 7 9.834730 9.863419 9.971175 10.028882 10.136817 10.165405 5 8 9.834865 9.863183 9.971682 10.028571 10.136817 10.165135 5 9.834999 9.863064 9.971935 10.028085 10.136817 10.1664866 5 10 9.835134 9.862946 9.97188 10.027512 10.137054 10.164866 5 11 9.835269 9.862827 9.972441 10.027559 10.137171 10.164361 11 9.835269 9.862829 9.97294 10.027559 10.137171 10.164361 12 13 9.8355738 9.862390 9.72948 10.026792 10.137291 10.164328 14 14 9.835672 9.862371 9.973201 10.026799 10.137540 10.164328 14 15 9.835675 9.862371 9.973201 10.026799 10.137540 10.164328 14 16 9.835677 9.862371 9.973301 10.026799 10.137540 10.164328 14 17 9.836075 9.862115 9.973301 10.026540 10.137838 10.163253 10.983647 9.861758 9.974719 10.025231 10.138321 10.163657 10.983647 9.861758 9.974719 10.025231 10.138321 10.163657 10.983647 9.861758 9.974719 10.025281 10.138321 10.163657 12 18 9.836878 9.861628 9.97573 10.022527 10.138360 10.163533 12 18 9.836878 9.861400 9.975479 10.024521 10.13842 10.163523 14 19 9.837649 8.861610 9.975479 10.024521 10.138600 10.163122 3 18 9.837649 8.86082 9.975732 10.024521 10.138600 10.163122 3 18 9.837649 9.86082 9.976732 10.023500 10.13938 10.162858 3 19 9.837649 9.86082 9.976744 10.02356 10.13938 10.162854 3 19 9.837649 9.86082 9.976744 10.02356 10.13938 10.162858 3 10 9.837649 9.86082 9.97697 10.023500 10.13938 10.162858 3 10 9.837649 9.86082 9.97886 10.022770 10.13948 10.16231 3 10 9.838749 9.86082 9.97886 10.022770 10.13948 10.16231 3 10 9.83974 9.85092 9.97886 10.02173 10.13958 10.16236 2 11 9.83974 9.85092 9.97851 10.022470 10.13948 10.16231 3 11 9.83974 9.85092 9.97852 10.02270 10.13948 10.16231 3 12 9.83974 9.85092 9.97852 10.02270 10.13948 10.16236 2 12 9.83974 9.85092 9.97852 10.02270 10.13948 10.16232 3 13 9.8384 9.98538 9.98538 10.01946 10.14124 10.16200 10.16066 10.16232 3 14 9.83974 9.85094 9.98586 10.01947 10.14269 10.16066 10.16066 10.16066 10.16066 10.16066 10.16066 10.16066 10.16066 10.16066 10.16066 10.16066 10.16066 10.16066 10.16066 10.160	3			9 970416	10.029584	10.136226		57
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8 9.834865 9.863183 9.971682 10.028318 10.136817 10.165135 9.835409 9.863664 9.97188 10.027812 10.137074 10.164866 5 10.835403 9.862827 9.972441 10.027539 10.137172 10.164731 4 10.835403 9.852879 9.972694 10.027306 10.137291 10.164397 4 10.983567 10.862871 9.973201 10.026799 10.137291 10.164328 4 10.835671 9.862373 9.973454 10.026799 10.137647 10.164462 4 10.835607 9.863373 9.973454 10.026799 10.137647 10.164462 4 10.835607 9.863115 9.97346 10.026799 10.137647 10.164462 4 10.835607 9.861115 9.97346 10.026793 10.137647 10.164462 4 10.835607 9.861115 9.97346 10.026793 10.137647 10.164462 4 10.835607 9.86115 9.97341 10.026793 10.137647 10.164403 4 10.98361 10.83561 10.83561 10.83561 10.83561 10.8	6	9.834595	9.863419	9.971175		10.136581	10.165405	5
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17	36	0.838610	0.850842	0.078768				24
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56 9.841247 9.857422 9.983826 10.016174 10.142578 10.158753 10.758753 9.841378 9.857390 9.984079 10.015921 10.142700 10.158622 10.158491 10.015964 10.158360 10.1586491 10.015964 10.158360 10.15836					TO THE PARTY OF TH			
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59 9.841640 9.857056 9.984584 10.015416 10.142944 10.158360 9.841771 9.856934 9.984837 10.015163 10.143066 10.158229	58					10.142822	10 158401	
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The state of the s	60	0.841771	0.856024	0.084837	10.015162			
Co-sine. Sine. Co-tang. Tang. Co-sec. Secant.			The second name of the second	-		-	-	-
	M	Co-sine.	Sine.	Co-tang.	Tang.	Co-sec.	Secant.	1

44 Degrees.

			44 De	grees.			_
×	Sine.	Co-sine.	Tang.	Co-tang.	Secant.	Co-sec	×
10	0.841771	9.856934	9.984837		10.143066	10.158229	60
1	9.841902	9.856812	9.985000	10.014010	10.143188	10.158098	60
1 2		9.856690	9.985343	10.014657	10.143310	10.157967	ς έ
3		9.856568	0.084406	10.014404	10.143422	10.157827	67
	9.842294	0.856446	0.985848	10.014152	10.143554	10.157706	66
1 5		9.856323	101680.0	10.013800	10.143677	10.157576	55
1 6		9.856201	9.986354	10.013646	10.143799	10.157706 10.157576 10.157445	54
1 7	9.842685	9.856078	9-986607	10.013393	10.143922	10.157315	53
8	9.842815	9.855956	9.986860			10.157185	
9	9.842946	9.855833	9.987112	10-012868	10.144167	10.157054	51
10	9-843076	9-855711	9.987365	10.012635	10.144289	10 156924	50
1 7	9.843206	9.855588	9.987618	10.012382	10.144412	10.156794	49
1 12		9.855465				10.1 56664	
1 13		9.855342				10.1 56534	
14		9.855219		10 011624	10-144781	10.156405	46
1 15	9.843725	9.855096	9 988629	10.011371	10.144904	10.156275	45
1 16	9.843855	9.854973	9-988882	10.011118	10-145027	10.156145	44
1 17	9.843984	9.854850	9.989134	10.010866	10.145850	10.156016	43
1 18	9.844114	9.854727	9.989387	10.010613	10.145273	10 155886	42
19	9 844243	9.854603	9.989640	10.010360	10.145397	10.155757	41
20	9 844372	9.854480	9 989893	10.010107	10-145520	10 155628	140
21	9.844502	9 854356	9.990145	10.009855		10.155498	
	9.844631	9.854233	9.000108	10.000604	10.145767	10.144160	38
23	9 844760	9.854109	9.990651	10.009349	10.145891	10.155240	37
24	9.844889	9.853986	9.990903	10.009097	40 146014	10.155111	36
2 3	9.845018	9.853862	9.991156	10.008844	10.446138	10.154982	35
	9 845 147	19.853738				10.154853	
27		9.853614	9.991002	10.008338	10.145380	10.154724	33
28		9-853490	9.991914	10.008086	10.140510	10.154595	32
	9.845533			10.007833	10.140034	10.154467 10.154338	31
_	9.845662		1	10.007580			
31		9.853118				10.154210	
	9.845919		9-992925	10.007075	10.147000	10.124081	28
	9.846047		9.993178	10.006812	10.147138	10.153953	2/
34	9.846304	9-852745	9.993430	10.000570	40 147250	10.153825	
	9.846432		0.002026	10.006064	10.147504	10 153568	3
37		9.852371	0-004180	10.006811	10.147610	10.153440	23
	9 846688		0.994441	10.005550	10.147752	10.152212	22
	9.846816		0.004604	10.00 (106	10.147878	10-153440 10-153312 10-153184	22
40	9.846944	9.854997	9.994947	10 00 50 52	10.148001	10.153056	20
41		9.851872				10.152929	
1 42	0.847100	9.851747	0.005453	10.004148	10.148212	10.152801	11
43	9.847127	9.853688	0.005705	10.004206	10.148378	10.152672	17
44	9.847454	9-851497	9.995057	10.004041	10.148502	10.152673	16
45	9.847582	9.851372	9.996210	10.003790	10.148613	10.152418	15
46	9.847709	9.851246	9.996463	10.003537	10.148754	10 152291	14
47		9.851121	9.996715	10.003286	10.148879	10.152164	13
48		9.850996	9.9 96 968	10.003032	10.149004	10.152036	14
	9.848091	9-850870	9.997221	10.002779	10.149130	10.151909	12
50		9.850745	9-997473	10.002527	10.149255	10.151782	10
51		9.850619	9-997726	10.002274	10.149381	10.151655	9
	9.848472		9-997979	10.002021	10.149507	IC 151528	8
53		9.850368	9.998231	10.001769	10.149632	10.151401	7
	9.848726		9.990484	10.001516	10.149758	10.151274	6
	9.848852		9-998737	10.001263	10 149884	10.151148	5
	9.848979		9-998989	10.001011	10.150010	10.151021	
	9.849106		9.999242	10.000758	10.150136	10.150894	3
	9.849232		9-999495	10.000505	10.150202	10.150708	2
59 60	9.849359	0.749011		10.000253			0
-	9.849485			10.000000	0.130515		
М	Co-sine.	Sine.	Co-tang.	Tang.	Co-sec.	Secant.	×

TABLE, III.

Natural Sines.

In this table the natural sines are exhibited to every degree and minute of the quadrant, and arranged so that the degrees corresponding to the sines are to be taken from the top of the page with their minutes in the left aide columns, and the degrees answering to the cosines from the bottom with their minutes in the right side columns.

The natural sine or co-sine of any number of degrees, &c. more than 90, is the same as the natural sine or co-sine of its supplement, found by subtracting them from 1800; or the natural sine or co-sine of an arch greater than 900 is the natural co-sine or sine of its excess above 90°.

To find the natural Sine or Co-sine of a given Number of Degrees, Minutes, and Seconds:

Or, to find the degrees, Minutes, and Seconds, corresponding to a given natural Sine or Co-sine.

These are to be found as directed for the logarithmic sines, &c. except that the differences to 100" are to be taken from the bottom of that column containing the given degrees in the former case, or the nearest natural sine or co-sine in the latter.

BXAMPLE L

The n	atural	sine	of 32°	2 t' is	•	-	•	•	•	'• 38' 15 ". 535090
mul	l sine	of the	given	degree	s and	mine	ıt es i	8 4OS	the na- , this oduct,	(, ,,,
is	•	-	•	• .	■.	•	-	-	-	,
Sun	a is the	e natu	ıral sin	e requ	ired	•	-	•	•	535274

TRAMPLE 11.

Required the natural Co-sine	of 7 LO	40'	25", or	1080	19'	35".
The natural co-sine of 71° 40' is The difference 460, multiplied by						
		_		-		

Remainder is the natural co-sine required - - - 314430

EXAMPLE III.

Required the Degrees, Minutes, and Seconds, answering to the natural Sine 495994.

The natural sine next less to that given is 495964, answering to 29° 44'; the difference between this natural sine and the given one is 30, to which two cyphers being added, and that divided by 422, the difference at the bottom of the column, gives the quotient 7" to be annexed to 29° 44'. Hence 29' 44' 7", or its supplement 150° 15' 53", are the degrees, &c. required.

EXAMPLE IV.

Required the degrees, Minutes, and Seconds, answering to the natual ral Co-sine 368805.

The natural Co-sine next greater to that given is 368936, to which answers 68° 21'; the difference between this natural sine and the given one is 131, to which two cyphers being added, and that divided by 451, the difference found at the bottom of the column, gives the quotient 29". Hence 68° 21' 29", or its supplement, 111° 38' 31" are the degrees, &c. required.

To find the natural versed Sine of a given Number of Degrees, Minutes, and Seconds.

If the given arch be less than 90°, find its natural co-sine, which subtract from 1000000, and the remainder will be the natural versed sine required. But if the given arch exceed 90°, find the natural co-sine of its supplement, which add to 1000000, and the sum will be the natural versed sine required.

EXAMPLE I.

Required the natural versed Sine of 20° 39'.

The natural co-sine of 20° 39' is 935752, which subtracted from 1000000, leaves 064248, the natural versed sine of 20° 39'.

EXAMPLE II.

Required the natural versed Sine of 146° 38' 40."

The natural co-sine of 33° 21' 20" (the supplement of 146° 38' 40") is 835274, which added to 1000000, the sum 1835274 is the natural versed sine required.

To find the Degrees, &c. corresponding to a given natural versed Sine.

Take the difference between the given natural versed sine and 1000000, and the remainder will be a natural co-sine; the degrees, &c. corresponding to which, will be those required, if the given natural versed sine be less than 1000000, but if otherwise, it will be their supplement.

EXAMPLE I.

Required the Degrees, &c. answering to the natural versed sine 098965.

The above subtracted from 1000000, leaves 901035, which taken as a natural co-sine, corresponds to 25° 42′ 20″.

EXAMPLE II.

Required the Degrees, &c. answering to the natural versed Sine 1160172. Here 1000000 subtracted from the above, leaves 160172, which taken out as a natural co-sine, corresponds to 80° 46′ 59″; therefore its supplement 99° 13′ 1″ are the degrees, &c. required.

Natural Co-sines.

Diff. to 485 | 485 | 484 | 484 | 483 | 483 | 482 | 481 | 480 | 478 |

K

0 173648 19080 27912 224951 341932 25819 275937 292372 309017 32558 60 1 173935 19193 203166 225333 142204 259100 275917 192428 309017 32584 1938 2 174121 19195 20561 212561 142569 159381 276470 192306 309547 336593 57 1 174759 19195 20541 12571 14275 21580 142769 159561 276470 192306 309547 336593 57 1 175750 192327 209313 126561 142561 159932 276756 192384 310143 316040 316944 157 1 175751 19252 200931 126561 142561 150059 27715 129049 27917 14248 310040 316944 157 1 175751 19252 200931 12725 12751 144461 1261247 127854 14456 110576 13723 144461 1261247 127854 14456 110576 13723 144461 1261247 127854 14456 126124 12785 14456 12612	м	10°	1 11"	. 12°	1 13°	. 140	ı 15°	1 69	170	180	. 190	×
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54 356738	372988	389114	405142	421036	436802	452435	467430	483182	498488
55 357010	373258	389392	405408	431300	437063	452008	468 187	485557	498740
56 357181	373528	389600	405073	921563	427326	453953	4023144	453792	\$95992
57 357 553 58 257 825	The second second	389938	La Contractor	421827	411848	453472	408038	484301	494440
58 357825	374337	390461		422355	418110	458731	469275	4N4555	499748
60 358368		390731	406737	422518	438371	453990	469473	4848411	500000
M 1999	68"	570	660	650	643	_	6119	. 614	604
				Natural	Cosine	1	-	-	1

SATURAL SINES

	-	-	-	-		250	200	400	-	-
308	210	3.0	35	-4"	300	369	37-	28	200	
	319038	519919							629320	
	515537	530100		559434		588250	1			
	515786	530659	545371	559916	-	588491	602512		619998	
	516035	530906		560157	574524				630024	
	516284		545858	9606398	\$74707		The second second		630076	
501782	510533	531399	546546	560880		100		617305	610000	
8 302012	517031	531891	546589	561121	575451	589666	001672	617494	611127	152
SOUMAG	A SALE OF THE REAL PROPERTY.		540833	561361		1289901	603904	617722	631353	51
502517	-	532384		561602	-	590136	604116	617951	031579	25
1 1000700	1	532530	547563	961083		590371	604367	618180	631804	133
5 505071	1 0 -	The same of	100000	502324		1590840		618637	Granes	
4 503 5 23	Acres 100 mars				1000		605062	618865	633450	46
5 503774	A COLUMN TWO	533615		\$62805			100000	619094	011100	+5
0 90403	519022		548536	563045 563286	577383	Marie Control		619551	011011	
3 50447		534106		553526	The second second		605988	619779	631161	
9 504775	519768	514598	949166	563766	578095	59 4248	606220	620007	631000	41
505030		534844	549500	564007	578332	-	606451	610139	PRESE	
1 504281	The same of	535000	549752	564247	578570		606683	020464	034056	89
21505531			\$49995 \$50238	564727	10000		607145	620920	STACON.	
\$ 506034	The second		550481	564967	579284		607376	521148	63471	36
5 506 28	1000	The second second		565207	579518	591053	607607	621376	014955	35
50653		TOTAL POLICE			The same of the	100 100 100	607838	641604	615tEc	54
8 50701	1000	The Park of the Pa	140	565927	579992		608300	621831	625630	
107 283	A STATE OF THE PARTY OF	100	1000	566166			Property of the last of the la	622287	615854	
0 50755			551937	566406	580703		608761	622515	61007E	712
1 507789	522747	537545	552180	566546	580940	595057	608992	622742	616303	29
3 508040		537790		566886			009223	622970	616527	
3 508 190	100.00	1		567125			600684	623425	5-00751	W.
5 50874				567604			100	613652	512300	53
509041	10000	538771	663392	567844	582123	TO SECOND		623880	637424	1
509291				568083				624102	0 17045	8
509540	No. of Lots	1000000		568562	100 20	The second second	610606	024534	615000	崩
51004		The second second		56880E	583069		611067	621789	616120	
1 1029		-		560040	583305	597392	611297	625016	615540	10
2 510543	Mark Colors		554844	169280	583541	597625	6:1527	625243	638703	155
3 510793	A COLUMN	The second		569519		597858		625470	61Eggs	
5 51129	A RECORDER OF	540730	THE RESERVE	569997				625097	6 To A To	15
51154	525451	100000	10400			1		000130	o Indias	13
51179	\$20709	541464	556054	570475	584733	598791	611677	626377	6 juli 16	474
5 1204	526950	A STATE OF THE PARTY OF THE PAR	556296	570714		599024	612907	626604	640110	H
9 512293	527203	541953	550537	570951	585429	599250	613107	620830	640261	6
51274	527697	543443	557021	571430	-	599732	-	627284	640-80	7
	527944						613526		641001	
513292	528191	542930	557504	571907	586137	000188	614056	627737	641210	-21
51354/		543174								
514040		543419				600885		628189		1
514290	The second second	543997	558469			601118			642110	18
514539	520420	544151	558710	573100	587314	601350	614203		042342	
1514789	1	544395				601583		029594		1
515038	58"	120	559193 550	550	544	501815	15001	010	4/19	
119	98.	3070				23	32	1000	-	-
ar a		-		atural	COAME	-				÷1
tf.to 418	413	409	404	399	394	390	385	380	374	
-	_		The same of the sa	THE RESERVE OF	THE RESERVE AND ADDRESS OF THE PERSON NAMED IN	THE REAL PROPERTY.			The second second	

	-	-		100	-		2		_	
81	40 °	410	429	43°	44°	4.50	46	470	480	49° ×
0	642788	656059		681998		707107	719340	731354	743145	754710 60
	643010			682211		1	719542	731552	743339	754900 59
3		656498		682424			719744	231750	743534	755091 58
A	641679	656937		682849		707723	719946	731949	743728	755472 56
5	643901	657156		683061		The second		732345	744117	755663 55
6	644124	657375	670427	683274		708340	720551	732543	744312	755853 54
2		657594		683486			720753	732741	744500	756044 53
8	PERMIT	657814		683698			720954	732439	744700	756434 54
10	644791	2 4	671074		The Park of the		721156	733437	744894	750425 51
	045013	-		-			731357	783334	745088	756615 50
11	645458	658689	671505	684547	096957	709366	731559	733532	745282	750805 49
13	645080	658008	A COLUMN TO A SECOND				721760	733730	745470	757185 47
14	645902	No. of Concession, Name of Street, or other party of the Concession, Name of Street, or other pa	672151				722163	734125	45864	757375 46
15	645124	659346	672367	685183	697790	710185	732364	734323	746057	757565.45
16	046340		672582			710390		734520	746251	757755 44
17	No. of Concession,	659783				710595	400000	734747	746445	757945 +3
19	647013	660220					722907	734915	740038	758134 42
20	047013	660439					723108	735112	747025	758324 41
-	547455	660657	673658	_				-	- 0	
-	647677	660875				711617	723771	735500	747218	758801 38
23	647898						733971	735900	747604	759082 37
2.4	648120				699663		724172	736097	747798	759271 36
45	648341	561530			100000	A CONTRACTOR OF THE PARTY OF TH	724372	736294	747991	759461 35
20	648563	A CONTRACTOR OF THE PARTY OF		687510	The second second	10000		736491	748184	759650 34
28	648784	662184		687721	A COLUMN TO SERVICE	Hart Wall	724773	736884	748377	759839 33
29	649227	662402	100000	1200			724974	737081	748763	760038 33
30	649448	662620			700909	The second second	725374	737277	748956	760406 30
TI	649669	-	-	-	-	-	725575	737474	749148	760595 29
32	649890	ALC: U	and the same of			10000	725775	737670	749341	760784 28
33	PROLIT	663273	676233	688987	701531	713362	725975	737867	749534	760972 27
34	650332						No. of the last	738063	749726	761161 26
33	650774	66-0-6		689620	4 1 2 2 2		726375	738259	749919	761350 25
1	650995	664144	677090	20500		714473	726575	738455	750111	761727 23
38	651216	664361	677304			714880	726974		750496	761915 23
39	651437	664579	677518	090251		715083	727174	739943	750688	762104 21
40	651657	664796	677732	69046:	702981	715286	727374	739239	750880	762292 20
44	551878	66,013	677946	690673	703188	715490	727573	739435	751072	702480:19
113	652098	665230		The second second	and the same of th		727773	739631	751254	702058.48
43	652319	565448	100000000000000000000000000000000000000	691093	STATE AND A	No. of Parts	727972	739827	751450	762856 17
1	652539	665882		691303	A COLUMN TWO IS NOT THE OWNER.	710099	728172	740023	751840	763044 16
46	5;1980	666099		1000	704221	716505	738570		752032	753432 15
47	653100	666316	1000		704428	1	728769	740609	752223	753608 43
4.8	653421	066532			704634	716911	728969	740805	752415	763796 12
49	653641	555749	The second	The second second	The second second	1 10000	729168	741000	752006	763984 11
H	653861	066956		_	705047	717310	739367	741195	752748	764171 10
51	654081	667183			705253		729566	741301	752989	764359 9
22	554301	662646	680295	69298	705459	717721	729765	741500	753181	704547 8
34	654241	667822	680725	693401	705065	713126	730161	741076	753572	754021 6
55	654961	668040	680934	6036:1	7.06078	718329	739361	742171	753755	705100 0
55	655180	608165	681147	093821	106184	718551	730460	742:66	753946	255205 4
57	655400	608182	681360	694030	706489	718733	730752	742501	754137	765483 3
33	655610	068914	681573		706693					705670 2
60	656059	669131	581998	694449 694658		719138	23125	74174	754519	705857 1
T	49*	488	479	468		4.10	438	400	41"	40° St
=		-		-						N N
-	LOST 4	-	1	-	- VACUE	Co-sine	-	1	-	
	Diff. to	369	363	357	352 34	6 340	334	327	331	315
-	-	-	-	-				1000		

NATURAL SINES.

			_	Sec.	-	-	-	-	-	-	
700	Tia	520	7 530	1.5	40	450 1	56°)	570	38"	1.59	
7500 +4	777446	78801	1 7986	25 800	017 8	19152 8	20018	838671	848048	8474	54
	777320						20200		848301		-
200	1000	Married .				19486.8		878987	8483 (6-1
	ALCOHOL: NAME OF TAXABLE PARTY.	78854				19652 8		839146	848410	4 100 100	181
750005					Mark and the		29688	834304	84866		en:
755791	777878	- 86 -	O TOTAL STATE				24850	839462	84881		
Annual Control	77 KG00	I DESCRIPTION OF THE PERSON NAMED IN COLUMN TWO IS NOT THE PERSON NAMED IN COLUMN TWO IS NAMED IN COLUMN TWO IS NAMED IN COLUMN TWO IS NAMED IN COLUMN TWO IS NAMED IN COLUMN TWO IS NAMED IN COLUMN TWO IS NAMED IN COLUMN TWO IS NAMED IN COLUMN TWO IS NAMED IN COLUMN TWO IS NAMED IN COLUMN TWO IS NAMED IN COLUMN TWO IS NAMED IN COLUMN TWO IS NAMED IN COLUMN TWO IS NAMED IN COLUMN TWO IS NAMED IN COLUMN TWO IS NAMED IN COLUMN TWO IS NAMED IN COLUMN				27 10 14		829620			201
707305	778043	78408	OR SHARE WELL			20.00	30012	100	84897	100000000000000000000000000000000000000	13
70735#	778436				212 8:		30174	K39778	84912		4DE
707538	118608	78944			Section 1979		10337	839930	49275	40000	ag e
767725	778791	78902			STATE OF THE PARTY		30499	840094	84943	3585	33
767911	778973	78974	8 8003	83 810	stas Ri	10817 8	30001	840251	844584	8.586	22/5
188007	779156	78997	7 8005	47 K10	894 82	S rRuce	10811	840409	849776	SERR	
706184	779338	79015	Division in	MOTOR A			30984	840567	84989	4100000	
	100	-		200	-		31146	840724	850046	Score	***
768470	779500		The same of	W 100		-		840882	850100	MA	
758656				1000		DOMESTIC OF		200			98
758841	and the same of		A	200	Section 198	DESCRIPTION OF THE PARTY OF		841039	8 50351		
	780007	No. of Concession, Name of Street, or other Persons, Name of Street, or ot	2 200				31631	841190	842404	425	88
769314				W 100	1914 8		31793	841354	850029		
769400	780430	79111	No. of Concession, Name of Street, or other Designation, Name of Street, Name				11954	841511	E 508 1 1	The second	
750585	780011	74140			1253 81		32115	841608	1000	146000	
769778	780794	79157	0 2011	23 811	423 82	22475	3=477	841825	KEILL	X6aL	19 1
700657	780970	74475	1 5022	97 812	592 8	226418	24418	SargSa	851360	(Acres	
775143							32599	842139	851425		
770328	781530	26211	No. of Lot		100	229718		842296	851571		
770553	100	79229	Mark William	Marie Control	100	23110 8		841452	851727	100	
	781701		7 8019	NA 7100	_		1 3082	841600	Scilia		
				64 813	and the	23467 2		841756	Neadly.		
770884		79204			4000000			842922	None Ma	100	
771009		79282	IN THE OWNER, THE			23035	13400				
771254	782246	I INDUSTRIAL	2 2			200	33505	143079	N 5 2 3 3 5		
771440	782427					Per 1 1 1 1 1 1 1	33723	N43335	052481		
771625	782005	79335	1 8030	27 014	110 8	14:20 8	13825	TESON	9 6 20/40	80.0	
771810	782789	79393	0 8040	0 214	284 8:	24291 8	34540	845,48	8 52791	10007	86
771995	782970	79370	7 8043	3 816	453 8	24456 8	34107	843704	85294	Strage	13 5
772179	783151	79388	4 8043	75 814	1022 8	246 20 8	34367	843860	85300	8520	12 2
772364	10.00	and the same of	2000	48 814	791 X	24785 8	34527	8441116	84324	8632	
772549	To the state of	79423	19 19 mm		1959 8:	14949 8	34688	844172	863350	8627	50 2
772734	783093	79441	W				34848	844328	85365	8624	_
772918	0.0						35008	844484	813707	The second second	-
773104	784055	79476		40000			35168	844640	8538 5		5M 31
773287	1 1000	79494					35328	844795	83400		-
773472					200	3 5770 8	ALC: UNKNOWN	844451	854158	100	
	-		-								55
773056	784596	100000000	Warmen or		6.000 1 1 1 1 1	200	35048	645100	92430	863=	12 11
and the same of	784776	100000000000000000000000000000000000000	0 0			200	35807	K45202	854459	4 745-614	
774024	784957	79565			COLUMN TWO	26262 8	35907	845417	854610	8634	12.1
774809	785137					26426 8	-	845573	85476	8056	
774393	785317	79600				26 590 8		845728	854911	8032	
774577	785497	79617	8 8066	17 816	809 8:	26753 3	36446	845883	85506	Section	
774761			4 8069	88 816	977 8:	26917 8	36609	846038	855211	8041	
774944	0 0	I SELECTION	100	60 817	145 8	270818	36764	846193	N5536	8642	75 1
775128	AL PRACTICAL	79670				27244 8	36924	846348	8.551.	8644	
775312	786217						37083	846503	85566		-
	-	-	-				17245	846658	-		
775495								846812	855816		
773079	786576	79723	3 4070	18 017	015 0	340	37401			8641	
	786756										
	786935										
	787114										
770413	787294	79793	5 8083	33 312	404 8	8 905 82	30036	+7431	NEWSDY	0 0 64	£1]
	787473										2.9
	787532										
	787832					288758			857017		10
277 146	788011	79863	6 XOGO	17 819	1152 8;	290388	38671	48048	85716	86.60	1.5
390	380	370	56	3	5* 1	540	35"-1	320	31"	2100	
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Diff. 10	100	200	1000	288	1 282	1000	1 400	1000	200	246	
1001	300	302	295	200	202	1 275	258	260	45.5	440	

-	60°	610	670	6.12	640	632	660	670	68"	690
M	866025	874620	882948	891007		906308	913545	020505	917184	933580
2	-	874761	883084				913064			933685
2		874902	883221				913782		Section 2.	933789
3	A COLUMN TO SERVICE AND ADDRESS OF THE PARTY	875042	883357	891402			913900			933893
4	866752	845183	883493	891534		906799		920959	The second second	933997
6	866897		100 00		899431	007044		921185		934101
17		875005	883902	891929	00000	907100		921299		934308
8	867187	875746	884038	892061		907189		921412	928053	
2	867331	875888	884109	892192	899939	907411		921525		934515
10	867476	-	_	892323	900005	907533	914705	921638		934619
12	867765	870167	884445	892455	900192	907655	914842	921750	928378	934:26
13			884717	892717	900445		915077	-		934929
14	868054	The second second	884852	892848	900572	908021		922088		
35		876727		892979	900098	908145		922201		
15	868343 868487	877006	885123 885258	893110	900825	The same of the	915546	922313	928917	935238
18		877146	885394	893371	901077		91,603		929133	935444
19	868776	877286		893502	901203	1000	915779	922650	929240	935547
20	868920	8-7425	885664	893633	001330	908751	915896	922762	939348	935650
21	869064	877565	885799	893763	901455		916013	922874	929455	A STATE OF THE PARTY OF THE PAR
24	869351	877704	885934 886069	893894	901581		916130			
24	869495	877983	886204	894154	901833	909236	200			936060
25	269639	878122		894284		909357	916479			
26	869782	878261	886473	894415	902084	Section 19 to 1	910395	N STANKS M	Mark Mark	Marie Company of the
27 28	810000	878400	886508	894545	902209	909599			930097	
20	870212	878678	The second second		902460					936570
30	870356	878817	887011	894934	902585	909961		923880		
31	870499	878956	887145	895064	902710	910087		923991		
32		879095	887279	895194	902836					936876
33 34	ALC: UNKNOWN	879233	887413 887548	895453	902961	Contract of the last of the la	917408	924213		
25		879510					917639			
36	871314	879649	887815	895712	903335	910684	917755	924546	931056	937282
37		879787	000	695841	903460		917870			
38		880063	888217	895470	903385		917986			937485
40		880201	888150	Sqbiiq			918216			
4	B71927	880339	888484	846358	903958	911284	-	925099		
42		880477	888017		904083					937889
43		880615	888751		904207		918501			
#	1	8808g1	888884 889017	896794 896873	904331	911762	918676	925430	931902	938091
45		881028		897001	004570		978906		932113	938292
47		881166	889283	897130	904703	912001	919021	925761	932219	938393
48		881303	889416		904817	913120	919135	925871	932324	938493
49	873064	881447	889549. 889682	897387 897515	905075	911139	919250	925980	932429	038694
		881716	889814	-			-	926200	-	
51	Design Street,	881853	200		905198		919593			938794
53	ALC: YES	881990	890080	807900	905445	912715	919707	925410	932849	038004
54	875772	882157	890213	898028	905569	912834	919821	926514	932954	939094
55		882254	800345	808156	905092	912953	919930	926638	933058	939194
		882401	890478	8984111	905030	913100		926857		939394
58	874338	882674	840742	898539	905062	913309	920277	926900	913172	939493
54		882811	890874	898666	906185	913427	920391			939593
00	_	_	891007					927184	933580	939693
M	290	280	270	26"	250	210	23	120	21	200
	-		100	N	atu si t	0.811115	-			
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4 70"	710	720	73°	740	75"	76"	770	780	790	126
0 939693	945519	951057	956305	961161	965926	970296	974370	978148	9816mg	60
The second second	945613		956390		955001	970366	974935		981683	
2 939891	The second second		No. of the last of	901422	966076	970436	974501	978268	951755	12
3 939991	445802	951326		961501	966151	970506	974566	978329	951793	100
4 940090		951415		961982	966226	970577	974631		981849	100
5 940189		951505		961662	466301	1070647	974596	978449	981904	55
0 940288		951594	200	961741	966376	970746	974761	978 000	981059	154
7 940387	946180			961811	966451	970786	974826	978 569	482014	188
	946274	951773	956983	961901	966526	970846	974891	978629	982054	188
9-940585	946368	951862	957067	961980	966600	970926	974956	978689	952123	Hall
0 940684	946462	120120	957151	962059	966675	970995	97.5030	978748	982178	100
1 940781		952040		962130	966749	-			o Kanan	
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6 941274	No. of Street, or other Designation of the last of the	y52484	957055	962534	967120	971342	975342	979045	982505	
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18 941471		952661	957822	962692	967268	971549	975471	979164	082412	14
19 941569	947394	952750	957906	962770	967342	971618	975535	979223	08285	
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6 942352		Marin Co.	958489	The second		972030	975980	979634	981989	3.5
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8 942447	The same of	953542	958654	963397		972100	976107	979750	No Sodo	33
9 942544	1	953629	958737	100000000000000000000000000000000000000		972234	970170	979809	983149	24
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1 942739		953804	958902	963708		972438	970359	979983	6,2308	29
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7 943319		954327	959314	984095		972776	970072	980271	983574	
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4 944-34	950425	955707	060775	905397	909501	973910	977722	981237	984452	17
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L L			80	72	03	55	47	38	30	21 1	3 4	ı
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TABLE IV.

THE

ANGLES

Which every Point and Quarter Point of the Compass makes with the Meridian.

Ю	RTH	POINTS	°	,	"	POINTS	800	TH
		Q1	2	48	45	01	,	
1		01	5	37	30			1
		03	8	26	15	1 . •		1
N. b. E.	N. b. W.	1	11	15	0		S. b. E.	S, b, W.
		11/4 11/2 13/4	14	3	45	1 ½ 1 ½ 1 ½		
		1 1 2	16	52	30	1 1 5		
			19	41	15			
N. N. E.	N. N. W.	2	22	30	0		S. S. E.	s. s. w.
	·	21	25	18	45			
		24	28		30			1 1
1		21	30	-	15			1
N.E.b.N.	N.W.b.N.	3	33	45	0		S. E. b. S.	S. W. L.S.
		31	36	33	45		1	1
		34	39	22	30	31	í	1
		33	42	11	15	33		
N. E.	N. W.	4	45	0	0		S. E.	s. w.
Į		41	47	48	45		l	
	ł	44	50	37	30	} 4 1	}	1 1
	•	4.3	53	26	15		1	1
N.E.b.E.	N.W.bW.	5	56	15	0	5	S. E. b. E.	S. W. b. W
	-	51	59	3	45	51		1
		5 1	61	52	30	54	į	1 1
		5 3	64	41	15	53	i .	1
E. N. E.	W. N. W.	6	67	3 0	0		E.S.E.	W. S. W.
		$6\frac{1}{4}$	70	18	45	61	ł	1
		61	73	7	30	61	Ì	1
		63	75	56	15		}	1
E. b. N.	W. b. N.	7	18	45	0	7	E. b. S.	W. b. S.
		74	81	33	45	71		
		$7\frac{1}{2}$	84	22	3 0	7 1		
		7 1/2 7 1/2 7 3/4	87	11	15	71 71 72 73 73 73 73 73 73 73 73 73 73 73 73 73	}	
East.	West.	8	90	0	0		East.	West.

TABLE V.

A TRAVERSE TABLE,

To every Degree and Quarter Degree of the Compass or Horizon.

EXPLANATION.

This Table is calculated for the easy and expeditious solution of the several cases of Right-angled Plane Trigonometry. It is generally esteemed a useful and requisite assistant to the Surveyor, the Navigator, and to every one, who has any concern with trigonometry in the exercise of his profession. The manner of using it must be very obvious to all, who are acquainted with the principles of that excellent branch of geometry; but to those, who have only a superficial knowledge of the subject, the following description and examples will be necessary.

In this Table, one of the acute angles—whether given, or required—if less than 45°, is found, to the nearest 15' at the top of the page; but, if more than 45°, it must be sought at the bottom, where the numbers are found in a retrograde order. And whether the angle under consideration, be at the top, or bottom, the Hypothenuse, if less than 120, is always in a Distance column; against which, in a column marked Laticade, is found the side contiguous to the angle; and in a column, marked Departure, the side opposite the angle.

When the given numbers exceed the limits of the table, any aliquot parts, such as a half, one third, &c. may be taken; and those found corresponding are to be doubled, trebled &c. that is, multiplied by the same figure, that the given number is divided by.

BXAMPLES

1. Let the Hypothemuse of a right angled triangle=96 and one of the acute angles=330 45'; required the sides.

Under 33° 45' at the top of the table, and against 96 in a Distance column, are found 79.84 in a Latitude column for the side contiguous to the given angle, and 53.34 in a Departure column for the side oppo-

site the given angle.

2. Let the sides of a right angled triangle be=89.23 and 66.02;

required the angles and Hypothenuse.

By inspecting this table, till these two sides are found against each other in adjoining columns of Latitude and Departure, the angle opposite the longest side is found to be 530 30°, the other, 360 30° and

In this manner all the cases of Right-angled Plane Trigonometry can be readily solved; but for more particular directions, beeks on this subject should be consulted.

84								
-	15	'	<u> </u>	30	, 1	Dist.	45	
Dist	Lat.	Dep.	Dist.	Lat.	Dep.	77	Lat.	Dep.
<u> </u>	1.00	0.00	-	1.00	0.0 1	1	1.00	10.0
1 2	2.00	10.0	2	2.00	0.02	2	2.00	0.03
3	3.00	0.01	3	3.00	0.03	3	3.00	0.04
1 4	4.00	0.03	4	4.00	0.03	4	4.00	0.05
_ 5	5.00	0.02	<u>;</u>	5.00	0.04	5	5.00	0.07
6	6.00	0.03	6	6.00	0.05	6	6.00	0.08
7	7.00	0.03	7	7.00	0.06	7 8	7.00	0.09
8	8.00	0.03	8	8.00	0.07	وا	8.00 4.00	0.10
10	9.00	0.04	10	9.00	0.09	10	10.00	0.12
<u> </u>	10.00	0.04		00.11	0.10	11	11.00	0.14
112	11.00 12.00	0.05	11.	12.00	0.10	12	12.00	0.16
13	13.00	0.05	13	13.00	0.11	13	13.00	0.17
14	14.00	0.06	14	14.00	0.12	14	14.00	0.18
15	15.00	0.07	15	15.00	0.13	15	15.00	0.20
16	16 00	0 07	16	16.00	0.14	16	16.00	0.21
17	17.00	0.07	17	17.00	0.19	17	17.00	0.22
18	18.00	0.08	18	1800	0.16	18	18.00	0.24
19	19.00	0.08	19	19.00	0.17	19	19.00	0.25
20	20.00	0.09	20	20.60	0.17	20	20.00	0.26
21	21.00	0.09	21	21.00	0.18	21	21.00	0.27
22	22.00	0 10	22	22.00	0.19	22	22.00	0.29
23	23.00	0.10	23	23 00	0.21	24	34.00	0.31
24	24.00 25.00	0.10	24 25	25.00	0.22	25	25.00	0 33
26		1	26	26.00	0.23	26	26.00	0.34
27	26.00 27 00	0.11	27	27.00	0.24	27	27 00	0.35
28	28.00	0.12	28	28.00	0.24	28	28.00	0.37
29	29.00	0.13	29	29.00	0.25	29	29.00	0.38
35	30.00	0.13	30	30.00	0.26	30	30.00	0.39
31	31.00	0.14	31	31.00	0.27	31	31 00	0.41
32	32.00	0.14	32	32.00	0.28	32	32.00	0.42
33	33.00	0.14	33	33.00	0.19	33	33.00	0.4
34	34.00	0.15	34	34.00	0.30	34	34 00	0.44
35	35.00	0.15	35	35.00	0.31	35	35.00	0.46
36	36 OO	0.16	36	36.∞	0.31	36	36.00	0.47
37	37.00	0.16	37	37.00	0.32	37	37.00	0.48
38 39	38.00	0.17	38	38.00	0.33	38	38.00	0.50
40	39.00 40.00	0.17	39 40	40.00	0.35	40	40.00	0.52
41		0.18		41.00	0.36	41	41.00	0.54
42	41 00	0.18	41	42.00	0.37	42	42.00	0.55
43	43.00	0.19	43	43.00	0 38	43	43 00	0.56
44	44.00	0.19	44	44.00	0.38	44	44.00	0.58
45	45.00	0.20	45	45.00	0.39	45	45.00	0.59
46	46.00	0.20	46	46.00	0.40	46	46.00	0.60
47	47.00	0.21	47	47.00	0.41	47	47.00	0.62
48	48.∞	0.21	48	48.QO	0.42	48	48.00	0.63
49	49.00	0.21	49	49.00	0.43	49	49.00	0.64
50	50.00	0.22	.50	50.00	0.44	50	50.00	
51	51,00	0.22	51	51.00	0.45	51	51.00	0.67 0.68
52	52.00	0.23	52	52.06	0.45	52	52.00 53.00	0.00
54	53.00 54.00	0.23	53	53.00 54.00	0.40	53 54	54.00	0.71
55	55.00	0.24	54	55.00	0.48	55	55.00	0.72
56	56.00	0.24	55	56.00	0.49	56	56.00	0.73
57	57.00	0.25	56	57.00	2.50	57	57.00	0.75
58	58.00	0.25	57 58	58.00	0.51	58	57.99	0.76
59	59.00	0.25	59	59.00	0.51	59	58.99	0.77
60	60.00	0.26	66	60.00	0.52	60	59.99	0.79
Dist.	Dep.	Lat	i t	Dep.	Lat.	Dist.	Dep.	Lat.
Ē	4:	5,	ءً ا	30	,	Ä	1.	5'
				Degre	_	-		

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1	וש	15	,	<u> </u>	3.,		<u> </u>	45	,	Į.
1	Dist	Lat.	Dep.	Dist.	Lat.	D.p.	Dist.	Lai	Dep.	ľ
	61 6. 1	61.00	0,27	61	61.00				0.80	l
	62	62.00	0.27	62	62.00	0.53	61 62	61.99	18.0	Į
	63	63.00	0.27	63	63.00	0.54	63	62.99	0.82	I
	64	64.00	0.28	64	64.00	0.56	64	63.99	0.84	ŀ
	65	65.00	0.28	65	65.00	0.57	65	64.99	0.85	ļ
-	66	66.00		66	66.00				0.86	ŀ
	6 7	67.00	0.29	67		0.58	66	65.99	0.88	ı
	€ 8	68.00	0.29	68	67.00	0.58	67	66.99	0.89	l
	69	64.00	0.30	69	69.00	0.59	-69	67.99 68.99	0.92	l
	7 0	70.00	0.31	70	70.00	0.61	70	69.99	0.92	ı
1-	_				,	·	-			ľ
	71	71.00	0.31	71	71.00	0.62	71	70.99	093	ı
	72	72.00	0.31	72	72,00	0.63	72	71.99	0.94	i
	73	73.00	0.32	73	73.00	0.64	73	72.99	0.96	ı
	74	75.00	0.32	74 75	74.60	0.65	74	73.99	0.97	l
	75		1.33		75.00		75	74.99		ł
	76	76.00	0.33	76	76.00	0.66	76	75.99	0.99	ı
	77	77.00	0.34	77 78	77.00	0.67	77	76.99	1.01	ı
	78	78.00	0.34		78.00	0.68	78	77.99	1.02	l
	79 80	79.00	0.34	79 80	79.60	0.69	79	78.99	1.03	l
- 1		80.00	0.35		80.00	0.70	80	79.99	1.05	l
	81	81.00	0.35	18	81.00.	0.71	18	80.99	1.06	ı
	82	82.00	0.36	82	82.00	0.72	82	81.99	1.07	ł
1	83	83.00	0.36	83	83.00	0.72	83	82.99	1.09	ı
	84	84.00	0.37	84	84-00	0.73	84	83.99	1.10	ı
	85_	85.00	0.37	85	85.00	0.74	85	84.99	1.11	ı
	86	86,00	0.38	86	86.00	0.75	86	85.99	1.13	ł
	87	87.00	0.38	87	87.00	0.76	87	86.99	1.14	l
	88	88.00	0.38	88	88.00	0.77	88	87 99	1.15	ł
	89	89.00	0.39	89	89.00	0.78	89	88.99	1.16	l
	90	90.00	0.39	90	90.00	0.79	90	89.99	1.18	ı
1	91	91.00	0.40	91	91.00	0.79	91	90.99	1.19	l
•	92	92.00	0.40	92	92.00	0.80	92	91.99	1.20	ı
	93	93.00	0.41	93	93.00	0.81	93	92.99	1.22	ł
	94	94.00	0.41	94	94.00	0.82	94	93-99	1.23	ł
Г	9	95.00	0.41	95	95.00	0.83	95	94.99	1.24	Į
١.	96	96.00	0.42	96	96.00	0.84	96	95.99	1.26	I
	97	97.00	0.42	97	97.20	0.85	97	96.99	1.27	ł
1	98	98.00	0.43	98	98.00	0.86	98	97-99	1.28	l
t	99	99.00	0.43	99	99.00	0.86	99	98.99	1.30	ŀ
1	00	100.0	0.44	100	100.0	0.87	100	99.99	1.31	ł
1	01	101.0	0.44	101	101.0	0.88	101	101.0	1.32	ı
	02	102.0	0.45	102	102.0	0.89	102	102.0	1.34	1
1	03	103.0	0.45	103	103.0	0.90	103	103.0	1 35	١
1	04	104.0	0.45	104	104.0	0.91	104	104.0	1.36	ł
1	05	105.0	0.46	105	105.0	0.92	105	105.0	1.37	ł
17	06	106.0	0.46	106	106.0	0.92	106	106.0	1.39	ı
•	07	107.0	0.47	107	107.0	0.93	107	107.0	1.40	l
	08	108.0	0.47	108	108.0	0.94	108	108.0	1.41	l
1	09	109.0	0.48	109	109.0	0.95	109	109.0	1.43	ĺ
1	10	110.0	0.48	110	110.0	0.96	110	110.0	1.44	ı
17	11	1110	0.48	111	111,0	0.97	111	111.0	1.45	ł
1	12	1120	0.49	112	112.0	0.98	112	112.0	1.47	ı
	13	113.0	0.49	113	113.0	0.99	113	113.0	1.48	ı
	14	114.0	0.50	114	114.0	0.99	114	1:4.0	1.49	ı
	ιġ	115.0	0.50	115	115.0	1.00	115	115.0	nisi	ŀ
1-	16	116.0	0.51	116	116.0	1.01	116	116.0	1.52	l
	17	117.0	0.51	117	117.0	1.02	117	117.0	1.53	ŀ
	18	118.0	0.51	118	118.0	1.03	118	118.0	1.54	ŀ
	19	119.0	0.52	119	119.0	1.04	119	119.0	1.56	l
	20	1200	0.52	120	120.0	1.05	120	120.0	1.57	ı
·-	_	Dep.	Lat		Dep	Lat.	;	Dep	lat.	ĺ
1	Diet.			ë: A			Dist	_	-	ŀ
	9.	45	· · · · · · · · · · · · · · · · · · ·	Lā.		0'	<u> </u>	13) <i>'</i>	Į
_				- 00	LUCUI					:

89 MEGREBS.

30	. 0		1.5	7	30		4:	,
Diet		Dep.	Lat.	Dep.	Lat	Dep.	Let	Dep
	Lat.	0.02	1.00	0.02	1.00	0.01	1.00	0.03
	2.00	0.03	2.60	0.04	2.00	0.05.	2.00	0.06
3	3.00	0.05	3.00	0.07	3.00	0.08	3.00	0.09
4	4.00	0.07	4.00 5.00	0.09	4.00 5.00	0.10	4.00 5.00	0.12
5	5.00	0.10	6.00	0.13	6.00	0.16	6.00	0.18
6	6.00 7.00	0.13	7 00	0.15	7.00	0.18	7.00	0.21
7 8	8.00	0.14	8.00	0.17	8.00	0.21	8.00	0.24
9	9.00	0.16	9.00	0.20	9.00	0.24	9.00	0.27
10	10.00	0.17	11.00	0.24	11.00	0.19	10.99	0.34
11	11.00 12.00	0.11	12.00	0.26	12.00	0.31	11.99	0.37
13	13.00	9.23	13.00	0.28	13.00	0.34	12.99	0.40
14	14.00	0.24	14.00	0.31	14.00	0.37	13-99	0.43
15	15.00	0.16	15.00	0.33	14.99	0.39	14-99	0.49
16	16.00	0.28	16.00	0.37	15.99 16.99	0.45	15.99 16.99	0.52
18	18.00	0.31	18.00	0.39	17.99	0.47	17-99	0.55
19	19 00	0.33	19.00	0.41	18.99	0.50	18.99	0.58
20	20.00	0 35	20.00	0.44	19.99	0.52	19.99	0.61
21	21.00	0.37	21.00	0.46 0.48	20.99 21.99	0.55 0.58	20.99	0.67
22 23	22.00 23.00	0.40	21.99	0.50	22.99	0.60	22.99	0.70
24	24.00	0.42	23.99	0.52	23.99	0.63	23.99	0.73
25	25.00	0.44	24 99	0.55	24.99	0.65	24-99	0.76
26	26,00	0.45	25.99	0.57	25.99	0.68	25.99	0.79
27	27.00	0.47	26.99 27.99	0.59	26.99 27.99	0.73	26.99 27.99	0.86
29	29.00	0.51	28.99	0.63	28.99	0.76	28.99	0.89
30	30 00	0.52	29.99	0.65	29.99	0.79	29.99	0.92
31	31.00	0.54	30 99	0.68	30.99	18.0	30.99	0.95
32	32.00	0.56	31.99	0.70	31.99	0.84	31.99	1.01
33 34	33.99	0.58	3 2.9 9	0.72	32.99 33.99	0.89	33.98	1.04
35	34-99	0.61	34 99	0.76	34.99	0.92	34.98	1.07
36	35.99	0.63	35.99	0.79	35.99	0.94	35.98	1.10
37	36.99	0.65	36 99	0.81	36.99	0.97	36.98	1.13
38	37-99 38.99	0.66	37·99 38.99	0.83	37.99 38.99	1.02	37.98 38.98	1.19
39 40	39.99	0.70	39.99	0.87	39.99	1.05	39.98	1.22
41	40.99	0.72	40.99	0.89	40.99	1.07	40.98	1.25
42	41.99	0.73	41.99	0.92	41.99	1.10	41.98	1.28
43	42.99	0.75	42.99	0.94	42-99 43-98	1.13	42.98 43.98	1-31 1-34
44	43 99 44-99	0.77	43.99 44.99	0.98	44 98	1.18	44.98	1.37
45	45.99	0.80	45.99	1.00	45.98	1.20	45 98	1.40
47	46.99	0.82	46.99	1.03	46.98	1.23	46.98	1-44
48	47-99	0.84	47.99	1.05	47.98 48.98	1.26	47.98	1.47
49	48.99 49-99	0.85	48.99 49 99	1.07	49.98	1.31	49.98	3.53
50	50.99	0.89	50.99	1.11	50.98	1.34	50.98	1.56
51 52	51.99	0.91	51.99	1.13	51.98	1.36	51.98	1.59
53	52.99	0.93	52.99	1.16	52.98	1.39	52.98	1.62
54	53.99	0.94	53.99	1.18	53.98 54.68	I-41 I-44	53 97 54-97	1.65
55	54.99	0.98	55.99	1.22	55.98	1.47	55.97	1.71
56	55.99 56.99	0.98	55.99	1.24	56.98	1.49	56.97	1.74
57 · 58	57.99	1.01	57.99	1.27	57.98	1.52	57-97	1.77
59	58.99	1.03	58.99	1.29	58.98	1.54	58 97 59-97	1.80
60	59.99	1.05	59.99 Date	1.31	59.98 Ten	1.57 Lat.	Dep.	Lat
Dist	Dep.	Lat.	Den.	Let	Dep.		15	
LA			4)°	30			1

\$8 Degrees.

Y 8	6	,	15	, ,	30	,	451		
5	Lat	Dep.	Lat	Dep.	Lat	Dep.	Lat.	Dep.	
61	60.99	1.96	60.99	1.33	60.98	1.60	60.97	1.86	
62 63	61.99	1.08	61.99	I.35 I.37	61.98 62.98	1 62 1	61.97 62.97	1.89	
64	63.99	1.12	63.98	1.40	63.98	1.68	63.97	1.95	
65	64-99	1.13	64.98	1.42	64 98	1.70	64-97	1.99	
66	65.99	1.15	65.98	1.44	65.98	1.73	65.97	2.02	
67	66.99 67.99	1.17	66.98 67.98	1.46 1.48	66.98 67.98	1.75	66-97 67.97	2.05	
69	68.99	1.20	68.98	1.51	68.98	1.81	68.97	A.11	
70	69.99	1.22	69.98	1.53	69.98	1.83	69.97	2.14	
71	70.99	1.24	70.98 71.98	1.55	70.98 71.98	1.86	70.97 71.97	2.17	
72 73	71.99	1.27	72.98	1.57	72.98	1.91	72.97	2.23	
74	73.99	1.29	73.98	1.61	73.97	1.94	73.97	2.26	
75	74-99	7.31	74-98	1.64	74-97	1 96	74-97	2.29	
76	75-99 76.99	1.33 1.34	75.98 76.98	1.66	75-97 76.97	1.99	75.96 76-96	2.32 2.35	
78	77.99	1.36	77.98	1.70	77.97	2.04	77.96	2.38	
79	78.99	1.38	78.98	1.72	78.97	2.07	78.96	2.41	
80	79-99	1.40	79.98	1.75	79-97	2.09	79.96	2.44	
81 82	80.99	1.41 J.43	80.98 81.98	1.77	80.97 81.67	2.12	80.96 81.96	2.47 2.50	
83	82.99	1.45	82.98	1.81	82.97	2.17	82.96	2.53	
84	83.99	1-47	83.98	1.83	83.97	2.20	83.96	2.57	
85	84-99	1.48	84.98	1.85	84-97	2.25	84.96	2.60	
87	85.99 86.99	1.50	85.98 86.98	3.00	86.97	2.25	85.96 86.96	2.66	
88	87,99	1.54	87.98	1.92	87.97	2.30	87.96	2.69	
89	88-99	1.55	88.98 89 98	1.94	88.97	2.33 2.36	88.96 89.96	2.72	
90	89.99	1.57	90.98	1.99	89.97	2.38	90.96	2.75	
92	90,99	1.61	91.98	2.01	91.97	2.41	91.96	2.81	
93	92.99	1.62	92.98	2.03	92.97	2.43	92.96	2.84	
94	93-99	1.64	93.98	2.05	93.97	2.40	93.96 94.96	2.87 3.90	
96	95-99	1.68	95-98	2.00	95-97	2.51	95.96	1.93	
97	96 99	1.69	96.98	2.12	96.97	2.54	96.95	2.96	
98	97.99	1.71	97.98	2.14	97.97	2.57	97.95	2.99	
100	98.98	I.73	98.98 99.98	2.16	98.97	2.59	98.95	3.02 3.05	
101	1010	176	101.0	2.20	101.0	2.64	101.0	3.08	
103	102.0	1.78	102.0	2.23	102.0	2.67	102.0	3.12	
103	103.0	1.80	103.0	2.25	103.0	2.70	103.0	3.15	
105	104.0	1.83	1050	2.29	105.0	2.72 2.75	104.0	3.21	
106	106.0	1.85	106.0	2.31	106.0	2.77	106.0	3.24	
107	107.0	1.87	107.0	2.33	107.0	2.80	107.0	3.27	
108	108.0	1.90	108.0	2.36	108.0	2.83	108.C	3.30 3.33	
110	110.0	1.92	110.0	2.40	110.0	2.88	110.0	3.36	
111	111.0	1.94	111.0	2.42	111.0	2.91	111.0	3.39	
1113	1120	1.95	112.0	2.44	1120	2.93	112.0	3.42	
1114	1140	1.97	1140	2.47	113.0	2.96	113.0	3.45 3.48	
115	115.0	2.01	115.0	2.51	115.0	3.01	115.0	3.51	
116	116.0	2.02	116.0	2.53	116.0	3.04	116.0	3.54	
117	1170	2.04	117.0	2.55	117.0	3.06	117.0	3.57 3.60	
119	119.0	2.08	119.0	2.60	119.0	3.12	119.0	3.63	
120	120.0	2.09	120.0	2.62	120.0	3.14	120.0	3 66	
Dig.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	
قا	0'		4		30	1	15	/	

88 DEGREES

1 5 1	0/		15	/	30	,	45	
¥.	Lat.	Dep.	Lat.	Вер.	Lut.	Der	Lat.	Dep.
1	3,00	0.03	1.00	0.04	1,00	0.04	1.00	0.03
2	\$.00 3.00	0.07	3.00	0.08	2.00 3.00	0.09	2.00 3.00	0.10
3 4	4.00	014	4.00	0.16	3-99	0.17	4.00	0.19
_5	5,00	0.17	5.00	0.20	5.00	0.23	4.99	0.24
6	6.00	0.21	6.00 6.99	Q.24 Q.27	5.99 6.99	0.26	5.99 6.99	0.34
7	7.00 8.00	0.28	7.99	0.31	7.99	0.35	7.49	0.38
9	8.99	0.31	8-99	0.35	8.99	0.39	8.99	0.43
10	9.99	0 35	4.99	0.39	9.99	0.44	9.99	0.48
11	10.99	0.38	10.99	0.43	10.99	0.48	10.99	0.53
. 13	12.99	0.45	12.99	0.51	12.99	0.57	12.99	0.62
14	13.99	0.49	11.99	0 55	13.99	0.61	13.98 14.98	0.67
15	14.99	052	14.99	0.59	15.98	0.70	15.98	0.77
16	15.99 16.99	0.56	15.99	0.67	16.98	0.74	16.98	0.82
18	17 99	0.63	17.99	0.71	17.98	0.79	17.98	0.86
19	18.99	0.66	18 99 19 98	0.75	19.98	0.83	18.98	0.96
21	20.99	0.73	20.98	0.82	20.98	092	20.08	1.61
23	21.99	0.77	21.98	0.86	21.98	0.96	21.97	1.66
23	22.99	0.80	22.98	0.90	22.98 23.98	1.00	22.97 23.97	1.10
24 25	23.99 24.98	0.87	34 98	0.98	24 98	1.09	24.97	1.10
26	25.98	0.91	25.98	1.02	25.98	1.13	25.97	1,25
27	26.98	0.94	26.98	1.06	26.97	1.18	16.97	1,25
28 29	27 98 28.98	1.01	27.98 28.98	1.10	27:97 28.97	1.22	27.97 28.97	I.34 1.39
30	29.98	1.05	29.98	1.18	29.97	1.3 f	29.97	1.44
31	30.98	1.08	30.98	1.22	30.97	1.35	30.96	1.49
32	31.98	1.12	31.98	1.30	31.97 32.97	1.40	31.96	1.58
33 34	33.98	1.15	33.97	1.33	33 97	1.48	33.96	1.63
35	34.98	1.22	34-97	1.37	34-97	1.53	34.96	1.68
36	35.98	1.26	35.97	1.41	35.97 36.96	1.57	35.96	1.73
37 38	36.98 37.98	1.29	36.97 37.97	1.45	37.96	1.66	30.96	1.78
39	38.98	1 36	38.97	1.53	38.96	1.70	38.96	1.87
40	39.98	1.40	39.97	1.57	39.96	1.74	39-95	1.92
41	40.98	1.43	40.97 41.97	1.61	43.96 41.96	1.79	40.95	197
42 43	42.97	1.50	42.97	1.69	42.96	L.88	42.95	106
44	43.97	1.54	43-97	1.73	43.96	1.92	43.95	2.11
45	44.97	1.61	44.97	1.81	44.96	201	44.95	2.16
46 47	45.97 46.97	1.64	45.96 46.96	1.85	45.90	2.05	45.95 46.95	2,26
48	47-97	1.68	47.96	1.88	47.95	2.09	47-94	2.30
49	48.97 49.97	1.71	48.96 49.96	1.92	48.95 49.95	2.14	48.94	23,
50 51	50.97	1.78	50.96	2.00	50.95	2.22	50.94	245
52	51.97	1.81	51.96	2.04	51.95	2.27	51.94	2.49
53	52.97	1.85	52.96	2.08	52 95	2.31	52.94	2.54
54 55	53-97 54-97	1.88	53.96 54.96	2.12	53 95 54.95	2.40	53-94 54-94	2.59 2.64
:5	55.97	1.95	55.96	2.20	\$5.95	2.44	55.94	2.69
7	56.97	1.99	56.96	2.24	56.95	2.49	56.93	2.73
58	57 96 58.96	2.02	57.96 58.96	2.28	57 94 58.94	2.53 2.57	57.93 58.93	2.75 2.83
59 60	54.96	2.09	59.96	3.36	59 94	2.62	59.93	288
	Dep	Li	Dep	Lat.	Dep.	Lat.	Dep.	Lat
7		7 .	4	7	30),	1.5	7

87 DEGREES.

1 0	0	,	15	,	30	7	45	7
Dist.	Lat.	Dep.	Lat	Dep.	Lat.	Dep.	Lat.	Dep.
61	60.96	2.13	60.95	2.39	60.94	2.66	60 93	2.93
62	61.96	2 16	61.95	2.43	61.94	2.70	61.93	2.97
63 64	62.96 63.96	2,20 2,23	62.95 63.95	2.47 2.51	62.94 63.94	2.75	62.93 63.93	3.02
65	64.96	2.27	64.95	2.55	64.94	2.84	64.93	3 12
66	65.96	2.30		2.59	U5.94	2.88	65.92	3.17
67 68	66.96 67. 9 6	2.34	66.95 67.95	2.63 2.67	66 94 67.94	2.92	66.92 67.92	3.21 3.26
60	68.g6	2.37 2.41	68.95	2.71	68.93	3.01	68.92	3.31
70	69.96	2.44	69.95	2.75	69.93	3.05	69.92	3.36
71	70.96	2.48	70.95	2.79	70.93	3.10	70.92	3 41
72	71.96	2.51	71.94	2.83 2.87	71.93	3.14	71.92	3.45
73 74	72.96 73.95	2.55	73.94	2.91	72.93	3.23	72 92 73.91	3.50 3.55
75	74-95	2.62	74-94	2.94	74:93	3.27	7491	3.60
76	75.95	2.65	75.94	2.98	75.93	3.32	75.91	3.65
77	76.95	2.69	76.94	3.02	76.93	3.36	76.91	3.69
78	77.95 78.95	2.72 2.76	77.94 78.94	3.06 3.10	77.93 78.92	3.40	77.91 78.91	3·74 3·79
79 80	79.95	2-79	79.94	3.14	79.92	3.49	79.91	3.84
18	80.95	2.83	80.94	3.18	80.92	3.53	80.91	3.89
82	81.95	2.86	81.94	3.2%	81.92	3.58	81.91	3.93
83 84	82.95	2.90	82.94 83.94	3.26	82.92 83.92	3.62 3.66	82.90 83.90	3.98
85	83.95 84.95	2.93 2.97	84.93	3.30	84.92	3.71	84.90	4.08
86	85.95	3.00	85.93	3.38	85.92	3.75	85.90	4-13
87	86.95	3.04	86.93	3.42	86.92	3.79	86.90	4.17
88	87.95	3.07	87.93	3.45	87.92	3.84	87.90	4.22
89 90	88.95 89.95	3.14	88.93 89.93	3.49	88.92	3.88 3.93	88.90 89.90	4.27
91	90.94	3.18	90.93	3.57	90.91	3.97	90.90	4.37
92	91.94	3.21	91.93	3.61	91.91	4.01	91.89	441
93	92.94	3.25	92.93	3 65	92.91	4.06	92 89	4.46
94	93.94	3.28 3.32	93.93	3.69	93.91	4.10	93.89	4.51
95	94 94		94.93	3.77	95.91	4.19	95.89	4.61
90	95.94	3.35 3.39	95.93 96.93	3.77	96.91	4.23	96.89	4.65
98	97-94	3.42	97 92	3.85	97.91	4-27	97.89	4.70
99	98.94	3.46	98.92	3.89	98.91	4 32	98.89 99.88	4.75 4.80
100	99.94 100.g	3-49	99.92	3.93	100.9	4.41	100.9	4.85
101	101.9	3.53 3.5 6	101.9	4.00	101.9	445	101.9	4.89
103	1329	3.59	102.9	4.04	102.9	4.49	102.9	4-94
104	103.9	3.63	103.9	408	103.9	4-54	103.9	4.99
105	104 9	3.66	104.9	4 12	104.9	4.58	104.9	5.04
106	105 9	3.70	105.9	4.16	105.9	4.67	105.y 106.g	5.09
108	107.9	3.77	107.9	4.24	107.9	4.71	107.9	5.18
109	108.9	3.80	108.9	4,28	108.9	4.75	108.9	5.23
110	109.9	3.84	109.9	4.32	109.9	4.80	109.9	5.28
111	110.9	3.87	110.9	4.30 4.40	110.9	4.89	110.9	5·33 5·37
113	111.9	3.91 3.94	112.9	4.44	112.9	4.93	112.9	5.42
114	113.9	3.98	113.9	4.48	113.9	4.97	113.9	5-47
115	114.9	4.01	114.9	4.51	114.9	5.02	114.9	5.52
116	115.9	4.05	115.9	4-55	115.9	5.06	115.9	5.57 5.61
117	116.9	4.08	116.9	4.59 4.63	116.9	5.10	116.9	5.66
119	118.9	4.15	118.9	4.67	118.9	5.19	118.9	5.71
120	119.9	4.19	119.9	4.71	119.9	5.23	1199	5.76
اید	Dep	Lat.	Dep.	Lat.	D-b	Lat.	Dep.	Lit
Dist.	01		45	NPC D		U'	15/	!

1	- U	1 0'		. 15	,	30)'	45'	
1	Dist	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
Į	-	1.00	0.05	1.00	0.06	1.00	0-06	1.00	0.07
1	2	2.00	0.10	2.00 3.00	0.11	2.00	0-12	2.00 2.99	0.13
ł	3 4	3.00 3.99	0.16	4.00	0.23	3.99	0-24	3.99	0,25
1	5	4.99	0.26	4.99	0.28	4.99	0.31	4-99	0.3
ı	6	5.99	0.31	5.99	0.34	5.99	0.37	5.99	0.39
1	7	6.99	0.37	6.99	0.40	6.99	0.43	7.98	0.45
1	9	7.99 8.99	0.42	7.99 8.99	0.45	7.99 8.98	0.55	8.98	0.59
ł	10	9.99	0.52	9.98	0.57	9.98	0.61	9.98	0.65
١	11	10.98	0 58	10.98	0.68	10.98	0.67	10.98	0.72
I	12	11.98	0.63	11.98	0.68	11.98	0.73	11.97	0.78
ı	13	12 98 13.98	0.68	13.48	0:79	13.97	0.85	13.97	0.92
1	15	14 - 8	0.79	14.98	0.85	14.97	0.92	14.97	0.98
ı	16	15 98	0.84	15.97	0.91	15.97	0 98	15.97	1.05
ł	17	16.98	0.89	16.97	0.95	16.97	1.04	16.96 17.96	1.11 1.18
I	18 19	17 98	0.94	17.97 18.97	1.02	17.97	1.16	18.96	1.24
ı	20	19.97	1.05	19.97	1.13	19.96	1.22	19.96	1.31
I	21	20.97	1.10	20.97	1.19	20.96	1.28	20.96	1.67
ı	22	21 97	1.15	21.97	1.25	21.96	1.34	21.95	1.44
I	23	22 97 23.97	1.20	22.96 23.96	1.30	22.96 23.96	1.40	22.95	1.50 11.57
I	25	24.97	1.31	24.90	1.42	24 95	1.53	24.95	1.64
ł	26	25.96	1.36	25.96	1.47	25.95	1.59	25.94	1.70
ł	27	26.96	1.41	26.96	1.53	26.95	ь65	26.94	1.81
I	28	27.96 28.96	1.47	27.96 28.95	1.59,	27.95	1.71	27.94 28.94	1.00
I	30	29.96	1.57	29.95	1.70	29.94	1.83	29.94	1.96
I	31.	30.96	1.62	30.95	1.76	30.94	. 1.89	30.93	2.03
I	32	31.96	1.67	31.95	2.83	31.94	1.95.	31.93	2.09
I	33 34	32.95	1.73 1.78	32.95 33.95	1.87	32.94 33.94	2.01	32.93 33.93	2.16
ł	35	33.95 34.95	1.83	34-94	1.98	34-93	2.14	34.93	2.29
ł	36	35.95	. 1.88	35.94	2.04	35.93	2.20	35.92	2.35
1	37	36.95	1.94	36.54	2.10	36.93	2.26	36.92	2.42
ı	38	37.95 38.95	2.04	37-94	2.15	37·93 38·93	2.32	37.92 38.92	2.49
1	40	39.95	2.00	39.94	2.27	39.93	2.44.	39.91	2.62
1	41	40.94	2.15	40.93	2.32	40.92	2.50	40.91	2,68
1	42	41.94	2.20	41.93	2.38	41.92	2.56	41.91	2.75
j	43 44	42.94	2.25	42.93 43.93	2.44	42.92 43.92	2.63 2.69	42.9.I 43.9.I	2.88 2.88
1	45	43.94	2:36	44.93	2.55	44.92	2.75	44.90	2.94
1	46	45.94	2.41	45.93	2.61	45.91	2.81	45.90	3.01
1	47	46.94	2.46	46.92	2.66	46.91	2.87	46.90	3.07
1	48 49	47.93 48 93	2.51	47.92 48.92	2.72	47.91 48.91	2.93 2.99	47.90 48.90	3.14 3.20
1	50	49.93	2.62	49.92	2:83	49.91	3.05	49.89	3.27
1	51	50.93	2.67	50.92	2.80	50 90	3.11	50.89	3-34
1	52	51.93	2.72	51.92	2.95	51.90	3.17	51.89	3.40
1	53 54	52.93	2.77 2.83	52.91 53.91	3.00	52.90 53.90	3.24 3.30	52.89 53.88	3-47 3-53
1	55	53.93 54.92	2.88	54 9 1	3.12	54.90	3.36	54.88	3.60
1	56	55.92	2.93	55.91	3.17	55.90	3.42	55.88	3.66
1	57	56.92	2.98	56.9 t	3.23	56.89	3:48	56.88	3.73
1	58	57.92 58.92	3.04 3.09	57.91 58.91	3.29 3.34	·57 89 58.89	3.54 3.60	57.88 58.87	3.79 3.86
}	59 60	59.92	3.14	59.90	3.40	59.89	2.66	59.87	3.92
1		Dep.	Lat.	Dep.	Lat.	Dep	LRt.	Dep.	Lat.
1	Dist	0,		45	,,	30), —	1:	5'
	سندح		*****	-	TARCIE				_

¥.	J'		1	,/	. 3	0/	'45/	
] 4	Lat	Dep	Lut	Dep.	Luc.	Dep.	Lat.	Dep
61	60.92	3.19	60.90	3.46	60.89	3.72	60.87	3.99
62	61.92	3.24	61.90	3.52	61.88	3.79	61.87	4.06
63	62.91	3.30 3.35	62.90 63.90	3.57 3.63	62.88	3.85 3.91	62.87 63.86	4.12
65	64 91	3.40	64.90	3.69	64.88	3 97	64.86	4.25
66	65.91	3.45	65.89	3.74	65.88	4.03	65.86	4 3 2
67	66.91	3.51	66.89	3.80	66.88	4.09	66 86	4.38
68	67 91	3.56 3.61	67.89 68.89	3.86	67.87 68.87	4-15	67.85 68.85	4-45
69 70	68.91 69.90	3.66	69.89	3.91 3 97	6y.87	4.21	69.85	4.58
71	70 90	3 72	70.89	4.03	70.87	4.33	70 85	4.64
72	71.90	3.77	71.88	4.08	71 87	4.40	71.85	4.71
73	72.90	3.82	72.88	4.14	72.86	4.46	72.84	4 77
74	73.90	3.87	73.88	4.20	73.86 74.86	4.52	73.84	4.84
75	74-90	3.93	75.88	4-25	75.86	4.64	74.84	4-91
76 77	75.90 . 76.89 ·	4 03	76.88	4.31	76.86	4.70	76.84	4-97 5-04
78.	77.89	4.08	77.87	4.42	77.85	4.76	77.83	5.10
79	78.89	4.13	78 87	4.48	78.85	4.82	78.83	5-17
80	79.89	4.19	79.87	4.54	79.85	4.88	79.83	5.23
81	80 89	4.24	80.87	4-59	80.85	4.94	80.83	5 30
€2 83	81.89 82.89	4 29	81.87 82.87	4.65	82.85	5.01	81.82 82.82	5.36 5.43
84	83.88	4.40	83.86	4.76	83.84	5 13	83.82	5.49
85	84.88	4.45	84.86	4.82	84.84	5.19	84.82	5.56
86	8 5.88	4.50	85 86	4.88	85.84:	5.25	85.82	5.62
87	86.88	4-55 4-61	86.86 : 87.86 :	4.93	86.84 87 .8 4	5.31	86.81 87.81	5.69
88	87.88 88.88	4.66	88 86	4-99 5.05	88.83	5·37 5·43	18.88	5.76 5.82
90	39.88	4.71	89 86	5 10	89.63	5.49	18.68	5.89
91	90.88	4.76	90.85	5.16	90.83	5.56	18.00	5.95
92	91.87	4.81	91.85	5.22	91.83	5.62	91.80	6.02
93	92.87	4.87	92.85 93.85	5.27	92.83 93.82	5.68	92.8C	6.08
94 95	93.87 94.87	4-92	94.85	5·33 5·39	94.82	5.74 5.80	93.80 94.80	6.15
96	95.87	5.02	95.85	5.44	95.82	5.86	95.79	6.28
97	96.87	5 08	96.84	5.50	96.82	5.02	96.79	6.34
98	97:87	5.13 .	97.84	5.56	97.82	58	97.79	6.41
99	98.86	5.18:	98.84 99.84	5.61	98.82 99.81	6.10	98.79	6.47
100	100.9	5.23	100.8	5.67	100.8	6.17	100.8	6.54
101	101.9	5 29 5-34	121.8	5.73 5.78	101.8	6.23	101.8	6.67
103	103.9	5.39	102.8	5.84	102.8	6.29	102 8	6.74
104	103.9	5.44	103.8	5.90	103.8	6.35	103.8	6.80
105	104.9	5.50	104.8	5 95	104.8	6.41	104.8	6.87
106 :	1059	5.55	105.8	6.01 6.07	105.8	6.53	105.8	6.93 7.00
107	107.0	5.65	107.8	6.12	107.8	6.59	107.8	7.06
109	108.9	5.70	108.8	6.18	108.8	6.65	108.8	7-13
110	109.8	5 76	139.8	6 24	109.8	6.72	109.8	7.19
411	110.8	5.81	110.8	6.29	8.011		110.8	7.26
1 12	113.8	5.86	111.8	6.35 6.41	111.8	6.84 6.90	111.8	7·33 7 39
1114	113.8	5.91 5.97	113.8	6 46	113.8	6.96	113.8	7.46
115	14.8	6.02	114.8	6.52	114.8	7.02	114.8	7.52
116	115.8	6.07	115.8	6.58	115.8	7.08	115.8	7.59
117	116.8	6.12	116.8	6.63	116.8	7.14	116.7	765
811	117.8	6.18	117.8	6.69 6.75	117.8	7.20	117.7	7.72
120	119.8	6.28	119.8	6.80	119.8	7-39	119.7	7.85
-	Dep	La.	D. p	Lat.	Dep.	Lat	Dep.	Lt
Dist	0		45		30		15	
, <u> </u>				DEGR				-

151	1	-	15	4	30	I i	45	
1816	Lat	$\widetilde{\mathbf{De}}_{\mathbf{l}^n}$	Lat.	D∈p.	Lat.	Dep	Lat	Dep
1	1.00	0.07	1.00	0.07	1.00	0.08	1.00	0.08
2	2.00	0.14	1.99	0.15	1.99	0.16	1.99	0.17
3	2.99	0.28	2.99 3.99	0.22	3.99	0.24	3.99	0.25
5	3.99 4.99	0.35	4 99	0.37	4.98	0.39	4.9	0.41
6	5.99	0.42	5.98	0.44	5.98	0.47	5.98	0.50
7	6 98	0.49	6.98	0.52	6.98	0.55	6.98	0.58
8	7.98	0.56	7.98	0.59	7.98	0.63	7-97	0.66
9	8.98	0.63	8.98	0.67	8.97	0.71	8.97	0.75
10	9.98	0.70	9.97	0.74	9.97	0.78	9.97	-
11.	10.97	0.77	10.97	0.82	11.96	0.86	10.96	0.91
13	11 97	0.91	11.97	0.96	12.96	1.02	12.96	1.08
14	13.97	0 98	13.96	1,04	13.96	1.10	13.95	1 16
15	14.96	1.05	14 96	1.11	14.95	1.18	14-95	1.24
16	15 96	1,12	15.96	1.19	15.95	1.26	15.95	1.33
17	16 96	1.19	16 95	1.26	16.95	1.33	1694	1 41
18	17.96	1.26	17.95	1.33	17.94	1.41	17.94	1.49
19	18.95	1.33	18.95	1.48	18.94	1.49	19.93	1.66
21	19 95	1.46		1.56	20 94	1.65	20.01	1.74
22	20 95	1.53	20 94	1.63	21.93	1 73	21.92	1.8.2
23	22.94	1.60	22.94	1.70	22 93	1.80	22.92	1.90
24	23 94	1.67	23.93	1.78	23.93	1.88	23.92	1.99
25	24.94	1.74	24.93	1.85	24.92	1.96	24.91	2.07
26	25.94	1.81	25.93	1.93	25.92	2.04	25.91	2.15
27	26.93	1.88	26.93	2.00	26.92	2.12	26.91	2.24
20	27.93	1.95	27.92	2.15	28.91	2.28	28 90	2.40
30	29.93	2.09	29.92	2,22	29.91	2 35	29.90	2.48
31	30.92	2.16	30.91	2.30	30.90	2.43	30.89	2.57
32	31.92	2.23	31.91	2.37	31.90	2.51	31.89	265
33	32.92	2.30	32.91	2.45	32.90	2.59	32 89	2.73
34	33 92	2-37	33.91	2.52	33 90	2.67	33.88 34.88	2.00
35	34.91	2.44	34.90	2.59	34.89	2.75	35.88	2.98
36	35.91	2.51	35.90	2.67	35.89	2.90	36.87	3.06
38	37.91	26.	37.90	2.82	37.88	2.98	37.87	3.15
39	38.91	2.72	38.89	2.89	38.88	3.06	38.87	3 23
40	39.90	2.79	39.89	2.96	39.88	3.14	39.86	331
41	40.90	2.86	40.89	3.04	49 87	3.22	40.86	3.40
42	41.90	2.93	41.88	3.11	41.87	3.30	41.86	3.48
43	42.90	3.00	42.88	3.19	42.87	3.37	43.8	3.64
45	44.89	3.14	44.88	3.33	44.86	3.53	44.85	3 73
46	45.89	3.21	45.87	3.41	45.86	3.61	45.84	3.81
47	46.89	3 28	46.87	3.48	46.86	3.69	46.84	3 89
48	47.88	3.35	47.87	3 56	47.85	3.77	47.84	3.97
50	48.88	3.42	48-87	3.63	48.85	3.84	48.83	4.14
-	49.88	3 49	49.86	3.71	49.85	3.92		
51	50.88	3.56	50.86	3.78	50.84	4.00	51.82	4.22
53	51.87	3.70	52.85	3.85	52.84	4.16	52.82	4.39
54	53.97	3.77	53.85	4.00	53.83	4 24	53.81	4-47
55	54.87	3.84	54 85	4.58	54.83	4.32	54 8	4 55
56	55 86	3.91	55.85	4.15	55.83	4.39	55.81	4.64
57	56.86	3.98	56.84	4.22	56.82	4.47	56.80	4.72
58	57.86	4.05	57.84	4.30	57.82 58.82	4.55	57.80 58.80	4.80
59 60	58.86	4-12 4-19	58.84 59.84	4·37 4·45	59.82	4.63	59.79	4-97
		Lat.	1)ep.	Lat.	Dep	Lat.	Dep.	Lat.
Dist.	Dep.		45		307		15	
	04	,		05 1777			1.4	

85 DEGREES.

• H		0'		5′	, 3u		1 43'	
P.	Lut	Dep	Lat.	Dep.	Lat	Dep.	Lat.	Dep.
61	60.85	4 26	60.83	<u> </u>	60.81			
62	61.85	4-32	64 83	4.52	61.81	4.79 4.86	60.79	5.05
63	62.85	4-39	62 83	4.67	62.81	4.94	62.78	5.22
64	63.84	4.46	63.82	4 74	63.80	5.02	63.78	5.30
65	64 84	4-53	64.82	482	64.80	5.10	64.78	5.38
66	6; 84	4.60	65.82	4.89	65.80	5.13	65.77	5-47
67	66.84	4-67	66.82	4-97	66.79	5.26	66.77	5.55
68	67.83 68 83	4.74	67.81	5.04	67.79 68.79	5.34	67.77 68.76	5.63
70	69.83	4 88	69.81	5.11	69.78	5.41 5.49	69.76	5.80
71	75.83	495	70.80	5 26	70.78	5.57	70.76	5.88
72	71 82	5.02	71.80	5 34	71 78	5.65	71.75	5.96
73	72.82	5.09	72.80	5.41	72.78	5.73	72.75	6.05
74	73.82	g. 16	73.80	5.48	73 77	5.81	73.75	6.13
75	74.82	5.23	74.79	5.56	74.77	5.88	74.74	6.21
76	75.81	5.30	75.79	5.63	75.77	5.96	75.74	6.29
77 78	76 81 177.81	5 37	76.79	5.71	76.76	6.04	76.74	6.38 6.46
79	78.81	5.44 5.51	77.79 78.78	5.78 5.85	77.76 78 76	6.20	77.73 78.73	6 54
86	79 81	5.58	79.78	5.93	79.75	6 28	79.73	6.62
81	80.80	5.65	80.78	6.00	80.75	6.36	80.72	6.71
82	81.80	5.72	81.77	6.08	81.75	6.43	81.72	6.79
83	82.80	9.79	82.77	6.15	82.74	6.51	82.71	6.87
84	83.80	5.86	83.77	6.23	83.74	6.59	83.71	6.96
85	84.79	5 93	84.77	6 30	84.74	6.67	84.71	7.04
86	85.79	6.00	85.76	6.37	85.73	6.75	85.70	7.12
87	86.79	6.07	86.76	6.45	86.73	6 83	86.70 87.70	7.20
89	87 79 88.78	6.14	87.7 6 88.7 6	6.52	87 73 88.73	6.90 6.48	88.6g	7.29 7.37
90	89.78	6.28	89.75	6.67	89 72	7.06	89.69	7.45
91	90.78	6.35	90.75	6.74	90.72	7.14	90.69	7.54
93	91 78	6 42	91.75	6.82	91.72	7.22	91.68	7.62
93	92.77	6.49	92.74	6.89	92.71	7.30	92.68	7.70
94	93.77	6.56	93-74	6.97	93 71	7.38	93.68	7.78
95	94.77	663	94.74	7.04	94.71	7.45	94.67	7.87
96	95.77	6.70	95.74	7.11	95.70	7.53	95.67	7.95
97 98	96.76 97.76	6.77 6.84	96.73	7.19	96.70	7.61 7.69	96.67 97.66	8.03 8.12
99	98.76	6.91	97 73 98.73	7.2 6 7.34	97 70 98.69	7.77	98.66	8 20
100	99.76	6.98	99.73	7.41	99.69	7.85	99.66	8.28
101	100.8	7.05	100.7	7 49	100.7	7.92	100.6	8.36
102	101.8	7.12	101.7	7.56	101.7	8.00	101.6	8.45
103	102.7	7.18	102.7	7.63	102.7	8.08	102.6	8.53
104	103 7	7.25	103.7	7.71	103.7	8.16	103.6	8.6r
105	104.7	7.32	104.7	7.78	104.7	8.24	104.6	8.69
106	105.7	7 39	105.7	7.86	305.7 306.7	8.32	105.6	8.78 8.86
107	106.7	7 46 7 53	100 7	7.93 8.00	107.7	8.40 8.47	106.6	8.94
109	108.7	7 60	108.7	8.08	108.7	8.55	108.6	9.03
110	109.7	7.67	109.7	8.15	109 7	8.63	109.6	9.11
111	110.7	7.74	110.7	8.23	110.7	8.71	110.6	9.19
112	113.7	7.81	111.7	8.30	111.7	8 79	111.6	9.27
113	112.7	7 88	112.7	8.37	1127	8.87	112.6	9.36
114	113.7	7.95 8.02	113.7	8.45	113.6	9.02	1136	9.44
115	114.7		1147	8.52	114.6			9.52
116	115.7	8.09 8.16	115.7	8.60 8.67	115.6	9.10	115.6	9.61
118	117.7	8.23	117.7	8.74	117.6	9.26	117.6	9.77
119	318.7	8.30	118.7	8.82	118.6	9.34	118.6	9.85
120	119.7	8.37	119.7	8.89	119.6	9.42	119.6	9.94
یر	Dep	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
ig I	U	,	45	5'	3	ν,	1	5'
								<u>.</u>

83 DEGREES.

-						0/	1	_
Dist	,0		-	/ T.D.		0/	45	
	La.	Dep	Lat.	Dep.	Lat	Dep.	Lat	Dep.
1 2	1.00	0.09	1.00	0.09	1.00	0.10 0.1g	1.00	0.10
3	2.99	0.26	2.99	0.10	2.99	0.19	2.98	0.30
4	3.98	0.35	3.98	0.37	3.98	0.38	3.98	0.40
_5	4.98	0.44	4.98	0.46	4.98	0.48	4-97	0.50
6	5.98	0.53	5.97	0.55	5.97	0.58	5.97	0.60
7 8	7.97	0.61	6.97 7 . 97	0.64	7.96	0.67	6.96 7.96	0.70
į,	8.97	0.78	8.96	0.82	8.96	0 86	8.95	0.90
10	9.96	0.87	9 96	0 92	9.95	0.96	9.95	1.00
11	10.96	0.96	10.95	1.01	10.95	1.05	10 94	1. to
1 ::	11.95	1.05	11.95	1.10	11.94	LIS	11.94	1.30
13 14	12.95	1.22	12.95	1.28	13.94	1.25	12.93	1.40
15	14-94	1.31	14 94	1.37	14.93	1.44	14.92	1.50
16	15.94	1.39	15.93	1.46	15.93	1.53	15.92	1.60
17	16.94	1.48	16.93	1.56	16.92	1.63	16.91	1.70
18	17.93	1.57	17.92	1.65	17.92	1.82	17.91	1.8e 1.g0
19	18.93	1.74	19.92	1.83	18.91	1.92	18.90	2.00
21	20.92	1.83	20.91	1.92	20.90	201	20 80	2.10
22	21.92	1.92	21.91	2.01	21.90	2.11	21.89	2.20
23	22.91	2.00	12.90	2 10	22.89	2-20	22.88	2.30
24	23.91	2.09	23.90 24.90	2.20	23 89 24.88	2.30	23.88 24.87	2.40 2.50
25 26	25 90	2.27	25.89	2.38	25.88		25.87	2.60
27	26.90	2-35	26.89	2.47	26.88	2.49	26.86	2.71
28	27.89	2.44	27.88	2.56	27.87	2.68	27 66	2.81
29	28.89	2.53	28.88	2.65	28.87	2.78	28.85	2.91
30	19.89	2.61	29.87	2.75	29.86	2.88	29.85	3.01
31 32	30.88	2.70	30.87 31.87	2.84	30.86 31.85	2.97 3.07	30.84	3.11 3.21
33	32.87	2.88	32.86	3.02	32.85	3.16	32 83	3.31
34	33.87	2.96	33.86	3.11	33.84	3.26	33.83	3.41
35	34 87	3.05	34.85	3.20	34.84	3.35	34.82	3.51
36	35.86 36.86	3.14	35.85 36.84	3.29	35.83	3.45	35.82	3 6z
37 38	37.86	3.22 3.31	30.04	3.39 3.48	36.83 ° 37.83	3.55 3.64	36.81 37.81	3.71 3.81
39	38.85	3.40	38.84	3.57	38.82	3.74	38.80	3.91
40	39.85	3.49	39.83	3.66	39.82	3.83	39.80	401
41	40.84	3.57	40.83	3.75	40.81	3.93	40.79	4.11
42	41 84	3.66	41.82	3.84	41.81 42.80	4.03	41.79	4.21
43	42.84	3.75 3.83	43.82	3.93 4.03	43.80	4.12	42.78 43.78	4.41
45	44 83	3.92	44.81	4.12	44-79	4.31	44.77	4.51
46	45 83	4.01	45.81	4.21	45.79	441	45.77	4.61
47	46.82	4.10	46.80	4.30	46.78	4.50	46.76	4.71
48	47.82	4-18	47.80 48.79	4-39 4-48	47.78 48.77	4.60	47.76 48.75	481 491
49 50	49.81	4.27	49.79	4-58	49.77	4-70 4-79	49.75	2.01
51	50.81	444	50.79	4.67	50.77	4.89	50 74	5.11
52	51.80	4-53	51.78	4.76	51.76	4.98	51.74	5.21
53	52.80	4.62	52.78	4.85	52.76	5 08	52.73	5.31
54 55	53·79 54·79	4-71 4-79	53·77 54·77	4-94 5.03	53.75 54.75	5.18 5.27	53-73 54-72	5.4E 5.51
56	55.79	4.88	55.77	5.12	55.74	5:37	55.72	5.61
57	56.78	4-97	56.76	5.22	56.74	5.46	56.71	5.71
58	57.78	5.06	57.76	5.31	57-73	5.56	57.71	5.81
59 60	58.78	5.14	58.75	5.40	58.73	5.65	58.70	5.91
	59.77 Den	5.23 Lat.	59.75 Dep	5.49 Lat.	59.72 Dan	5.75 Lat	59.70	Lut.
Dist.	Dep 0				Dep.		Dep.	
0	0	<u> </u>	45/		30	'	15	

4	1 0		1 15	· · · · ·	30)/ I	45'		
Diat	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
61	60.77	5.32	60.74	5.58	60.72	5.85	60.69	6.11	
62	61.76	5.40	61.74	5.67	61-71	5 94	61.69	6.21	
63	62.76	5.49	62.74 63.73	5.76 5 86	62.71 63.71	6.04 6.13	62.68 63.68	6.31 6.41	
65	64.75	5.67	64.73	5.95	64.70	6.23	64.67	6 51	
66	65.75	5.75	65.72	6.04	65.70	6.33	65.67	6.61	
67	66.75	5.84	66.72	6.13	66.69	6.42	66.66	6.71	
68	68.74	5.93 6.01	67.71 68.71	6.22	67.69 68.68	6.52 6.61	67.66 68.65	6.81 6.91	
70	69.73	6 10	69.71	6.41	69.68	6.71	69.65	7.01	
71	70.73	6.19	70.70	0.50	70.67	6.81	70.64	7.11	
72	71.73	6.28	71.70	6.50	71.67	6.90	71.64	7.21	
73 74	72.72	6.36	72 69 73.69	6.68	72.66	7.00	72.63 73.63	7.31 7.41	
75	74.71	6.54	7469	6.86	74.65	7.19	74.62	7.5 I	
76	75.71	6.62	75.68	6 9	75 65	7.28	75.62	7.61	
77	76.71	671	76.68	7.05	76.65	7.38	76 61	7.71	
78 79	77.70	6.80 6.89	77.67 78.67	7.14	77.64	7.48 7.57	77.61 78.60	7.81 7.91	
80	79.70	6.97	79.66	7.23	79.63	7.67	79.60	8.02	
181	80.69	7.06	80 66	7-41	80.63	7.76	80.59	8.12	
82	81.69 82.68	7.15	81.66	7.50	81.62	7.86	81.59	8.22	
83 84	83.68	7.23 7.32	8:465 83.65	7.59	82 62 83.61	7.96 8.05	8 2.58 8 3.58	8.32 8.42	
85	84.68	7.41	84.64	7-78	84 61	8.15	84.57	8.52	
86	85.67	7.50	85.64	7.87	85.60	8.24	85.57	8.62	
87	86.67	7.58	86.64	7.96	86.60	8.34	86.56	8.72	
88	87.67 88.66	7.67 7.76	87.63 88.63	8.05	87 59 88.59	8.43 8.53	87.56 88.55	8.82 8.92	
90	89.66	7.84	89.62	8.14	89.59	8.63	89.55	9.02	
91	90.65	7.93	90.62	8.33	90.58	8.72	90.54	9.12	
92	91.65	8.02	91.61	8.42	91.58	8.82	91.54	9.22	
93	92.65 93.64	8.11 8.19	92 61	8.51	92.57	8.91 9.01 .	92-53	9.32	
94	94.64	8.28	93 61 94-60	8.60 8.60	93.57 94.56	9.11	93.53 94.52	9.42	
96	95.63	8.37	95.60	8.78	95.56	9.20	95.52	9.61	
97	96.63	8 45	96.59	8.88	96.55	9.30	96 51	9.72	
98	97.63 98.62	8.54 8.63	97.59	8.9	97.55	9.39	97.51	9.82	
100	99.62	8.72	98.58 99 .58	9.06	98.54 99-54	9.49 9.58	98.50	9.92	
101	100.6	8.80	100.6	9.24	100.5	9.68	100.5	10.12	
102	101.6	8.89	101.6	9.33	101 5	9.78	101.5	10.22	
103	102 6	8.98	102.6	9.42	102.5	9.87	102.5	10.32	
104	104.6	9.06 9.15	103.6 104.6	9.52	103.5	9·97 10.06	103.5	10.42	
106	105.6	9.24	105.6	9.70	105.5	10.16	105.5	10.62	
107	106.6	9.33	106.6	9.79	106.5	10.26	106.5	10.72	
108	107.6	9.41	107.5	9 88	107.5	10.35	107.5	10.83	
100	108.6	9.50 9.59	108.5	9-97	108 5	10.45	108.5	10.92 11.02	
111	110.6	9.67	110.5	10.16	110.5	10.64	110.4	11.12	
112	111.6	9.76	111.5	10.25	111.5	10.73	111.4	11.22	
113	112.6	9.85	112.5	10.34	112.5	10.83	112.4	11.32	
114	113.6	9.94	113.5	10.43	113.5	10.93	113.4	11.42	
116	115.6	10.11	115.5	10.61	115.5	11.12	115.4	11.62	
117	116.6	10.20	116.5	10.71	116.5	11.21	116.4	11.72	
118	117.6	10.28	117.5	10.80	117.5	11.31	117.4	11.82	
120	118.5	10.37	118.5	10.89 10.98	118.5	11.40	118.4	11.92	
-	Dep.	Lat	Dep.	Lut.	Dep.	Lat.	D. p.	Lat.	
Dist	0		4		30		15'		
			-20		317				

84 DECREES.

15	1 0	, ——	1] 30)′	45		
E E	Lat.	D-p	L.t.	Dep.	Lat.	Dep	Lat.	1 Dep
	0.99	0.10	0.99	0.11	0.99	0.11	0 99	0.12
3	1.99	0.21	2.98	0.22	1.99	0.23	1.99	0.35
4	3.98	0.42	3.98	0.44	2 98 3.97	0.45	3.97	0.47
_5	4-97	0.52	4.97	0.54	4.97	0.57	4.97	0.59
6	5.97	0.63	5 96	0.65	5 96	0.68	5.96	0 71
7 8	6.96 7.96	0.73	6.96 7.95	0.76	6.96 7.95	0.79	7.94	0.82
9	8.95	0.94	8.95	0 98	8 94	1.02	8.94	1.06
10	9.95	105	9.94	1.09	9.94	1.13	9.93	1 18
11	10.94	1.15	10.93	1.20	10.93	1.25	10.92	1.29
13	12.93	1 36	12.92	1.42	12.92	1.47	12.91	1.53
14	1392	1.46	13.92	1.52	13.91	1.58	13.90	1.65 1.76
16	14.92	1.67	14.91	1.74	15.90	1.81	15.89	1.88
17	16.91	1.78	16.90	1.85	16.89	1.92	16.88	2.00
18	17.90	1.88	17.89	1.96	17.88	2.04	17.88	2.12
19 20	18.90	2.09	19.88	2.18	18.88	2.15	18.87	2.35
21	20.89	2.20	20.88	2.29	20.86	2.38	20.85	2.47
22	21.88	2.30	21 87	2.40	21.86	2.49	21.85	2.59
23 24	22.87 23.87	2.51	22.86 23 86	2.50 2.61	23.85	2.72	22.84	2.70 2.82
25	24.86	2.61	24 85	2.72	24.84	2 83	24.83	2.94
26	25.86	2.72	25.85	2.83	25.83	2.94	25.82	3.06
27 28	26.85 27.85	2.82	26.84 27.83	3.05	26.83 27.82	3.06	26.81	3.17
29	28 84	3.03	28.83	3.16	28 81	3.28	28.80	3.41
30	29 84	3.14	29.82	3.27	29.81	3.40	19.79	3.53
31	30.83	3.24	30.82	3.37 3.48	30.80	3.51	30 79 31.78	3.64 3.76
32 33	32.82	3.45	32.80	3.59	31.79	3.74	32.77	3.88
34	3381	3.55 3.66	33.80	3.70 3 8 I	33.78	3 85	\$3.76	4.00
35 36	34.81	3.00	35.79	3.92	34 78	4 08	34-76	4.11
37	36.80	3.87	36.78	4.03	\$5.77 \$6.76	4.19	35.75 36.74	4-35
38	37.79	3 97	37.77	4.14	37.76	4 30	37.74	447
39 40	38.79	4.08	38.77 39:76	4.25 4.35	38.75, 39.74	4.41	38.73 39.72	4-58 4-70
41	40 78	4.29	40.76	4.46	40.74	4 64	40 72	482
42	41.77	4.39	41.75	4-57	41.73	4.75	41.71	4-94
43	42.76	4.49 4.60	42 74 43.74	4.68	42.72 43.72	4 87 4.98	42.70 43 70	5.Q5 \ 5.17
45	44.75	4.70	44 73	4.90	44 71	5.09	44.69	5.29
46	45.75	4.81	45.73	5.01	45.70	5.21	45 68	5.41
47 48	46.74	4 9 1 5.02	46.72 47.71	5.12 5.23	45.70 47 69	5.32	46.67 47.67	5.52 5 64
49	48.73	5.12	48.71	5.33	48.69	5.55	48.66	5.76
50	49.73	5.23	49.70	5.44	49 68	5.66	49.65	5.88
51 52	50.73	5.33 5.44	50.70	5.55 5.66	50.67	5.77 5.89	50 65	5.99
53	51.72 52.71	5.54	51 69 52 69	5.77	51.67 52.66	6.00	51.64 52.63	6.23
54	53.70	5.64	53.68	5.88	53.65	6.11	52.63	6.35
55	54.70	5.75	54.67	6.10	54.65	6.23	54.62	6.46
56 57	55.69 56.69	5.96	56.66	6.21	55 64 56.63	6.45	55.60	6.70
58	57.68	6.06	57.66	6.31	57.63	6.57	57.60	6.82
59 60	58.68 59.67	6.17	58.65 59.64	6.42 6.53	58.62 59.61	6.68 6.79	58.59 59.58	6.93 7.05
	1)ep.	Lat.	Dep.	Lat.	Dep.	Lat.	. Dep.	Lat.
Dist	U	1	4				15	

83 DEGREES,

ı	0	U	,	1 1	j /	3	0'	4	,	ı
-	Dist	Lat	D-p	Lac	De	Lat.	D. p.	Lat.	To	I
1	61	60.67	6.38	60.64	6.64	60.61	6.91	60.58	7.17	l
1	Ú2	61 66	6.48	61.63	6.75 6.86	61 60	7.02	61 57	7.29 7.40	ŀ
3	63 64	62.65	6.59	62.63 63.62	6.97	62.60	7.13	63.56	7.52	l
1	65	64.64	6.79	64.6	7 08	64.58	7 36	64.55	7.64	ļ
1	66	65 64	6 90	65.61	7.19	65.58	7.47	65.54	7.76	
1	61	66.63	7.00	66.60 67.60	7.29	66.57	7.58	66 54 67.53	7.88 7.99	
1	68 69	67.63 68.62	7.11	68.59	7.40 7.51	67.56 68.56	7.70 7.81	68.52	8.11	l
4	70	69.62	7.32	69.58	7.62	69 55	7.92	69.51	8.22	ı
1	71	70.61	7 42	70 58	7-73	70.54	8.04	70.51	8.35	ı
1	72	71.61	7.53	71.57	7 84	71.54	8.15	71.50	8.46 8.58	ĺ
1	73 -74	72 60 73.59	7.63 7.74	72.57 73.56	7.95 8.06	72.53	8.38	72.49	8.70	
1	75	74-59	7.84	74.55	8.17	74.52	8 49	74.48	8.8;	ı
1	76.	75.58	7.94	75.55	8.27	75.51	8 60	75.47	8.93	ı.
	77	76.58	8.05.	76.54	8.38	76.51	8.72 8.83	76.47	9.05 9.17	
;	78 79	77-57 78.57	8.15	77·54 78.53	8.49 8.60	77.50 78.49	8.94	77.46 78.45	9.17	ı
1	80	79.56	8.36	79 52	8.71	79 49	9.56	79.45	9 40	ļ.
1	81	80.56	8.47	80.52	8.82	80 48	9.17	80.44	9.52	ĺ
	82	81.55	8.57	81.51	93	81.47	9.28	81.43	9.64	l.
1	83 84	82.55 83.54	8.68 8.78	82.51 83.50	9.04	82.47 83.46	9.40 9.51	82.42 83.42	9.76 9.87	
1	85	84.53	8.88	84.49	9 25	84.45	9 62	84.41	9.99	ļ
1	86	85.53	8.99	85.49	9.36	85.45	9.74	85.40	10 [1	ľ
1	87	86.52	9.09	86 48	9.47	86.44	9.85	86.40	10.23	ŀ
1	88 8g	87.52 88.51	9.20	87.48 88.47	9.58 9.69	87 43 88.43	9.96	87.39 88.38	10.34	ı
1	93	89.51	9.41	89.47	9.80	89.42	10.19	89 38	10.58	l
1	91	90.50	9.51	90.46	9.91	90.42	10.30	90 37	10.70	ĺ
1	92	91.50	9.62	91.45	10.02	91.41	10.41	91.36	10.81	l
1	93	92.49	9.72	92.45 93.44	10.12	92.40	10.53	92.36	11.05	ŀ
1	94 95	94.48	9.93	94.44	10 34	94-39	10.75	94.34	11 17	l
	96	95.47	10.03	95.43	10 45	95.38	10.87	95.33	11.28	l
1	97	96.47	10.14	96.42	10.56	96 38	10.98	96.33	11.40	l
1	98	97.46 98.46	10 24	97.42	10.67	97.37 98.36	11.09	97.32 98.31	11.52	l
1	99	99.45	10.45	99.41	10.89	99.36	11.32	99.31	11.75	ı
-	101	100.4	10.56	100.4	11 00	100.3	11 43	10C.3	11.87	l
1	102	101.4	10.66	101.4	11.10	101 3	11.55	101.3	1199	l
1	103	102.4	10.77	102 4	11.21	102.3	11.66	102.3	12.22	ł
1	105	1044	10.98	104.4	11.43	104.3	11.89	104.3	12.34	
	106	105.4	11.08	105 4	11.54	105.3	12 00	105.3	12.46	
1	107	106 4	11.18	106.4	1165	106.3	12.11	106 3	12 58 12.69	ı
1	109	107.4	11.29	107.4	11.76	107 3	12.23	107.3	12.81	l
1	110	109.4	11 20	109.3	11.98	109 3	12.45	109 2	12.93	ŀ
į	111	1104	11.60	110.3	12.08	110.3	12 57	110 2	13.05	ŀ
1	112	111.4	11.71	111.3	12,19	111.3	12.68	111.2	13.16	ĺ
1	113	112.4	11.81	112.3	12.30	112.3	12.79	112.2	13.28	ı
-	114		12.02	114.3	12,52	1143	13.02	114.2	13.52	l
j	116	115.4	12.13	115.3	1263	115.3	13.13	115.2	13.63	ĺ
]	117	116.4	12.23	116.3	12.74	116.3	13.24	116.2	13.75	
1	811		12.33	117.3	12.85	117.2	13.36	117.2	13.87	
]	119	118.3	12.44	119.3	13 06	1	13.58		14.10	
1	-	1) p	Lat	Dep	Lu	D.p.	Lat.		Lista	
1	Dist	- 6		4			<u></u>	15/		2
	=_			0.1	DECO				-	

TE	0	1	1 1	1	1 30	/	45	,
) st	Lat	Dep	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
_	0.99	0.12	0.99	C.13	0.99	0.13	0.99	0.13
2	1.99	0.24	1.98	0.25	1.98	0.26	1.98	0.27
3 4	2.98 3.97	0.37	2.98	9.38	2.97 3.97	0.39	2 97 3 96	0.40
1 5	4.96	0.61	4.96	0.63	4.96	0.65	4.95	0.67
6	5.96	073	5 95	0.76	5.95	0.78	5.95	0.81
7 8	6.95	0.85	6.94	0.88	6.94	0.91	6.94	0.94
1 5	7 94 8.93	0 98	7.94 8.93	1.01	7·93 8·92	1.04	7.93 8.92	1.08
10		1.22	9.92	1.26	9.91	1.31	9.91	1.35
11	10 92	1.34	10.91	1.39	10.91	1.44	10.90	1.48
12	11.91	1.46	11 90	1.51	11.90	1.57	11.89	1.62
13	12.90	1.58	12.90	1.64	12.89	1.70	13.87	1.75
15	14.89	1 83	14.88	1.89	14.87	1.96	14.86	2.02
16	15 88	1.95	15.87	2.02	15.86	2.09	15.85	2.16
17	16.87	2 07	16.86	2.15	16.85	2.22	16.84	2.29
18	17.87	2.19	17.86	2.27	17.85	2.35	17.84 18.83	2.43
20	19.85	2.44	19.84	2.52	19.83	2.61	19.82	2.70
21	20.84	2.56	20.83	2.65	20.82	2.74	20.81	2.83
22	21.84	2 68	21.82	2.78	21.81	287	21.80	2.97
23	22.83	2.86	22.82	3.03	22.80	3.00	22.79	3.10
25	24 81	3.05	24.80	3.16	24.79	3.26	24 77	3.37
26	25.81	3.17	25.79	3.28	25.78	3.39	25.76	3.51
27	26.80	3.29	26.78	3:41	26.77	3.52	26 75	3.64
28	27.79 28.78	3.41	27.78	3.53 3.66	27.76 28 75	3.65 3.79	27.74 28.74	3.78 3.91
30	29.78	3 66	29.76	3.79	29.74	3.92	29.73	4.05
31	30.77	3.78	30.75	3.91	30 73	4.05	30.72	4.18
32	31.76	3.90	31.74	4.04	31.73	4.18	31.71	4.32
33	32.75	4.02	32.74	4.16	32.72 33.71	4.31 4.44	32.70 33.69	4.45
35	34.74	4.27	34.72	4.42	34.70	4-57	34.68	4.72
36	35.73	4-39	35.71	4 54	35.69	4.70	35.67	4.85
37	36.72	4.51	36 70 37.70	4.67 4.80	36.68	4.83	36.66	4-99
38 39	38.71	4.75	38.69	4 92	37.67 38.67	4.95 5.09	37.65 38.64	5.12
40	39.70	4.87	39.68	5.05	39.66	5.22	39.63	5.39
41	40.69	500	40.67	5.17	40.65	5.35	40.63	5.53
42	41.69	5.12	41.66 42.66	5.30	41.64	5.48	41.62	5.66
43 44	43 67	5.24	43.65	5·43 5·55	42 63 43.62	5.61 5.74	42.61 43.60	5.80 5.93
45	44 66	5.48	44.64	5.68	44.62	5.87	44-59	6.07
46	45.66	5 61	45.63	5.81	45.61	6 20	45.58	6.20
47	46.65	5.73	46 62	5.93 6.06	46.60	6.13	46.97	6.34
48 49	48.63	5.8 5 5.97	47.62 48.61	6 18	47.59 48.58	6.27 6.40	47.56 48.55	6.47 6.61
50	49.63	6.09	49.60	6.31	49.57	6.53	49.54	6 74
51	50.62	6.22	50.59	6.44	50.56	6.66	50.53	6.88
52	51.61 52.60	6.34 6.46	51.58	6.56 6.69	51.56	6.79	51.53	7.01
53 54	53.60	6.58	52.58 53-57	18.6	52.55 53.54	6.92 7.05	52.52 53.51	7.15 7.28
55	54.59	6.70	54.56	6.94	54-53	7.18	54.50	7.42
56	55.58	6.82	55.55	7.07	59.52	7.31	55.49	7.55
57	56.58	6.95	56.54	7.19	56.51	7.44	56.48	7.69
58 59	57.57 58.56	7.07	57·54 58.53	7·32 7·45	57.50	7.57	57·47 58.46	7.82 7.96
60	59.55	7.31	59.52	7.57	59.49	7.83	59.45	8.09
Dist	Dep.	Lat.	Dep .	Lat.	Dep.	Lat	Dep.	Lat.
اقا	G'		45"		30			<u>5</u>

82 DEGREES.

10	0	1	1:	5/	· 3	0'	45	,
ist	Lat.	Dep.	Lat.	Dep.	Lat.	D p.	Lat	D.p.
61	60 55	7.43	60.51	7.70	60.48	7.96	60.44	8.23
62	61.54	7.56	61.50	7.82	61.47	8.09	61.43	8.36
63	62.53	7.68	62.50	7.95 8.08	62.46	8.22 8.35	62.42	8.50
64	64.52	7.92	63.49° 64.48	8.20	63.45 64 44	8.48	64.41	8.77
66	65.51	8.04	65.47	8.33	65.44	8.61	65.40	8.90
67	66.50	8.17	66.46	8.46	66.43	8.75	66.39	9.04
68	67.49	8.29	67.46	8.58	67.42	8.88	67.38	9.17
69 70	68.49	8.41 8.53	68.45 69.44	8.71 8.83	68.41 69.40	9.01	68.37 69.36	9.30 9.44
71	70.47	8.65	70.43	8.96	70.39	9.27	70.35	9.57
73	71.46	8.77	7642	9.09	71.38	9.40	71.34	9.71
73	72.46	8.90	72.42	9.21	72.38	9.53	72-33	9.84
74	73.45	9.02	73.41	9.34	73.37	9.66	73.32	9.98
75	74-44	9.14	74.40	9.46	74.36	9.79		:
76	75.43	9.26	75.39 76.38	9.59	75.35	9.92	75.31 76.30	10.25
78	77 42	9.51	77.38	9.84	77.33	10.18	77.29	10.52
79	78.41	9.63	78.37	9.97	78.32	10.31	78.28	10.65
80	79.40	9.75	79.36	10.10	79-32	10 44	79.27	10.79
81	80.40	9.87	80.35	10.22	80.31 81.30	10.57	80.26 81.25	10.92 11.06
82	81.39	10.12	81.34 82.34	10.35	82 29	10.70	82.24	11.19
84	83.37	10.24	83.33	10.60	83.28	10.96	83.23	11.33
85	84.37	10.36	84.32	10.73	84.27	11.09	84.22	11 46
86	85.36	10.48	85.31	10.85	85.26	11.23	85.21	1160
87	86 35	10.60	86.30	10.98	86.26 87.25	11.49	86.21	11.73
88 89	87.34 88.34	10.72	87.30 88.29	11.11	88.24	11.62	88.19	12.00
90	89.33	10.97	89.28	11.36	89.23	11.75	89.18	12.14
91	90.32	11.09	90.27	11.48	90.22	11.88	90.17	12.27
92	91.31	11.21	91.26	11.61	91.21	12.01	91.16	12.41
93	92.31	11.33	93.26	11.74	92.20	12.14	92.15	12.54
94 95	93.30	11.58	94.24	11.99	94 19	12.40	94-13	12.81
96	95.28	11.70	95.23	12.12	95.18	12.53	95.12	1295
97	96.28	11.82	96,22	12.34	96.17	12.66	96.11	13.08
98	97.27	11 94	97.22	12.37	97.16	12.79	97.10	13.22 13.35
99	98.26	11.07	98.21	12.49	98.15	12.98	99.10	13.49
101	100.2	13.31	100.2	12.75	100.1	13.18	100.1	13.62
102	101.2	12.43	101.2	12.87	101.1	13.34	101.1	13.75
103	102.2	11.55	102.2	13.00	102.1	13.44	102.1	13.89
104	103.2	11.80	103.2	13.12 13.25	103.1	13.57	103.1	14.02
105	104.2	13.92	105.2	13.38	105.1	13.84	105.0	14.29
106	105.2	13.04	105.2	13.50	106.1	13.97	106.0	14.43
108	107.2	13.16	107.1	13.63	107.1	14 10	107.0	14.56
109	108.2	13.28	1.801	13.76	1.801	14.23	0.801	14.79
110	109.2	13-41	109.1	13.88	109.1	14.36		14.83
111	110.2	13.65	1.011	14.01	110.1	14.49 14.62	110.0	14 97
113	112.2	13.77	112.1	14.26	112.0	14.75	112.0	15.34
114	113.2	13.89	113.1	14.39	113.0	14.88	113.0	15.37
115	114.1	14.02	114.1	14.51	114.0	15.01	113.9	1551
911	115.1	14.14	115.1	14.64	115.0	15.14	114.9	15.04
117	116.1	14.26 14.38	116.1	14.89	117.0	15.40	116.9	15.91
119	118.1	14.50	118.0	15.02	118.0	15.53	117.9	16.05
120	119.1	14.62	119.0	15.14	119.0	15.66	118.9	16.18
Dist.	Dep.	Lat.	Dep.	Lat	Dep.	Lat	Dep.	Late
12	0	,	45	/	30	,	1.	,,

	0		15		30	11	4.5	,
Dist.	Lat	Dep.		Dep.	Lat.	Dep.	Lat.	Dep.
1	0.99	0.14	0.99	0.14	0.99	0.15	0.99	0.15
2	1.98	0-28	1.98	0.29	1.98	0 30	1.98	0 30
3	2.97	0.42	2.97	0.43	2.97 3.96	0.44	2.97 3.95	0.46
5	3.96 4.95.	0.56	3.96 4.95	0.72	4.95	0.74	4.94	0.76
6	5.94	0.84	5.94	0.86	5.93	0.89	5.93	0.91
7	6.93	0.97	6.93	1.00	6.92	1.03	6 92	1.06
8	7.92	1.11	7.92	1.15	7.91 8.90	1.18	7.91 8.90	1.22
10	8.91 9.90	1.25	8.91 9.90	1.43	9.89	1.48	9.88	1.52
1	10.89	1.53	10.89	1.58	10.88	1.65	10.87	1.67
12	11.88	1.67	11.88	1.72	11.87	1.77	11 86	1.83
13	12 87	1.81	12.87	2.01	12.86	1.92	. 12.85 13.84	1.98
14 15	13.86	2.09	13.86 14.84	2.15	14.84	2.22	14.83	2.28
16	15 84	2,23	15.83	2.30	15.82	2 37	15.81	2-43.
17	16,83	2-37	16.82	2.44	16.81	2.51	16.80	2.59
18	1782	2-51	17.81	2.58	17.80	2.66	17.79	2.74
19	18.82 19.81	2.64 2.78	18 80	2.73	18.79 19.78	2.96	19.77	3.04
23	20.80	2.92	20.78	3.01	20.77	3.10	20.76	3.19
22	21.79	3.06	21.77	3.16	21 76	3.25	21.74	3.35
23	22 78	3.20	22.76	3.30	22.75	3 40	22.73	3.50
24	- 23.77	3.34	23.75	3-44 3-59	23.74 24 73	3.55 3.70	23.72 24.71	3.65 3 80
25	24.76	3.48	24.74	3.73	25.71	3.84	25.70	3.96
26 27	25.75 26.74	3.62 3.76	26.72	3.87	26.70	3.99	26.69	4.11
28	27.73	3.90	27.71	4.02	27.69	4.14	27.67	4.26
29	28.72	4.04	28.70	4 16	28.68 29.6;	4.29	28.66 29.65	4.41
30	29.71	4.18	30.68	4.30	30.66	4.58	30.64	4.72
31 . 32	30.70 31.69	4-31 4-45	31.67	4 45	31.65	4.73	31.63	487
33	32.68	4 59	32.66	4-74	32.64	4.88	32.62	5.02
34	33.67	4.73	33.65	4.88	33.63	5.03 5.17	33.60	5.17
35	34 66	4.87	34.64	5.02	34.62	5.32	34.59	5.32
36 37	35.65 36.64	5.01	35.63 36.62	5.17 5.31	35.60 36.59	5.47	36.57	5.63
38	37.63	5.29	37.61	5.45	37.58	5.62	37.56	5.78
39	38.62	5.43	38.60	5.60	38.57	5.76 5.91	38.55	5.93 6.08
40	39.61	5 57	39.59	5.88	39.56	6.06	39·53 40·52	6.24
41 42	40.60	5.71 5.85	40.58	6.03	40.55	6.21	41 51	6.39
43	42.58	5.98	42-56	6.17	42.53	6.36	42.50	6.54
44	43.57	6.12	43-54	6.31	43,52	6.65	43.49	6.69
45	44.56	6 26	44.53	6.46	44.51		44 48	
46 47	45.55	6.40	45.52 46.51	6.00	45.49 46.48	6.80	45.46 46.45	7.00
48	47.53	6 68	47.50	6.89	47.47	7.09	47.44	7.30
49	48.52	6 82	48.49	7.03	48.46	7.24	48.43	7.45
50	49.51	6.96	49.48	7.17	49.45	7.39	49.42	7.61
52.	50.50	7.10	50.47 51.46	7.32 7.46	50.44	7.54	50 41	7.76 7.91
53	51.49 52.48	7.38	52.45	761	52.42	7.83	52.38	8.06
54	53.47	7.52	53 44	7.75	53.41	7.98	53-37	8.21
55	54.46	7.65	54 43	7.89	54.40	8.13	54-36	8.37
56.	55.46	7.79	55.42 56.41	8.18	55.38	8.28	55.35 56.34	8.52 8.67
57 158	56.45 57 44	7.93 8.07	57.40	8.32	56.37 57.36	8.57	57-33	8.82
59	58.43	8.21	58.39	8.47	58.35	8.72	58.31	8,98
60.	59.42	8.35	59.38	8.61	59.34	8.87	59.30	9.13
Dist.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
I Z	l. 0'	·	4.5	51	30)'	15	·'

i U	1 (0'		15'		30'		1 451	
Die	Lat	Dep	Lat.	, Dep	Lut.	Dep.	Lat.	Dep.	
61	60.41	8.49	60.37	8.75	60.33	9 02	60.29	9.28	
62	61.40	8.63	61.36	8.90	61.32	9.16	61.28	9.43	
63 64	63.38	8.77	62.35	9.04	62.31	9.46	62.27 63.26	9.58	
65	64.37	9.05	64.33	9.33	64.29	961	64.24	9.89	
66	65.36	9.19	65.32	9 47	65.28	9.76	65.23	10.04	
67	66.35	9.32	66.31	9.61	66.26	9.90	66.22	10.19	
68 69	67.34	9.46	67.30	9.76	67 25 68.24	10.05	68.20	10.34	
70	69.32	9.74	69.28	10.04	69.23	10.35	69.19	10 65	
71	70.31	9.88	70.27	10.19	70.22	10.49	70.17	10.80	
72	71.30	10.02	71.25	10.33	71.21	10.64	71.16	10.95	
73	72.29	10.16	72.24	10.48	72.20	10.79	72.15	11.11	
74 75	73.28	10.30	73.23	10.76	73.19	11.09	73.14	11.41	
76	75.26	10.58	75.21	10.91	75:17	11.23	75.12	11.56	
77	76.25	10 72	76.20	11.05	76.15	11.38	76.10	11 71	
78	77.24	10.86	77.19	11.19	77.14	11.53	77.09	11.87	
79 80	78.23	10.99	78.18	11.34	78.13	11.68	78.08	12.02	
81	80.21	11.27	80.16	11.62	80 11	11.97	80 06	12.32	
82	81.20	11.41	81.15	11.77	81.10	12.12	81.05	12.47	
83	82.19	11.55	82.14	11.91	82.09	12.27	82 03	12.63	
84	83.18	11.69	83.13	112.05	83 08	12.42	83.02	12.78	
85	84.17	11.83	84.12	12.20	84 07	12.56	84.01	12.93	
86	85.16	11.97	85.11	12.34	85.06	12.71	85.00	13.08	
88	87.14	12.25	87.09	12.63	87.03	1301	86.98	13.39	
89	88.13	12 39	88.08	12.77	88.02	13.16	87.96	13.54	
90	89.12	12.53	89.07	1291	89.01	13.30	88 95	13.69	
91	90.11	12.66	90.06	13.06	90.00	13.45	89 94	13.84	
92	91.10	12.80	91.05	13.20	90.99	13.60	90.93	14.15	
94	93.09	13.08	93.03	13.49	92.97	13.89	92.91	14.30	
95	94.08	13.22	94.02	13.63	93 96	14.04	93.89	14.45	
96	95.07	13.36	95.01	13.78	94.95	14.19	94 88	14.60	
97 98	96.06	13.50	96.00	13.92	95.93	14 34	95.87	14.76	
99	98.04	13.78	97.98	14.21	97.91	14.49	97.85	15.06	
100	99.03	13.92	98.97	14.35	98.90	14.78	98.84	15.28	
101	100.0	14.06	99.95	14.49	99 89	14-93	99.82	15.36	
102	101.0	14.20	100.9	14.64	100.9	15.08	100.8	15.52	
103	103.0	14.33	101.9	14.78	101.9	15.22	101.8	15.67	
105	104.0	14.61	103.9	15.07	103.8	15.52	103.8	15.97	
106	105.0	14.75	104.9	15.21	104.8	15.67	104.8	16.13	
107	106.0	14.89	105.9	15.35	105.8	15.82	105.8	16.28	
108	106.9	1 5.03	106.9	15.50	106.8	15.96	106.7	16.43 16.58	
1109	107.9	15.17	107.9	15.78	107.8	16.11 16.26	107.7	16.73	
1111	109.9	15.45	109.9	15.93	109.8	16.41	109.7	16.89	
712	110.9	15.59	110.8	16.07	8.011	16.55	110.7	17.04	
113	111.9	15.73	111.8	16.21	8.116	16.70	111.7	17.19	
114	112.9	15.87	112.8	16.36 16.50	112.7	16.85	112.7	17.341	
116	114.9	16.14	114.8	16.65	114.7		1147	17-49	
117	115.9 -	16.14	115.8	16.79	115.7	17.15	114.6	17.80	
118	116.9	16.42	116.8	16.93	116.7	17.44	116.6	17.95	
1119	117.8	16.56	117.8	17.08	1	17.59	117.6	18.10	
120	118.8 Then	16.70		17.22 Lat.		17,74	1,18.6	18.25	
<u>i</u>	Dep.	Lat	De p.		Dep	Lat.	Dep.	Lat.	
. <u>ā</u> .	<u>0</u>	·	45		30		15		
			51	DEGRE	TID.			8	

 	0/		15	,	30	,	45	, ,
Dist	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lut.	Dep.
-	0.99	0.16	0.99	0.16	ŏ.99	0.17	0.99	0.17
2	1.98	0.31	1.97	0.32	1.97	0.33	1.97	0.34
3	2.96 3.95	0.47	2.96 3.95	0.48	2. y6 3.95	0.50	2.96 3.94	0.51
4 5	4.94	0.78	4 94	0.80	• 4 93	∵83	4.93	0.85
6	5.93	0.94	5.92	0.96	5.92	0.99	5.91	1.02
7	6.91	1.10	6.91	1.13	6.90	1.16	6.90 7.88	1.19
8	7.90 8.8 ₉	1.25	7.90 8.88	1.29 1.45	7.89 8.88	1.32	8.87	1.35 1.52
10	9.88	1.56	9.87	1.61	9.86	1.65	9.86	1-69
11	10.86	1.72	10.86	1.77	10.85	1.82	10.84	1.86
12	11.85	1.88	11.84	1.93	11.84	1.98	11.83	2.03
13 14	12.84	2.03	12.83	2.09	12.82	2.15	13.80	2.20 2.37
15	14.82	2.35	14.80	2.41	14-79	2.48	14.78	2.54
16	15 80	2.50	15.79.	2.57	15.78	2.64	15.77	2.71
17	16 79	2.66	16.78	2.73	16.77	2.81	16.75	2.88
18	17.78	2.82	17.77	2.89 3.05	17.75	2.97 3.14	17.74	3.05 3.22
19	19.75	2.97 3.13	19.74	3.21	19.73	3.30	19.71	3.39
21	20.74	3.29	20.73	3.38	20.71	3.47	20.70	3.56
22	21 73	3.44	21.71	3.54	21.70	3.63	21.68	3.73
23	32.72	3.60	22.70	3.70	22.68	3.80	22.67 23.65	3.90 4.06
24	23.70 24.69	3.75 3.91	23.69	4.02	24.66	4.13	24.64	4.23
26	25.68	4.07	25.66	4.18	25.64	4.29	25.62	4.40
27	26.67	4.22	26.65	4-34	26.63	4.46	26.61	4-57
28	27.66	4.38	27.64	4.50	27.62	4.62	27.60 28.58	4.74
29 30	28,64 29.63	4.54 4.69	28.62	4.82	29.59	4.79 4.95	29.57	4.91 5.08
31	30.62	4.85	30 60	4.98	30.57	5.12	30.55	5.25
32	31.61	5.01	31.58	5.14	31.56	5.28	31.54	5.42
33	32-59	5.16	32.57	5.30	32.55	5.45	32.52	5.59
34 35	33.58 34-57	5.32 5.48	33.56 34.54	5.47 5.63	33 53 34-52	5.61	33.51 34.49	5.76 5.93
36	35.56	5.63	35.53	5.79	35.51	5.94	35.48	6.10
37	36.54	5.79	36.52	5.95	36.49	6.11	36.47	6.27
38	37.53	5.94	37.51	6.11	37.48	6.27	37-45 38.44	6.44 6.60
39 40	38.52 39.51	6.10	38.4 9 39.48	6.43	38-47 39-45	6.44	39.42	6.77
41	40.50	6.41	40.47	6.59	40 44	6.77	40,41	6.94
42	41.48	6.57	41.45	6.75	41.42	6.93	41.39	7.11
43	42.47	6.73	42.44	6.91	42.41	7.10	42.38	7.28
44	43.46	6.88 7.04	43.43	7.07	43.40	7.26	43.36 44.35	7·45 7.62
46	44-45	7.20	45.40	7.39	45.37	7.59	45.34	7.79
47	46.42	7.35	46.39	7.55	46.36	7.76	46.32	7.96 8.13
48	47.41	7.51	47.38	7.72	47.34	7.92	47.31	
49 50	48.40	7.66 7.82	48-36 49-35	7.88	48.33 49.31	8.09 8.25	48.29 49.28	8.30 8.47
51	50.37	7.98	50.34	8.20	50.30	8.42	50.26	8.64
52	51.36	8.13	51.32	8.36	51.29	8.58	51.25	8.81
53	52.35	8.29	52.31	8.52	52.27	8.75	52.23	8.98
54 55	53.34	8.45 8.60	53.30 54.28	8.68 8.84	53.26 54.25	9.08	53.22 54.21	9-14 9-31
56	54.32	8.76	55.27	9.00	55.23	9.24	55.19	9.48
57	55.31 56.30	8.92	56.26	9.16	56.22	9.41	56.18	9.65
58	57.29	9.07	57.25	9.32	57.20	9-57	57.16	9.82
59 60	58.27	9.23	58.23	9.48 9.64	58 19 59-18	9.74	58.15	9.99
	59.26	9.39 Lat.	59.22 Dep.	Lat	Dep	9.90 Lat	Dep	Lat.
Dist	Dep.		10ep. 45		30'		15	
<u> </u>	0	,	4)3		30		13	

ſ	ם	0/		15		30'		45'	
1	Dist.	Lat	Dep.	Lat.	Dep	Lat	Dep.	Lat	Dep
ſ	61	60.25	9.54	60 21	9.81	60.16	10.07	60.12	10.33
1	62	61.24	9.70	61.19	9.97	61.15 62.14	10.23	61.10	10.67
1	64	63.21	10.01	63.17	10 29	63.12	10.56	63.08	10.84
1	65	64-10	10.17	64.15	10 45	64.11	10.73	64.06	11.01
1	66 67	65 19	10.32	66.13	10.61	65.09 66.08	10.89	65.05	11.18
1	68	67.16	10.64	67.12	10.93	67.07	11.22	66.03	11.35
ł	69	68.15	10.79	68.10	11.09	68 05	11.39	68.00	11.69
ŀ	70 71	70.13	10.95	70.08	11.41	69 04	11.55	68.99	11.85
1	72	71.11	11.26	71.06	11.57	70.03 71.01	11.72	69.97 70.96	12.02
ł	73	72.10	11.42	7205	11.73	72.00	12.05	71.95	r2.36
ł	74 75	73.09 74.08	11.58	73.04 74.02	11.90	72.99 73.97	12.21	72-93 73 92	12.53
1	76	75.06	11.89	75.0I	12.22	74.96	12.54	74.90	12.87
ı	77	76.05	12.05	76.00	12.38	75-94	12.71	75.89	13.04
ł	78 79	77.04 78.03	12.20	76.99 77.97	12.54	76.93	12.87	76.87 77.86	13.21
1	80	79.02	12.51	78.96	12.86	77.92 78.90	13.20	78.84	13.55
ľ	18	80.00	12.67	79 95	13.02	79.89	13.37	79.83	13.72
1	82 83	80.99 80.99	12.83	80.93 81.92	13.18	80.88 81.86	13.53	80.82 81.80	13.89
1	84	82.97	13.14	82.91	13.34	82.85	13.70	82.79	14.06
ŀ	85	83.95	13.30	83.89	13.66	83.83	14.03	83.77	14.39
ı	86 87	84.94	13.45	84.88	13.82	84.82	14.19	84.76	14.56
ı	88	85.93 86 [.] 92	13.61 13.77	85.87 86.86	13.98	85.81	14 36	85.74 86.73	14.73
I	89	87 90	13.92	87.84	14.31	87.78	14.69	87.71	15.07
ŀ	90	88.89	14.08	88.83	14 47	88.77	14.85	88.70	15.24
ı	91 92	89.88 90.87	14.24 14.39	89.82 90.80	14.63 14.79	89.75 90.74	15.02	89.69 90.67	15.41
1	93	91.86	14.55	91.79	14-95	91.72	15.35	91.66	15.75
ł	94 95	92.84 93.83	14.70	92 78	15.11	92.71	15.51	92.64	15.92
ŀ	96	94.82	14.86	93.76	15 27	93.70	15.68	93.63	16.09
I	97	95.81	15 17	95.74	15.59	95.67	16.01	95.60	16.43
1	98 99	96.79	15.33	96.73	15.75	96.66	16.17	96.58	16.60
ŀ	100	97.78 98.77	15.49 15.64	97-71 98.70	15.91 16.07	97.64 98 63	16.34 16.50	97.57 98.56	16.77
•	101	99.76	15.80	99.69	16 24	99.61	16.67	99.54	17.10
	102	100.7	15.96	100.7	16.40	100.6	16.83	100.5	17.27
	03	101.7	16.11 16.27	101.7 102.6	16.56 16.72	101.6	17.00	101.5	17.44
	05	103.7	16.43	103.6	16.88	103.6	17.33	103.5	17.78
-	06	104.7	16.58	104.6	17-04.	104.5	17.50	104.5	17.95
	07	105.7	16.74 16.90	105.6	17 20 17.36	105.5	17.66 17.83	105.5	18.12
ŀ	109	107.7	17.05	107.6	17.52	107.5	17.99	107.4	18.46
1	10	108.6	17.31	108.6	17.68	108.5	18.16	108.4	18.61
ł,	12	109.6 110.6	17.36	109.6	17.84	109.5	18.32	109.4	18.80
ŀ	13	111.6	17.68	110.5	18.16	110.5	18.65	110.4	18.97
	114	112.6	17.83	112.5	18.32	112.4	18.82	1124	19.31
7-	16	113.6	17.99		18 49	1134	18.98	113.3	19.4
ŀ	137	114.6	18.15 18.30	114.5	18.65	114.4	19.15	114.3	19.
•	18	116.5	18.46	116.5	18.97	116.4	19.48	116.3	19.0
	20	117.5	18.62	117.5	'19.13 19.29	117.4	19.64	117.3	20.
ľ	٠ <u>.</u>	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	1
Ì	Dist		, ==	45		30	<u></u>		
	-				The Car				-

TOA			TA PRINCIPLIA.					
10	0'		16	7.	30	,	43	
Dist.	Lat.	Dep.	Lat	D:p	Lat.	Dep.	Lat.	Dep.
1	0.98	0.17	0.98	0 18	0.98	0 18	0.98	0.19
1 2	1.97	0.35	1.97	0.36	1.97	0.36	1.96	0.37
3	295	0.52	2.95	0.53	2.95	0.55	2.95	. 0.56
4	3.94	0.69	3.94	0.71	3.93	0.73	3.93	0.75
5	4.92	0.87	4.92	0.89	4.92	0.91	4.91	0.93
6	5.91	1.04	5.90	1.07	5.90	1.00	5.89	1.12
7 8	6.89 7.88	1.22	6.89	1.25	6.88 7.87	1.28	6.88 7.86	1.31
	7.86 8.86	1.39	7.87 8.86	1.42	8.85	1 64	8.84	1.68
10	9.85	1.74	9.84	1.78	9.83	1.82	9.82	1.87
1	10.83	1.91	10.82	1.96	10.82	2.00	10.81	205
12	11.82	2.08	18.11	2.14	11.80	2.19	11.79	2.24
13	12.80	2.26	12.79	2.31	12.78	2.37	12-77	2.42
14	13.79	2 43	13.78	2.49	13.77	2.55	13.75	2.61
15	14.77	2.60	14.76	2.67	34-75	2.73	14.74	_
16	15.76	2.78	15.74	2.85	15 73	2.92	15.72	2.98 3.17
17	16.74	3.13	16.73	3.03	16.72	3.10	16.70	3.36
18	18.71	3.30	18.70	3.38	18.68	3.46	18.67	3.54
20	19.70	3.47	1968	3.56	19.67	3.64	19.65	3.73
21	20.68	3.65	20.66	3.74	20.65	3.83	20 63	3.92
22	21.67	3 82	21.65	3.91	21.63	4.01	21,61	4-10
23	22.65	3.99	22.63	4.09	22.61	4.19	22 60	4-29
24	23 64	4.17	23.62	4-27	23.60	4-37	23.58	4-48 4-66
25	24.62	4.34	24.60	4.45	24.58	4.56	24.56	4 85
26	25.61	4.51	25.59	4.63	25.56	4.74	25.54 26.53	5.04
27 28	26.59 27.57	4.69	26.57	4.98	27 53	5.10	27.51	5.22
29	28 56	5.04	28.54	5.16	28.51	5.28	28.49	5-41
30	29.54	5.21	29 52	5.34	29.50	5 47	29.47	5.60
31	30.53	5.38	30.51	5.52	30 48	5.65	30.46	5 78
32	31.51	5.56	31.49	5.69	31 46	5.83	31.44	5.97
33	32.50	5.73	32.47	5.87	32.45	10.0	32,42	6.16
34	33.48	6.08	33.46	6.05	33.43	6.20	33.40	6 34 6.53
35	34.47		34.44	6.41	34.41	6.56	34-39	0.71
36	35-45 36.44	6.43	35 43 36 41	6.58	35.40 36.38	6.74	35-37 36.35	6.90
37 38	37.42	6.60	37.39	6 76	37.36	6.92	37.33	7.09
39	38.41	6.77	38.38	6.94	38.35	7.11	38.32	7.27
40	39.39	6.95	39.36	7.12	39.33	7.29	39.30	7.46
41	40.38	7.12	40.35	7.30	40.31	7 47	40.28	7.65
42	41.36	7.29	41.33	7.47	41.30	7.65	41.26	7.83 8.02
43	42.35	7.47	42 31	7 65	42.28	7.84 8.02	42.25	8.21
44	43.33 44.32	7.64	43.30	801	44.25	8.20	44.21	8.39
45	45.30	7.99	45.27	8.19	45*23	8.38	45.19	8.58
46 47	46.29	8 16	46.25	8.36	46.21	8.57	46.18	8.77
48	47.27	8.34	47.23	8.54	47.20	8.75	47.16	8.95
49	48.26	8.5 t	48.22	8.72	48.18	8.93	48.14	9.14
50	49.24	8.68	49.20	8.90	49.16	9.11	49.12	9-33
51	50.23	8.86	50.19	9.08	50.15	9.29	50.11	9.51
52	51.21	9.03	51.17	9.25	51.13	9.48	51.09	9.70
53	52.19 53.18	9.20 9.38	52.15	9.43	53.10	9.84	53.05	10.07
54 55	54.16	9.55	54 12	9.79	54.08	10.02	54,03	10.26
56	55.15	9.72	55.11	9.96	55.06	10.21	55.02	10.45
50	56,13	9.90	56.09	10.14	56.05	10.39	56,00	10.63
58	57.12	10.07	57.07	10.32	57.03	10.57	56 98	10.82
59	58.10	10.25	58.06	10.50	58.01	10.75	57.96	11.00
60	59.09	10.42	59.04	10.68	59.00	10.93	58.95	11.19
Dist	Dep.	Lat	Dep.	Lat	Dep.	Lat.	Dep.	Luti
Ä	0	•	45	5′	\$0)′	1	5,

٠	-	0'		15'		30'		45	
1	Dist.		Dep.			La			
1.		La'.		Lat.	Dep		Dep	Lu	Dep.
ł	61 63	00.07 61.06	10.77	60,03 61 01	10.85	59.98 60.96	11.30	59.93. 1 60.9ì	11.38
1	63	52.04	10 94	61.09	11 21	61.95	11.48	61 89	11.75
I	64	63.33	míi	62.98	11.39	62.93	11.66	62.88	11.94
Ì	65	6401	11.29	63.46	1 8 57	63 91	11.8;	63 86	12.12
ı	66	65.00	11.46	64.95	11.74	64.89	12.03	64.84	12.31
1	67	65.98	11.63	65.93	11.92	65.88	12 21	65.82	12.50
1	68	66.97	11.81	66.yı 67.yo	12.10	66.86 67.84	12.39	66 81	12.68
Ì	69 70	67.95 68.94	12.16	68 88	12.46	68.83	12.76	68.77	13.06
ł	71	64.92	12 33	69.87	12.63	64.81	12.94	69.75	13.24
ı	72	70.91	12 50	70.85	12.81	70.79	13.12	70.74	3.43
ł	73	71 84	12.68	71.84	12.99	7178	13.30	71.72	13.62
ł	74	72.88	12.85	72.82	13.17	72.76	13.49	72.70	13.80
L	75	73.86	13.02	73.80	13.35	73 74	13.67	73.68	13 90
1	76	74.85	13.20	74.79	13 52	74-73	13.85	74 67	14 18
ł	77	75.83 76.82	13.37	75 77 76.76	13 70	75.71 76.69	14.03	75.65 76.63	14.36
İ	78 ·	77.80	13.54	77-74	14.86	77.68	14.40	77.61	14.74
Ţ	80	78.78	13.89	78.72	14.24	78 66	14.58	78.60	14.92
ľ	81	79-77	14.07	79.71	14.41	79.64	14.76	79.58	45. i.i
ı	82	80 75	14.24	80.69	14.59	80.63	14.94	80.56	15.30
·I	83	81.74	1441	81.68	14.77	81.61	15.13	81.54	15.48
ł	84	82.72	14.59	82.66 83.64	14.95	82.59	15 31	82.53	15.67
Į.	85	83.71	14.76		15.13	83.58	15.49	83.51	15.85
ı	86	84.69 85.68	14 93	84.63 85.61	15.30	84 56 85-54	15.67	84.49 85.47	16.04
ı	87 88	86.66	15.28	86.60	15.48	85.53	16.04	86 46	16.41
I	89	87.65	15.45	87.58	15.84	87.51		87 44	16.60
ł	90	88.63	15.63	88.56	16 o i	88:49	16.40	88.42	16.79
I	91	89.62	15.80	89.57	16 19	89.48	16.58	89.40	16.97
ı	92	90.60	15.98	90.53	16.37	90.46	16.77	90.39	17.16
ŧ	93	91.59	16.15	91.52	16.55	91.44	16.95	91 37	17.35
1	94	92.57	16.32	92.50 93.48	16.73 16 90	92.43	17.13	92.35	17.53
ł	95	93.56	16.67		17.08	94-39	17.49	94.32	· -
ŧ	96 97	94-54	16.84	94·47 95·45	17.26	95.38	17.68	94.32	17.91
ł	98	96.51	17.02	96 44	17.44	96.36	17 86	96.28	18.28
i	99	97.50	17.19	97.42	17.62	97.34	18.04	97.26	18.47
ŀ	100	98.48	17.36	98.40	17 79	98.13	18.22	98.25	18.63
	101	99-47	17-54	99.39	17.97	99.31	1841	99.23	18.84
	102	100.4	17.71	100.4	18.15	100.3	18.59	100.2	19.03
	103	101.4	17.89	101.4	18.33 18.51	101.3	18.95	101.2	19.21
	105	103 4	18.23	103.3	18.68	103.2	19.13	103.2	19.59
٠.	106	104.4	18 41	104.3	18.86	104.2	19.32	10:01	19.77
•	107	105.4	18.58	105 3	19.04	105.2	19.50	105.1	19 06
ŀ	108	106.4	18.75	106.3	19 22	106 2	19.68	106.1	20,14
	109	107.3	18 93	107.3	19.40	107.2	19 86	107.1	20.32
1-	110	108 3	19.10	108.2	19.57	10 .2	20.05	108.1	20 52
	111	109 3	19.28	109.2	19.75	109.1	20.23	109.1	20.70
ı	112	110.3	19.45	110.2	19.93	111.1	20.41 20.59	110.0	20 89
	114	112.3	19.80	112.2	20.29	1121	20.77	112.0	21.26
	115	113.3	19.97	113.2	20.46	113.1	20.96	1130	21.45
1-	116	114.2	20.14	114.1	26.64	114.1	21 14	114.0	21.60
1	117	115.2	20.32	115.1	20 82	115.0	21.32	1149	21.82
7	118	116.2	20.49	116.1	21.00		21.50	115.9	22.01
	119	117.2	20.84	117.1	21.18	117.0	21.69	117.9	22.20
1				Dep		Dep.	Lar		·
ļ	Dist	Den	Lat.		Lat.			Dep.	Lut.
Ţ	2	U	.	4	.)'	'	301	• · 1	:1

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Die	Lat	Dep.	Lat.	Dep.	Lat	Dep.	Lat.	Dep
-	0,98	0.19	0.98	0.20	0.98	0.20	0.98	0.20
	1.96	0.38	1.96	0.39	1.96	0.40	1.96	0.41
3	2.94	0.57	2.94	0.59	2.94	0.60	2.94	0.61
4	3 93	0.76	3.92	0.78	3.92	0.80	3.92	0:81
15	4.91	0.95	5.88	0.98	5.88		4.90	1.02
6	5.89 6.87	1.14	6.87	1.17	6.86	1 20	5.87 6.85	1.22
7	7.85	1.53	7.85	1.56	7.84	1.59	7.83	1.63
9	8 8 3	1.72	8.83	1.76	8.82	1.79	8.81	1.83
10	9.82	1.91	9.81	1.95	9.80	1.99	9.79	2.04
11	10.80	2.10	10.79	2.15	10.78	2.19	30.77	2.24
12	11.78	2.29 2.48	11.77	2.34 2.54	11.75	2.39	11.75	2.44
14	13.74	2.67	13.73	2.73	13.72	2.79	13.71	2.85
15	14.72	2.86	14.71	2.93	14-70	2.99	14.59	3.05
16	15.71	3.05	15.69	3.12	15.68	3 19	15.66	3.26
17	16.69	3.24	16.67	3.32	16.66	3.39	16.64	3.46
18	17.67	3.43 3.63	17.65	3.51 3.71	17.64	3.59 3.79	17.62	3.67 3.89
20	19.63	3.82	19.62	3.90	19.60	3.99	19.58	4.07
31	20.61	4.01	20.60	4.10	20.58	4.19	20.56	4.28
22	21 60	4.20	21 58	4.29	21.56	4-39	21.54	4.48
23	22,58	4-39	22.56	4.49	22 54	4-59	32.52	4.68
34	23 56 24 54	4.58	23.54 24.52	4.68 4.88	23.52 24.50	4.98	23.50 24.48	4.89 5.09
25	25.52	4.96	25.50	5.07	25.48	5.18	25.46	5 29
27	26 50	5.15	26 48	5.27	26.46	5.38	26.43	5.50
28	27-49	5.34	27.46	5 46	27.44	5.58	27.41	5.70
29	28.47	5.53	28.44	5.66	28.42	5.78	28.39	ş.91
30	29.45	5 72	29.42	5.85	29.40	5.98	29.37	6 11
31 32	30.43 31.41	6.11	30.40	6.05 6.24	30.38	6.18	30.35	6.31 6.52
33	32.39	6.30	32.37	6.44	32 34	6.58	31.33	6.72
34	33.38	6.49	33.35	6.63	33.32	6.78	33.29	6.92
35	34 36	6.68	34-3-3	6 8 3	34.30	6.98	34.27	7.13
36	35.34	6.87	35.31	7.02	35.28	7.18	35.25	7.33
37 38	36.32	7.25	36.29 37.27	7.22	36.26 37.24	7.38	36.22 37.26	7-53 7-74
39	38.28	7.44	38 25	7.61	38.22	7.78	38 18	7.94
40	39.27	7.63	39-23	7.80	39.20	7.97	39.16	8.15
41	40.25	7.82	40.21	8.00	40.18	8.17	40. ¥4	8.35
42	41.23	8.01	41.19	8.19	41.16	8.37	41.12	8.55
43	42.21	8.20 8.40	42.17	8.39 8.58	42.14	8 57 8.77	43.08	8.76 8.96
45	44-17	8.59	44-14	8.78	44.10	8.97	44.06	9.16
46	45.15	8.78	45.12	8.97	45.08	9.17	45 04	9.37
47	46.14	8.97	46.10	9.17	46.06	9.37	46.03	9.57
48	47.12	9.16	47.08 48.06	9.36	47.04	9.57	46 99	9.77
49 50	49.08	9.35	49.04	9.56 9.75	48 02	9.77	47·97 48.95	9.98 10.18
51	50.06	9.73	50.02	9.95	49.98	10.17		
52	\$1.04	9.92	51.00	10.14	50.96	10.37	50.91	10.39
53	52.03	10.11	51.98	10.34	51.94	10.57	51.89	10.79
54	53.01	10.30	52.96	10.53	52.92	10.77	52.87	11.00
55	53.99	10.49	53.94	10.73	53.90	10 97	53.85	11.20
57	\$4.97 55.95	10.88	54.92 55 90	10.93	54.88 55 86	11.16	54.83 55.81	11.40
58	56.93	11.07	56.89	11.32	56.84	11.56	56 78	11,81
1 59	57.92	11.26	57.87	11.51	57.82	11.76	57.76	12.01
-00,	58.90	11.45	58.85	11.71	58.80	11.96	58.74	12.22
Dist	1)ep_	Late	Dep.	Lat	Dep.	Lat.	Dep.	Lat.
10		/	45	70000	30	′ '	15	,

17	0	f	1 1	5/	} 3	91 .	45	
1 5	Lat	Dep	Lat	Dep	Lat.	Dep.	Lut.	Dep.
61	59.88	11.64	59.82	11.90	59.78	12 16	59.72	12.42
62	60.86	11.83	60.81	12.10	60.76	12.36	60.70	12.63
63	61.84	12 02.	61.79	12.29	61.74	12.56	61.68	12.83
64 65	63.81	12.40	63.75	12.68	63.70	12.96	63.64	13.24
66	64.79	12.59	64.73	12.88	64.68	13.16	64 62	13.44
67	65.77	12.78	6571	13.07	65.66	13.36	65.60	13.64
68 69	66.75	12.98	66.69 67.67	13.27	66.63	13.56	66.58	13.85
70	68.71	13.36	68.66	13.66	68.59	13.96	68.53	14 25
9.71	69.70	13.55	69.64	13.85	69.57	14.16	69.51	14 46
7.3	70.68	13.74	70.62	14.05	70.55	14.35	70 49	14.66
7.4	71.66	13.93	71.60	14.24	71 53	14.55	71.47	15.07
7.5	73.62	14.31	73.56	14.63	73.49	14.95	73.43	15.27
76	74.60	14 50	74-54	14.83	74-47	15.45	74-41	15.48
77	75.59	14.69	75,52	15.02	75.45 76.43	15.35	75.39 76.37	15 68
78	76.57	14.88	76.50	15.22	77.41	15.55	77.34	16.09
80	78.53	15.26	78 46	15.61	78.39	15.95.	78.32	16 29
81	79.51	15.46	79-44	15.80	79.37	16.15	79-30	16.50
82	80.49	15.65	\$0.42	16.00	80.35 81.33	16.35 16.55	80.28 81.26	16.70
8; 84	81.48 82.46	16.03	82.30	16.39	82.31	16.75	82.24	17.11
8.	83.44	16.22	83.37	16.58	\$3.29	16.95	83.22	17.31
86	84.42	16.41	84.35	16.78	\$4.27	17.15	84.20	17.51
85	85.40 86.38	16.60	\$5.33 86.31	1 6 .97	\$5.25 \$6.23	17.35 17.54	85.18 86.16	17.72
89	87.36	16.98	87.29	17.36	87.21	17.74	87.14	18.12
90	88.35	17.17	\$8 27	17.56	\$8.19	17.94	88.11	18.33
91	89.33	17.38	89 25	17.75	\$9.17	18.14	89.09	18.53
93	90 31	17.55	90.23	17 95	90.15	18.34	90.07 9 t.65	18.74
93	91.29	17.94	91.21	18 34	92.11	18.74	92.03	19.14
95	93.25	18,13	93.1.7	18.53	93.59	18.94	93.01	19.35
96	94-24	18.32	94.10	18 73	94.07	19.14	93.99	19.55
97 98	95.22	18.51 18 70	95.14 96.12	18.92 19.12	95.05	19.34 19.54	94.97 95.95	19.75
99	97.18	18.89	97.10	19.31	97.01	19.74	96.93	20.16
100	98.16	19.08	98.08	19.51	97.99	19.94	97 90	20.36
101	99.14	19.27	99.06	19.70	98.97	20.14	99.86 99.86	20.57
103	1.001	19.46	100.0	19.90	99.95	20.34 20.53	100.8	20.98
304	102, 1	19 84	102.0	20.29	101.9	20.73	101.8	21.18
105	103.1	20.04	103.0	20.48	102.9	20.93	102 8	21.38
106	104.1	20.23 20.42	104.0	20.68 20.87	103.9	21.13 21.33	103.8	21.59
107	105.0	20.42	105.9	21.07	105.8	21.53	105.7	21.99
109	107.0	20.80	106.9	21.26	106.8	21.73	106.7	22.20
110	108.0	20 99	107 9	21 46	107.8	21.93	107.7	22.40
411		21.18	108.9	21.85	108.8	22.13	108.7	22.81
112	110.9	21.56	110.8	22.05	110.7	22.53	110.6	23.01
114	1119	21.75	8.116	22.24	111.7	22.73	111.6	23 22
415		21 94	112,8	32 44	112.7	22 93	113.6	23 42
#16	113.9 114.9	22.12	114.7	22.63	114.6	23.33	114.5	23.62
118	115.8	22.52	115.7	23.02	115.6	23.53	115.5	24.03
#19	116.8	22.71		23.22		23.72	116.5	24.23
# 20	117.8	22.90	117 7 De;	$\frac{23.41}{1}$	117.6 Dep.	121.92 Dit.	Dep.	21 44 Lui
12	Dep	Lat.		<u>L:</u>			1:	-
12)/		INEC: D	30	, 		

1 5	2. [07		15	7	30	01	1 4	7
1		Lat	Dep.	Lat.	Dep.	Lat	Dep.	Lat.	Dep
-	7	0.98	0.19	0.98	0.20	0.98	0.10	0.98	0.20
	2 4	1.96 2,94	0.38	1.96 2.94	0.39	1.96 2.94	0.40	1.96 3.94	0.41
	3 4	3.93	0.76	3.92	0.78	3.92	0.80	3.92	0.81
	3	4.91	0.95	4.90	0.98	4.90	1.00	4.90	1.02
	6	5.89	1.14	5.88	1.17	5.88	1 20	5.87	1.22
l	7 8	6.87 7.85	1.34	6.87 7.85	1.37	6.86 7.84	1.40	6.85 7.83	1.43
	9	8 83	1.72	8.83	1.76	8.82	1.79	8.81	1.83
	ó	9.82	1.91	9.81	1.95	9.80	1.99	9.79	2.04
	1	10.80	2.10	10.79	2.15	10.78	2.19	10.77	2.24
	3	11.78	2.29	11.77	2.34 2.54	11.75	2.39	11.75	2.44 2.65
	4	13.74	2.67	13.73	2.73	13.72	2.79	13.78	2.85
	5	14.72	2.86	14.71	2.93	14-70	2.99	14.59.	3.05
	6	15.71	3.05	15.69	3.12	15.68	3 19	15.66	3.26
	8	16.69	3.24	16.67	3.32 3.51	16.66	3·39 3·59	16.64 17.62	3.46
	lg	18.65	3.63	18 63	3.71	18.62	3.79	18.60	3.89
	ió.	19.63	3.82	19.62	3.90	19.60	3.99	19.58	4.07
	11	20.61	4.01	20,60	4.10	20.58	4.19	20.56	4.28
	12	21 60	4-20	21 58	4.49	21.56	4.39 4.59	21.54	4.48 4.68
	14	23 56	4.58	23.54	4.68	23.52	4 78	23.50	4.89
	25	24 54	4.77	24.52	4.88	24.50	4.98	24.48	5.09
	16	25.52	4.96	25.50	5.07	25.48	5.18	25.46	5 29
	17	26 50 27.49	5.15 5.34	26 48 27.46	5.27	26.46 27.44	5.38	26.43 27.41	5.50 5.70
•	19	28.47	5.53	28.44	5.66	28.42	5.78	28.39	5.91
	\$O	29.45	572	29.42	5.85	29.40	5.98	29.37	6 11
	} I ,	30.43	5.92	30.40	6.05	30.38	6.18	30.35	6.31
	12 13	31.41	6.11	31.39	6.24 6.44	31.36	6.38	31.33 32.31	6.72
	34	33.38	6.49	33-35	6.63	33.32	6.78	33.29	6.92
	35	34 36	6.68	34-33	6.83	34.30	6.98	34.27	7-13
	6	35.34	6.87	35.31	7.02	35.28	7.18	35.25	7.33
	8	36.32 37.30	7.25	36.29 37.27	7.22	36.2 6 37.24	7.38	36.22 37.26	7-53 7-74
	39	38.28	7-44	38 25	7.61	38.22	7.78	38 18	7-94
-	10	39.27	7.63	39-23	7.80	39.20	7.97	39.16	8.15
	ħ1	40.25	7.82	40.21	8.00	40.18	8.17	40.14	8.35
	12 13	41.23	8.20	41.19	8.39	42.14	8.37 8.57	41.13	8.55 8.76
14	14	43.19	8.40	43.15	8.58	43.12	8.77	43:08	8.96
_	15	44-17	8.59	44-14	8.78	44.10	8.97	44.06	9.16
	16	45.15	8.78 8.97	45.12	8.97	45.08 46.06	9.17	45.04	9.37
	8	47.12	9.16	47.08	9.17	47.04	9:37	46.02 46.99	9-57
4	19	48.10.	9.35	48.06	9.56	48.02	9.77	47-97	9.98
1-	90	49.08	9.54	49.04	9.75	49.00	9.97	48.95	10.18
• •	5 I 5 2	50.06	9.73 9.92	50.02	9.95	49.98	10.17	49.93	10.39
	53	52.03	10.11	51.08	10.14	50.96 51.94	10.37	50.91	10.59 10.79
1 :	54	53.01	10.30	52.96	10.53	52.92	10.77	52.87	11.00
_	55	53.99	10.49	53-94	10.73	53.90	10.97	53.85	11.20
	56 57	54-97 55-95	10.88	54.92 55 90	10.93	54.88 55 86	11.36	54.83	17.40
	8	56.93	11.07	56.8 9	11.32	56.84	11.56	55.81 56.78	11.61
1 5	9	57.92	11.26	57.87	11.51	57.82	11.76	57.76	18.01
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	61	59.67	L2.68	59.61	12.94	\$9.55	13.20	59.50	13.46
1	62	60.65	12.89	60.59	13.16	60.53	13.42	60.47	13.68
1	63 64	61.62	13.10	61.57	13.37	61.51	13.64	61.45	13.90
1	65	62.60	13.31	62.54	13.58		13.85	62.42	14.12
1		63.58	13.51	63.52	13 79	63.46	14.07		14.35
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1	67 68	65.54	13.93	65.47	14.22	65.41	14.50	65.35	14.79
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	71	69.45	4.76	69.38	15.06	69.32 70.29	15.37 15 58.	69.25	15.67
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ı	78	76.30	16.22	76.22	16.55	76.15	16.88	76.08	17.21
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	86	78.25	16.63	78. t8	16.97	78.10	17.32	78.03	17.66
1	81	79.23	16.84	79:16	17.19	79.08	17 53	79.00	17.88
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ı	84	82 16	17 46	82.09	17.82	82.01	18.18	81.93	18.54
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1	96	93.90	19.96	93.81	20.37	93.72	20.78	93.63	21.19
1	97	94 88	20.17	94.79	20.58	94 70	20.99	94 61	21.41
1	98	95.86	20.38	95.77	20.79	95.68	21.21	95.58	21.63
1	99	96.84	20.58	96.75	21.01	96.65	21.43	96.56	21.85
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,	2.92	0.67	2.92	0.69	2.92	0.70	2-91 3-89	0.75	
4	3.90 4.87	0.90	3.89 4.87	0.92	3.89 4.86	1.17	4.86	1.19	
6	5.85	1.35	5.84	1.38	5.83	1.40	5.83	1.43	
	6.81	1.57	6.81	1.60	6.81	1.63	6.80	1.66	
7 8	7 80	1.80	7.79	1.83	7.78	1.87	7.77	1 90	
10	8.77	2.02	8.76 9.73	2.06 2.2y	8 75 9-72	2.10	8,74 9:71	2.38	
11	9.74	2.47	10.71	2.52	10.70	2.57	10.68	2.61	
12	11.69	2.70	11.68	2.75	11.67	2.80	11.66	2.85	
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17	15.59 16.56	3.82	16.55	3.90	16 53	8.97	16.51	4.04	
18	17.54	4.05	17.52	4-13	27.50	4.20	17.48	4.28	
39	18.51	4.27	18.49	4 35 4.58	18.48 19.45	4-44	18.46 ·	4-75	
20	19.49	4.50	19.47	4.81		4.90	20.40	4-99	
23 23	20,46	4.72	20.44	5.04	20.42	5.14	21.37	5.43	
23	22.41	5.17	22.39	5.27	22.36	5.37	22.34	5-47	
24	23.38	5.40	23.36	5.50	13:34	5.60 5.84	23.31 24.28	5.70	
25	24.36	5 62	24.33	5.73	24.31	6 07	25.25	5.94 6.18	
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72	27.28	6.30	27.25	6.42	27.23	6.54	27.20	6.66	
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30	29.23	6.75	29.20	6.88	29.17	7.00	29.14		
31	30.81 31.18	6.97 7.20	30.17	7.81 7.33	30.14	7.24	30.11	7.37 7.61	
32	32.15	7.43	32.12	7.56	32.09	770	32:05	7.84	
34	33.43	7.65	33.09	7.79	33.06	7.94	53.03	8.08	
35	34.10	7.87	34.07	8.02	34.03	8.17	34.00	8.32	
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37 38	37.03	8.55	36.99	8.71	36.95	8.87	36.91	9.23	
39	38.00	8.77	37.96	8.94	37-92	9.10	37.88	9.27	
40	38.97	9.00	38.94	9.17	38.89	9-34	38.85	9.51	
41	39.95	9.22	39.91 40.88	9.40	39.87 43.84	9.57	39.83 40.80	9-75 9-98	
43	40.92	9.45	41.86	9.86	4181	10.04	41.77	10.22	
44	42.87	9.90	42.83	10.08	42 78	10.27	42.74	10,46	
45	43.85	10-12	43.80	10.31	43.76	10.51	43.71	10 70	
46	44 82	10 35	44.78	10.54	44.73	10.74	44.68	10.93	
47	45.80 46.77	10.57	45.7 5 46 72	10.77	45.70	10.97	40.62	11.41	
49	47.74	11.09	47.70	11.23	47.65	11.44	47.60	11.65	
50	48.72	11.25	48.67	11.40	48.61	11.67	48.57	11.88	
51		11.47	49.64	11.69	49.59	11.91		12.12	
52 53	50.67 51.64	11.70	50.62	11.92	50.56	12.14	50.51	12.36	
54		12.15	52.56	12.38	52.51	12.61	52.45	12.84	
55	53.59	12.37	53.54	12.61	53.48	12.84	53.42	13.07	
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62	60:41	13 95	60.35 61.32	14.31	61 26	14.47	60.22	14.74
64	62,36	14.40	62.30	14.67	62.23	14 94	62.17	14.97
65	63.33	14.62	63.27	14.40	63.20	15.17	63.14	15.45
66	64.31	14.85	64.24	15.13	64.18	15.41	64.11	15.69
67	65.28	15.07	65.22	15.36	65.15	15.64	65.08	15 93
68 69	66.26	15.90	66.19	15.59	66.12	15.87	66.05	16.16
70	68.25	15.52	68.14	15.81	68.07	16.11	67.99	16.40
71	69.18	15.97	69.11	16.27	69 54	16.57	68.97	16.88
72	70.15	16.20	70-08	16.50	70.0	16.81	69.94	17.11
73	71.43	16.42	71.06	16 73	70 y8	17.04	70.91	17.35
74	72 40	16 65	72.03	16.96	71.96	17.28	71.88	17.59
75	73.08	16.87	73.00	17-19	72.93	17.51	72.85	17.83
75	74.05	17.10	73.98	17.42	73.90	17.74 17.98	73.82	18 06 18.30
78	76.00	17.32	74.95	17.88	75.84	18.21	74-79 75-76	18.54
79	76.98	17 77	76.90	18.11	6.82	18.44	76.74	18.78
80	77.95	18.00	77.87	18 34	77.79	18.68	77.71	19.01
81	78.92	18.22	78.84	18.57	78.76	18.91	78.68	19.25
82	79.90 80.87	18.45	79.84	18.79	79·7·3 80.71	19.14	79.65	19.49
84	81.85	18.00	80.79 84.76	19.02	84.68	19.51	81.59	19.73
\$ 85	82.82	19.12	82.74	19.48	82.65	19.84	82.56	20.20
80	83.80	19.35	83.71	19.71	83.62	20.08	83.54	20.44
87	84.77	19.57	84.68	19.94	84.60	20.31	84.51	20.68
88	85.74	19.80	85.66	20.17	85.57	20.54	85.48	20.92
90	86.72 87.69	20.02	86.63 87.60	20.40	86, 54 87 5 t	20.98	86.45 87.42	21.15
91	88.67	20.47	88.58	20.86	88.49	21.24	88.39	21.63
92	89.64	20.70	89.55	21.09	89.46	21.48	89 36	21.87
93	90.62	20.92	90.52	21.32	90.43	21.71	90.33	22.10
94	91.59	21.15	91.50	21.54	91.40	21.94	91.31	22.34
96	92.57	21.60	92.47	21.77	92.38		92.28	22 58
97	93.54	21.82	93.44 94.42	22.23	93.35 94.32	22.41	93.25	23.06
98	95.49	22.05	95.39	22.46	95.29	22.88	95.19	23.29
199	96.46	22.37	96.36	22.69	96 26	23.11	96.16	23.53
1	97.44	22.50	97.34	22.92	97.24	23.34	97.13	23 77
101	98.41	22.72	98.31	23.15	98.21	23.58	98.11	24.24
103	100.4	23.17	100.3	23.61	100.2	24.04	99.08	24.48
104	101.3	23.40	101.2	23.84	101.1	24.28	101.0	24.72
105	102.3	23.62	102.2	24.07	102.1	24.51	102.0	24.96
106	103.3	23.84	103.2	24 30	103.1	24.75	103.0	25.19
107	104-3	24.07	104.3	24.52	104.0	24.98	103.9	25.43
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116	113.0	26.0g	112.9	26.59		27 08	112.7	27.57
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1118	115.0	26.54	114.9	27.05	114.7	27.55	114.6	28.05
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1.	Dist.	Lat·	Dep.	Lat.	Dep.	Lat.	D _t p.	Lat.	De
I	61 62	59-19	14.76	59.12	15.02	59 06	15.27	58.99	15.5
ı	63	61.13	15.00	60.09	15.26	60.03 60.99	15.52	59.96 60.93	15.7
1	64	62.10	15.48	62:03	15.75	61.96	16.02	6189	16.2
1	65	63.07	15.72	63.00	16.00	62.93	16 27	62.86	16.5
ı	66 67	64.04	15.97	63.97 64.94	16.25	63.90 64.87	16.53	63.83	16.8
ı	68	65.98	16.45	65.91	16.74	65.83	17.03	65.76	17.0
١	69	66.95	16.69	66.88	16.98	66.80	17.28	66.73	117.5
Į.	70	67.92	16 93	67 85	17.23	67.77	17.53	67.69	17.8
1	71 72	68.8g 6g.86	17.18	68.82 69.78	17.48	68.74 69.71	17.78	68.66 69.63	18.0
ł	73	70.83	17.66	70.75	17.97	70.67	18.28	70.59	18.5
ı	74	71.80	17.90	71.72	18.22		18.53	71 56	18.8
1	75	72-77	18.14	72.69	18.46		18.78	72.53	19.1
1	76 7 7	73.74 74.71	18.39	73.66 7.4.63	18.71	73.58 74.55	19.03	73 50	19.3
1	78	75.68	18.87	75.60	19.20	75.52	19.53	75.43	19.8
. [79	76.65	19.11	76.57	19.45	76.48	19.78	76.40	20.1
1	80	77.62	19.35	77.54	19.69	77.45	20.03	77.36	20.3
١	8 t 8 z	78.59 79.56	19.60	78.51 79 48	19.94	78.42 7 9 .39	20.28	78.33	120.8
ı	83	80.53	20.08	80.45	20.43	80.36	20.78	80.26	21.1
ł	84	81.50	20.32	81 42	20.68	81.32	21.03	81.23	21.3
ŀ	85	82.48	20.56	82 38	20.92	82.29	21.28	82.20	21.6
ı	86 87	83.45 84.42	20.81 31.05	83 35 84.32	21.17	83.26 84.23	21.53	83.17	21.9
١	88	85.39	21.29	85.29	21.66	85.20	22.03	85.10	22.4
1	89	86.36	21.53	86.26	21.91	86.17	22.28	86.07	22.6
ŀ	90	87.33	21 77	87.23	22.15	87.13	22.53	87.03	22.9
1	91	88.30 89.27	22.01 12.26	88.20 89.17	22.40	88.10 89.07	22.78	88.00 88.97	23.1
ı	93	90.24	22.50	90.13	22.89	90.04	23.29	89.94	23.6
1	94	91.21	22.74	91.11	23.14	91.01	23.54	90.90	23.9
ŀ	95	92.18	22.98	92.08	23.38	91.97	23 79	91.87	24.1
I	96 97	93.15	23.22 23.47	93.05	23.63 23.88	92.94 93.91	24.29	92.84	24.7
١	98	95.09	23.71	94.98	24.12	94.88	24 54	94-77	24.9
I.	99	96.06	23.95	95.95	24.62	95.85	24.79	95-74	25.1
1-	101	97.03	24.43	95.92	24.86	96.81	25.04	96.70	25.4
	102	98.97	24.68	98.86	25.11	97.78	25.29	98.64	25.9
	103	99.94	24.92	99.83	25.35	99.72	25.79	99.61	26.2
	104	100.9	25.16	100.8	25.60 25.85	100.7	26 04	100.6	26.4
-	106	102.9	25.40	102.7	26.09	102.6	26.29	102 5	26.0
ŀ	107	103.8	25.89	103.7	26.34	103.6	26.79	103.5	27.2
	801	1048	26.13	104.7	26 58	104.6	27.04	104.4	27.5
	109	105.8	26.37 26.61	105.6 106.6	26.83 27.08	105.5	27.29	105.4 106.4	27.7 28.0
1:	111	107.7	26.85	107.6	27.32	107.5	27.54	107.3	25.2
ŀ	112	108.7	27.10	108.6	27.57	108.4	28.04	108.3	28.5
	13	109.6	27.34	109.5	27.82	109.4	28.29	109.3	28.
	114	111.6	27.58 27 82	110.5	28.06 28.31	110.4	28.54 28.79	110.2	29.0
- 1-	16	112.6	28.06	112.4	28.55	112.3	29.04	112.2	29.5
	17	113.5	28.30	113.4	28.80	113.3	29.29	113.1	29;
	118	114.5	28.55	1144	29.05	114.2	29.54	114.1	30.0
	20	115.5	28.79 29.03	115.3	29.29 29.54	115.2	29.80 30 0 ç	115.1	30.
1	ني	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	L
1	Dust.		,	45		30	·		5/
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-	5	0,		15	1	30	,	45'	
١	Dist.	Lat.	Dep.	Lut.	Dep.	Lat.	Dep.	Lat	Dep.
-	-	0.97	0.26	0.96	0.26	0.96	0.27	0.96	0.27
ì		1.93	0.52	1.93	0.53	1.93	0.53	1.92	0.54
ı	3	2.90 3.86	0.78	2.89 3.86	1.05	2.89 3.85	0.80	2.89 3.85	1.00
ı	5	4.83	1.29	4.82	1.32	4.82	1.34	4.81	1.36
	6	5.80	1.55	5.79	1.58	5.78	1.60	5.77	1.63
ì	?	6.76	1.81	6.75	1.84	6.75	1.87	6.74	1.90
1	8	7.73, 8.6g	2.07	7.72 8.68	2.10	7.71 8.67	2.14	7.70 8.66	2.17
1	10	9.66	2.59	9.65	2.63	9.64	2.67	9.62	2.71
-	11	10.63	2.85	10.61	2.89	10.60	2.94	10.59	2.99
ł	12	11.59	3.11	11.58	3.16	11.56	3.21	11.55	3.26
1	13	12.5 6 13.5 2	3.36 3.62	12.54 13.51	3.42 3.68	12.53	3.47	12.5 L 13.47	3.53 3.80
l	15	14-49	3.88	14.47	3.95	1445	4.01	14.44	4-07
	16	15.45	4.14	15.44	4.21	15.42	4,28	15.40	4-34
1	17	16.42	4.40	16.40	4-47	16.38	4-54	16.36	4.61
I	18	17.39 18.35	4.66	17.37	4·73	17.35	4.81 5.08	17.32	4.89 5.16
ı	20	19.32	5.18	19.30	5.26	19.27	5-94	19.25	5-43
1	21	20.28	5.44	20.26	5.52	20.24	5.61	20.21	5.70
	22	21.25	5.69	21.23	5.79	21.20	5.83	21.17	5.97
	23 24	22.22	5.95 6.21	23.15	6.05 18.6	22.16	6.15	23.14	6.24 6 51
	25	24.15	6.47	24.12	6.58	24.09	6.68	24.06	6.79
1	26	25.11	6.73	25.08	6.84	25.05	6.95	25.02	7.06
	27	26.08	6.99	26.05	7.10	26.02	7-22	25.99	7.33
	28 29	27.05 28.01	7.25	27.01 27.98	7.36 7.63	26.98 27.95	7.48	26.95 27.91	7.6a 7.87
	30	28 98	7.76	28.94	7.89	28.91	8.02	28.87	8.14
	31	29.94	8.01	29 91	8.15	29.87	8.28	29.84	8.41
	32	30.91	8.28	30.87	8.42	30.84	8,55	30.80	8.69
	33 34	31.8 8 32.84	8.54 8.80	31.84 32.80	8.68 8.94	31 80 32.76	8.82 9.00	31.76	8.96 9.23
	35	33.81	9.06	33.77	9-21	33.73	9.35	33,69	9.50
ľ	36	34-77	9.32	34-73	9-47	34.69	9.62	34.65	9-77
	37 38	35.74 36.71	9.58 9.84	35.70	9.73	35.65	9.89 10.16	35.61 36.57	10.04
	39	37.67	10.09	36.66 37.63	10.26	36.62 37.58	10.42	37.54	10.59
•	40	38.64	10.35	38.59	10.52	38 55	10.69	38 50	10.86
	41	39.60	1061	39-56	10.78	39-51	10.96	39.46	11.13
	42	40.57	10.87	40.52	11.05	40.47	11.22	40.42	11.40
	43 44	42.50	11.39	41.49	11.57	42.40	11.76	42-35	11.94
	45	43-47	11.65	43.42	11.84	43.36	12.03	43 31	12.21
•	46	44-43	11.91	44.38	12.10	44-33	12.29	44.27	12.49
	47 48	45.40 46.36	12.16	45.35 46.31	12.36	45.29 46.25	12.56	45.24	12.76
	49	47.35	12.68	47.27	12.89	47.22	13.09	47.16	13.30
	śó	48.30	12.94	48 24	13.15	48.18	13.36	48.12	13.57
	5 I	49.26	13.20	49.20	13.41	49.15	13.63	49.09	13.84
	52 53	50.23 51.19	13.46	50.17	13 68 13 94	50.11	13.90	50.05 51.01	34.11 34.39
	54	52.16	13.98	52.10	14.20	52.04	14-43	51.97	14 66
	55	53.13	14.24	53.06	14 47	53.00	14.70	52.94	14.93
1	56	54.09	14.49	54 03	14-73	53.96	14.97		15.20
1	57 58	55.06 56.02	14.75 15.01	54-99 55.96	14.99	54-93 55.89	15.23	54.86 55.82	15.47 15.74
1	59	57.99	15.27	56.92	15.52	56.85	15.77	56.78	16,02
	6ó	57.96	15.53	57.89	15.78	57.82	16 03	57-75	16.29
1	Dist	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
ļ	ā.	.0		45	5'	3	0'	13	5'

Dist	0		1:	51	3	0/	4	57		
St	Lat	D-p.	Lat	D·p	Lat	Dep.	Lat.	Ī		
61	58.92	15 79	58.85	16.04	58 78	16.30	58.71	7		
62 63	59.89 60.85	16.05	59.82	16.31	59.75 60.71	16.57	59.67 60.63	: I		
64	61.82	16.56	61.75	16.83	61.67	17 10	61.60	1		
65	62.79	16.82	62.71	17.10	62.64	17.37	62.56	1		
66 67	63 75 64.72	17.08	63.68 64.6 4	17.36 17. 62	63.60 64.56	17.64	63.52 64.48	1		
68	65.68	17.60	65.61	17.89	65.53	18.17	65.45	1		
69 70	66.65 67.61	17.86 18.12	66.57	18.15	66.49	18.44	66.41	,1		
71	68.58	18.38	67.54	15.68	68 42	18.71	68 33	1		
72	69 55	18.64	69.46	18.94	69.38	19.24	69.30	1		
73	70.51	18.89	70.43	19.20	70.35	19.51	70.26	1		
74 75	71.48	19.15	71.39	19.46 19.73	71.31	19.78 20.04	71.22	2		
76	73.41	19.67	73.32	19.99	73.24	20 31	73 15	2		
77	74.38	19.93	74.29	20.25	74.20	20.58	74.11	2		
78 30	75.34 76.31	20.45	75.25 76.22	20 52	75.16 76.13	20.84 21.11	75.07 76.03	2		
79 80	77.27	20.71	77.18	21 04	77.09	21.38	77.00	2		
18	78.24	20.96	78.15	21.31	78.05	21.65	77 46	2		
82 83	79.21	21.22	79-11	21.57	79.02 79.98	21.91 22.18	78.92 79.88	2 2		
64	81.14	21.74	81.04	22.09	80 95	22 45	80 85	2		
85	82.10	22.90	82.01	22.36	81.91	22.72	81.81	2		
86 87	83.07 84.04	22.26	82.97	22.62	82.87	22.98	82 77	2		
88	85.00	22.52 22.78	83.94 84.90	23.15	83.84 84.80	23.25	83.73 -84.70	2		
89	85.97	23.03	85.87	23.41	85,76	23.78	85.66	2		
90	86.93	23.29	86.83	23.67	86 73	24.05	86.62	2		
91 92	87.90 88.87	23.55 23.81	87.80 88.76	23.94	87.69 88.65	24.32 24.59	87.58 88 55	2 2		
93	89.83	24.07	89.73	24.46	89.62	24.85	89.51	2		
94 95	90.80 91.76	24.33 24.59	90.69 91.65	24.72 24.99	90.58	25.12 25.39	90.47	2 2		
96	92.73	24.85	92.62	25.25	91.54	25.65	91.43	2		
97	93.69	25.11	_	25 51	93 47	25.92	93.36	2		
98	94-66	25.36	94.55	25.78	94 44	26.19 26.46	94 32	2 2		
100	96 59	25.62	95.51 96.48	26.04 26.30	95.40 96.36	26.72	95.28 96.25	2		
101	97-56	26.14	97 44	26.57	97-33	26.99	97.21	2		
102	98.52	16.40	98.41	26.83	98.29	27.26	98.17	2 2		
103	100.5	26.66 26.92	99-37	27.09 27.36	99 25	27.53	99.13	2		
105	101.4	27.18	101.3	27.62	101.2	28.06	101.1	2		
106	102.4	27.43	102.3	27.88	102.1	28.33	102.0	2		
107	103.4	27.69	103.2	28.4.f	103.1	28.59 28.86	103.0	2 2		
109	105.3	28.21	105.2	28.67	105.0	29.13	104.9	2		
110	106.3	28 47	106.1	28.93	106.0	29.40	105.9	2		
112	107.2	28.73	107.1	29.20 29.46	107.0	29.66 29.93	106.8	3		
413	109.1	29.25	109.0	29.72	108.9	30.20	108.8	3		
314	1.011	29.51	110.0	29.99	109.9	30.47	109.7	3		
116	112.0	30 02	111.0	30.25	111.8	30 73	110.7	3		
117	113.0	30.28	112.9	30.77	112.7	31.27	112.6	3		
1118	114.0	30.54	113.8	31.04	113.7	31.53	113.6	3		
1120	114.9	30.50	114.8	31.30	114.7	31.80	114.5	3		
1	Dep.	!at.	Dep.	Lat.	Dep.	Lut	Dep.	=		
ä		,,	4	5,7	30		15	•		
	74 DEGREES.									

E	1 37		1.5	57	30'		45'	
Dist	Lat.	Dep.	Lat.	Dep.	Lat.	Dep	Lat.	Dep.
-	0.96	0.28	0.96	0.28	0.96	0.28	0.96	0.29
2	1.92	0.55	1.92	0.56	1.92	0.57	1.92	0.58
3	2.88	0.83	2.88	0 84	2.88	0.85	2.87	0.86
4	3.85	1.10	3.84	1.12	3.84 4.79	I.14 I.42	3.83 4.79	1.15
5	4.81	1.38		1.68				1.73
6 7	5.77 6.73	1.65 1.93	5.76 6.72	1.96	5.75 6.71	1.70 1.99	5.75 6.70	2.02
8	7.69	2.21	7.68	2.24	7.67	2.27	7.66	2.31
9	8.65	2.48	8.64	2.52	8.63	2.56	8.62	2.59
10	9.61	2.76	9.60	2.80	9.59	2.84	9.58	2.88
11	10.57	3.03	10.56	3.08	10.55	3.12	10.53	3.17 3.46
12	11.54	3.31 3.58	11.52	3.36 3.64	11.51	3 41 3.69	11.49	3.75
13 14	12.50	3.86	13.44	3.92	13.42	3.98	13.41	403
15	14.42	4.13	14.40	4.20	14.38	4.26	14.36	4.32
16	15.38	4.41	15.36	4.48	15.34	4.54	15.32	4-61
17	16 34	4.69	16.32	4.76	16.30	4.83	16 28	4.90
18	17.30	4.96	17.28	5.04	17.26	5.11	17.24	5.19
19	18.26	5.24	18.24	5.32	18.22	5.40	18.19	5.48 5.76
20	19.23	5.51	19 20	5.60	19.18	5.68	19.15	
21	20.19	5.79 6.06	20.16	5.88	20.14	5.96 6.25	20.11	6.05
22 23	21 15	6.34	22.08	6 44	21.09	6.53	22.02	6.63
24	23.07	6.62	23.04	6. 🕶	23.01	6.82	22.98	6.92
25	24.03	6.89	24 00	7.00	23.97	7.10	23.94	7.20
26	24.99	7.17	24.96	7.28	24.93	7.38	24.90	7.49
27	25.95	7.44	25.92	7.56	25.89	7.67	25.85	7.78
28	26.92	7.72	26.88	7.84	26.85	7.95	26.81	8.07 8.36
29 30	27.88 28.84	7.99 8.27	27.84 28.80	8.12 8.39	27.81 28.76	8.24 8.52	27.77 28 73	8.65
				8.67		8.80	29.68	8.93
31	29.80 30.76	8.54 8.82	29.76 30.72	8.95	29.72 30.68	9.09	30.64	9.22
33	31.72	9.10	31.68	9.23	31.64	9.37	31.60	9.51
34	32.68	9.37	32.64	9.51	32.60	9.66	32 56	9.80
35	33 64	9 65	33.60	9.79	33 56	9.94	33.52	10.09
36	34.61	9.92	34.56	10.07	34.52	10.22	34-47	10.38
37 38	35.57	10.20	35.52 36.48	10.35	35.48	10.51	35.43	10.66
39	36.53 37-49	10.47	37.44	10.03	36.44 37.39	10.79	36.39 37-35	11.24
40	38.45	11 03	38.40	11.19.	38.35	11.36	38.30	11.53
41	39.41	11.30	39.36	11.47	39-31	11.64	39.26	11.82
42	40.37	11.58	40.32	11.75	49.27	11.93	40.22	12.10
43	41.33	11.85	41.28	12.03	41.23	12.21	41.18	12-39
44	42.30	12.13	42.24	12.31	42.19	12.50	42.13	12.68
45	43.26	12.40	43.20	12.59	43.15	12.78	43.09	12.97
46	44.22	12.68	44.16	12.87	44.11	13.06	44.05	13.26
47 48	45.18	12.96	45.12 46.08	13.15	45.06 46.02	13.35	45.01 45.96	13.83
49	47.10	13.51	47.04	13.71	46.98	13.92	46.92	14.12
50	48 06	13.78		13.99	47 94	14.20	47.88	14.41
51	49.02	14.06	48.96	14.27	48.90	14.48	48.84	14.70
52	49.99	14.33	49.92	14.55	49.86	14.77	49.79	14.99
53	50.95	14.61	50.88	14.83	50.82	15.05	50.75	15.27
54 55	51.91 52 87	14.88		15.11	51.78	15.34	51.71 52.67	15.56 15.85
56				15 39	52.74	15.62		16.14
57	53.83 54.79	15.44	53.76 54.72	15.67	53.69 54.65	15.90	53.62 54.58	16.43
58	55.75	15.99	55.68	16.23	55.61	16.47	55.54	16.72
59	56.71	16.26	56.64	16.51	56.57	16.76	56.50	17.00
60	57.68	16.54	57.60	16.79	57-53	17.04	57.45	17.29
ایدا	Dep	Lat.	Dep.	Lat.	Dep	Lat.	Dep.	Lat.
Dist.	0/		45/		30'		15/	

15	1 0	0′		51	30)'	45'	
Dia	Lat	Dep	Lat.	Dep.	Lat	Dep.	Lat	Dep.
61	58.64	16.81	58.56	17.07	58.49	17.32	58.41	17.58
62	50.60	17.09	59.52	17.35	59.45	17.61	\$9.37	17.87
63 64	61.52	17.37	60.48	17.63	60.41	17.89	60.33 61.28	18.16
65	62 48	17.92	62.40	18.19	62.32	18.46	62.24	18.73
66	63.44	18.19	63.36	18.47	63.28	18.75	63.20	19.02
67		18.47	64.32	18.75	64.24	19.03	54.16	19.31
68	65.37 66.33	18.74	65.28	19.03	65.20	19.31	65.11	19.60
70	67.29	19.29	67.20	19.59	67 12	19.88	67.03	20.17
71	68.25	19.57	68.16	19.87	68.08	20.17	67.99	20.46
72	69.21	1985	69.12	20 15	69.04	20.45	68.95	20 73
73	70.17	20.12	70.08	20.43	69.99	20.73	70.86	21.04
74	71.13 72.09	20.40	71.04	20.71	70.95	21.30	71.82	21.33
76	73.06	20.95	72.96	21.27	72.87	21.59	72.78	21,90
77	74 02	31 22	73.92	21.55	73.83	21.87	73.73	22.19
78	74.98	21 50	74.88	21.83	74-79	22.15	74-69	22.48
79 80	75.94 76.90	21.78	75 84 76.80	22.11	75.75 76.71	22.44	75.65	22.77
81	77.86	22-05		22.39	77.66	23.01	77.56	23.06
82	78.82	22.33	77.76	22.95	78 62	23.29	78.52	23.34 23.63
83	79.78	22.88	79.68	23.23	79.58	. 23.57	79.48	23.92
84	80.75	23.15	80.64	23.51	80.54	23.86	80.44	24.21
85	81.71	23.43	81.60	23.79		.24.14	81.39	24.50
86 87	82.67 83.63	23.70	82.56 83 52	24.07 24.35	82.46 83.42	24.43 24.71	82.35 83.31	24.78 25.07
88	84 (9	24.26	84.48	24.63	84.38	24.99	84.27	25.36
89	85.55	24.53	85.44	74.90	85.34	25.28	85.22	25.65
90	86.51	24.81	86.40	25.18	86.29	25.56	86.18	25.94
91	87.47 88.44	25.08	87.36 88.32	25.46	87.25 88.21	25.85 26.13	87 14	26.23
93		25.36 25.63	89.28	25.74 26 02		26.41	89.05	26.51 26 80
94	9Ó 36	25.91	90.24	26.30	90.13	26.70	90.01	27.09
95	91.32	26.19	91.20	26.58	91.09	26.98	90.97	27.38
96	92-28	26.46	92.16	26.86	92.05	27.27	91.93	27 67
97 98	93.24 94 20	26.74	93.12	27.14 27.42	93.96	27.55 27.83	92.88	27.96 28.24
99	95.16	27.29	95.04	27.70	61.92	28.12	94 80	28.53
100	96.13	27.56	96.01	27.98	95.88	28.40	95.76	28.82
101	97 09	27.84	90.97	28.26	96.84	28.09	96.71	29.11
102	98.05	28.12	97 93 98.8g	28.54 28.82	97.80 98.76	28.97 29.25	97.67	29.40 29.68
104	99.97	28.67	99.85	29.10	99 72	29.54	99.59	29.97
105	100.9	28.94	100.8	29.38	100.7	29 82	100.5	30.26
106	101.9	29.22	8.101	29.66	101.6	30.11	101.5	30.55
108	102.9	29.49	102.7	29.94 30.22	102.6	30.39 30.67	102.4	30.84
109	103.8	30.04	103.7	30.22	103.6	30.07	104.4	31.13
110	105.7	30.32	105 6	30.78	105 5	31.24	105.3	31.70
111	106.7		106.6	31.06	106 4	31.53	106.3	31.99
1112		30 87	107.5	31.34	107.4	31.81	107.2	32 28
1113	108.6	31.15		31.62	108.3	32.09 32.38	108.2	32.57 32.85
115	-	31.70	110.4	32.18	110.3	32.66	110.1	33.14
116		31.97	111.4		111.2	32.95	711.1	33.43
117	112.5	32 25	112.3	32.74	112.2	33.23	112.0	33.72
1118	113.4	32.53 32.80	113.3	32.02	113.1	33.80	113.0	34.01
120		,33.08	• -	33 30 33.58	115.1	34.08	114.0	34.30 34.58
1	D.p.	Lat.	Dep.	Lat.	Dep.	Lat	Dep.	Lat.
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1	Lat.	Dep.		Dep.	-	Dep.	Lat.	Dep.
1 :	0.96	0.29	0.96	0.30	1.91	0.30 0.60	0.95	0.30
3	2.87	0.88	2.87	0.89	2.86	0.90	2.86	0.91
1 4	3.83	1.17	3.82	1.19	3.81	1.20	3.81	1.22
Š	4.78	1.46	4.78	1.48	4-77	1 50	4.76	1.52
6	5.74	1.75	5.73	1.78	5.72	1.80	5.71	1.83
7 8	7.65	2.05 2.34	6.69 7.64	2.08	7.63	2.10 2.41	7.62	2.13
1. 9	8 61	263	8 60	2.67	8.58	3.71	8.57	2.74
10	9.56	292	9.55	2.97	9.54	3.01	9.52	3.05
111	10.52	3.22	10.51	3.26	10.49	3.31	10.48	3.35
12	11.48	3.51	11.46	3.56	11.44	3.61	11.43	3.66
13	12.43	3.80 4.09	13.37	3.86	12.40	3.91 4.21	13.33	3.96 4.27
14	13.39	4-39	14.33	445	14-31	4.51	14.29	4-57
16	15.30	4.68	15.28	4.74	15.26	4.81	15.24	4.88
17	16.26	4-97	16.24	5.04	16.21	ğ, 11	16.19	5.18
18	17.21	5.26	17.19	5.34	17.17	5.41	17-14	5 49
19	18.17	5.56	18 15	5.63	18.12	6.01	18.10	5.79 6 10
20	19.13	_	20.06	6.23	20 03	6.31	20.00	6-40
21 22	20.08	6.14	21 01	6.52	20.98	6.62	20.95	6.71
23	22.00	6.72	21.97	6.82	21.94	6.92	21.91	7.01
24	22.95	702	22.92	7.12	22 89	7 22	22.86	7.32
25	23-91	7.31	23.88	7.41	23.84	7.52	23.81	7.62
26	2486	7.60	24.83	7.71 8.01	24.80	7.82	24.76 25.71	7.93 8.23
27 28	2582	8.19	25.79 26.74	8.30	25.75	8.42	26.67	8.54
29	27.73	8.48	27.70	8.60	27.66	8.72	27.62	8.84
30	28.69	8.77	28.65	8.90	28.61	9.02	28.57	9.25
31	29.65	9.06	29.61	9.19	29.57	9.32	29.52	9-45
32		9.36	30 56	9.49	30.52	9.62 9.92	30.48 31.43	9.76 10.06
33 34	31.56	9.65	32-47	9.79	31.47	10.22	32.38	10.37
35	33-47	10.23	33-43	10.38	33.38	10.52	33.33	10.67
36	34-43	10.53	34.38	10.68	34-33	10 83	34.29	10.98
37	35.38	10.82	35.34	10.97	35.29	11.13	35.24	11.28
38	36.34	11.11	36.29 37.25	11.27	36.24 37-20	11.43	36.19	11.58
39 40	38.25	11.69	38 20	11.86	38.15	12.03	38.10	12.19
41	39.21	11.63	39.16	12.16	39.10	12.33	39.05	12 50
42		12.28	40.11	12 45	40.06	12 63	40.00	12.80
43	41.12	12 57	41.07	12.75	41.01	12.93	40.95	13.11
1 44	42.08	12.86	42.02 42.98	13.05	41.96 42.92	13.23 13.53	41.91	13.42
45	43.03		43.93	13.64	43.87	13.83	43.81	14.02
47	43.99	13.45	44.89	13.94	44.82	14-13	44.76	14-33
48	45.90	14.03	45.84	14.23	45.78	14.43	45.72	14.63
49	46.86	14.33	46.80	14.53	46.73	14.73	46.67	14-94
50		14 62	47.75	14.83	47-69	15.04	47.62	15.24
51 52	48.77	14.91	48.71 49.66	15.12	48.64 49.59	15.34 15.64	48.57 49.52	15.55 15.85
53	50 68	15.50	50.62	15.72	50.55	15.94	50.48	16.16
54	51.64	15.79	51.57	10.01	51.50	16 24	51.43	16.46
55	52.60	16.08		16.31	52.45	16.54	52.38	16.77
56	53-55	16.37	53.48	16.61	53-41	16.84	53-33	17.07
57 58	54-51	16.67 16.96		16 90 17.20	54.36 55.32	17.14 17.44	54·29 55·24	17.38 17.68
59	55.47 56.42	17.25	56.35	17.50	56.27	17.74	56.19	17.99
60	57.38	17-54	57.30	17.79	57.22	18.04	57-14	18.29
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Dist.	Lat	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
61	58.33	17.83	58.26	18.09	58.18	18 34	58.10	18.60
62	59.29	18.13	59.21	18.39 18 68	59.13	18.64 18.94	59.05 60.00	18.90
63 64	60.25	18.42	60.17	18.98	60.08	19.25	60.00	19.21
65	62,16	19.00	62.08	19.28	61.99	19.55	61.91	19.82
66	63.12	19.30	63.03	19.57	62.95	19.85	62.86	20.12
67 68	65.03	19.59	63.99 64.94	19.87 20.16	63.90 64.85	20.15 20.45	63.81 64.76	20.43 20.73
69	65.99	20.17	65.90	20.46	65.81	20.75	65.72	21.04
70	66.94	20 47	66.85	20.76	66.76	21.05	66.67	21.34
71	67.90	20.76	67.81	21.05	67.71	21.35	67.62	21.65
72 73	68.85 69 81	21.05	68.76 69.72	21.35 21.65	68.67 69.62	21.65	68.57	21.95
74	70.77	21.64	70.67	21.94	70.58	22.25	70.48	22.56
75	71.72	21.93	71.63	22.24	71.53	22.55	71.43	22 86
76	72 68	22.22	72 58	22.54	72.48	22.85	72.38	23.17
77	73.64 74.59	22.51 22.81	73·54 74·49	22.83 23.13	73-44 74-39	23.15 23.46	73.33	23.47
79	75.55	23.1Q	75.45	23.43	75.34	23.76	75.24	24.08
80	76.50	23.39	76.40	23.72	76.30	24.06	76.19	24.39
81 82	77.46	23.68	77.36 78.31	24.02	77.25	24.36 24.66	77.14	24.69 25.00
83	78.42 79.37	23.97 24.27	79.27	24.32 24.61	78.20 79 16	24.96	79.05	25.30
84	80.33	24.56	80.22	24.91	11.08	25.26	80.00	25.61
85	81.29	24 85	81.18	25.21	81.07	25.56	80.95	25.91
86 87	82.24	25.14	82.13 82.00	25.50	82 02	25.86 26.16	81.91 82.86	26.22 26.53
88	83 20 84.15	25.44 25.73	84.04	26.10	82.97 83 93	26.46	83-81	26.83
89	85.11	26.02	85.00	26.39	84.88	26.76	84.76	27.13
90	86.07	26.31	85.95	26.69	85.83	27.06	85.72	27.44
91 92	87.02 87.98	26.61 26.90	86.91 87.86	26:99 27.28	86.79 87.74	27.36 27.66	86.67 87.62	27.74
93	88.94	27.19	88.82	27 58	88.70	27.97	88.57	28.35
94	89.89	27.48	89.77	27.87	89.65	28.27	89.53	28.66
95	90.85	27.78	90.73	28.17	90.60	28.57	90.48	28.96
96 97	91.81	28.07 28.36	91.68 92.64	28.47 28.76	91.56 92.51	29.17	91.43	29.27
98	93.72	28.65	93.59	29.06	93.46	29.47	93.33	29.88
100	94.67	28.94	94-55	29.35	94.42	30.07	94.29	30.18 30.49
101	95.63	29.24	95.50	29.65	95.37	30.37	95.24	30.79
102	96.59 97.54	29.53	96.46 97.41	29.95 30.25	96.33	30.67	97.14	31.10
103	98.50	30.11	98.37	30.54	98.23	30.97	98.10	31.40
104	99.46 100.4	30.41	99.32	30.84 31.14	99.19	31.27	99.05	31.71
106	101.4	30.70	101.2	31 43	101.1	31.87	101.0	32.32
107	102.3	30.99 31.28	102.2	31.73	102.0	32.18	101.9	32.62
108	103.3	31.58	103.1	32.03	103.0	32.48	102.9	32.93
110	104.2	31.87 32 16	104-1	32.32 33.62	104.9	32.78	103.8	33.23 33.54
111	106.1	32.45	106.0	32.92	105.9	33.38	105.7	33.84
112	107.1	32.73		33.21	106.8	33.68	106.7	34-14
113	108.1	33.04	107.9	33.51	107.8	33.98 34.28	107 6	34.45
1115	110.0	33.33 33.62	108.9	33.81 34.10	108.7	34.58	109.5	34.75 35.06
416	110.9	33.92	110.8	34-40	110.6	34.88	110.5	35.36
117	111.9	34.21	111.7	34.70	111.6	35.18	111.4	35.67
110	112.8	34-50	112.7	34-99	112.5	35.48	112.4	35.97 36.28
120	114.8	34-79 35.08	113.6	35.29 35.59	114.4	36.08	114.3	36 58
ندا	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
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Di st.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0.95	0.31	0.93	0.31	0.95	0.32	0.95	0.32
3	2.85	0.62	1.90	0.94	2.85	0.95	1.89 2.84	0.64 0.96
4	3.80	1.24	3.80	1.25	3.79	1.27	3-79	1.29
_5	4.76	1.55	4-75	1 57	_4·74 5.60	1.59	473	1.61
6 7	5.7 I 6.66	1.85	5.70 6.65	1.88 2.19	6.64	1.90	5.68 6 63	1.93 2.25
g g	7.61	2.47	7.60	2.51	7.59	2 54	7.58	2.57
9	8.56	2.78	8.55	2.82 3.13	8.53 9.48	2.86 3.17	8.52 9.47	2.89 3.21
10	9.51	3.40	10.45	3.44	10.43	3 49	10.42	3.54
12	11.41	371	11.40	3.76	11.38	18.8	11.36	3.86
13	12.36	4.02	12.35	4.07 4.38,	12 33	4.13 4.44	12.31	4.18
14	13.31	4.33 4.64	13.30	4.70	14.22	4.76	13.26	4.82
16	15 22	4.94	15.20	5.01	15.17	5.08	15.15	5.14
17	16.17	5 25	16.14	5.32	16 12	5 39	16.10	5.46
18	17 12	5.56 5.87	17.09	5.64 5.95	17 07	5.71 6.03	17.04	5.79 6.11
20	19.02	6.18	18.99	6.26	18.97	6 35	18.94	6.43
21	19.97	6 49	19 94	6.58	1991	6.66	19.89	6.75
22	20.92	6.80 7.11	20.89	7.20	20.36	6.98 7.30	20.83	7.07
23 24	21 87 22 83	7.42	21 84	7.52	22.76	7.62	22 73	7.71
25	23.78	7.73	23.74	7.83	23.71	7.93	23.67	8.04
26	24.73	8.03	24.69	8.14	24 66	8.25	24.62	8.36 8.68
27 28	25.68 26.63	8.34 8.65	25 64 26.59	8.46	25.60 26.55	8.57 8.88	25.57 26.53	9.00
29	27.58	8.96	27.54	9.08	27.50	9.20	27.46	9.32
30	28.53	9.27	28.49	9.39	28 45	9.52	28.41	9.64
31	29.48	9.58	29.44	9.71	29.40	9.84	29.35 30.30	9.96
32 33	30.43	9.89	30.39	10.33	30 35	10.47	31.25	10.61
34	32.34	10.51	32.29	10.65	32.24	10.79	32.20	10.93
35	33.29	10.82	33.24	10.96	33.19	11.11	33.14	11.25
36 37	34.24 35.19	11.12	34.19	11.27	34.14 35.09	11.42	34.09 35.04	11.57
38	36.14	11.74	36.09	11.90	36.04	12.06	35.98	12.21
39	37.09	1205	37.04	12.21	36.98	12.37	36.93 37.88	12.54
40	38.04	12.36	37-99	12.53	37 93	1301	38.82	13.18
41	38.99 39.94	12.67	38.94	13.15	39.83	13.33	39.77	13.50
43	40.90	13.29	40.84	13.47	40.78	13.64	40.72	13.82
44	41 85	13.60 13.91	41.79	13.78	41.73 42.67	13.96	41.66	14.14
46	43.75	14.21	43 69	14.41	43.62	14.60	43.56	14.79
47	44.70	14.52	44.64	14.72	44.57	14.91	44.51	15.11
48	45.65	14.83	45.59	15.03 15.35	45.52	15.23	45.45 46.40	15.43
49 50	46.60 47.55	15.14	46.54 47 49	15.66	46.47 47.42	15.87	47-35	16.07
51	48.50	15.76	48.43	15.97	48.36	16.18	48.29	16.39
52	49.45	16.07	49.38	16.28	49.31	16.50	49.24	16.71
53 54	50.41 51.36	16.38 16 69	50.33	16.60	50 26 51.21	16.82	50 19	17.04
55	52.31	17.00	52.23	17.22	52.16	17.45	52.08	17.68
56	53.26	17.31	53.18	17.54	53.11	17.77	53.03	18.00
57	54.21	17.61	54.13	17.85	54.05	18.09 18.40	53.98 54.92	18-32 18.64
58 59	55.16 56.11	17.92 18.23	55.08 56 03	18.16	55.00 55.95	18.72	55.87	18.96
60	57 06	18.54	56.98	18.79	56.90	19.04	56.82	19.29
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1		Dep.	Lat.	Dep.	Lat.	Dep	<u>Lut</u>	De	
61	58.01	18.85	57 93 58.88	119.10	57.85	19.36	57.76	19.6	
63		19.47	59.83	19.42	59.74	19.99	· 58.71	19.9	
64		19.78	60.78	20.04	60.69	20.31	60.60	10.5	
65	61.82	20.09	61.73	20.36	61.64	20.62	61.55	20.8	
66	62.77	20.40	62.68	20 67	62.59	20.94	62 50	21.2	
68	63.72	20.70	63.63	20.98	63.54	21.26	63.44	21.5	
69	64.67	21.01	64.58	21.30	64 49	21.58	64.39 65.34	21.8	
70		21.63	66.48	21.92	66.38	22.21	66.29	22.5	
71	67.52	21.94	67.43	22 23	67.33	22.53	67.23	22.8	
72	68.48	22.25	68.38	22.55	68.28	22.85	68.18	23 1.	
73	69.43	22 56	69.33	22.86	69.23	23.16	, 69 13	23.4	
74	70.38	22.87	71 23	23.17 23.49	70.18	23 48 23.80	79.07 71.02	23.7	
76	72.28	23.49	72.18	23.80	72.07	24.12	71.97	24.4	
77	73-23	23 79	73.13	24.11	73.02	24 43	7291	24.7	
78	74.18	24.10	74.08	24.43	73.97	24.75	73.86	25.0	
79 80	75.13	24.41	75.03	24.74	74-92	25.07	7481	25.3	
1	76.08	24.72	75.98	25.05	75.87	25.38	75.75	25.7	
81	77.64	25.03 25.34	76.93 77.88	25.37 25.68	76.81	26.70	76.70 - 77 65	26.0.	
83	78.94	25.65	78.83	25.99	78.71	26.34	78.60	26 6	
84	79.89	25.96	79.77	26.31	79.66	26.65	79-54	27.C	
85	80.84	26.27	80.72	26 62	80.61	26 97	80.49	27 3:	
86	81.79	26.58	81.67	26.93	81.56	27.29	81 44	27.6	
87 88	82 74 83.60	26.88	82.62	27.25	82 50	27.61 27.92	82.38	27.9	
89	84.64	27.50	84 52	27.87	84.40	28.24	84.28	28 6	
90	85.60	27.81	85.47	28 18	85.35	8 56	8 g. 22	28.9	
91	86 55	28 12	85.42	28.50	86.30	28.87	86.17	29.2	
92	87.50	28.43	87.37	28 81	87.25	29.19	87.12	29.5	
93	88 45 89.40	28.74 29.05	88.32 89.27	29 44	88 19 89.14	29.51	88.06	30.2	
95		29.36	90.23	29.75	90.09	30.14	89 96	30.5	
96	91 30	29.67	91.17	30.06	91.04	30.46	90.91	30.81	
97	92.25	29.97	92.12	30.38	91.99	30.78	91.85	31.11	
98	93.20	30.28	93.07	30.69	92.94	31.10	92.80	31.50	
100	94 15	30.90	94.02 9+97	31.32	93.88 94.83	31.41 31.73	93.75 94 69	31.8:	
101	96.06	31.21	95.92	31.63	95.78	32.05	95.64	32.40	
102	97.01	31.52	96.87	31.94	96.73	32.36	96.59	32.7	
103	97.96	31.83	97.82	32.26	97.68	3268	97-53	33 11	
104	98.91	32.14	98.77	32.57	98.63	33.00	98.48	33.41	
105	99.86	32.45	99.72	32.88	99 57	33.32	99-43	33.75	
106	8.101	32.76 33.06	100.7 101.6	33.20 33.51	100.5	33.63 33.95	100.4	34. 0 7	
108	102.7	33-37	102.6	33.82	102.4	34 27	102.3	34.71	
109	103.7	33.68	103.5	34.13	103 4	34-59	103.2	35-Q4	
110	104.6	33.99	1045	34.45	104 3	<u>34-90</u>	104.2	35 3	
111	105.6	34.30	105.4	34.76	105.5	35.22 35·54	105.1	3 Ş. 4	
112	106.5	34.61 34.92	106.4	35.07 35.39	106.2	35·54 35.86	106.1	36. 4 36. 3	
114	108.4	35.23	108.3	35.70	108.1	36.17	108.0	36.4	
115	109.4	35.54	109.2	36.01	109 1	36.49	108 9	36. g	
116	110.3	35.85	I 10.2	36.33	110.0	36.81	109.8	37.	
117	111.3	36.16	111.1	36.64	111.0	37.12	1 10.8	37.	
119	112.2	36.46 36.77	113.1	36.95 37.27	111.9	37-44 37-76	112.7	37. 9 38 4	
120		37.08	114.0	37.58	113.8	38.08	113.6	38	
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-2	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep-
1	0.95	0.33	0.94	0.33	0.94	0.33	0.94	0.34
2	1.89	0.65	1.89	0.66	1.89	0.67	1.88	0.68
3	2.84	0.98	2.83	0.99	2.83	1.00	2.82	1.01
4 5	3.78	1.30	3.78 4-72	1.65	3 77 471	1.34	3.7.6 4.71	1.55
- 6	4-73 5 67		5.66	1.98	5.06	2.00	5.65	
7	6.62	1.95	6.6t	2.31	6.60	2-34	6.59	2.03
8	7.56	2.60	7.55	2.64	7.54	2.67	7.53	2.70
9	8.51	2.93	8.50	2.97	8.48	3.00	8.47	3.04
10	9.46	3.26	9.44	3.30	9.43	3 34	9-41	3.38
11	10.40	3.58	10 39	3.63	10.37	3.67	10-35	3.72
13	11.35	3.91 4.23	11.33	3.96 4.29	11.31	4.34	11.29	4.06
14	12.29	4.56	13.22	4.62	13.20	4.67	13.18	4-39 4-73
15	14.18	4.88	14.16	4 95	14.14	5.01	1412	5.07
16	15.13	5.21	15.11	5.28	15.08	5.34	15.06	5-41
17	1607	5.53	16.05	5.60	16.02	5.67	16.00	5.74
41	17.02	5.86	16.99	5.93	16.97	6.01	16.94	6.08
19 20	17.96 18.91	6.19	17.94 18 88	6.26 6.59	17 91 18.8 5	,6.34 6.68	17.88	6.76
21.	19.86	6 84	19 83	6.92	19.80	7.01	19.76	7.10
22	20.80	7.16	20.77	7.25	20.74	7.34	20.71	7.10
23	21.75	7.49	21.71	7.58	21.66	7.68	21.65	7.77
24	22.69	7.81	22.66	7.91	22.62	8.01	22.59	8.11
25	23.64	8.14	23.60	8.24	23.57	8.35	23.53	8.45
26	24.58	8.46	24-55	8.57	24.51	8.66	34.47	8.79
27 28	25.53 26.47	8.79 9.11	25.49 26.43	8.90 · 9.23	25.45 26.39	9.01 9.35	25.41 26.35	9.12 9.46
29	27.42	9.44	27.38	9.56	27.34	9.68	27.39	9.80
30	28.37	9.77	28.32	9.89	28.28	10.01	28.24	9.14
31	29.31	10.09	29.27	10.22	29.22	10-35	29.18	10.48
32	30.26	10.42	30.21	10.55	30.16	10.68	30.12	18.01
33 34	31.20	10.74	31.15	11.21	31.11 32.05	11.02	31.06	11.15
35	33.09	11 39	33.04	11.54	32.99	11.66	32.94	11.83
36	34-04	11.72	33 99	11.87	33-94	12,02	33.88	12.17
37	34.98	12.05	34-93	12.20	34.88	14.35	34.82	12.50
38	35 93	12.37	35.88	12.53	35.82	12.68	35.76	23.84
39 40	36.88 37.82	12.70	36.82 37.76	12.86	3 9. 76	13.02	36.73	13.18
41			38.71	<u> </u>	38.65	13.35	37.65	13.52
42	38.77 39.71	13-35	39.65	13.52	39-59	13.69	38.59 39.53	13.85 14.19
43	40.66	14.00	40.60	14.18	40.53	14.35	40.47	14-53
44	41.60	14.33	41.54	14.51	41.48	:4 69	41.41	14.87
45	42.55	14.65	43.48	14.84	42.42	15.01	48.35	15.21
46	43.49	14.98	43.43	15.17	43.36	15.36	43-29	15.54
47 48	44-44 45.38	15.30	44-37 45-32	15.50	44.30	15.69	45.18	15.88 16.22
49	46.33	15.95	46.26	16.15	46.19	16.36	46.12	16.56
50	47.28	16.23	47.20	16.48	47.13	16.69	47.06	16.90
51	48 22	16.60	48.15	16.81	48.07	17.02	.48.00	17.33
52	49.17	16 93	49.09	17.14	49.02	17.36	48.94	17.57
5 3	50.11	17.26 17.58	50.04	17.47	49.96	17.69	49.88	17.91
54 55	52.00	17.91	50.98 51.92	17.80	50.90	18.36	50.82 51.76	18.25 18.59
56	52.95	18.23	52.87	18.46	52.79	18.69	5271	18.92
57	53.89	18.56	53.81	18.79	53.73	19.03	53.65	19.26
58	54.84	18.88	54.76	19.12	54-67	19.36	54-59	19.60
59 60	55.79	19.21	55.70	19.45	55.62	19.69	55.53	19.94
	56.73 Dan	19.53	56.65	19.78	56.56	20.03	56.47	20.28
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62 59-57 20.51 59.48 20.77 29.39 21.03 59.39 21.29 60.45 21.65 60.45 21.65 60.45 21.65 60.45 21.65 60.45 21.65 60.45 21.65 60.45 21.65 60.45 21.65 60.45 21.65 60.45 21.65 60.45 21.65 60.45 21.65 60.45 21.65 60.45 21.65 60.45 21.65 60.45 21.65 60.45 21.65 60.45 21.65 21.	1				1				1	
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67 62:35 a1.81 63.25 a2.09 63.16 a2.77 63.06 a2.64 68 63.00 a2.64 66.40 a2.70 64.00 a2.98 66.69 f6 f1.44 a2.46 65.14 a2.75 65.04 a7.03 64.94 a2.33 f6 f6.94 a2.79 66.09 a2.79 66.09 a2.79 66.09 a2.79 66.09 a2.79 66.09 a2.79 66.09 a2.79 66.09 a2.79 66.09 a2.79 66.09 a2.79 66.09 a2.79 66.09 a2.79 66.09 a2.79 66.09 a2.79 66.09 a2.79 67.0 66.19 a2.79 68.82 a2.67 68.81 a4.37 68.71 a4.69 77 a2.69 a2.70 68.81 a4.37 68.71 a4.69 77 74.00 a2.77 67.0 69.65 a4.40 69.76 a2.70 69.65 a2.40 77 72.69 a2.99										
68 64 30 22.14 64.20 22.42 64.10 22.70 64.00 22.98 69 65.24 22.46 66 14 12.75 65.04 21.03 64.40 23.32 70 66.09 22.79 66.09 23.79 66.09 23.74 65.08 23.65 65.98 23.27 65.88 23.65 71 67.13 23.12 67.03 23.44 66.93 24.07 68.81 24.37 68.71 24.07 68.02 23.74 67.87 24.03 67.76 24.33 24.07 74.69 23.74 69.02 24.09 69.86 24.07 69.65 24.07 69.65 25.01 75.70 91 24.42 70.81 24.73 70.70 70.70 71.86 24.74 71.75 25.06 77.00 22.74 70.80 25.07 72.69 25.34 70.70 57.71 72.80 25.07 72.69 25.39 72.58 25.07 72.47 86.02 77.70 15.71 74.53 26.05 72.58 25.07 72.47 86.02 72.58 25.07 72.59 25.04 70.59 25.24 70.15.71 74.53 26.05 72.58 25.07 72.47 86.02 72.59 25.04 70.15.71 74.53 26.05 72.59 25.04 70.15.71 74.53 26.05 72.59 25.04 70.15.71 74.53 26.70 75.29 27.03 25.37 72.59 27.03 25.37 72.47 26.77 72.42 26.70 75.29 27.03 27.37 72.47 26.77 72.42 26.70 77.24 27.73 27.73 27.74 26.77 77.24 27.73 27.73 27.74 26.77 77.24 27.73 27.73 27.73 27.73 27.74 27.24 27.25 27.03 27.73 27.74 27.25 27.03 27.73 27.74 27.24 27.25 27.03 27.73 27.37 77.18 27.73 27.										
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72 68.08 23.44 67.97 23.74 67.87 24.03 67.76 24.33 69.02 23.77 68.92 24.07 68.81 24.37 68.97 24.09 69.85 24.07 68.81 24.37 69.97 24.09 69.85 24.07 68.81 24.37 69.55 24.07 79.91 24.42 70.81 24.73 70.70 25.04 70.59 25.34 70.75 70.91 24.42 70.81 24.73 70.70 25.04 70.59 25.34 77.80 25.07 72.60 35.39 72.58 25.70 72.47 80.23 73.64 25.72 73.53 26.04 71.43 63.63 72.64 26.05 73.64 26.05 73.64 26.05 73.64 26.05 73.64 26.05 75.64 26.05 26.	70									
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113 106.8 36.79 106.7 37.26 106.5 37.72 106.4 38.18 114 107.8 37.11 107.6 37.58 107.5 38.05 107.3 38.52 115 108.7 37.44 108.6 37.91 108.4 38.29 108.2 38.86 109.7 37.77 109.5 38.54 109.3 38.72 109.2 39.20 117 110.6 38.09 110.5 38.57 110.3 39.06 110.1 39.54 116.6 38.42 111.4 38.90 111.2 39.39 111.1 39.87 112.5 38.74 112.3 39.23 112.2 39.72 112.0 40.24 112.5 38.74 112.3 39.56 113.1 40.06 112.9 40.55 40.5				109.7	36.93	105.6	37.39	105.4	37.85	
115 108.7 37.44 108.6 37 91 108.4 38.79 108.2 38.86 116 109.7 37.77 109.5 38.24 109.3 38.72 109.2 39.20 117 110.6 38 09 110.5 38.57 110.3 39.06 110.1 39.54 118 111.6 38.42 111.4 38.90 111.2 39.39 111.1 39.87 119 112.5 38.74 112.3 39.22 112.2 39.72 112.0 40.21 120 113.5 39.07 113.3 39.56 113.1 40.06 112.9 40.55 120 Dep. Lat. Dep Lat. Dep. Lat. Dep. Lat. Dep. Lat.	113	106.8								
116 109-7 37.77 129.5 38.24 109.3 38.72 109.2 39.20 117 110.6 38.09 110.5 38.57 110.3 39.06 110.1 39.54 118 111.6 38.42 111.4 38.90 111.2 39.39 111.1 39.87 120 113.5 38.74 112.3 39.22 112.2 39.72 112.0 40.22 120 113.5 39.07 113.3 39.56 113.1 40.06 112.9 40.55 2										
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7	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
-	0.94	0.34	0.94	0.35	0.94	0.35	0.94	0.35	
2	1.88	0.68	1.88	0.69	1.87	0.70	1.87	2.71	
3	2.83 3.76	1.37	2.81 3.75	1.04	2.81 3.75	1.05	2.81 3.74	1.06	
4	4.70	1.71	4.69	1.73	4:68	1.75	4.68	1.77	
6	5.64	2.05	5.63	2.08	5.62	2.10	5.61	2.13	
7 8	6.58	2.39	6.57	2.42	6.56	2.45	6.55	2.48	
	7 53	2.74	7.51	2.77	7.49	2.80	7.48	2.83	
.9	8.46 9.40	3.08	8.44 9.38	3.12	8 43	3 15 3.50	9.35	3.19	
10		3.76	10.32	3.46	9.37	3.85	10.29	3.54	
12	10.34	4.10	11.26	4.15	11.24	4.20	11.22	4-25	
13	12,22	4.45	12.20	4.50	12.18	4-55	12.16	4-61	
14	13.16	4-79	13.13	4.85	13.11	4.90	13.09	4-96	
15	14.10	5.13	14.07	5.19	14.05	5.25	14.03	:5.31	
16	15.04	5.47 5.81	15.01	5.54 5.88	14.99	5.60	14 96 15.90	5.67 6.02	
17.	15.97	6.16	16.89	6.23	16.86	5.95 6.30	16.83	6.38	
19	17.85	6.50	17.83	6.58	17.80	6.65	17.77	6.73	
30	18.79	6 84	18.76	6.92	18.73	7.00	18.70	7.09	
21	19.73	7.18	19.70	7 27	19.67	7 35	19.64	7-44	
22	20.67 21.61	7.52 7.87	20.64	7.61 7.96	20.61 21.54	7.70 8.05	20.57 21.51	7-79 8.15	
23 24	22.55	8.21	23.52	8.31	22.48	8.40	22.44	8.50	
25	23.49	8.55	23.45	8.65	23.42	8.76	23.38	8.86	
26	24 43	8.89	24.39	9.00	24.35	9.11	24 31	9.21	
27	25.37	9.23	25.33	9.35	25.29	9.46	25.25	9.57	
28	26.31	9.58	26.27	9.69 10.04	26.23	9.81	26.18	9.92	
29 30	27.25 28.19	9 92	27.27	10.04	27.16 28 10	10.51	27.12 28.05	10.27	
31	29.13	10.60	29.08	10.73	29.04	10.86	28.99	10.98	
32	30.07	10.94	30.02	11.08	29.97	11.21	29.92	11.34	
33	31.01	11.29	30.96	1142	30 91	11.56	30.86	11.69	
34	31 95	11.63	31.90	11.77	31.85	11.91	31.79	12.05	
35	32.89	11.97	32.84	12.11	32.78	12.25	32.73	12.40	
36 37	33.83 34-77	12.31	33.77 34.71	12.46	33.72 34.66	12.61	33.66 34.60	12.75 13.11	
38	35.71	13.00	35.65	13.15	35.59	13.31	35.54	13.46	
39	36.65	13.34	36.59	13.50	36.53	13.66	36.47	13.81	
40	37-59	13.68	37.53	13.84	37.47	14.01	37.41	14-17	
41	38.53	14.02	38.47	14.19	38.40	14.36	38.34	14.53	
42	39.47 40.41	14.36 14.71	39.40 40.34	14.54 14.88	39-34 40-28	14.71	39.28 40.21	14.88	
43	41.35	15 05	41.28	15.23	41 21	15.41	41.15	15.59	
45	42.29	15.39	42.22	15 58	42.15	1576	42.08	15.94	
46	43 23	15.73	43.16	15.92	43.09	16.11	43.02	16.30	
47	44.17	16 07	44.09	16.27	44.02	16.46	43.95	16.65	
84	45.11 46.04	16.42 16.76	45.03	16.61	44.96	16.81 17.16	44.89 45.82	17.01	
49 50	46.98	17.10	45.97 46.91	17.31	46.83	17.51	46.76	17.36 17.71	
51	47 92	17.44	47.85	17.65	47.77	17.86	47.69	18.07	
52	48.86	17.79	48.79	18.00	48.71	18.21	48.63	18.42	
53	49.80	18.13	49-73	18.34	49.64	18.36	49.56	18.78	
54	50.74 51.68	18.47 18.81	50.66	18.69	50.58	18.91	50.50	19.13	
55	52.62	19.15	51.60	19.04	51.52	19 26	51 43	19.49	
56 57	53.56	19.15	52.54° 53.48	19 38	52.45 53.39	19.61 19.96	52.37 53.30	19.84	
58	54.50	19.84	54.42	20.07	54.33	20.31	54-24	20.55	
59	55.44	20.18	55.35	20 42	55.26	20 66	55:17	20.90	
60	56.38	20.52	56.29	20.77	56.20	21.01	56.11	21 26	
Dist	Dep	Lat.	Dep	Lat.	Dep.	Lat	Dep.	Luc	
a :	0'		45		30	/	. 1	5'	
			60	DEGRI	28.9				

DECIMAL.

45' **69 DEGREES.**

			20	DEGIN				125
Dist	0		1:	5'	30'		451	
	Lat.	Dep.	Lat	Dep.	Lat.	Dep.	Lat.	Dep.
61	57-32	25.86	57.23	21.11	57.14	21.36	57.04	21.61
62		21.21	58.17	21.46	58.07 59.01	21.71	57.98	21.97
64	59.20 60.14	21.89	60.04	22.15	59.95	22.48	59.85	22.67
65	61.08	22.13	60.98	22.50	60.88	22.76	60.78	23.03
66	62.02	22.57	61.92	22.84	61.82	23.61	61.72	23.38
67		22.92	62.86	23.19	62.76	23.46	62.65	23.74
68	63.90 64.84	23.26 23.60	63.30	23.54	63.69 64.63	23.81	63.59	24.09
70	65.78	23.94	65.67	24.23	65.57	24.16 24.51	64.52	24.45 24.80
7:	66.72	24.18	66.61	24.57	66.50	24.86	66.39	25.15
72	67.66	24.63	67.55	24.92	67.44	25.21	67.33	25.51
73	68.60	24.97	68.49	25.27	68.38	25.57	68 26	25.86
74	69 54	25.31	69.43	25 61	69.31	25.92 26.17	69.20	26.42 26 57
75	70.48	25.65	70.36	25.96	70.25	26 62	70.14	26.43
76 77	71.42	25.99 26.34	71.30	26.30 26.65	71.19	26.97	71.07. 72.01	27.28
78	73.30	26 68	73.18	27.00	73.06	27.32	72.94	27.63
79	74.24	27.02	74.12	27.34	74.00	27.67	73.88	27.99
80	75.18	27 36	75.06	27.69	74.93	28 02	74.81	28.34
81	76.12	27.70	75 99	28.04	75:87	28.37	75.75	28 7C
82 83	77.05	28.05 28.34	76.93	28.38 28.73	76.81	28.72 19 07	76.68	29.05 29 41
84	78.93	28.73	78.81	29.07	78.68	29.41	78.55	29.76
85	79-87.	29.07	79-75	29 42	79.62	29.77	79.49	30.12
86	\$0 81	29.41	80.68	29.77	80.55	30 12	80 42	30.47
87	81.75	29.76	81.62	30.11	81.49	30.47	81.36	30.83
88 80	82.69 83.63	30 10 30.44	82;56 83.50	30.46 30.80	82 43 83 36	30.82	82 29 83:23	31.18 31.53
90	84.57	30.78	84.44	31.15	84 30	31.52	84.16	31.89
91	85.51	31.12	84.38	31.50	85.24	31.87	85.10	32.24
92	86.45	31 47	86.31	31.84	86.17	32.23	86.03	32.59
93	87.39	31.84	87.25	32.19	87.11	32.57	86 97	32.95
94	88.33 89.27	32.15 32.49	88.19 89.13	32.54 32.88	88.05 88.98	32.92 33.27	87.90 88 84	3 ,.30 33.66
95	90.11	32.83	90.07	33.23	89.92	33.62	89.77	34.01
97	91.15	33 18	91.00	33.57	90.86	33.97	90.71	3+ 37
98	92.09	33.52	91.94	33.92	91.79	34.32	9164	34.72
99	93.03	33.86	92.88	34-27	92.73	34.67	92 58	35.07
100	93.97	34.20	93.82	34.61	93 67	35.02	93.51	35.43
101	94.91 95.85	34-54 34-89	94.76 95.70	34 96 35.30	94.60	35.37 35 72	94 45 95.38	35.78 36.14
103	95.05	34.23	96.63	35.65	96.48	36.07	96 32	36.49
104	97.73	35.57	97 57	36.00	97.41	36.42	97.25	36.85
105	98.67	35 91	98.51	36.34	98.35	36.77	98.19	37.20
106	99.61	36.25	99.45	36.69	99 29	37.12	99.12	37.55
107	100.5	36.60 36.94	100 4	37.03 L	100.2	37.47 37.82	1,001	37.91 38.26
109	102.4	37.28	102.3	37.73	108.1	38.17	101.9	38.62
110	103.4	37.62	103.2	38.07	103.0	38.52	102.9	38.97
111	104.3	37 96	104.1	38.42	104 0	38.87	103.8	39-33
112	105.2	38.31	105.1	38.77	104.9	39.22	104.7	39.68
113	107.1	38.65 38.99	106.0	39.11 39.46	105.8	39·57 39·92	105.7	40.03
114	108.1	39.33	107.9	39.80	107.7	40 27	107.5	40.74
116		39.67	108.8	40.15	108.7	40.62	108.5	41.10
117		40.02	109.8	40.50		40.97	109.4	41.45
811	T10.9	40 36		40.84	110.5	41.52	110.3	41.81
611	111.8	40.70	111.6	41.19	111.5	41.67	111.3	42.52
120		41.04		41.53		Lat.	Dep.	
ă	Dep.	Lat.	Dep.	Lat	Dep.			La:
عا	0		45	DEGR	30	<i>,</i> ,	· 15	

DI	0,	-	1 154 30'				The second secon		
Dist.	Lat	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
I	0.93	0.36	0.93	0.36	0,93	0.37	0.93	0.37	
2	1.87	0.72	1.86	0.72	1.86.	0.73	1.86	0.74	
3	2.80	1.08	2.80	1.09	2.79	1.10	2.79	11.11	
4	3.73	1.43	3.73	1.45	3.72	1.47	3.72	1.48	
5	4.67	1.79	4.66	-	4.65		_	2.23	
6	6.54	2.15	5.59	2.17	6.51	2.20	6.50	2.59	
7	7-47	2.87	7.46	2.90	7.44	2.93	7.43	2.96	
9	8.40	3.23	8.39	3.26	8,37	3.30	8.36	3-34	
10	9-34	3.98	9.32	3.62	9.30	3.67	9:29	3.71	
11	10.27	3.94	10.25	3.99	10.23	4.03	10.22	4.08	
12	11.20	4.30	11.18	4-35	11.17	4.40	11.15	4.45	
-13	12.14	4.66	12.12	5.07	13.03	5 13	13.00	5.19	
14	13.07	5.02	13.05	5.44	13.96	5.50	13 93	5.56	
16	14.94	5.73	1491	5.80	14.89	5.86	14.86	5.93	
17	15.87	6.09	15.84	6.16	15 82	6.23	15.79	6.30	
18	16,85	6.45	16.78	6.52	16.75	6.60	16.72	6.67	
19	17.74	6.81	17.71	6.89	17.68	6 96	17.65	7.04	
20	18.67	7.17	18.64	7.25	18.61	7 33	18.58	7.41	
21	19.61	7.53	19.57	7.61	19.54	7.70	19.51	7.78	
22	20.54	7.88	20.50	7 97	20.47	8.06	20,43	8.15	
23	21,47	8.60	21.44	8.34	22.33	8.80	22 20	8.89	
25	23 34	8.96	23.30	9.06	23.26	9.16	23.22	9.26	
26	24.27	9.32	24.23	9.42	24.19	9 53	24.15	9.63	
27	25.21	9.68	25.16	9.79	25.12	9.90	25.08	10.01	
28	26,14	10.03	26.10	10.15	26.05	10.26	26 01	10.38	
29	27.07	10.39	27.03	10.51	26.98	10.63	26.94	10 75	
30	28.01	10.75	27 96	10.87	27 91	11.00	27.86	11.12	
31	28 94	11.11	28.89	11.24	28.84	11.73	28.79	11.49	
32	30.81	11.47	30.76	11.60	39.77	12 09	30.65	12.23	
33	31.74	12.18	31.69	12 32	3163	12.46	31.58	12.60	
35	32.68	12.54	3262	12.69	32.56	12.83	32.51	12.97	
36	33.61	12.90	33.55	13.05	33.50	13.19	33.44	13.34	
37	34-54	13.26	34.48	13.41	34-43	13.56	34-37	13.71	
38	35.48	13.62	35 42	13 77	35.36	13.93	35.29	14.08	
39	36.41	13.98	36 35	14.14	36.29	14.29	36.22	14 45	
40	37.34	14-33	37.28	14 50		_	38 08	15.19	
41	38.28	14.69	38.21	14.86	38 15	15.39	39.01	15.56	
42	40.14	15.41	40.08	15.58	40.01	15.76	39.94	15.93	
43	41.08	15.77	41.01	115.95	40.94	16 13	40.87	16.30	
45	42.01	16.13	41.94	16.31	41.87	16.49	41.80	16 68	
46	42.94	16.48	42.87	16.67	42.80	16.86	42.73	17.05	
47	43.88	16.84	43.80	17.03	43 73	17.23	43.65	17.42	
48	44.81	17.20	44.74	17.40	44.66	17.59	44.59	17.79	
49	46.68	17.92	46.60	18.12	46.52	18.33	46.44	18.53	
50		18.28		18.48	47.45	18.69	47-37	18.90	
51	48.55	18.64	47.53	18.85	48.38	19.06		19.27	
53	49.48	18.99	49.40	19.21	49.31	19.42	49 23	19.64	
54	50 41	19.35	50 33	19.57	-	19.79		20.01	
55	51.35	19.71	51.26	19.93	51.17	20.16	51.08	20.38	
56	52.28	20.07	52.19	20 30	52.10	20.52	52.01	20.75	
57	53.21	20.43	53.12	20.66	53.03	20.89		21.12	
58	54.15	20.79	54.06	21.38	53.96	21.62	53.87	21.49	
60	55.08	21.14	54.99	21.75	55.83	21.99	55.73	22.23	
Dist.	Dep	Lat.	Dep.	Lat	Dep.	Lat.	Dep.	Lat.	

D	01		1	5'	30	,	4	5'
Dist	Lat	Dep	Lat.	Dep,	Lat	Dep.	Lat.	Dep.
61	56.95	21.86	56.85	22.11	56 76	22.36	56.66	22.60
63	57.88	22-22	57.78	22 47	57 69	22.72	57-59	22.97
64	59.75	22.58	58.72	22 83	59.55	23.46	58.52	23.35
65	60.68	23 29	60.58	23 56	60.48	23.82	60.37	24.09
66	61.62	23.65	61.51	23.92	61.41	24.19	61.30	24.46
67	62 55	24.01	62.44	24.28	62.34	24.56	62.23	24.83
68	63.48	24.37	63.38	24.65	64.20	24.92	63.16	25.20
70	65.35	25.09	65.24	25.37	65.13	25.66	65.00	25.94
71	66.28	25.44	66.17	25.73	66.06	26.02	65.95	26.31
72	67.22	25.80	67.10	26.10	66.99	26.39	66.87	26.68
73	68.15	26.16	68.04	26.46	68.85	26.75	67.80	27.05
74 75	70.02	26.52	68 97	26 82	69.78	27.12	68.73	27.42
76	70.95	27.24	70.83	27.55	70.71	27.85	70.59	28.16
77	71.89	27.59	71.76	27.91	71.64	28.22	71.52	28.53
78	72.82	27.95	72.70	28.27	72.57	28.59	72.45	28.90
79 80	73.75	28.31	73.63	28.63	73.50	28.95	73.38	29.27
81	74 69		74.56	29.00	74-43	29.32	74-30	30.02
82	76.55	29.39	75.49 76.42	29.72	75.36 76.29	30.05	75.23	30.39
83	77.49	29.74	77.36	30.08	77.22	30.42	77.09	30.76
84	78.42	30.10	78.29	30.44	78.16	30.79	78.02	31.13
85	79.35	30.46	79.22	30.81	79.09	31.15	78.95	31.50
86	80.29	30.82	80.15	31.17	80.02	31.52	79.88	31.87
88	82.16	31.54	81.08	31.53	81.88	32.25	81.74	32.61
89	83.09	31.89	82.95	32.26	82.81	32.62	82.66	32.98
90	84 02	32 25	83.88	32.62	83.74	32.99	83.59	33.35
91	84.96	32.61	84.81	32 98	84 67	33-35	84.52	33.02
92	85.89	32.97	85.74	33-34	85.60	33.72	85.45 86.38	34.46
94	87.76	33 69	87.61	34.07	87.46	34-45	87 31	34.83
95	88.69	34.04	88.54	34-43	88.39	34.82	88.24	35.20
96	89.62	34.40	89.47	34.79	89.32	35.18	89.17	35 57
97	90.56	34.76	90.40	35.16	90.25	35.55	90.09	35.94
99	91.49	35.48	91.34	35.52	92.11	35.92	91.02	36.69
100	93.36	35.84	93.20	36.24	93 04	36.65	92.88	37.06
101	94.29	36.20	94.13	36.61	93.97	37-02	93.81	37-43
102	95.23	36.55	95.06	36.97	94.90	37-38	94 74	37.80
103	96.16	36.91	96.00	37.33	95.83	37.75	95.67	38.17
105	98.03	37 63	97 86	38.06	97 69	38.48	97.53	38.91
106	98.96	37.99	98.79	38.42	98.62	38.85	98.45	39 28
107	99.89	38.35	99.72	38.78	99-55	39.22	99.38	39.65
109	8.001	38.70	100.7	39.14	100.5	39.58	100.3	45.02
110	101.8	39.06	101.6	39.51	101.4	39.95	101.2	40.39
III	103.6	39.78	103.5	40.23	103.3	40 68	103.1	41.13
112	104.6	40.14	104.4	40.59	104.2		104 0	41.50
113	105.5	40.50	105 3	40.96	105 1	41.41	105.0	41.87
114	106.4	40.85	106.2	41.32	106.1	42 15	105.9	42.24
116	108.3	41.57	108.1	42.04	107.9	42.51	107.7	42.98
117	109.2	41.93	109.0	42.41	108.9	42.88	108.7	43.36
118	110.2	42.29	110,0	42.77	109.8	43.25	109.6	43.73
1119	111.1	42.65	111.8	43.13	110.7	43.61	110.5	44-10
1	Dep.	43.00 Lat.	Dep.	43.49 Lat.	Dep.	43.98	111.5 Den	44-47 Lat.
st.	Dep.	-	_	5'	3(Market .	Dep.	51
Q	0		the same of the sa	DECH	Annual Contractions	-	-	-

1 0.93 0.37 0.93 0.38 0.92 0.38 0.92 0.38 0.92 0.38 0.92 0.38 0.92 0.38 0.92 0.38 0.92 0.38 0.92 0.38 0.92 0.38 0.92 0.38 0.92 0.38 0.92 0.38 0.92 0.38 0.92 0.38 0.92 0.38 0.92 0.75 0.75 0.370 0.151 3.70 1.55 3.70 1.55 3.70 1.55 3.70 1.55 3.70 1.55 3.70 1.55 3.70 1.55 3.69 1.55 3.70 1.55 3.70 1.55 3.69 1.55 3.70 1.55 3.69 1.55 3.70 1.55 3.69 1.55 3.70 3.66 7.38 3.39 3.41 8.31 3.44 8.30 3.37 3.37 3.33 3.41 8.31 3.44 8.30 3.37 3.37 3.37 3.37 3.38 3.37 3.38 3.37 3.38 3.37 3.38 3.39 3.34 3.38 3.39 3.34 3.38 3.39 3.34 3.38 3.39 3.34 3.38 3.39 3.34 3.39 3.34 3.39 3.34 3.39 3.34 3.39 3.34 3.39 3.34 3.39 3.34 3.39 3.38 3.39 3.39 3.39 3.30 3.39 3.30 3.39 3.30 3.39 3.30 3.39 3.30 3.39 3.30 3.39 3.30 3.39 3.30 3.39 3.30 3	
1 0.93 0.37 0.93 0.38 0.92 0.38 0.93 0.37 2 1.85 0.76 1.85 0.76 1.85 0.77 1.84 0.77 1.15 2.77 2.10	ep
3 2.78 1.14 2.77 1.15 3.70 1.53 3.69 1.64 3.70 1.53 3.69 1.63 3.69 1.63 3.69 1.63 3.69 1.63 3.69 1.61 3.70 1.53 3.69 1.61 1.61 1.61 1.61 1.61 3.70 1.53 3.69 3.66 1.61 1.	.39
4 3.71 1.50 3.70 1.51 3.70 1.93 3.69 1.91 4.61 1.87 4.63 1.89 4.62 1.91 4.61 1.89 4.62 1.91 4.61 1.89 4.62 1.91 4.61 1.81 4.61 1.81 4.61 1.91 4.61 1.81 1.91 4.61 1.81 1.91 4.61 1.81 1.91 4.61 1.81 1.91 4.61 1.81 1.91 4.61 1.83 3.65 7.42 3.00 7.40 3.03 7.39 3.06 7.38 3.39 3.44 8.30 3.34 1.01 4.91 1.01 4.91 1.01 4.91 1.01 4.91 1.01 4.91 1.01 4.91 1.01 4.91 1.02 4.91 1.02 4.91 1.02 4.91 1.02 4.91 1.02 4.91 1.02 4.91 1.02 4.91 1.02 4.11 1.02 4.11 1.02 4.11 1.	77
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44 40.50 17.19 40.43 17.37 40.35 17.54 40.27 17.72 45 41.42 17.58 41.35 17.76 41.27 17.94 41.19 18.12 46 42.34 17.97 42.26 18.66 42.18 18.34 42.10 18.53 47 43.26 18.36 43.18 18.55 43.10 18.74 43.02 18.53 48 44.18 18.76 44.10 18.95 44.02 19.14 43.93 19.33 49 45.10 19.15 45.02 19.34 44.94 19.54 44.85 19.73 50 46.03 19.54 45.94 19.74 45.85 19.94 45.77 20.14 51 46.95 19.93 46.86 20.33 47.59 20.74 44.68 20.54 52 47.87 20.22 47.87 20.23 47.69 20.74 47.69 20.74 49.71							17.15	39.36	17.32
46 42.34 17.97 42.26 18.66 42.18 18.34 42.10 18.53 47 43.26 18.36 43.18 18.55 43,10 18.74 43.02 1.8.93 48 44.18 18.76 44.10 18.95 44.02 19.14 43.93 19.33 49 45.10 19.15 45.02 19.34 44.94 19.54 44.85 19.73 50 46.03 19.54 45.94 19.74 45.85 19.94 46.85 19.73 51 46.95 19.93 46.86 20.13 46.77 20.34 46.68 20.54 52 47.87 20.32 47.78 20.53 47.60 20.94 47.60 20.94 48.79 20.71 48.70 20.92 48.60 21.13 48.51 21.35 54 49.71 21.10 49.61 21.23 49.52 21.13 48.51 21.75 55 50.63	44								
47 43.26 18.36 43.18 18.55 43.10 18.74 43.02 18.93 19.13 19.13 43.93 19.33 19.33 19.34 44.02 19.14 43.93 19.33 19.34 19.54 44.02 19.54 44.94 19.54 44.85 19.73 20.14 45.85 19.94 44.85 19.73 20.14 45.85 19.94 44.85 19.73 20.14 45.85 19.94 46.68 20.53 46.77 20.34 46.68 20.54 47.78 20.53 47.60 20.34 46.68 20.54 47.60 20.94 47.60 20.94 47.60 20.94 47.60 20.94 47.60 20.94 47.60 20.94 47.60 20.94 47.60 20.94 47.60 20.94 47.60 20.94 47.60 20.94 47.60 20.94 47.60 20.94 47.60 20.94 21.13 48.51 21.35 21.55 25.55 20.63 21.23 21.23 21	1								
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49 45.10 19.15 45.02 19.34 44.94 19.54 44.85 19.73 50 46.03 19.54 45.94 19.74 45.85 19.94 45.77 20.14 20.12 20.14 45.87 20.14 45.67 20.34 46.68 20.54 20.53 47.69 20.74 47.69 20.94 47.69 20.94 47.69 20.94 48.61 21.33 48.51 21.33 21.35 55 50.63 21.49 50.53 21.71 50.44 21.93 50.34 22.55 57 52.47 22.27 52.37 22.50 52.27 22.73 52.17 22.55 58 53.39 22.66 53.29 22.90 53.19 23.13 53.09 23.76 59.427 23.29 54.12 23.53 54.00 23.76 50.21 23.92 54.91 24.16	48								
50 46.03 19.54 45.94 19.74 45.85 19.94 45.77 20.14 51 46.95 19.93 46.86 20.13 46.77 20.34 46.66 20.54 52 47.87 20.32 47.78 20.93 47.69 20.74 47.60 20.94 53 48.79 20.71 48.70 20.92 48.69 21.13 48.51 21.33 54 49.71 21.10 49.61 21.33 49.52 21.53 49.43 21.75 55 50.63 21.49 50.53 21.71 50.44 21.93 50.34 23.15 56 51.55 21.88 51.45 22.21 51.35 22.33 51.26 22.55 57 52.47 22.27 22.37 52.17 22.96 22.27 22.73 52.17 22.95 58 53.39 22.66 53.29 23.90 53.19 23.53 54.00 23.76			19.15			44-94	19.54	44.85	19.73
52 47.87 20.32 47.78 20.53 47.60 20.74 47.60 20.94 53 48.79 20.71 48.70 20.92 48.60 21.13 48.51 21.35 54 49.71 21.10 49.61 21.32 49.52 21.53 49.42 21.75 55 50.63 21.49 50.53 21.71 50.44 21.93 50.34 21.75 56 51.55 21.88 51.45 22.81 51.36 22.33 51.26 22.55 57 52.47 72.27 52.37 22.50 52.27 22.73 52.17 22.96 58 53.39 22.66 53.29 23.96 54.12 23.53 54.00 23.76 59 54.31 23.05 54.21 23.29 5412 12.53 54.00 23.76 60 55.23 23.44 55.13 23.68 55.02 23.92 54.92 24.16	50	46.03	19.54						
\$\begin{array}{cccccccccccccccccccccccccccccccccccc				46.86					
54 49.71 21.10 49.61 24.32 49.52 21.53 49.43 21.75 55 50.63 21.49 50.53 21.71 50.44 21.93 50.34 22.15 56 51.55 21.88 51.45 22.11 51.36 22.33 51.26 22.55 57 52.47 22.27 52.37 22.50 52.27 22.73 52.17 22.95 58 53.39 22.66 53.29 22.90 ,5319 23.13 53.09 23.76 59 54.37 23.05 54.27 23.29 5411 23.53 54.00 23.76 60 55.23 23.44 55.13 23.68 55.02 23.92 54.91 24.16									
55 50.63 21.49 50.53 21.71 50.44 21.93 50.34 22.15 56 51.55 21.88 51.45 22.81 51:36 22.33 51:26 22.55 57 52.47 22.27 52:37 22.50 52.27 22.73 52.17 22.96 58 53.39 22.66 53.29 22.90 .53:19 23.13 53.09 23.36 59 54.37 23.44 55:13 23.68 55:02 23.92 54:92 24:16 60 55:23 23.44 55:13 23.68 55:02 23.92 54:92 24:16									21.75
56 51.55 21.88 51.45 22.81 51:36 22.33 51:26 22.55 57 52.47 22.27 52:37 22.50 52:27 22.73 52:17 22.96 58 53:39 22.66 53:29 22.90 .53:19 23:13 53:09 23:36 59 54:37 23:44 55:13 23:68 55:02 23:92 54:92 24:16									
57 \$2.47 \$22.27 \$2.37 \$22.50 \$2.27 \$22.73 \$24.17 \$23.96 58 \$3.39 \$22.66 \$3.29 \$22.90 \$31.19 \$23.13 \$3.09 \$23.36 59 \$4.31 \$23.05 \$4.21 \$23.29 \$411 \$25.53 \$4.00 \$23.76 60 \$5.23 \$23.44 \$55.13 \$23.68 \$5.02 \$23.92 \$4.92 \$4.16			21.88	51.45	22.11	51136.	22.33		
59 54.31 23.05 54.21 23.29 54111 123.53 54.00 23.76 60 55.23 23.44 55.13 23.68 55.02 23.92 54.92 24.16	57	\$2.47						, -	
60 55.23 23.44 55.13 23.68 55.02 23.92 54.98 24.16			ı						
المستعارين إستند استبعار ستنسب الشمسانية ومناه المتعارية والمتعارية									
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	iğ.		<u></u>	45					5,

13	1' 0'	,	1 15	,	1 3	0'	45'	
L.	Lat	Dep.	Late	Dep	Lat.	Dep	Lat	Div
61	\$6.15	23.83	56.09	24.08	55.94	24:32	. 55.83	24.57
62	57.99	24.23 24.62	56.97	34-47 34-87	55 86	24:72	56.75	24-97
6:	58.91	25.01	54.80	15.26	58.69	25.52	58.58	25.78
65	59.83	25.40	59.72	25.66	59 61	25.92	59.50	26 18
66	60.75	25.79	60 64	26.05	60.53	26.32	60.41	26.58
67 68	62.59	26.18 26 57	61.56	26 45 26 84	61.44	26.72	61 39	16.98 17.39
69	63.51	26.96	63.40	27.24	63.28	27.51	63.16	27.79
70	64.44	27 35	64 32	27.63	64.19/	27.91	64.07	28.19
71	66.38	27 74	66.15	28.42	65 II - 66.03	28.31 28.71	64.99 65. 9 0	28.6C
72 73	67-20	28.52	67.07	28.82	66.95	29-11	66.82	29.40
74	68.12	28.91	67.99	29.21	67.86	29.51	67.73	29.80
1.75	69.04	29.30	68.91	29.61	68.78	29.91	68.65	30.21
76 77	70.88	29,70 30,00	69 83 70.75 '	30.40	70.61	30.30	69.56 1 70.48	30.64
78	71.80	30 48	71.67	30.79	71.53	31.10	71.39	31.41
79	72.72	30.87	72.58	31.18	72.45	31.50	7231	31.82
80	73.64	31.26	73.50	31.58	73.36	31 90	73.22	32.22
8 t	75.48	31.65	74-42	31 97 32.37	74.28 75.30	32.30	7414	33.03
83	76.40	32.43	76.26	32.76	76.12	33.10	75.97	33.43
84	77.32	32.82	77.18	33.16	77.03	33.49	76.89 77.80	33.83
85	79.16	33.60	7.9 02	33.55	77.95	33.89	78.74	34-23
87	80.08	33 99	79.93	33-95 34- 34	79.78	34.69	7963	35.04
88	81.00	34.38	80.85	34-74	80.70	35.09	80.55	35.44
89 93	81.93	34-78 35 •7	81.77 82.6g	35.13 35.53	81.62	35.49 35.8g	81.46 1 82.38	35.84 36.25
97	83.77	35.56	83 61	35.92	83.45	36.29	83.29	36.65
92	84.60	35.95	84.53	36.32	84.37	36.68	84 2 #	37.05
93	85.61	36 34	85.45	36.71	85.29	37 08	85.12 . 86.04	37.46
94	86.53 87.45	36.73	86.37 87.29	37.50	86 20 87.12	37.48 37.88	86.95	37.86 38 26
96	88.37	37.51	88.20	37.90	88.04	38.28	87.87	38 66
97	89-249	37.90	89.12	3 8. 249	88 95	38.68	88.79	39.07
98	90.21	38. 3 9 38. 58	90.04 90. 96	38.68 30.08	89.87	39. 08 39. 48	89.70 93.62	39·47 39.87
100	91.13	39.07	91.88	39.47	90.79	39.87	91.53	40.27
101	92.97	39.46	92 80	39.87	92.62	40.27	92.45	40.68
102	93.89	39.85	93.72	40.26	93.54	40 67	93.36	41.08
103	94.81	40.25 40. 64	94-64	40. 66 41 05	94.41	41.07 41.47	94.28	41.48
105	96.65	41.03	96.47	41.45		41.87	96.11	12.29
106	97.57	41.42	97-39	41.84		42.27	97.02	42.69
107	98.49	41.86	, ,	42.63	98.13	43.67	97-94 98-85	43.09
108	100.3	42.5g	99.23	43.03	99.04		99-77	43.90
110	101.3	42.98	101.1	43 42	100.9			44.30
111	102.2	43.37	102.0	43.82	101,8	44 26	101.6	44.70
1112		43.76	102 9	44.81 44.61	103.6	44 66	102-5	45.11
113	104-9	44.15	103.8	45.00	104.5	45.46	. 104.3	
115	105.9	44.93	105.7	45.40	105.5	45.86	105.3	46.32
116	106.8	45.32	106.6		106.4		106.2	
117	109.7	45.72 4 6. 81	107.5	46.19	107-3	46.65	108.0	47.13
119	109.5	46.50		46.97	-109.1		108.9	47.93
1 20	110-5	46.89	110.3	47.37	110.0	47.85	109.8	
4	Dep.	Lat.	D p	Lat.	Dep	Lat.	Dep:	
Dist.	U		45	nucus	30)′	1 · 1.	5′

1 8	. ' 0'		15/		30)	45":	
Diet	Lat.	Dep	Lat	Dep.	Lat.	Dep.	Lat	Dep.
1	0.91	0.41	0.91	0.41	0.91	140	0.91	0.42
2	1.83	0.81	1.82	0.82	1.88 2.73	0.83	1.82	D.84 1.26
3 4	3.65	1.63	3.65	1 64	3.64	1.66	3.63	1.67
5	4-57	2.03	4.56	2.05	4.55	2.07	4-54	2.09
6	5.48	2.44	5.47	2.46	5-46	249	5.45	2.51
F 3	7-31	3.25	6.38 7.29	2.88 3.29	9.37 7.28	2.90 3.32	6 36 7.27	2-93 3-35
1 9	8.22	3 66	8.21	3.70	8.19	3 73	8.17	3-77
10	9.14	4.07	9.12	4.11.	9.10	4.15	9.08	4.19
111	10.05	4.47 4.88	10.03	4-52	10.01	4.56	9.99	4.61 5.02
12	12.88	5 29	10.94	4.93 5.34	10.92	4.98 5 39	10.90	5.44
14	13 79	5.69	12.76	5.75	12.74	5.81	12.71	5.86
15	13.70	6.10	13.68	6.16	13.65	6.22	13.62	6.28
16	14.62	6.91 6.21	14.59	6.57 6.98	14.56	6.64 7.05	14.53 15.44	6.70 7.12
17	15.53	7.32	15.50	7 39	15.47 16 38	7.46	16.35	7:54
19	17 36	7.73	17.32	7.8ò	17.29	7.88	17.25	7.95
20	19.27	8.13	18 24	8.21	18.20	8.29	18.16	8.37
21	19.18	8.54 8.95	19 15	8.63 9.04	19.11 20.02	8.71 9.12	19.07	8.79 9.21
23	2101	9.35	20.97	9.45	20.02	9.54	20.89	9.63
24	21.93	9.76	21.88	9.86	21.84	9.95	21.80	10.05
25	22.84	10.17	22.79	10.27	22.75	10.37	22.70	10.47
26 27	23.75	10.58	23.71	10.68	23.66 24 57	10.78	23.61 24.52	10.89 11.30
28		11.39	25.53	11.50	25.48	11.61	25.43	11.72
29	,	111.80	26.44	12.91	26.39	1203	26.34	12.14
30	27.41	12.20	27.35	12.32	27.30	12.44	28.15	12.56
31	28.32	13.61	28.26 29.18	12.73	28.21	13.27	29.06	13.40
33		13.42	30.00	13.55	30 03	13.68	29.97	13 82
34		13.83	31.70	13.96	30.94	14.10	30.88	14-23
35		14.24	31.91	14.38	31/85	14.93	31.78	14 65
37	33.80	14.64 15.Q5	33.74	14.79	32.76 33.67	15.34	33.60	15-49
38	3471	15.46	34.65	15 61	34-58	15.76	34.51	15.91
39 40	1 - 2 -	15.86	35.50	16.02	35.49	16.17	35.42	16.33
41		16 68	36.47	16.84	37.31	17.00	37.23	17.17
42	38.37	17.08	38.29	17.25	38.22	17.42	38.14	17.58
43	39.28	17.49	39.21	17.66	39-13;	17.83	39.05	18.00
44	41 11	18.30	40.12	18.48	40.04	18.25 18.66	\$9.96 40.87	18.42
46	42.02	18.71	41.94	18 8g	41.36	19.08	41.77	19.26
47	42.94	19.12	42 85	19.30	42.77	19.49	42.68	19.68
48		19.52	43.76	1971	43.68	19.91	43.59	20.10
49 50	44.76 45 168	19.93	44-68 45-59	20.13	44.59	20.32 20.73	44.50 45-41	20.51 20.93
51	46.59	20.74	46.50	20.95	46.41		46.32	21.35
52	47.50	21.15	47.48	21.36	47.32	21.56	47.22	21.77
53	48.42	21.56	48.32	21.77	48.23			22.19
54 55	49·33 50.25	21.96	49.24 50,15	28.59	49.14	22.81		23.61
56	51.16	22.78	51.06	-	50.96		50.86	23.44
57	52.07	23.18	51.97	23.41.	51.87	23.64	51.76	23 86
58	52.99	23.59	52.88	23.82	52.78	24.05 24.47		24.28
59 60	53.90 54.81	24.40	53.79 54.71		53.69 54.60	24.88	\$3.58 54.49	24.70
4	Dep	Lat.	Dep.		Dep	Lat.	Dep.	_
P. F.	Dep Lat.		45	7	30	7	15	;

Ì	Dist.	0'		1.	5'	30'		451	
l		Lat.	Dep.	Lat.	Dep	Lat.	Dep.	Lat.	Dep.
1	61	55.73	24.81	55.62.	25.05	55.5L	25.30	55.40	25.54
1	62 63	56 64 57-55	25.22 25.62	50-53 57-44	25.46	57.33	25.71	56 30 57.21	25.96 26.38
1	64	58.47	26.03	58.35	26.29	58 24	36.54	58.12	26.79
I	65	59.38	26.44	59.26	26.70	59.15	26.96	59.03	27.21
ł	66	60.29	26.84 27.25	60.18	27.11	60.06	27.37	59.94 60.85	27.63 28.05
1	68	62.12	27.66	61.09	27.52	60.97 61.88	28.20	61.75	28.47
i	69	63.03	28.06	62.91	28.34	62.79	28.61	62.66	28.89
ı	70	63.95	28.47	63.83	28.75	63.70	29.03	63.57	29.31
ı	71 72	64.86	28.88 29.29	64.74	39.16 29.57	64.61	29.44 29.86	64.48	29.72 30,14
1	73	66.69	29.69	66.56	29.98	66.43	30.27	66.29	30.56
ł	74	67.60	30.10	67.47	30.39	67.34	30.69	67.20	30.98
ı	75	68.52	30.51	68.38	30.80	68.25	31.10	68.11	31.40
1	76 77	69 43 70.34	30.91	69.29 70.21	31.21	69.16 70.07	31.52	69.03 69.93	31.82 32.24
ł	78	71.26	31.73	71.12	32.04	70.98	32.35	70.84	32.66
1	79	72.17	32.13	72.03	32.45	71.89	32.76	71.74	33.07
I	80	73.08	32.54	72 94	32.86	72.80	33.18	72.65	33.49
ı	81	74.91	32.95 33-35	73.85 74.76	33.27 33.68	73.71	33.59 34.00	73:50 74:47	33.91 34.33
1	83	75.82	33 76	75 68	34.09	75.53	34.42	75.38	34-75
1	84	.76.74	34-17	.76.59	34.50	76.44	34.83	76.28	35.17
1	85	77.65	34-57	78.41	34-91	77.35	35.25	77.19	35.59 36.00
ł	87	79.48	34.98	79.32	35.32	79.17	36.08	79.01	36.42
I	88	80.39	35.79	80.24	36.14	80.08	36.49	79.92	36.84
l	89	81.31	36.20	81.15 82.06	36.55.	80 99 81.90	36.91 37.32	80.82	37 26
ı	90	83.13	36.61	82.97	36.96	82.81	37.74	82.64	37.68
ı	91 92	84.05	37.48	83.88	37.79	83.72	38.15	83.55	38.52
1	93	84.96	37 83	84-79	38.20	84.63	38.57	84.46	38.94
ı	94	85.87 86.79	38.23 38.64	85.71 86.62	38.61 39.02	85.54 86.45	38.98 39.40	85.37 86.27	39·35 39·77
I	95	87.70	39.05	87-53	39-43	87.36	39.81	87.18	40.19
ı	97	88.61	39.45	88.44	39.84	88.27	40.23	88.09	40.61
ı	98	89.53	39.86	89.35	40.25	89.18	40.64	89.00	41.03
I	99	90.44	40.27	90.26	40.66	90.09	41.05	89 91 90.81	41.87
I	101	92.27	41.08	92.09	41.48	91.91	41.88	91.72	42.28
Į	102	93.18	41.49	93.00	41.89	92.82	42.30	92.63	42.70
	103	94.10	41 89	93.91	42 30	93 73	42.71	93.54	43.12
	104	95.01	42.30 42.71	94.82 95:74	42.71	94.04	43.54	94 45	43.54 43.96
١	106	96.84	43.11	96.65	43.54	96.46	43.96	96.26	44.38
I	107	97.75	43.52	97.56	43.95	97-37	44-37	97.17	44.80
Ì	108	98.66	43.93	98.47 99.38	44.36	98.28	44-79 45.20	98.08	45.22 45.63
1	110	100.5	44-33 44-74	100.3	44-77 45-18	100.1	45.62	99.90	46.05
ı	111	101:4	45.15	101.2	45.59	101.0	46.03	100.8	46.47
- 1	112	102.3	45.55		46.00		46.45	101.7	46.89
	113	103.2	45.96 46.37	103.0	46.82	103.8	46.86	103.6	47·31 47·73
	115	105.1	46.77	103.9	47.23	104 6	47.69	104.4	48.15
-	116	106.0	47.18	105.8	47.64	105.6	48.10	105.3	48.56
	117	106.9	47.59	106.7	48.05	106.5	48.52	106.3	48.98
ì	118	107.8	48.40	107.6	48.46 48.88	107.4	48.93	107.2. 108.1	49.40 49.82
ļ	1 20	109.6	48.81	109-4	49.29	109.2	49.76	109.0	50.24
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1	0.91	0.43	0.90	0.85	0.90	0.43	0:90 1.80	0.43
3	2.73	1.27	2.81	1.28	1.8t	1.39	3.70	1.30
4	3.63	1.69	3.62	1.71	3.61	1.72	3.62	1.74
	4-53	2.11	4-52	2,13	4.51	2.15	450	2.17
6	5-44	2.54	5.43	2.56	5.42	2.58	5.40	2.61
?	6.34	2.96	6.33	2.99	6.32	3 01	6.30	3.04
8	· 7 25	3.38 3.80	7.24 8.14	3.41	7.22 8 12	3·44 3·87	7.21 8.11	3.48 3.91
ıć.	9.06	4.25	6.04	4.27	903	4.31	9.01	4-34
11	9-97	4.65	995	4 69	. 993,	4-74	9.91	4.78
12	10.88	5.07	10.85	5.12	10.83	5.17 5.60	10.81	5.21 5.65
14	11.78	5.49 5.92	12.66	5.55 5.97	11.73	6.03	12.61	6.08
15	13.59	6.34	13-57	6.40	13.54	6.46	13.51	6.52
16	14.50	6.76	1447	6.83	14-44	6.89	1441	6.95
17	15.41	7.18	15.38	7.25	15.34	7 32	19.31	7 39
18	16.31	7.61	16.28	7.68	16.25	7.75	17.11	7.82
19	17.22	8.03 8.45	17.18	8.10 8.53	17.15	8.18 8.61	10.81	8 25 8.69
21	19.03	8.88	1899	8.96	18.95	9 04	18.91	9.12
22	19.94	9.30	19.93	9.38	19.86	9.47	19.82	9.56
23	20.85	9.72	20.80	9.8€	20.76	9.90	20.72	9-99
34	\$1.75	10.14	\$1.7E	10.24	21.66	10.33	21.62	10.45
25	2206	10.57	22.61	10.66	22.56	10.76	22.52	10.86
26 27	23.56	10.99 11.41	23.52	11.09	23.47 24.37	11.62	23.42 24 32	11.50. 11.73
28	25.38	11.83	25.32	11.04	25.27	12.05	25.22	12.16
29	26.28	12.26	26.23	12.37	26.18	12.48	26.12	12.60
30	27.19	12 68	27.13	12.80	27.08	12.91	27.02	13.03
31	28, 10	13.10	28.04	53.82	27.98	13.35	27.93	13-47
32	29.00 29.91	13.52	28.94	13.65	28 88 29-79	13.78	28.82	13.90
33 34	30.81	14.57	39-75	14 50	30.69	14.64	30.62	14.77
35	31.72	14.79	31.66	14 93	31.59	15.07	31.52	15.21
36	32.63	15.21	32.56	15.36	3249	15.50	32-43	15.64
37	33.53	15.64	33.46	15.78	33.40	15.93	\$3.33	16.07
38 39	34·44 35·35	16 06	34-37 35-27	16.64	34.30 35.20	16.79	34-23 35-13	16.51
40	36.25	16.90	36.18	17.06	36.10	17.22	36.03	17.38
41	37.16	17.33	37.08	17.49	37.01	17.65	36.93	17.81
42	38.06	17.75	37-99	17.92	37.91	18.08.	37-83	18.25
43	38.97	18.17	38.89 39.80	18.34	38.81	18.52	38.73 39.63	18.68
44	39.88 40.78	19.02	40.70	19.30	40.62	19.37	40.53	19.55
46	41.69	19.44	41.60	19 62	41.52	19.80	41-43	19.98
.47	42 60	19.86	42.51	20.05	42.43	20.23	42.33	20.42
48	43-50	20.29	43-41	20 48	43.32	20.66	43.23	20.85
49	44.41	20.71	4432	20.90 21.33	44-23	21.10	44-13	21.72
50	45.32		45.22	11.76	46.03	21.96	45.94	22.16
51 52	46.22 47.13	21.55	45.13	22 18	46.93	22.39		21.59
53	48.03	22.40	47-94	22.61 .	47.84	22.82	47-74	23.03
54	48.94	22.82	48.84	23.03	48.74	23.25	48:64	
55	49.85	23.24	49.74	23.46	49.64	23.68		23.89
56	50.75	23 67	50.65	23.89 24.31	.50054	24.1.8 24.54	50.44	
57 58	51.66 52.57	24.09	51.55 52.46	24.74	51.45 52.35	24.57	.52-24	
59	53.47	24 93	53.36	25.17	53:25	25.40	53-14	45.63
60	54.38	25.36	54-27	25.59	54:16	25.83	54-04	
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61	55.28	25.78	55.17	26.02	55.06	26.26	54-94	26.50	
62 63	56.19	26.20 26.63	56.08 56.98	26.45 26.87	56 86	26.69	56.74	26.94	
64	58.00	27.05	57.89	27.30	57 77	27.55	57.64	27 37 27 80	
65	58.91	27.47	58.79	27.73	58.67	27.98	58.55	28.31	
66 67	59 82	27.89 28.32	59.69 60.60	28.15	59.57 60.47	28.41 28.84	59.45	28.67	
68	61.63	28 74	61.50	29.01	61.18	29.27	61.25	29.11 29.54	
69	63.54	29.16	62.41	29 43	62.28	29.71	62.15	29.98	
79	63.44	30.01	63.31	30.29	64.08	30.14	63.05	30.41	
72	65.25	30.43	65.12	30.71	64.99	31.00	64:85	31.28	
73	66.16	30 85	66.03	31.14	65.89	31.43	65.73	31.71	
74 75	67.07 67.97	31.27	66.93 . 67.83	31.57	66.79	31.86	66.65	32.15	
76	68.88	32.12	68.74	32.43	68.60	32.72	68.45	33.03	
77	69.79	32.54	69.64	32 85	69.50	33.15	69.35	33.45	
78 79	70.69 . 71.60	32.96 33-39	70.55	33-27 33-70	70.49	33.58 34.01	70.25	33 89	
80	72.50	33 81	72.36	34.13	73.21	34.44	72.06	34.76	
18	73-41	34-23	73.26	34.55	73.11	34.87	72 96	35-19	
82 83	7432	34 65 35.08	74.17	34.98	74-91	35.30	73.86	35 68	
84	76-13	35.50	75 97	35.83	75.82	36.16	75.66	36.06 36.46	
85	77-04	35.92	76.88	36.26	76.72	36.59	76.56	36.93	
86 87.	77.94	36.35	77.78	36.68	77.63	37.02	77.46 78.36	37.36	
88	79-76	36.77 37 19	78.69 79-59	37-11	78.53	37.45	79.26	37.80 J	
89	80.66	37 61	80.50	37.96	80.33	38.32	80.16	38.67	
90	81.57	38.04	81.40	38.39	81.23	38.75	81.96	39 10	
91 92	83.38	38 88	83.31	39.02	82.14	39.18 39.61	82.86	39-53 39-97	
93	84.29	39.50	84.11	39.67	83.94	40.04	83.76	40.40	
94 95	86.10	39-78 40.15	85.02 85.93	40.10	84.84	40.47 40.90	84.67 85.57	40 84	
96	87.01	40.47	86.83	40.95	86.65	41.33	86.47	41.27	
97	87.91	40.99	87.73	41.38	87.65	41.76	87 37	42.14	
98 99	88.82. 89.72	41.42	88.64 89.54	41.80	88.45 89.36	42.19	88.27 89.17	42.58	
100	90.63	42.26	90.45	42 66	90.26	43.05	90.07	43.01 43.44	
101	91.54	42.68	91.35	43.08	91.16	43.48	90.97	43.88	
103	9244	43-11	92.25	43.51	92.06	43.91	91.87	44.31	
104	93-35 94-26	43·53 43 95	93.16 94.06	43·94 44.36	93.87	44-34	92.77 93.67	44.75 45.18	
105	95.16	44-38	94-97	44 79	94-77	45.20	94.57	45.62	
106	96.97 96.97	44.80	95.87 96.78	45.22	95.67	45.63	95.47	46.05	
108	97.88	45. 22 45.64	97 68	45.64	96.58 97.48	46.06	96.37 97.28	46. 92	
109	98.79	46.07	98.59	46 50	98.38	46.02	98.18	47-35	
110	99.69	46.49	99.49	46.92	99 28	47.36	99.08	47.79	
112	100.0	47.33	100.4	47.78	100.1	47.79	99.98	48.22 48.66	
123	102.4	47.76	102.2	48.80	102.0	48.65	8,101	49.09	
114	103.3	48.60	103.1	48.63	103.8	49.08	102.7	49.53	
116	105.1	49.02		49 48	1047	49.51	104.5	44.96 50.40	
117	106.0	49.45	105 8	49.91	105.6	50.37	105.4	50.83	
118	106.9	49.87	106.7	50.76	106,9	50.80	106.3	51.26	
120	108.8	50.71	108.5	51.19	107.4	51.66	107.2	51.70 52.13	
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5 4.49 2.19 4.48 2.21 4.47 2.33 4.46 2.25 6 5.39 2.63 5.38 2.65 5.37 2.68 5.36 2.70 7 7.19 3.51 7.18 3.54 7.10 3.57 7.14 3.60 8 7.19 3.51 7.18 3.54 7.10 3.57 7.14 3.60 10 8.99 4.88 9.87 4.87 9.84 4.91 9.82 4.95 11 9.89 4.82 9.87 4.87 9.84 4.91 9.83 4.95 12 10.79 5.26 10.76 5.31 10.74 5.35 10.72 5.40 13 11.65 5.70 11.65 5.75 11.65 5.30 11.161 5.85 15 13.48 6.58 13.45 6.63 13.42 6.69 13.39 6.75 15 13.48 6.58 7.94							1.34	2.68	1.35
6 5 39 2.63 5.38 2.65 5.37 2.68 5.36 2.70 6.39 3.07 6.38 3.10 6.26 3.12 6.25 3.15 6.26 3.12 6.26 3.17 3.60 8.09 3.05 8.07 3.98 8.05 4.02 8.04 4.05 9.00 8.99 4.58 8.07 4.42 8.05 4.02 8.04 4.05 9.00 8.99 4.58 8.07 4.42 8.05 4.02 8.04 4.05 9.00 10 8.99 4.58 8.07 4.42 8.05 4.02 8.04 4.05 11.0 9.53 4.50 11.66 5.31 10.74 5.35 10.72 5.40 11.6 5.70 11.6 5.75 11.6 5.70 11.6 5.75 11.6 5.70 11.6 5.75 11.6 5.70 11.6 5.75 11.6 5.70 11.6 5.75 11.6 5.70 11.6 5.75 11.6 5.70 11.6 5.70 11.6 5.75 11.6 5.70 11.									
7 6.9 3.07 7.18 3.54 7.16 3.57 7.14 3.60 7.19 9.80 3.95 8.07 3.98 8.05 4.02 8.04 4.05 8.09 4.98 8.97 4.43 8.95 4.46 8.93 4.50 1.1 9.89 4.88 9.87 4.87 9.84 4.91 9.82 4.50 1.1 1.1 9.89 4.88 9.87 4.87 9.84 4.91 9.82 4.50 1.1 1.1 9.89 4.88 9.87 4.87 9.84 4.91 9.82 4.50 1.1 1.1 9.89 4.88 9.87 4.87 9.84 4.91 9.82 4.50 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.		-	-						
8 7.19 3.51 7.18 3.54 7.10 3.57 7.14 3.00 10 8.99 4.88 8.97 4.43 8.95 4.06 8.93 4.50 11 9.89 4.82 9.87 4.87 9.84 4.91 9.82 4.95 12 10.79 5.26 10.76 5.31 10.74 5.35 10.72 5.40 11 12.48 5.70 11.66 5.75 11.63 5.80 11.61 5.85 14 12.48 6.58 13.45 6.61 12.53 6.25 11.63 5.80 11.61 12.48 6.58 13.45 6.63 13.41 6.69 13.30 6.75 16 14.18 7.09 11.435 7.08 14.23 7.14 14.23 7.20 11 7.5.28 7.45 15.25 7.52 15.21 7.59 15.18 7.65 18 16.18 7.89 16.14 7.96 16.11 8.03 16.07 8.10 19 17.08 8.33 17.04 8.40 17.00 8.48 16.97 8.55 19 17.08 8.77 17.94 8.85 17.90 8.92 17.86 9.00 17.08 8.77 17.94 8.85 17.90 8.92 17.86 9.00 181 18.87 9.21 18.83 9.29 18.79 9.37 18.75 9.45 12 19.77 9.64 19.73 9.73 19.69 9.82 19.65 9.49 12 19.77 9.64 19.73 9.73 19.69 9.82 19.65 9.49 12 12.77 10.52 22.24 11.06 22.37 11.15 22.31 11.25 12 22.37 11.40 23.32 11.50 23.27 11.60 23.22 11.20 12 24.27 11.82 24.23 11.94 84.16 12.05 84.11 12.15 23 22.67 12.71 26.04 12.38 8.59 12.48 10.07 12.43 10.80 24 25.77 12.77 25.11 12.38 5.06 12.49 25.00 12.00 25 26.06 13.15 26.91 13.27 26.85 13.39 26.79 13.15 28.91 26 12.78 13.15 28.79 14.15 28.51 11.15 28.32 11.25 28 25.17 12.27 23.11 12.38 25.06 12.49 25.00 12.00 28 28.79 14.03 88.70 13.71 27.74 13.83 27.68 13.95 28 25.79 14.03 38.70 13.71 27.74 13.83 27.68 13.95 28 25.70 12.71 26.04 12.83 85.95 12.49 25.00 12.00 28 26.96 13.15 26.91 13.27 26.85 13.39 26.79 13.50 28 28.76 14.03 38.70 14.15 28.64 14.28 28.58 14.40 29.73 14.25 28.58 14.40 29.73 14.25 28.25 14.25 28.25 14.25 28.25 14.25 28.25 14.25 28.25 14.25 28.25 14.25 28.25 14.25 28.25 14.25 28.25 14.25 28.25 14.25 28.25 14.25 28.25 14.25 28.25 14.25 28.25 14.25 28.25 14.25 28.25 14.25 28.25 14.25 28.25 12.25 28.25 28.25 28.25 28.25 28.25 28.25 28.25 28.25 28.25 28.25 28.25 28.25 28.25 28.25 28.25 28.25 28.25 2								2 -	
10	8				3.54		3.57		3.60
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16 14.38 7.01 14.35 7.08 14.32 7.14 14.29 7.20 17 15.28 7.45 15.25 7.52 15.31 7.59 15.18 7.65 18 16.18 7.89 16.14 7.96 16.11 8.03 16.07 8.10 19 17.08 8.33 17.04 8.40 17.00 8.48 16.97 8.55 20 17.98 8.77 17.94 8.85 17.90 8.92 17.86 9.00 81 18.87 9.21 18.83 9.29 18.79 9.37 18.75 9.45 20 0.06 20.63 10.77 20.68 10.66 9.82 19.65 9.90 24 21.57 10.96 22.42 11.06 22.37 11.15 22.32 11.25 25 22.47 11.96 24.22 11.06 22.37 11.15 22.23 11.25 26 0.71 1									
17 15.28 7.45 15.25 7.52 15.21 7.59 15.18 7.65 18 16.18 7.89 16.14 7.96 16.11 8.03 16.07 8.10 17.08 8.33 17.04 8.40 17.00 8.92 17.86 9.00 18.87 17.99 8.77 17.94 8.85 17.90 8.92 17.86 9.00 18.87 9.21 18.83 9.29 18.79 9.37 18.75 9.45 19.23 20.67 10.08 20.63 10.17 20.58 10.86 20.54 10.35 24 21.57 10.96 24.42 11.06 22.37 11.15 22.32 11.25 22.47 10.96 22.42 11.06 22.37 11.15 22.32 11.25 22.247 10.96 22.42 11.06 22.37 11.15 22.32 11.25 28 25.17 12.27 25.11 12.38 25.06 12.49 25.00 12.60 20.63 20.63 20.63 20.63 20.63 20.63 20.63 20.63 20.63 20.63 20.63 20.63 20.63 20.63 20.63 20.64 20.58 10.86 20.54 10.35 22.47 10.96 22.42 11.06 22.37 11.15 22.32 11.25 22.27 24.27 11.84 24.22 11.90 23.27 11.15 22.32 11.25 28 25.17 12.27 25.11 12.38 25.06 12.49 25.00 12.60 20.63 20.6	_								,
18 16.18 7.89 16.14 7.96 16.11 8.03 16.07 8.10 19 17.08 8.33 17.04 8.40 17.00 8.43 16.97 8.55 20 17.98 8.37 17.94 8.85 17.90 8.92 17.86 9.00 21 18.87 9.21 18.83 9.29 18.79 9.37 18.75 9.45 22 19.77 9.64 19.73 9.73 19.69 9.82 19.65 9.90 23 20.67 10.08 20.63 10.17 20.58 10.86 20.54 10.35 24 21.50 10.96 22.42 11.06 22.37 11.15 22.32 11.25 25 22.47 10.96 22.42 11.06 23.27 11.15 22.32 11.25 26 23.37 11.40 23.32 11.94 24.11 12.15 22.32 11.25 26 25.77 12.71 26.04 22.80 12.11 22.11 23.22 12.91 25.0	1		1 '						
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51 45.84 22.36 45.74 22.56 45.64 22.76 45.54 22.95 52 46.74 22.80 46.64 23.00 46.54 23.20 46.43 23.41 53 47.64 23.23 47.53 23.44 47.43 23.65 47.33 23.86 54 48.53 23.67 48.43 23.88 48.33 24.09 48.22 24.54 49.11 24.76 55 49.43 24.11 49.23 24.77 50.12 24.99 50.01 25.21 56 50.32 24.99 51.12 25.21 51.01 25.43 50.90 25.66 57 51.23 24.99 51.12 25.21 51.91 25.88 51.79 26.11 58 52.13 25.43 52.92 26.10 52.80 26.33 52.69 26.56 59 53.93 26.30 53.81 26.54 53.70 26.77 53.58 27.01									
52 46.74 22.80 48.64 23.00 46.54 23.00 40.53 23.65 47.33 23.86 48.53 23.67 48.43 23.88 48.33 24.09 48.22 24.31 55 49.43 24.11 49.33 24.34 49.22 24.54 49.11 24.76 56 50.33 24.55 50.32 24.77 50.12 24.99 50.01 25.21 57 51.23 24.99 51.12 25.21 51.01 25.43 50.90 25.66 58 52.13 25.43 52.02 25.65 51.91 25.88 51.79 26.11 59 53.03 26.30 53.81 26.54 53.70 26.77 53.58 27.01									22.95
54 48.53 23.67 48.43 23.88 48.33 24.09 48.22 24.31 55 49.43 24.11 49.33 24.33 49.22 24.54 49.11 24.76 56 50.33 24.55 50.32 24.77 50.12 24.99 50.01 25.21 51.01 25.43 50.90 25.61 52.21 51.01 25.43 50.90 25.61 52.21 51.01 25.43 50.90 25.66 53.93 26.30 53.81 26.54 53.70 26.77 53.58 27.01	52	46.74	22.80	46.64	23.00	46.54		46.43	
55 49-43 24-11 49-33 24-33 49-22 24-54 49-11 24-76 56 50-33 24-55 50.32 24-77 50.12 24-99 50.01 25-21 57 51-23 24-99 51.12 25-21 51.01 25-43 50.90 25.66 58 52.13 25-43 52.02 25.65 51.91 25.88 51.79 26.11 59 53.03 26.30 53.81 26.54 53.70 26.77 53.58 27.01 60 53.93 26.30 53.81 26.54 53.70 26.77 53.58 27.01							1		
56									
57 51.23 24.99 51.12 25.21 51.01 25.43 50.90 25.66 58 52.13 25.43 52.02 25.65 51.91 25.88 51.79 26.11 59 53.03 26.30 53.81 26.54 53.70 26.77 53.58 27.01	_						24.99		25.21
59 53.03 26.30 52.92 26.10 52.80 26.33 52.69 26.56 60 53.93 26.30 53.81 26.54 53.70 26.77 53.58 27.01	57		24.99	51.12	25.21	51.01		20.90	
60 53.93 26.30 53.81 26.54 53.70 26.77 53.58 27.01									
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	Dist	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat	Dep.
1	61	54.83	26.74	54.71	26.98	54-59	27.22	54-47	27.46
1	52	55.73	37.18	55.61	27.42	55.49	47.66 . 48.11 .	55.36 56.36	27:91 18.36
ı	63 64	57.52	27.62 28 06	56.50	27.86 28.31	56.38	28.56	57-16	28.81
	65	58.42	28.49	58.30	28.75	58.17	19.00	58.04	29.26
	66	59.22	28.93	59.19	29.19	59.07	29.45	58.94	29.71
1	67	63.22	29.37	60.09	29.63	59.96	29.90	59.83	30.16
·	68	6611	29.81	61.88	30.08 30.52	60.86 64.74	30.34	61.62	30.61 31.06
	70	, 62.02 61.92	30.25 30 69	61.78	30.96	5265	31.23	62.51	81.51
	71.	63.81	31.12	63.68	31.40	63.54	31.68	61.40	31.96
	72	5471	31.56	54-57	34.84	64.44	32.18 .		32.41
1	73	55.61	32.00	55.47	32.39	Ъ5.33.	32.57 :		32.86
J	24.1	66.54	32.44	66.37	32.78	56.23 57.11	33.02 33.46	66.97	33 34
	75	67.41	32.88	68.16	33.61 33.61	68.02	33.91	67.87	34.21
·	76 77	68.34 69.21	33.32	69.06	34.06	58.91	34.16	68.76	34.66
	78	70.11	34.19	69.96	34.50	69.80	34.80	59.65	35.14
1	79	71.00	34.63	70.85	34.94	70.70	35.25	70.55	35 56
1	13	71.90	35.07	91.75	35.38	71.59	35.70		36.01
-	81	72.80	35.51	72.65	35.83	72 49	36. E4 36. 59	7233	36.46 36 91
1	83	73.70	35.95 36.38	73.54	36.27 35.7.1	74-28	37.03	7412	37.36
1	84	75.50	36.84	75-34	37.05	75.17	37.48	75.01	37.81
1	85	76.40	37.26	·76.23	37.59	76.07	37 93	75.90	38.26
1	86	.77.30	37.70	77.43	38.04	76.96	38.37	76.80	38.71
	87	78.20	38.14	78.03	38.48	77.86	38.82 39.27	77 69	39 16 39.61
1	88 8g	79.0g	38,58 39.01	78.92 79.82	38.91 39.36	78.75. 79.65	39.71	79.48	40.06
	90	80.89	39.45	80.73	39.81	\$0.54	40.16	80.37	40.51
1	93	\$1.79	39 89	81.62	40.15	81.44	40.60	81.36	40.96
1	92	\$2 69	40.13	\$2.51	40.69	\$2 33	41 05	82,15	41.41
	93	3.59	40.17	83.41	41.13	83,23 84,12,	41.50	83.05	41.86
1	94 95	\$4.49 \$5.39	41.11 41 65	84.31 85.20	42.02	85,02	42.39	84.82	42.76
	96	86.28	42.08	86:10	41.46	85.91	42.83	85.73	43.21
1	97	87.18	42.53	87.00	42.90	86.81-	43 28	86:62	43.66
1	98	80.88	41.96	87.89	43.34	87.70	43.73	87.51.	44 14
	99	88.98	43.40	88.79 89.69	43.79	88 60- 89.49	44.62	88.40 89.30	44.5 6 45.01
1	_	89.88	43.84	90.58	44.67	90.39	45.07	90.19	45.46
1	101 102	90.78 91.68	44.71	91.48	45.11	91.38	45 51	91.08	45.91
1	103	92.58	45.15	92.38	45.56	92.18	45.96	91.98	46 36
	104	93-47	49.59	93-27	46 00	93.07	46.40 46.85	92.87	46.81
ł	105	94:37_	46.03	94.17	46.44	93.97	47.30	93,76	47.26
ı	106	95.37	46.47	95.07	46.88 47.32	94.86 95.76	47.30	94 66	47.71 48 16
1	107	96.17 97.07	46.gt	96.86	47.77	96.65	48.19	96.44	48.61
1	100	97.97	47 78	97.76	48.21	97.55	48.64	97.33	49.06
1	OI E	98.87	48.23	98.66	48.65	98.44	49.08	98.23	49.51
	111	99.77	48.66	99.55	49.09	99-34	49.53	99.12	49.96
4	112	100.7	49.10	100.4	49.54 49.98	100.2	49.97 50.43	100.0	50.41
4	113 114	101.6	49.54 49.97	101.3	50.42	102.0	50.87	105.9	50.86
1	115	103 4	50.41	103.1	50 86	102.9	51.31	102.7	\$1.76
	116	104.3	50.85	1040	51.38	103 8	51.76	103.6	52.21
1	117	104.2	51.29	104.9	51.75	1047	52.21	104.5	52.66
-1	118	106.1	51.73	105.8	52:19	104.6	52.65 53.10	105 4	53.11
ł	119	107.0	52.60	107.6	53.07	107.4	53.54	107.2	54.01
1		Dep.	Lat.	Dep.	Lat	Dep.	Lui	Dep.	
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P.	Lat	Dep.	Lat.	Dep	Lat.	Dep.	Lat.	Dep
1	0.89	0.45	0.89	10.46	0.89	0.46	0.83	0.47
3	1.78 2.67	0.91 1.56	2.67	0.92 1.37	1.77	D.9%	4.77 2.65	0.93
3 4	3.56	1.82	3.56	183	3.55	1.85	3-54	1.86
_5	4.46	2 27	445	2.29	444	2 31	443	2.33
6	§-3 5	2.72	5.33	2-75	5.32	2-77	5.31 6.19	2.79 3. 26
- 7 8	6.24 7.13	3.18 3.63	7.11	3.21 3.66	6.21 . 7.10	3.23	7.08	3.72
9	8.02	4.09	8.00	4.13	7.98	4.16	7.96	419
10	8.91	4.54	8.89	4.58	8.87	4.61	8.85	4-66
11	9.80 10.69	4-99 5-45	9.78	5.04	9.76 20. 54	5.08 5.54	9.73	5.13 5.59
13	11.58	5.90	11.56	5.95	21.53	6.00	1450	6 05
14	12.47	6.36	12.45	6.41	72.43	6.46	1239	6.58 6.98
15	13.37	6.81	13-34	7.33	13.31	7-19	13.27	7-45
16	14.26	7-26 7-72	15.11	7.78	14:19	7.85	15.04	7-92
18	16.04	8.17	16 00	8.24	15.97	8.31	15.93	8.38
19 20	16.93 17.82	8.63 9.08	16.8g	8.70 9.16	16.55	8.77 9.24	17.70	8.85 9.81
1	18.76	9 53	18.67	9.62	18.62	9.70	18.68	9.78
22	19.60	9.99	19.56	10.07	19.51	10,16	19.47	10.34
23	20.49	10.44	20.45	10.53	20.40	10.62	20.35	10.71 11.17
25	21 38	10.90	21.34	10.99	22.18	11.08 E1.64	24.24	11.64
26	23.17	11.80	23.11-	11.90	23.06	12.01	23.01	12.11
27	24.06	12.26	24 00	12.36	23.95	12.47	25.89	12.57
28	24.95	12.71	24.89 25.78	12.82	. 24.84 85.72	12.93	24.78 25.66	13.04
30	26.73	13.62	26.67	13.74	26.61	13.85	26.55	13.97
31	27.62	1407	27.56	14.19	27.50	14.31	27.43	14-43
32	28.51	14-53	28.45	14.65		14.79	\$8.32	14-9 7 15-37
33 34	29:40 30,26	14.98	29.34 30 23	15.11	30.16	15.24	30.00	15.83
35	31.19	15.89	31.12	16.03	31.05	16.16	10.97	16.30
36	32.08	16 34	32,00	16.48	31:93	16.62	31.86	16.76
37 38	32-97	16.80	32.89 33.78	16.94	32.82	17.08	32 74 33.63	17 83 17.69
39	34.75	17.71	34-67	17.86	34/59	18.01	34-51	18.16
40	35.64	18.16	35.56	18,33	35.48	18.47	35-40	18.62
41 42	36.53 · 37.42	1861 19.07	36.45 37.34	18.77	36.37 37.25	18.93	36.28	19.56
43	38.31	19.52	38.23	19.69	38.14	19.86	38.05	20 02
44	39.40	19.98	39.11	20.15	39.03	20.32	38.94	20.49
45	40.10	20.43	40.01	20.60	39 92	20.78	39.82	20.95
47	40.99	21.34	40.89	21.52	40.80	21.24	41.59	21.42
48	42.77	21.79	42.67	21.98	42.58	32 16	42.48	22.35
49 50	44.55	22.25	43.56 44.45	22.44	43.46 44-35	22.63 23.09	43.36	23.28
51-	45.44	23.15	45.34	23.35	45.24	23.55	45.13	23.75
52	46.33	25.61	46.23	23.81	46.12	24.01	46.02	24.21
53	47.23	24.06	47.12	24.27	47 01	24.47	46.90	24.68
54 55	48.11	24.52 24.97	48.90	24.73 25.18	47.90 48.79	24-93 25 40	47.79	25.14 25.61
- 56	49.90	25.42	49.78	25.64	49.67	25.86	49.56	26.07
57	50.79	25.88	50.67	26.10	50.56	26 32	50.44	26.54
58 59	51.68 52.57	26.33 26.79	52.45	26.56 27.01	\$1.45 \$2.33	26.78 27.24	51.23 52.21	27.01 27-47
60	53.46	27.24	53.34	27.47	53.82	27.70	53.10	27.94
ي -	Dep.	Lai	Dep.	Lut.	Dep	Lat	Dep.	Lat.
Dist.	0/		4	,/	30'		13	

or negaters.

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1 2	LAL	Dep.	Lat	D-p.	Lat.	D-p	Lat	Dep.
61	5435	27.69	5+23	27 93	54.11	28.17	53.98	28.40
60	55.84	28.60	56.01	28.39 28 8 g	54-99 55.88	28 63 29.09	54-87 55-75	28.87
63	57.02	29.06	56.90	29.30	56.77	29.55	56.64	29.80
65	57-92.	29.51	57-79.	29.76	57.66	30.01	57.52	30.26
66	58.81	29.96	58.68	30.22	58-54	30.48	58.41	30.73
68	59.70 60.59	30.47	59:56 60:45	30.68	59-43 60.32	30.94 31.40	59.29 60.18	31.66
69	61.48	31.33	61.34	31.59	61.20	31.86	61.06	32.13
70	62.37	31.78	62.23	32.05	62.09	32.32	62.83	32.59
71 72	63:26	32.23	63.12 64.01	32.97	62.98 63.86	32.78	63.72	33.52
73		33.14	6490	33.44	64.75	33.71	64.60	33 99
74	4: 50	33.60 34.05	65.79	33.88	65.54	34.17	65.49 66.37	34.46 34.92
75	67:72	34-50	67.57	34.80	67.41	35.09	67.26	35-39
77	68.61	34 96	68.45	35 26	68.30	. 35-55	68.14	35.85
78	69.50	35.48	69.34	35.71		36.02	69.03	36.32 36.78
79 80	70 gg	35.87 36.33	70.23 71.13	36.63	70.07	36.48 36.94	69.91 70 80	37.25
11		36.77	7401	37.09	71 85	37-49	71.68	37.71
82	73.06.	37.43	72.90	37 55	72.73	37.86	73.57	38 18
83 84	73-95 : 74-84		73.79	38.00 38.46	73.62	38.33 38.79	73-45	38.65 39.11
85	75.74	38.59	25-57	38.92	75.40	39 25	75.22	39.58
86	76.63	39.04	76.46	39-38	76.28	39.71	76.11	40.04
87	77-53.		77.34	39.84	77-17	40.17	76.99 77.88	40.51
88 9	7841 79-30	39-95 40-41	78.23	40 75	78.94	40.63	78.76	41.44
90	80.19	40.86	80.01	41.21	79.83	41.56	79-65	41.91
91	81.08	41.31	80.90	41.67	80.72	42.02	80.53	42.84
93	\$1,97 \$1.86	41.77	.81.79 82.68	42.12	81.61 . 82.49	42.48	81.42 82.30	43.30
94	83.75	42.68	83.57	43.04	83.38	43.40	83.19	43.77
95	84.65	43.13	84.46	43.50	84.27	43 87	84.07	44 23
96 97	85.54 86.43	43.58	85 35 86.23	43 96	85.15 86.04	44-33 44-79	84.96 85.84	44.70 45.16
98	87.32	44-49	87 12	44.87	86.93	45.25	86.73	45.63
99	86.10	44-95	88.90,	45-33	87.81 88.70	45.71	87.61 88.50	46.10
101	89.99	45.85	89.79	45.79	89.59	46.04	89.38	47.03
101	90 88	46.31	90.68	46.70	90.48	47.10	90.27	47.49
103	91.77	46.76	91.57	47.16	91.36	47.96	91.15	47.96
104	92.66	47.67	92.46	47.62 48.08	92.25	48.48	92.04	48.42 48.89
106	94.45	48.12	94-24	48.53	94.02	48.91	93.81	49 36
107	95-34	48.58	95.12	48.99	94.91	49 41	94.69	49.82
109	96.23 97.12	49 03 49 49	96.90	49.45	95.80	49.87	95,58	50.29 50.75
110	10.86	49.94	97.79	50 37	97-57	50.79	97.35	51.22
111	98.90	50.39	98.68	50.82	98.46	51.25	98.23	51.68
112	99.79	50.85	99 57	51.28		51.72	99.12	52.15
113	100.7	51.30	100.5	51.74	100.2	52.18	100.9	53.08
115	103.5	52.21	102.2	52 66	102.0	53.10	101.8	53 55
116	103.4	52.66	103.1	53.11		53.56	132 7	54.01
317 £18	104.2	53 12 53 57	104.0	53.57 54.03	103.8	54.02	103.5	54-48 54-9 4
119	106.0	54.02	105.8	54-49	105.6	54-95	105.3	55.41
3 20	106 9	54.48	106.7	54-94	106.4	55.41	106.2	55.87
ng H	Dep.	Lat.	Dep.	Lat.	Dep.	Lui	Dep.	Lit
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	Dist	Lat	Dep.	Lat.	Dep.	Lat.		Lat.	Dep.	L
1-	;	0 88		0.88		0.88	Dep.	0.88	0.48	ſ
1	1	1.77	0.47	1.76	0.47	1.76	0.48	1.75	0.96	į
I	3	2.65	1.41	2.64	1.42	2.64	1.43	2.63	1-44	l
1	4	3.53	1.88	3.52	1.89	3.52	1.91	3.51	1.92	l
_	5	4.41	2.35	4.40	2.37	4.39	2.39	4.38	2.40	ŧ
1	6	5.30	2.82	5.19	2.84	5.27	2.86	5.26	2.89	ł
1	7	6 18 7.06	3.29 3.76	7.05	3.31	6.15 7.03	3.34	7.01	3.37	ł
1	9	7.95	4.23	7.93	4.26	7.91	4.29	7.89	4-33	ł
1	10	8.83	4.69	18.8	4.73	8.79	4.77	8.77	4.81	ļ
-	11	9.71	5.16	9.69	5.21	9.67	5.25	9 64	5.29	ŀ
•	12	10.60	5.63 6.10	10.57	5.68	10.55	5.73 6.20	10.52	5.77 .6 25	ľ
	13	11.48	6.57	11.45	6.63	11.42	6.68	11.40	6.73	I
	14	13.24	7.04	13.21	7.10	13.18	7.16	13.15	7.21	ı
_	10	14.13	7.51	14.09	7.57	14.06	7.63	14.03	70	I
	17	15.01	7.98	14.98	805	14-94	8.11	14.90	8.18	L
	18	15.89	8.45	15.86	8.52	15 82	8.59	15.78	8.66 9.84	ľ
	19	16.78	9.39	16.74	8.99 9.47	17.58	9.07	17.53	9.62	ľ
1-	20	18.54	9.86	18 50	9.04	18.46	10.02	18.41	10.10	ľ
	21	19.42	10.33	19 38	10.41	19.33	10.50	19.29	10.58	Ł
	23	20.31	10 85	20.26	10.89	20.21	10.97	25, 16	11.06	ľ
1	2.4	21.19	11.27	21.54	11.36	21.09	11.45	21,04	11.54	ŀ
-	25	22.07	11 74	22 02	11.83	21 97	1195	21.92	12.02	ľ
	26	22 96	12.21	22.90	12.78	22.85	12.41	22 79 23.67	12.51	ł
	27	23 84	13.15	24.66	13.25	24 61	13.36	24.55	13.47	l
	20	25.61	13.61	25.55	13.73	25.49	13.84	25.43	13.95	L
1	30	26.49	14.08	26.43	14.20	26.36	14.31	26 30	14 43	ŀ
	31	27.37	14.55	27 .	14.67	27 24	14.79	7.18	1491	ŀ
	32	28.25	15.02	28.19	15.15	28.12 29.00	15 27	28.06 · 28.93	15.39	ŀ
	33	29.14 30.02	15.49 15.96	29 07 29.95	15.62	29.88	15.75	29.81	15.82	ľ
	34	30.90	16.43	30 83	16 57	30 76	16.70	30.69	16.83	ŀ
1-	36	31.79	16 90	31.71	17.04	31 64	17.18	31.56	17.32	ŀ
	37	32.67	17.37	32 59	17.51	32.52	17.65	32.44	17.80	ŀ
	38	33.55	17.84 18.31	33.47	17.99	33.40	18.61	33.32	18.28	l
	39	34-44 35-32	18.78	34-35 35 24	18.93	34-27 35-15	19.03	34.19 35.07	18,76	I
-	40	36.20	19.25	36 12	19.41	36.03	19.56	35.95	19.73	I
	41 42	_	19.72	37.00	19.88	36.91	20.04	36.82	20.20	ł
	43	37.97	20.19	37.88	20.35	37.79	20 52	37.70	20.68	ł
	44	38.85	20.66	38.76	20.83	38 67	20.99	38 58	21.16	ŀ
	45	39 73	21.13	39.64	21.30	39.55	2 47	39.45	21.64	L
	46	40 62	21 60	40.52	21.77	40.43	21.95 22 43	40.33	22.13 22.61	ł
1	47	41.50	22.59	42.28	22.72	42.18	22 90	42.08	23.09	l
	49	43.26	23.00	43.16	23.19	43.06	23 38	42,96	23 57	ŀ
	50	44.15	23.47	44.04	23.67	43 94	23.86	43 84	24.05	ł
1	51		23.94	44 93	24 14	44.82	24.34	44.71	24 53	l
1	52	45.91	24.41 24.88	45.81	24.61	45.70	24.81	45.59	25.01	I
	53 54	47.68	25.35	47-57	25.56	47.46	25.77	46.47 47.34	25.4 9 25.97	ĺ
	55	48.56	25.82	48 45	26.03	48.33	26.24	48 22	26.45	l
-	56	49.45	26.29	49.33	26.51	49.21	26.72	49.10	26 94	Į
•	57	50.33	26.76	50.21	26.98	50.09	27.20	49-97	27.42	t
1	58	51.21	27.23	51.09	27.45	50.97	27.68	50.85	27.90	ĺ
1	59 6 0	52.09 52,98	27.70	51.97 52.85	27 93 128.40	51.85 52.73	28.15 28.63	51.73 52.60	28.38 28.86	ı
		Dep	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lil	ŀ
ŀ	Dist	0		45		30/		15		ľ
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छ	0′		15	,	3	04	45"	
Dist	Lat	Dep.	Late	Dep.	Lat.	D-p	Lat	D
61	53.86	28.64	53-73	28.87	53.6 E	29.11	53.48	29 54
63	5474 55.63	29.11	54.62	29.85	54-49	30.06	54.36	29.8 30.3c
64	56.51	30.05	56.38	30.29	55-37 56 24	30.54	55.23	30.7
65	57-39	30.52	57.26	30.77	57-12	31.02	56.99	31 20
66	58:27	30.99	58.14	31.24	58.00	31.49	57 86	31.7
67 68	59-16	31.45 31.48	59.90°	31.71	58.88 59.76	31 97	58.74	32.,
69	60192	32.39	60 78	32.66	60.64	32 92	60.49	33.41
70	61.81	32.86	61.66	33.13	61.52	33.40	61 37	33.6
71	62.69	33. 33 . 33. 80	62.54 63.42	33. 61 34.08	63.47	33.88 34.3 6	62.25	34.1 , 34 b
73	63.57 64.46	34.27	6435	34.55	6.3.15	34.83	64.00	35.1
74	65.34	34.74	69.19	35.03	65.03	35.31	64.88	35-59
.75	66.22	35.81	66.07	35 50	65.91	35.79	65.75	36.07
76 77	67.50	35.68 36.15	66.95	35 97 36.45	66.79 67.67	36.26 36.74	66.63	36.56° '37.04
78	68,87 .	36.62	68.76	36.92	68.55	37.83	68.38	37.52
79	69.75	37.09	69.59	37.59	69 43	37.70 38.17	69.26	38.00
80	7 0.64	37.56	7947.	37.87.	70.31	38.65	79.14	38.48
81 82	71.54	38.50	7423	38.81	7 % 18 72.06	39.13	7489	39.44
83	73.28	38.97	73.11	39.29	72.94	39.60	7477	39.92
84 85	74.87 75.05	39.44 39.91	7 3-99 -74-88	39 7 6 40 23	73.82	40.08 40.56	73.65 74.52	40.40
86	75.93	40.37	75.76	40.71	75.58	41.04	75.40	41.37
87	76.82	40.84	76.64	41.18	76.46	41.51	76.28	41.85
88	77.70	41.35	77.52 78.40	41.05	77-34	41.99	77.15	42.33 42.81
90	78.58	41.78	79 28	42.60	78-21	42.94	78.91	43.29
91	80.35	48 72	80.16	43 97	79.97	43.42	79 78	43.77
92	81.23	43.19	81.04	43:55	80.85	43.90	80.66	44.25
93 94	82411	43.66 44.13	81.93	44.49	81.73 82.61	44 38 44 85	81.54	44 73
95	83/88	44 60	83.68	44.97	83.49	45.33	83,29	45.64
96	84.76	45.07	84.57	45.44	84.37	45.81	84.17	46.17
97 . 98	85 65 :86.43	45.54 46 OI	85.45 86.33	45.91	185.25	46.76	85,Q4 85,Q3	46.66 47-14
99	87.41	46.48	87.21	46.86	87.00	47.24	.86,80	47.62
100	88.29	46.95	88.09	47.33	87 88	47.73	87.67	48.10
101	89.18	47 42	88.97	47 81 48.28	88.76	48.16 48.67	88.55 89.43	48.58
102	91.94	47.89 48.36	89.85 90.73	48.75	89,64 90.52	49.15	90.30	49.06 49.54
104	91.83	48.82	91161	49.23.	91.40	49.62	91.18	50.02
105	92.71	49.39	92.49	49.73	92.28	50.10	92.06	50.50
106	93.59	49.7 6 50. 2 3	93.37	50.05	93.15	50.58 51.06	92.93	50.98
108	95.36	50.70	95.14	51.44	94.91	51.53	94-69	51.95
109	96.24	51 27	96,02	51.99	95.79	52.01	95.56	53.43
10	97.12	51 64	96.90	53.07	96.67	52.49	96.44	53-39
111	98.89	52.58	97.78	52-54	97-55 98-43	52.96 53 44	98.19	53.87
113	99-77	53.05	99.54	53.49	99.31	53.92	99.07	54-35
114	100.7	53.52	100.4	53 90 54 43	100.2	54.40 54.87	99.95	54.8 <u>3</u>
116	102.4	53- <u>99</u> 54-46	100.3	54.90	101.9	55-35	101.7	55.79
117	109.3	54-93	103.1	55.38	102.8	22.83	102.6	56.28
118	104.3	55.40	103.9	55.85	103.7	56.30	108.5	57.24
1 19	106.0	55.87 56.34	104.8	56.33 56.80	104.6	56.78 57.26	104.3	57-72
-	Dep.	Let.	Dep	Lat.	Dep.	Lat.	Dep.	Lat
ă.	0	-	45	,	30	7	1.	5,

		0/		57	30	/	45	,
Di at					-			-
1	Lat	Dep.	Let	Dep.	Lat.	Dep.	Lat.	Dep.
1	0.87	0.48	0.87	0.49	0.87	0.49	0.87	0.50
2	1.75	0.97	1:75 2.63	0.98	2.61	0.98	2.60	1.49
3	2.62	1.45	3.49	1.47	3.48	1.97	3.47	1.98
4	3.50 4.37	2.42	4.36	2.44	4-35	2.46	4.34	2 48
- 5	5.25	2-91	5.24	2:03	9.22	2.95	5.21	2.98
7	6.12	3 39	6.11	3.42	6.09	3-45	6.08	3-47
8	7.00	3.88	€.98	3.91	6.96	3.94	6.95	3.97
9	7.87	4.36	7.85	440	7.83	4-43	. 7.81	4:47
ıó	8.75	4.85	8.73	4.89	8 70	4.92	8.68	4.96
11	9.62	5.33	9.60	5.37	9 57	5.42	9-55	5.46
12	10.50	5.82	10.47	5.86	10.44	5.40	10.42	5-95 6-45
13	11.37	6.79	11.34	6.84	12.18	6.80	12.15	6.95
14	13.12.	7.27	13.09	7.33	13.06	7 39	13.03	7.44
15		7.76	13.96	7.82	13.93	7.88	13.89	7.94
16 17	13 99 14.87	8.24	14.83	8.31	14.80	8.37	14.76	8 44
18	15.74	8.73	15.70	8.80	15.67	8.86	15.63	8.93
19	16.62	9.21	16.58	9.18	16 54	9 36	16.50	943
20	17.49	9.70	17.45	9.77	17.41	9.85	17.36	9.92
21	18.37	10.18	1842	10.26	18.28	10.34	18.43	10.43
22	19.24	10.67	19.19	10.75	19.15	10.83	19-10	10.93
23	20.12	11.15	50:07	11.73	20.02	11.82	20.84	11.91
24	20.99	12,12	20.94	12.22	21.76	12.31	21.70	12.41
25		1261	12.68	12.70	23.63	12.80	22.57	12.90
26 27	23.74 23.61	13.09	23.56	13.19	23.50	13.30	23.44	13.40
28	24 49	13.57	24:43	13.68	24-37	13.79	24 31	
29		14.06	25.30	14.17	25.24	14.28	25.18	14.39
30	26 24	14-54	26.17	14.66	26.11	14-77		14 89
31	37.11	15.03	27.05	15.15	26.98	15.27	26.91	15.38
32	27.99	15.56	27.92	15.64	27.85	15.76	27.78 28.64	16.38
33		16.48	28.79 29,66	16.64	28.72	16.74		16.87
34	29.74 30.61	16.97	30.54	17.10	30 46	17.23	30.39	17-37
36	31.49	17.45	31.41	17.59	31.33	17.73	31.26	17 86
37		17.94	32.28	18.08	32.20	18.22	32.12	18.36
38		18.42	33.15	18.57	33-07	18.71	32,99	18 86
39	34.11	18.91	34.03 .	19.06	33.94	19.20		19.35
40	34.98	19.39	34.90	19.54	34.81	19.73	34-73	
41	35.86	19.88	35.77	20.03	35.68	20.19	35,60 36 46	,20.34 20.84
42	36.73	20.36 20.85	30.64	20.52	36.55	21.17	37-33	21 34
43	37.61 38.48	20.05	37.52	21.50	38.30	21.67	38.20	21.83
44 45	39.36	21.82	39.26	21.99	39.17	22.16	39.07	22.33
46.	40.23	22.30	40.13	22 48	40.04	22.65	39.94	22.83
47	41,11	22.79	41.01	22.97	40.91	23.14	40.81	23.32
48	41.98	23.27	41.88 •		41.78	23.64	41.67	23.82
49		23.76	42.75	23.94	42 65	24.13	42.54	24.31 24.81
50		24.24	43.62	24.43	43:52		ــــــــــــــــــــــــــــــــــــــ	
51	44.61	24 73	44.50	24.92	44-39 45-26	25.61	44.28	25.80
52	45.48	25.21 25.69	45 .3 7	25.41 · 25.90	46.13	26.10	46.01	,26.30
53	46.35	26.18	47.11	26.39	47.00	26.59	46.88	26.80
54	48.10	26.66	47.99	26.87	47.87	27.08		27.29
	48.98	27.15	48.86	27.36	48.74	27.58	.48.62	27 79
56 57	49.85	27 63	49.73	27.85	49.61	28.07	49-49	28.28
58	50.73	28.12	50,60	28.34		28.56		28.78
59	51.60	28.60	51,48	28.83		29.05	51.22	29.28 29.77
60	52.48	29.09	52.35	29.32	52.22	29.55		Late
1	Dep.	Lat.	Dep	Lat.	Dep.	Lut.	Dep.	
1.5	. 0'		4	J'	30	/	1 1:	5′.

T H	. 0'		15.		30'		451	
F.	Lat	Dep.	Let.	Dep	Lat.	Dep.	Lab	Dep.
61	52-35	29-57	53.23	20.81	53.09	30.04	52.90	30.27
62	54-28	30.06	54.09	30.89	53.96	30.53	53.83	30.77
63	55.10	30:54	54-97	30.78	54.83	31.02	54.70	31.26
65	55.98 56.85	31.03	55.84 56.71	31.27 31.76	55.70 56.57	31.52	55.56 56.43	31.76
66	57-72	33.00	57.58	32.25	57.44	32.50	57.30	32.75
67	58.60	32.48	58:46	32.74	58 38	32.99	58.17	33.25
68	59.47	32.97	59-33	33.23	59.18	33-48	59.04	33.74
70	60 35	33-45	61.07	33.71 34.20	60.05	33. 98 34. 4 7	59.91 60.77	34-74
72	62.10	34-42	.61.95	34.69	61.80	34.96	61.64	35.23
72	62.97	34.91	62.83	35.18	63.67	35-45	62.51	35.73
73	63:85	35.39	63.69	35.67	63.54	35.95	63.38	36.22
74 75	65.60	35.88 36.36	64.56	36.65	65.28	36.44 ·	64.25	36.72 37 22
76	66.47	36.85	66.31 .	37.14	66.15	37-42	65.98	37.71
77	67.35	37.33	67.18	37.62	67.02	37.92	66 85	38.21
78.	68.22	37.82	68.05. 68.93	38.31 18.60	67.89 68.76	38.41	67.78	38.70
79	69.97	38.30 38.78	69.80	39.09	69.63	38.90	68 59 69.46	39.20
1	70.84	39.17	70.67	39.58	70.50	39.89	70.32	40.19
80	71.72	39.75	71.54	40.07	71.37	40 38	71.19	40.69
83 84	72.59	40.24	73.43	40.56	73.34	40.87	72.06	41.19 41.68
85	73-47 74-34	40.72	74.16	41.04 41.53	73.98	41.36	72.93	42.18
86	75.22	\$1.69	75.03	42.02	74.85	42.35	74.67	42.67
87	76.09	42.18	75.91	42.51	75.72	42.84	75-53	43.17
88	76.97	42.66	75.55	43.00	76.59	43 53	76.40	43.67
90	77.84 78.72,	43.15 - 43.63	78.52	43.49 43.98	78.33	43.83	77.27 78.14	44.66
91	79-59	44-12	79.40	44-46	79.20	44.81	79.01	45.16
92	80 47	44.60	80.37	44-95	80.07	45.90	79.87	45.65
93	81.34 82.11	45.09	81.14	45-44	80.94 81.81	45.80 46.29	8074	46.64
94	83.09	45.57	8289	45.93 46.42	8268	46.78	8248	47.54
96	83.96	46.54	83:76	46.91	83.55	47.27	83.35	47.64
97	·84.84	47.03	84.63	47.40	84.42	47.77	84.22	48.13
98	85.71 °	48.00	85.50 86.38	47 88 48.37	86.17	48.86	85.08	48.67
100	87.46	48.48	87.25	48.86	87.04	49-24	86.82	49.62
101	88,34	48.97	88.12	49-35	87.91	49-73	87.69	50.12
101	89.21	49.45	88.99	49.84	88.78	50.23	88.56	50.61
103	90.09	49.94	89.87 90.74	50.33 50.83	89.65 90.53	50.72	90.42	51.11
105	91.84	50.91	95.61	51.31	91-39	51 70	97.16	52.10
106	92.71	51.39	92.48	51.79	92 26	52.20	92.03	52.60
107	93.58	51.87	93.36	52.28	93.13	52.69	92.90	53. to
108	94.46 95.33	52.36	94.23	52.77	94.87	53.67	93.77	53.59 54.09
110	96.21	53.33	95.97	53 75	.95.74	54.17	95.50	54.58
111	97.08	53.81	96.85	54.24	96.61	54.66	96.37	55.08
212	97.96	54.30	97.72	54-73	97-48	55.15	97-24	55.58
213.	98.83	54.78 55.27 .	98.55 99.46	55.21 55.70	98.35	55.64	98-11 98-97	56.C7
115	100.6.	55.75	100.3	56.19	100.1	56.63	99.84	57.06
116	101.5	56.24	101.2	56.68	101.0	57.13	100.7	57.56
117	102.3	56.72	102.1	57.17 57.66	101.8	57.61	101.6	58.06
119	103.2	57 21 57.69	103.8	58.15	102.7	58.60	103.4	58.5 5 59.0 5
1 20	105.0	58.18	1047	58.63	1044	59.09	104.2	59-55
z i	Dep.	Lat.	Dep.	Lat	Dep.	Lut	De j .	Lat.
Dia	Ú	,	45	DRCD	30		15	

· E	0/		15	,	30),	45	
Diet	Lnt.	Dep.	Lat	Dep.	Lat.	Dep.	Lat.	Dep.
-	0.87	0.50	0.86	0.50	0.84	0.51	0.86	0.51
2	1-73	1,00	1.75	1,01	1.72	1.02	2.78	1.02
3	8.60	1.50	2.59	1 51	2.58	1.58	0.58	2.05
4	3.46 4.33	2.50	9.46 4.31	2.53	3:45 4:31	2.03 2.54	3.44 4.30	2.56
- 5	.5.29	3.00	6.13	3.08	5.17	3.05	5.16	3.07
7	6.06	3 50	6.03	3.53	6.03	3.55	601	3.58
8	6.93	4.00	6.ge	4-03	4.89	4.06	6.88	4.09
10	7.79 8.66	4.50 5 00	7.77 8.64	4.53 5.04	7.75 8.51	4.57°	7.73 8.59	5.81
-11	9.53	5.50	9.50	5-54	9.48	5.58	945	5.62
12	10.39	6.00	10.37	6.05	16.34	6.09	10.31	6.44
13	11.26	6 50	11.23	6.55	11.20	6 60	1 17	6.65 7-16
14	13.13	7.00 7.5G	12.96	7.56	11:06	7.41	12.69	7.67
16	13.86	8.00	13.84	8.06	43.79	8.12	13.75	8.18
17	1472	8.50	14.69	8.56	1465	863	14.66	8.69
*8	1559	9.00	15.55	9.07	35.51	9.14	15.47	9.10.
19	16.49	9.50	16.41	9.57	16 37	9.94	16.33	9.71
20	18.19	10.50	18 14	10.58	48.00	10.66	18.04	10.74
21	19.05	11.00	19.90	11.06	18.96	11.47	18.9.1	18.25
23	19.92	1150	19.87	11.50	19.82		19.77	11.76
24	20.78	12 00	20.73	12 09	20.68	12.48	20.65 21.45	12.27
25	22.52	12.50		13.10	82.40	13.20	92 34	13.29
26 27	23.38	13.50	22.46	13.00	23.26	13.70	23.20	13 80
28	24.25	14.00	24.19	14.61	84 15	14.21	1406	14.32
29	25.11	14.50	2505	14.61	24 99	15.23	23 92	14.83
30	25.98	15.00	25.92	15.61	25.85	15.73	R6.64	15.85
31	27.71	15.50	26.78 27.64	16.13	26.91	16.24	87.50	16 36
33	28,58	16 50	28.51	16.64	18.43	16.75	18.16	16.87
34	29.44	17.00	29.57	17.15	29.30	17.26	10.08	17.38
35	31.18	18.00	30.23	18.14	30 16	18.27	20.04	18-41
36 37	32.04	18.50	31.10	18 64	31.88	18.78	31.80	18.92
38	3291	19.00	32.83	19.14	32.74	19.29	3266	19.43
39	33-77	19.50	33.69.	19.65	33.60	19.79	33-52	19.94 a 20.45
40	34 64	20.00	34-55		34-47	20.81	3438	20.96
41 42	35.51 36.37	20.50 21.00	35.42 36.28	20.65.	35.33	21 32	36.10	21.47
43	37.24	21.50	37.14	21.66	37.05	21.82	16.95	21.99
44	38.11	22.00	38.01	28.17	37 91	22.33	37.81	23. 90 1 23.01
45	38.97	22.50	38.87	22.67	38.77	23 35	38:67	23.52
46	39.84 40.70	23.00	39-74 40-60	23.17	39.63	23.85	19:53	24.03
48	41 57	24.00	41.46	24.18	41.36	24.36	41.25	24-54
49	42.44	14.50	42 33	24.68	42.22	24.87	42.11	25.05
50	43.30	25.00	43.19	25.19	43.08	24.38	42.97	25.50
51 51	44.17 45.03	25 50 26.00	44.06 44.92	25.69	43.94	25.88 26.39	43.83	26.59
53	45.90	26.50	45.78	26.70	45.67	26.90	45.55	27.30
54	46.77	37.00	46.65	27.20	46 53	27.41	46.41	27.61 28.72
55	47.63	27.50	47 51	27.71	47.39	27.91	48.11	28.63
5 6	48 50 49 36	28.00 28.50	48.37 49.24	28 21 28 72	48.25	28.42 28.93	48.94	29.14
58	50.23	29.00	50.10	29.22	49 97	29.44	49.85	29.65
59	51.10	29.50	50.97	29.72	50.84	29.94	50 70	30.17
60	51.96	30.00	51.83	30 23	51.70	30 45	51.50	30.68
Dist.	Dep.	lat.	Dep.	Lat .	Dep.	Late	Dep.	Lar.
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1 5	. 0	,	1 1:	51	30)'	4	;'
] 🖁	Lat.	Dep	Lat.	Dep.	Lat	Dep.	Lat	Dep.
61	52.83	30.50	52.69	30.73	52.56	30.96	52.42	31.19
62	53.69	31.00	53.96	31.23	53.42	31.47	53.28	31.70
63 64	54.56 55.43	31.50	55.29	32.24	55.14	32.48	55.00	32.72
65	56.29	32.50	56.15	32.75	56 01	32.99	55.86	33.23
66	57.16	33.00	57.01	33.25 33.75	56.87	33.50 34.01	56 72 57.58	33.75 34.26
67	58.02	33 50	57.88 58.74	34.26	57 73	34.51	58-44	34.77
69	59.76	34.50	59.60	34.76	59 45	35 02	59.30	35.28
70	60.62	35.90	60.47	35.16	60.31	35.58	61.01	35 79 36.30
71	61.49	35.50 36.00	61.33	35.77 36.27	61.18	36.04 36.54	61.88	36.84
72 73	63.22	36.50	63.06	36.78	62.90	37.05	62.74	37.32
74	64:09	37.00	63.93	37.28 37.78	63.76	37.56 38.07	63.60 64.46	37.84
75	64 95	37.50	65.65	38.29	65.48	38.57	65.31	38.86
76 77	65.82 66.68	38.00 38.50	66.52	38.79	66.35	39.08	66.17	39 37
78	67 55	39.00	67.38	39 29	67.21	39.59		39.88
79 80	65.42 69.28	39.50 40 00	68.24	39.80 40.30	68.07 68.93	40 60	68.75	40.39 40.90
1 ===	70.15	40.50	69.97	40.81	69.79	41.11	69.61	41.41
82	71.01	41.00	70.83	41.38	70.65	4462	79.47	41.93
83	71.88	41.50	71.70	41.81	71 52 -	42.13		42.44
84	72.75 73.61	42.00 42.50	72.56	42.82	73 24	43.14	73 05	43.46
86	74 48	43.00	74.29	43.32	74.10	43.65	73.91	43.97
87	75.34	43.50	75.15	43.83	74.96	44-16 44-66		144-48
88	76.21 77.08	44.00	76.02	44-33 44-84	75.82 76.69	45.17		44-99
90	77.94	45.00	77.75	45.34	77-55	45.68	77-35	46 92
91	78.81	45.50	78.61	45.84	78.41	46.19	78.21	46.53
12	79.67	46.00	79·47 80.34	46.35	79.87 80.12	46.69 47.20	79.07 79.92	47.04
93	\$0.54 \$1.41	46.50	\$1.30	47.35	80.99	47.71	80.78	48.06
95	82.27	47.50	82.06	47.86	81.85	48.32	81.64	48.57
96	83.14	48 00	83.93	48.36 48.87	82.72 83.58	48.72 49.33	82.50 85.36	49.08 49.60
97	84.00 84.87	48.50 4 0 .00	83.79 84.66	49-37	84.44	49-74	84.22	50.11
99	85.74	49.50	85.52	49 87	85.30	50.25	85.08	50.63
100	86.60	50.00	86.38	50 38	86 16	50.75	85.9 <u>4</u> 86.80	51.64
101	87.47 88.33	50.50	87.25 88.11	50.88 51. 38	87 Kg	51.26 51.77	87 66	52.15
103	89.20	51.90	88.97	51 89	88.75	52.28	88.52	52 66
104	90.07	91.00	89.84	52.39	89 8 1 90.47	53.89	89.38 90.14	53.17 53.69
105	90 93	53 50	90.70	53.40	91.33	53.80	91.10	54.20
107	91.80	53.00	91.57 98.43	53.40	92.19	54-31	91.96	54,78
108	93.53	54.00	93.29	54 41	93 06	54.81	92.81	55.23
109	94 40	54.50 55.00	95.02	54.91 55.42	93-91	55.32 55.83	94 53	55.24
1	95.26	55.50	95.89	55.92	9:.64	56.54	95.39	56.75
112	96.99	56.00	96.75	56.42	96.50	56.84		57.24
113	97.86	56.50	97 61	56.93	97.36	57.35 57.86	97.11	57.78
114	98.73 99.59	57.00	98.48 99.34	57-43 57-93	99 09	58.37	98.83	58.89
116	100.5	\$8.00	100.2	58.44	99-95	58.87	99.69	59.31
117	101.3	58.50	101.1	58.94	100.8	59.38	100.6	59.88 60 33
118	103.1	59.00 59.50	102.8	59-4 5 59-9 5	104.7	59. 89	103.4	60.84
1 30	103.9	62.00	103.7	60 45	108.4	60.90	103.1	61.36
1	Dep.	Lat	Dep.	Lit	Dep.	Lat	Dep.	
ā	0.		4:	5'	30)'	1	51

. 61	. 0/		15	,	30)/	46	5'
Dist.	Lat.	Dep	Lat.	Dep.	Lat	Dr .	Lat.	Dep
-	0.86	0.51	0.85	0.52	0.85	0.52	0.85	0.53
1 : 0	1.71	1.03	1.71	1.04	1.71	1.04	1.70	1.05
3	2.57	1.55	2.56	1.56	2.56	1.57	2.55	1.5¢ 2.10
[4]	3.43	2.06	3.42 4.27	2.08	3 41 4.26	2.61	3.40 4.25	2.63
-5	5.14	3.00	<u>5.13</u>	3.11	Ç.13	3 13	510	3.16
7	6.00	3.61	5.48	3.63	5-97	3.06	5.95	3.68
8	6.\$6	4.12	6.84	415	6.82	4.18	6.80	4.21
9	7.71	4-64	7.69 8 55	4.67	7.67 8.53	4.70 5.22	7.65 8.50	4-74 5 26
10	8.57	5.15	9.40	5-19	9 38	5.75	9-35	5.79
11	9.43	5.67 6. 18	10.26	6.23	10.23	6.27	10.20	6 31
13	16.14	6.70	1611	6.74	11.08	6.79	11.05	6.84
14	13.00	7 24	1297	7.26	11.94	7.32	11.90	7.37
15	12.86	7.73	13.82	7.78	12 79	8.36	12.76	8.42
16	13.71	8 24 8.76	13.68	8.30 8.82	13.64	8.88	13.61	8.95
17	14.57	9.27	15.39	9-34	15.35	9.40	15.31	9-47
19	16.29	9.79	16.24	9-86	16.20	9.93	16.16	10.00
20	17.14	10.70	17.10	10.38	17.05	10-45	17.01	10.52
2!	18.00	10.82	17.95	10.89	17.91	10.97	17.86 18.71	11.58
22	18.86	11.33*	19.66	11.41	18.76	11.50	19.56	12.10
24	20 57	12 36	20.52	12.45	20 46	12.54	20.41	12 63
. 25	21 43	15 88	21 37	12.97	21:32	13.06	21.26	13.16
26	22.29	13.39	22.23	13.49	22 17	13.59	22,11	13.68
27	23.14	13.91	23.08	14-01	23.02	14.11	22.96	14-21
18	24.00	14.48	24.79	14.53	24.73	15.15	24.66	15.26
30	25.71	15.45	25.65	15.56	25.58	15.68	25.51	15.79
31	26 57	15.97	26 50	16.08	26.43	16 20	26.36	16.31
32	27.43	16.48	27.36	16.60	27.18	16.72	27.21 28.06	16.84
33	28.29	17 00	28.21	17.12	28.14. 28.99	17.24	28.91	17.37
34	29.14 30.00	17 51	29.92	18.16	29.84	18.29	19.76	18.42
36	30.86	18.54	30.78	18 68	30.70	18.81	30.61	18.94
37	31.72	19.06	31.63	19.19	31.55	19.33	31.46	19.47
38	32.57	19.57	32-49	19.71	32 40	19.85 20.38	32.31 33.16	20.00
39 40	33-43 34-29	20.60	33-34 34-20	20.23	33-25 . 34-1 I	20.90	34.01	21.05
41	35.14	21.12	35-05	21.27	34.96	21.42	34-86	21.37
42	36.00	21.63	35-91	21.79	35.81	21.94	35.71	32.10
43	36.86	22.15	\$6.76	22 31	36: 66	22.47	36.57	22.63
1 44	37.72	22.66 23.1%	37.52 38.47	22.83 23.34	37.52 38.37	22.99	37 42 38.27	23.15 23.68
45	38.57		39-33	23.86	39,22	24.03	39.12	24.21
46	39-43 40.29	23 69	40.18	24 38	40.07	24.56	39.97	24.73
48	41.14	24.72	41.04	24 90	40.93	25.08	40.82	25.26
49	4200	25.24	41.89	25.42	41.78	25.60 26.12	41.67	25.78 26.31
10	42.86	25.75	42.75	25.94	42.63	26.65		26.84
51	43.72 44.57	26.27 26.78	43.60	26.48	43.48	27.17	43.37	27.36
93	45.43	27.30	45.31	27.50	45.19	27.69	45.07	27.89
54	46.29	27.81	46.17	28.01	46.04	28.21	45.92	28.42
95	47.14	28,33	47.02	28.53	46 90	28.74	46.77	28.94
56	48.00	28.84	47.88	29.05	47.75	29.26 29.78	47.62 48.47	29.47 29.99
57 58	48.86	29.56 29.87	48.73.	29.57 30.09	48.60	30.30	49.37	30.52
1 59	50.57	30.39	50-44	30.61	.50.31	30 83	50.17	31.05
60	\$1143	30.90	51.29	31.13	51.16	31.35	51.02	31.57
坦	1)ep.	Lat.	Dep.	Lat.	Dep.	Lah	Dep.	Lat.
aj fr	. ()/	45	/	30)/	15	5'

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P. P.	Lat	Dep.	Lat	Dep.	Lat.	Dep.	Lat	Dep.
61	52.29	31.42	52.15	31.05	52.01	31.87	51.87	32.10
62	53.14	31.93	53.00	32 16	52.86	32.39	52.72	32.63
63	54.00 54.86	32.96	53.86	3 2.68 3 3.20	53.72	33.44	53.57	33.55
64	55.72	33.48	\$4-71 \$5-57	33 72	\$4 57 55.42	33.96	55 27	34.20
66	\$6.57	33.99	56.42	34.24	56.27	34.48	56.12	34.73
67	57 43	34.51	57.28	34.76	\$7.13	3 6.01	56.98	34.25
68	58.29	35.04	58.13	35.88	57.98	35.53	57.82	35.78
69 70	59 14 60.00	35.54 36.05	58.99 59.84	35.80 36.31	58.83 59.68	36.05	58.67	36.34 36 Sus
_	60 86	36 57	60.70	36.83	60 54	37.10	60 37	37.36
71 72	61.72	37.08	61.55	37.35	61.39	37.02	61.23	37.89
73	62 57	37.60	62.41	37.87	62.24	38.14	62.08	38.41
7.4	63.43	38.11	63.26	28.39	63.10	38 66	62.93	38.94
75	64.29	38 63	64:12	38.91	63.95	39.19	63.78	39.47
76	66.00	39.14 39 66	64.97	39.43	64.80 65.65	39.78	64-63 65-48	39.99 40 53
77	66.86	49.17	66.68	40.46	66.21	40.75	66 33	41.04
79	67.72	40.69	67.54	42.98	67.36	41.28	67.18	41.57
80	68.570	41.20	68.39	41.50	68.21	41.80	68.03	41.10
81	69 43	41.72	69.25	42.02	69.06	41.32	68.88	42.62
82	70.29	42.33	70.96	43.06	69:92 -70.77	42.84	69.73 70.58	43 15
84	72 00	43.26	71.81	43-58		43.89	71.43	44.20
85	.72 86	43 78	72.67	44.10	72.47	44.41	72.28	44-73
86	73.72	44.49	73.52	44.61		44.93	73.13	45.25
87	74-57	44.81	74 38	46.13		45.46	73-98	45.78
88,	75.43 76.29	45.84	75.23	45.65 46.17		45.98 46.50	74-83 75.68	46.83
89	77.25	46 35	76.94	46.69	76.74	47 02	76.53	47.36
91	78.00	46-87	77.80	47.25	77.59	47 55	77.38	47.84
92	78.86	47.38	78.65	47.73	78.44	48.07	178,23	18.46
93	79.72	47.90	'79-51	48.25	7930	48.99	79.08	48.94
94	\$0.58 \$1.43\	48.41	\$0.36 \$1.22	48.76 49.28	80,15	49.64	79.93 :80.78	49.47 49.99
95	82.29	49 44	82:07	49 80	81,85	50.16	81.63	50.52
96 97.	83.15	49.96	82.93	50 32	82.71	50.68	82.48	51.04
98	84.00	50.47	83.78	50.84	:83 56.	51.20	83.33	51.57
99	84.86	50.99	84.64	51.88	84.41	51 73	84.18	51.40
100	85.72	51.50	\$5.49		85.26	52 25	85.89	52.62
101	86.57 87.43	52.02 58.53	86.35 187.20	52.91	86.12 86.97	52.77 53.29	-86.74	53.15 53.67
102	88.29	53.05	88.06	53.43		53 82	\$7.59.	54.10
404	89.15	53.56	98.91	53.95	88167	54.34	.\$8.44	54 73
105	90.00	54.08	89.77	54-47	89.53	54.86	89 29	55.25
105	90.86	54.59	90.62	54 99	93.38	55.38	90.14	55.78
128	91.72	55.62	91.48	56.03	91,13	55.91 50.43	90.99	56.83
100	93.43	56.14	93.19	56.55	92,94	56.95	92.69	57.36.
110	94.29	56.65	94.04	57.06	93.79	57.47	93-54	57.88
111	95.15	57-17	94-90	57.58		58.00		58.41
112	96.00	57.68	95.75	58.10	95.50	58.53	95.24.	58.94
113	96.86 97.72	58.20	96:61	,8.62 59.44	96 35	59.04	96.94	59.40
115	98.57	59.23	98.31	59.66	98.05	60.00	97.79	60.51
116	99.43	59.74	99417	60.18	98.91	60.61	-98.64	61.04
117	100.3	60.16	100.0	60.70	9976		99.49	61.57
811		60.77	100.9	61.22	109.6	61.65	100.3	61.62
119	102.0	61.80	101.7	61.73	101.5	62.70	101.2	63.15
	Dep.	Lat	-	Lat	Dep.	Lat.	Dep	Late
Dist.	13Cp.		4		30		15	<u> </u>
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7	Lat.	Dep	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0.85	0.53	0.85	0.53	0.84	6.54	0.84	0.54
2	1.70	1.06	1.69	1.07	1.69	1.07	1,68	1.0
3	2.54	1.59	2,54	1.60	2.53	1.61	2.52	1.62
4	3-39	2.12	3.28	2.13	3 37	2.15	3.36	216
1_5	4.24	2.65	4.25	2.67	4.22	2.69	4.21	2.70
6	5.09	3.18	5.071	3.20	5.06	3.22	5.05	3-25
7 8	6 78	3.71 4-74	5.92 6.77	3-74	6.75	J.76 4.30	5.89 6.73	3-79 4-33
1;	7.63	4-77	7.61	4.80	7.59	4.84	7.57	4.87
100	8.48	5.30	8.46	5.34	8-43	5.37	8.41	5.41
111	9.33	5.83	9.30	4.87	9.28	5.91	9.25	5.95
12	10.18	6.36	10.15	6.40	10,12	6.45	10.09	6.49
23	11.02	6.89	10.99	6.94	10.96	6.98	10-93	7.03
14	11.87	7.42	11.54	7.47	11.81	7:52	11.77	7.57
15	12.72	7.95	12.69	8.00	12.65	8.06	12.62	8.11
16	13.57	8.48	13.53	8.54	13-49	8.60	13.46	8.66
17	14.41	9.02	14.38	9.07	14.34	9.13	14.30	9-20 9-74
13	15.26	10.07	15.22	9.61	16.02	10.31	15.98	10 28
20	16.96	10 60	16.91	10.67	16.87	10 75	16.82	10.82
31	17.81	11.13	17.76	11.21	17.74	11.28	17.66	11.36
22	18.66	11 66	18 61	11.74	18.55	11.82	18.50	11.90
23	19.51	14.19	19 45	12.23	19.40	12.36	19.34	12.44
24	20.35	12.72	20.30	12.81.	20.24	12.90	20.18	12.98
25	21.20	13.25	21 14	13.34	21.08	13.43	21.03	13.53
26	22 05	13.78	21.99	13.87	21.93	13.97	21.87	14.07
27	22 90	14.31	12.83	14.48	22.77	14.51	22-71	14.61
29	23.75 24.59	14.84	23.68	14-94	13.61 24.46	15.04	44 39	15.69
30	25.44	15.90	25.37	16.01	15.30	16.12	25.23	16.23
31	26.20	16.43	26.22	16.54	26 15	16.66	26.07	16.77
32	27.14	16.96	27.06	17.06	26.99	17.19	26.91	17.31
33	27.99	17.49	27.91	17.61	27.83	17.73	27.75	17.85
34	18.83	18.02	28.75	18.14	28.68	18.27	28,60	18.39
35	29.68	18-55	29.60	18.68	29.52	18.81	19-44	18.93
36	30.53	19.08	30.45	19.21	30.36	19.34	30.28	19.48
37	31.38	19.61	31.29	19.74	31.21	20 43	31.96	20.56
390	33.07	20.67	\$2.98	20.81	32.89	20.95	32.80	21.10
40	33.92	21.20	33.83	21.34	33.74	21.49	33.64	21.64
41	3477	21.73	24.67	21.88	34.58	22.03	34 48	22.18
42	35 62	22.26	35.52	23.41	35 42	22 57	35.32	22.72
43	36.47	22.79	36.37	22.95	36.27	23.10	36.16	23.26
. 44	37.31	23 32	37.24	23.48	37-31	23.64	37.01	23.80
45	38.16	23.85	38.06	24.01	37.95	24.18	37.85	24.34
46	39-OI	24.38	38 90	24.55	38.80	24.72	-38.69	24.88
47	39.86	24-91 25-44	39-75	25.08	39.64 40.48	25.25	39-53 40.37	25.43 25.97
49	41.55	25.97	41.44	26.15	41.33	20 33	41.21	26.51
50	42.40	26 50	42.29	26.68	42.17	26.87	42 05	27.05
	43.25	27.03	43.13	27.21		27.40	42.89	27.59
52	44.10	27 56	43.98	27.75	43.86	27.94	43-73	28.13
53	4495	28.09	44.82	28.28	44.70	28.48	44 58	28.67
54	45.79	28.62	45.67	28.82		29.01	45-43	29.21
95	46.64	29.15	46.52	29.35		29.55	46.26	29.75
56	47.49	29.68	47.36	29.88		30.09	47.10	30.2g 30.84
57	48 34 49 19	30.21 30.74	48-21	30.42 30.95	48.07 48.92;	30.63 21.16	47-94 48.78	3238
59	50.03	31.27	49.90	31.48		31.70	49.62	31.92
. 60	50.8	31.80	\$0.74	32.02		34.24	50.46	3246
1	Dep.	Lat	Dep	Lat.	Dep.	Lat.	Dep	Lat
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=	Lat.	Dep.	Lat.	Dep	Lat.	Dep.	Lat.	Dep.
61		2.33	51.59	32-55	51.45	32.78	51.30	33.00
62 63		2.86 ¹ 3.38	52.44 53.28	33.08 33.62	52.29 53.13	33.31	52-14	33-54 34 08
64	54.28 3	3.91	54-13	34.15	53.98	34-39	53.83	34.62
65		4-44	54-97	34.68	54.82	34.93	54.67	35.16
66		4·97 5· 5 0	55.82	35.72 35.75	55.66 56.51	35.46 36.00	\$5.51. \$6.35	35.70
68	1	6.03	57-54	34.29	\$7.35	36.54	57.19	36 79
69 70		6.56	58.36	36.82	58 19	37.07	\$8,03	37 33 38.87
73		7.62	59-20	37-35 37-89	19.88	37.61	59.87	38.41
72		8.15	60.89		60.72	38.69	\$9.71 60,55	38.95
73		8.68	61.74	38.95	61.57	39.12	61.40	39.49
74 75	- 1 . خ . م	9.74	63.43	39.49	62.41	39-76 40 30	62.24 63.08	4 0.03 4 0 .57
76		0.27	64.28	40.55	64.10	40.83	\$3.92	41.11
77	45.30 4	0.80	65-12	41.00	64.94	41.37	44 76	41.66
78 79		1.33	65.97 66.81	41.62	65.78 66.63	41.91	65.60; 66.44	42.74
80		2.39	67.66	41.69	67:47	41.98	67.28	43.28
81		2.93	68.50		68.31	43.52	68,12	43.82
82		3.49	9:35	43.76	90.00	44.06 44.60	69.97	44.36
83 84		3.98 4.51	71.04		70.84	45.13	69.81 70.65	44.90 45.44
85		5.04	71.89	44.36	71.69	44.67	71.49	45.98
86		5.57		44.89	72.53	46.21	72.33	46.52
87 88		6.10 6.63	73.58	46.42	73.38 74.22	46.75 47.28	73.17	47.06 47 61
89	75-48 4	7.16	75,27	47.49	75.06	47.82	74.85	48.15
90		7.69		48.03	75.91	48.36	75.69	48.69
91		8.22 8.75	76 96 17.81	48.56	76.75	48.89	76.53 77.38	49.23
92 93		9.28	78.65	49.63	78.44	49-43	78.22	49.77
94	7972 4	9.81		50.16	79.28	50.51	79.06	50.85
95		0.24	80.34	50.69	80.13	5 1.04	79.90	51.39
96 97		0.87	12.01	51.76	80 97 81.81	51.58	80.74 81.48	51.93 52.47
98	83:11 5	1.93	82,88	₹2.2g	82.65	52.66	82.42	53.02
100		2 46 1.99	\$3.73 \$4.57	5 1.85 5 1.3 6	83.50 84 34	53.19 53.73	83.26	53.56. 54.10
101		3.52	85.42	53 90	85.18	54-27	84.94	54.64
103	86.50 5	4.05	86.26	54-43	86.03	54 80	85.79	54.18
104		4.58	87.11 87.96	54.96	86 87 87.74	55.34 55.88	86.63	54.72
105		5.13 5.64	88.8o	56.03	88.56	56.42	87-47 88 31	50.26 50.80
106		6.17	89.65	56.56	89.40	50.95	89.15	57.34
107		6.70	90.49	57.10	90.24	57-49	89 99	57.88
104		7 23	91.34	57.6 3 58.16	g1.09	5803 58.57	90.83	58.42 58.97
1 10	93.29 5	8.29	93.03	58.70	92 77	59.10	92.51	59.51
111		1.82	93.88	59.23	93.62	59.64	93.36	60.05
112		9.35 9.88	94.72	59.7 6 60. 30	94.46	60.18	94 20	60.59 61.13
314	96.68 6	0.41	96.41	60.83	96.15	61.25	95.88	61.67
215		0.94	97.26	61.37	96.99	61.79	96 72	62.21
116		1.47	98.10	61.90	97.83 98.68	62.33	97.56	62.75
118	100.1-6		90.95	62.97		62.86 63.40	98:40 99:24	63.83
1 59	100.9 6	3.06	100.6	63.50	1004	63.94	100.1	64.38
120		3.59	101-5	04-03	101.2	64.48	100.9	64.92
Dist	Dep.	Lat	Dep.	Lat	Dep .	-	Dep.	Lat.
1.11	-		45	TWP C: 12			. 15	

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7	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep
—	0.84	0.54	0.84	0.55	0.83	0.55	0.83	0.56
2	⊩68	1.09	1.67	1.10	r.67	1.10	1.66	1.11
3	21.52	1.63	2.51	1.64	2.50	1.66	2.49	2.22
4	3.35	2.18	3.35	2.19	3-34 4-17	2.76	3.33 4.16	2.78
_5	4-19	2.72	4 18	2.74		<u> </u>		3.33
6	5.03	3.27	5.02	3.29	5.00	3.34 3.86	4.99 5.82	3.89
8	5.87 6.71	3.81 4.36	5. 85 6. 6 9	3.84 4.39	6.67	4.42	6.65	4-44
,	7.55	4.90	7-53	4-93	7.51	4.97	7.48	5.00
10	8.39	5.45	8.36	5.48	8.34	5.52	8.31	5.56
111	9.23	5.99	9.20	6.03	9.17	6.07	9.15	6 11
12	10.06	6.54	10.04	6.58	10.01	6.62	9898	6.67
13	10.90	7.88	10.87	7.13	10:84	7.18	10.81	7.22
14	11:74	7.63	11.71	7.68	11.67	7.73	11-64	7.78 /8.33
15	12.58	8.17	12.54	8.22	12.51	8.88	12.47	
г6	13.42	8.71	13.38	8.77	13.34	8.83	43.30	8.89
17	14.26	9.26	14:22	9.32	14-18	9.38	14-14	9.44
18	15.10	9 80	15:05	9.87' 10.42	15.01	9.93 10.4 9	15.80	10.56
19	15.93	10.35 10.8g	16.73	10.97	16.68	11.04	16.63	11.11
			17.56	11.51	17.51	11.59	17.46	11.67
21	17.61 18.45	11.44	18.40	12.06	18.35	12.14	18.29	12.22
22 23	19.19	12.53	19.23	12.61	19.18	11.69	1942	12.78
24	20.13	13.07	20 07	13.16	20:01	13.15	19:96	13.33
25	20.97	13.62	20.91	13.71	20.85	13.80	20.79	13.89
26	21.81	14.16	21.74	14.36	21.68	14.35	41.62	14.44
27	12.64	14.71	22.58	14.80	22.51	14.90	:42.45	15.00
28	23.48	15.25	23.42	15.35	23 35	15.45	23.28	15.56
29	24.32	15.79	34 25	15.90	24.1%	16.56	24.11	16.67
30	25.16	10 34	25.09	16.45	25.02			17 22
3 i	26.00	16.88	25.92	17.00	25.85	17.11	25.78 26.61	17.78.
32	26.84	17.43	26:76	17 55	26/68	18.21	27.44	18.33
33	27.68 28.51	17.97	28.43	18.64	28.35	18.77	28:27	18.89
35	29.35	19.06	29.27	19.19	19.19	19.32	19110	19.44
. 36	30.19	19.61	30.14	19.74	10.02	19.87	29.53	20.00
37	31.03	20.15	30.94	20 29	30.85	20.43	30176	20.56
38	31.87	20.70	31.78	20 84	31769	20.97	31760	21.14
39	32.71	21.24	22:62	21.38	32.52	21.53	32 43	21.67
40	33.55	21.79	33.45	21.93	33 36	22.08	33.26	22.22
41	34-39	22.33	34.29	22.48	34.49	22.63	34.09	22.78
42	35-22	22 87	35.12	23.03	35.02	23.18	34.93	23.33 23.89
43	36.06	23.42	35.96	23.58	35.86 36.69	23.73 24.29	35.75 36.58	24.45
44	36.90 37.74	23.96 24 51	37.53	24.67	37.52	24.84	37:42	25.00
45			38.47	25.22	38.36	25.39	38.25	35.56
46	38.58 39.42	25.05 25.60	39.81	25.77	39419	25.94	39.08	26.11
48	40.26	26.14	40.14	26.32	40 03	26.49	39:91	26.67
149	41.09	16.69	40.98	€6.87	40.86	27.04	40.74	27.22
50	41.93	27.23	41.81	27.41	41.69	27.60	41.57	27.78
, 51	42.77	27.78	42.65	27.96	42.53	28.15	42.40	28.33
52	43.61	28.32	43.49	28.51	43.36	28.70	43.24	28.80
53	44-45	28.87	44.32	29.06	44.20	29.25	44.07	29 45 30.00
54	45.29		45.16 46.00	29.61 30.16	45.03	29.80 30.36	44.90 45.73	30.56
55	46.13	29.96			45.86			31.11
56	46.97	30.50	46.83	31.25	46.70	30.91	46.56	31.67
57		31.04	47.67	31.25	47.53 48.37	31.4 6 32.01	47.39 48.23	32.22
58	.48.64 49.48	31.59	49.34	3235	49.20	32.56	49.06	32.78
60		32.68	50.18	32.90	50.03	33.12	49.89	33-33
1		Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
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7	Lat-	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
61	51.16	33.22	51.01	13.45	50.87	33.67	50.72	33.89
62	52.00	33-77	51.85	33.99	51.70	34.22	51.55	34-45
63	52.84	34.31	52.69	34-54	52 53	34-77	52.38	15.00
65	53.67 54.51	34.86 35.40	53-52 54-36	15.09 35.64	53.37	35.32	53.21 54 O5	35.56 36.11
66	55.35	35.95	55.19	36 19	55.04	36.43	54.88	36.67
67	56.19	36.49	56.03	36.74	55.87	36.98	55.7.1	37.22
68	57.03	37.04	56.87	37.28	56.70	37-53	56.54	37.78
69	57.87	37.58	57.70	37.83	57-54	38.08	57 37	38.33
70	58.71	38.12	58.54	38.38	58.37	38.64	58.20	38.89
71 72	59 55 60.38	38.67 39.24	59.38	38.93	59.21 60.04	39.19 39.74	59.03 59.87	39·45 40.00
73	61.32	39.76	64.05	40.03	60.87	40.29	60.70	40.56
74	62.06	40.30	61.89	40.57 -	61.71	40.84	61.53	41.11
75	62.90	40,85	62.73	41 12	62.54	41 40	62 36	41.67
76	63.74	41.39	63.56	41.67	63.38	41.95	63-19	42.22
77 78	64.58	41.94 42.48	64.39	42.22	64 21	42.50	64.85	42.78
79	66.25	43.03	66.07	43.32	65.88	43.60	65.69	43.89
80	67.09	43.57	66.90	43,86	66.71	44.16	66.52	44-45
81	67.93	44 12	67.74	44.41	67.54	44-71	67.35	45.00
82	68.77	44.66	68.58	44.96	68.38	45.26	68.18	45.56
83	70.45	45.75	70.25	45.51	70.05	45.84 46.36	69.01 69.84	46.11 46.67
85	71.29	46.29	71 08	46.60	70 88	46.91	70.67	47.22
86	72-13	46.84	71.92	47.15	71.71	47 47	71.51	47.78
87	72.96	47.38	72.76	47.70	72 55	48.02	72.34	48 33
88	73.80	47-93	73.59	48.25	73.38	48.57	73-17	48.89
90	74.64	48.47	74-43	48.80	74.22	49.12	74.00	49.45 50.00
91	76.33	49.56	7601	49.89	75.88	50.23	75.66	50.56
92	77.16	50.11	76.94	50-44	76.72	50.78	76.50	51.11
93	78.00	50 65	77.77	50 99	77-55	51.33	77.33	51.67
94	78.84	\$1.20	78.61	\$1.54	78.39	51.88	78.16	52.22
95	79 67	51.74	79.45 80.28	\$2.09	79.22	52.43	78.99	52.78
96 97	80.51	52.29	81.12	52.64 53-18	80.05 80.89	52.99 53.54	79.82 80.65	53.89
86	84 19	53.37	81.96	53.73	81.72	54.09	81.48	54-45
99	83.03	53.92	82.79	54.28	82 55	54.64	82.32	55.00
100	83.87	54.46	83.63	94.83	83.39	55.19	83.15	55.56
101	84.71	55 01	84 46	55-38	84,22 85.06 -	55.75	83.98	56 11
102	86.38	55.55	85.30 86.14	55.93 56.47	85.89	56.30 46.85	85.64	56.67 57.22
104	87.22	56.64	86.97	57-02	86.72	57 40	86.47	57.78
105	88 v6	57.19-	87.81	57.57	87.56	57 950	87.30	58 33
106	88.90	57.73	88.65	58.12	88.39	58.51	88.14	58.89
107	89.74	58.82	: 89 48 90.32	59.23	89.23 90.06	59.61	88 97 89.80	59 45 60.00
109	91.42	59.37	92.16	59.76	90.89	60.16	90.63	60.66
110	92.35	59.91	9199	60.31	91.73	60.71	91.46	61.11
111	93.09	60.45	92.83	60.86	92.56	61.26	92.29	61.67
1112	'93-93	61.00	93.66	61.41	93.40	61.82	93-12	62.22
113	94-77 . 95.61	61.54	94.50	61.96	94 23	62 37 82.92	93.96	62.78 63.34
115	96.45	62.63	96.17	63.05	95.90	68.47	95.62	63.89
116	97.19	63.18	97.01	63.60	96.73	64.02	96.45	64.45
147	98.12	63 72	97.85	64.15	97.56	64.58	97.28	65.00
118	98.96	64.27	98,68	64.70	98.40	65.13	98.11	65 56
119	99.80	64.81	99.52	65.35	99-43 100.1	65.68	98.94 99.78	66.67
+	Dep.	Lat.	Dep.	Lat.	Dep.	Lat	Dep.	Lat
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Di a	Lat.	Dep.	Lat	Dep.	Lat.	Dep.	Let.	Dep.
-	0.83	0.56	0.83	0.56	0.82	0.57	0.81	0.57
2	1.66	1.13	1.65	1.13	1.65	1.13	1,64	1.74
3	2.49 3.32	1.68	2.48 3.31	1 69 2.25	3.30	1.70 2.27	2.46	2.38
\$	4.15	2.80	4.13	2.81	4.13	283	4.11	2.85
6	4.97	3.36	4.96	3.38	4-94	3-40	493	3.42
1 7	5.80	391	5.79	3-94	5.77	3 96	. 5.75	3.99
1 2	6.63 7.46	503	6.61 7.44	4.50 5.07	6.59 7.42	4-53 5 10	6.57 7.39	4.50 5.23
10	8.19	5.59	8.27	5.63	8.24	.5.66	8.22	5.70
111	9.12	6.15	9.09	6.19	9.07	6.23	9.04	6.27
112	9.95	671	992	6.75	9.89	6 80 7-36	9.8 6 19.68	6.84 7-41
13	10.78	7.27	10.75	7 32 7.88	11.54	7.93	11.50	7.98
15	13 44	8.39	12.40	8.44	12 36	8.50	12.32	8.55
16	13.26	8.95	13.23	9.20	13.19	9.06	13.15	9.12
17	14 09	9.51	14.05	9.57	14.01	9.63	13.97	9.69 10. 26
18	14.92	10.07	14.88	10.13 10.69	15.66	10.76	15.61	10.83
20	16.58	11.18	16.53	11.26	+6 48	11.33	16.43	11.40
21	17.41	11.74	17.36	11.82	17.31	11.89	17.25	11.97
32	18.24	12 30	18 18	12.38	18.13	12.46	18,08	12.54 13 11
23	19.07	12.86	19.81	12.94	19.78	13.59	19.78	13.68
25	20.73	13.98	20.66	14.07	20 60	14.16	20.54	14-25
26	21 55	14 54	21.49	14.63	21 43	14.73	21.36	14.82
•7	22 38	15.10	22.32	15.20	22.25	15.20 15.86	23 18	15.39 15.96
28	23.21	15.66	23.14 23.97	15 76	23.08	16.43	25.83	16 53
30	24.87	16 78	24.80	16.88	24.72	16.99	24.65	17.10
31	25.70	17.33	25.62	17-45	25.55	17.56	25 47	17.67
32	26.53	17.89	26.45	18.01	26.37	18.13 18.69	26.29 27.11	18.24
33 34	27.35	18.45	27.28	18 57	27.20	19.26	21.94	19.38
35	29.02	19.57	28 93	19 70	28.84	19.82	28.76	19.95
36	29.85	20.13	29.76	20.26	29.67	20.39	29.58	20.52
37	30.67	20.69	30.58	20.82	30 49	20.96 11.52	30.40 31.21	21.66
38	31.50	21.25	31 41	21.95	31.32	22.00	32.04	22.23
46	33.16	22.37	33.06	22.51	32.97	22.66	32.87	22.80
41	33 99	22.93	33.89	23.07	33-79	23.22	33.69	23.37
42	34.81	23 49	34 72	23.64	34.61	23.79	34-51	23-94 24-51
43	35.65 36.48	24.60	35·54 36-37	24.76	35.44 36.26	24.50	35.33	25.08
45	37.31	25.16	37.20	25.33	37 09	25.49	36.97	25.65
46	38.14	25 72	38 02	25.89	37.92		37.80	25.22
47	38.96	26.18	38.85	26.45	38.73	20.62	38.62	26.79 27.36
48	39.79 40. 62	26.84 27.40	39.68° 40.50	27.58	39.56 40.38	27.75	40 16	27.93
50	41.45	27 96	41.33	28.14	41.81	28.32	41.08	28.50
51	42.28	28.52	42.16	28.70	42.03	28.89	41.90	29.07
52	43.11	39 D8	42 98	29.27	42.85	29.45	4273	29,64
53 54	43.94 44.77	29.64 30.20	.43.81 44.64	29.83 30.39	43.68	30.02 30.59	43.55	30.98
55	45.60	30.76	45.46	30.95	45.33	31 15	45.19	34.35
56	46.43	31 31	46.29	31.52	46 15	31.72	46.01	31 92
57	47.26	31.87	47-12	32.08	46.98	32.89	46.83	38.49
58	48.68	38.43	47·94 48.97	32.64. 3 3 .22	47.60	32.85 32.48	47.66 48.48	33.63
59 60	48,91 49-74	32.99 33.55	49.60	33.77	49-45	33.98	49.30	34.80
1	Dep.	Lat.	Dep.	Lat	Dep.	Lat	Dep.	LAL
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Dist.	Lat	Dep.	Lat	Dep.	Lat.	Dep.	Lat.	Dep.
61	52.57	34-11	50.42	34.33	59.27	34-55	50.12	34-77
62	51.40	34.67	51.25	34.89	51.10	35.12	50.94	35.34
63	53.23	35.23	52.08	35.46 36.02	51.92	35.68	51.76	35.91 36.48
64	53.06 53.89	35.79 36.35	53.73	36.58	53-57	36.82	53.41	37.05
66	5473	36.91	54-55	37.15	54-39	37.38	54.23	37.62
67	55.55	37-47	55.38	37.71	56.04	37.95 38.52	55.87	38.19 38.76
.48 69	56.37 57.80	38.03 38.58	57.93	38.97 38.83	56.86	39.08	56.69	39.33
70	\$8.03	39.14	57.86	39.40	57-69	39.65	59.52	39.90
71	58.86	39.70	58.69	39.96	58.51	40.21	58.34	40.47
72	\$9.60 60.52	40.86 40.83	59.51 60.34	40.52	59.34 60.16	40.78	59.98	41.61
73 74	61.35	41.38	61.17	41.65	60.99	41-91	60.80	42 18
75	62.18	41.94	61,99	42.31	61.81	42.48	61.62	42.75
76	63.01	42.50	62,82	42.77	62.63	43.05 43.61	62.45	43.32 43.89
77	63.84 64.66	43.96 43.63	63.65 64.47	43-34 43-90	64.28	44.18	64.09	44.46
79	65.49	44.18	65.30	44.46	65.31	44-75	64.91	45.03
80	66.32	44.74	66.13	45.02	65.93	45.31	65.73	45.60
81 82	67.15 67.98	45.39	66.95 67.78	45.59 46.15	66.75	45.88	66.55	46.74
83	68.81	45.85	68.61	46.71	68.40	47.01	68.20	47.31
84	69.64	46.97	69.43	47.28	69.23	47.58	69.02	47.88 48.45
85	70.47	47.53	70,26	47.84 48.40	70.05	48.14 48.71	70 06	49.02
86 87	71.30	48.09 48.65	71.09 • 71.91	48.96	71.70	49 28	71.48	49.59
88	72.96	49.21	72.74	49.53	72.52	49.84	72.30	50.16
-89	73.78	49-77	73.57	50.09	73-35 74-17	50.98	73.13 73.95	50.73
90	74-61	50.33	74-39	51.22	75.00	51.54	74-77	51.87
94	75-44	51.45	76.05	51.78	75.82	58.11	75.59	57-44
98	77.10	52.00	76.87	52.34	76.6 <u>4</u> 77.47	52.68	76.41	53.01
94 95	77.93 78.76	53.12	77.70	52 90 53-47	78.29	58 24 53.84	78.06	54.15
96	79-59	53.68	79-35	54-03	79-12	54-37	78 88	54-72
97	80.42	54-34	\$0.18	54-59	79.94	54-94	79.70	55.29
98	81.25 82.07	54.80 55.36	81.83	55.72	80.76 81.59	56.07	80.52 81.34	55 86 56.43
99	82.90	55.92	82.66	56.28	82.41	56.64	82.16	57.00
101	83.73	56.48	83.49	56.84	83.24	57.31	82.99	57-57
102	84.56	57.04	84.31	57.41	84.06 84.88	57-77 . 5 8-24	83.81 84.63	58.14 58.71
101	85.39 86.22	57.60	85.14	57.97 58.53	85.71	58.91	85.45	59.28
105	87.05	58.72	86.79	59.09	86.53	59.47	86.27	59.85
106	87.98	59-27	87.62	59 66	87.36 88.18	60 04 60.61	87.09 87.92	60.42
107	88.71 89.54	59.83 60.30	8,3 45 89.17	60.22	10.28	61.17	88.74	61.56
109	90.37	60.95	90.10	61.35	89 83	61.74	89.56	62.13
110	91.19	61.51	90.92	61.91	90.65	62.30	90.38	62.70
111	92.02	62.07	91 75 92 48	62.47 63.03	91.48	62.87	91.20	63.84
E13	92.85 93.68	62.63 63.19	93.40	63.60	93.13	64.00	92.85	64.41
114	94.51	63.75	94.23	64.16	93.05	64-57	93.67	65.55
115	95.84	64.31	95.06	64.72	94-77	65.14	94-49	66.12
116	96.17 - 97.00	64.87 65.43	95.88	65. 39 65.8 5	96.42	66.27	96.13	66.69
118	97.83	65.98	97.54	66.44	97.25	66.84	96.95	67.26
119	98.66	66.54	98.36	67.54	98.07	67.49 67.97	97 78 98.60	67 83 68.40
	99.48 Dep	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
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1 %	Lat	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	1 le
1	0 82	0.57	_C.82	0.58	6.81	0.58	0.81	
1 2	1.64	1.15	1.63	1.15	1.63	1.16	1.62	LP
] 3	2 46	1.72	2.45	1.73	2.44	1 74	2.43	L.T.f
4	3 28	2 29	3.27	2.3₹	3.26	2.32	3.25	
_ 5	4.10	2.87	4.08	2.89	4-07	2.90	4.06	2.92
6	4.91	3.44	4.90	3.46	4.88	3.48	4.87	
7	5.73	4.01	5.72	4.04	5.70	4.06	5.68	
8	6 55	4.59	6.53	4.62	6.51	4.65	6.49	4.6
9	7.37	5.16	7.35	5.19	7-33	5.23	7-3	
10	8.10	5.74	8.17	5.77	8,14	5.81	8.12	
111	0.01	631	8.98	6.35	8.96	6.39	8.93	
12	9.83	6.88	9.80	6.93	9.77	6.97	974	
13	10.65	7.46	10.62	7.50 8 08	10.58	7.55 8.13	10 55	
14	11.47	8.60	11.43	8.66	11.40	8.71	11.36	امسل
15	12.29		12.25					
16	13.11	9.18	13.07	9.23	13.03	9.29	12.99	
18	13.03	9.75	13.88	10.39	14.65	10.45	13.80 14.61	
- 19	14.74	10.90	14.70	10.97	15.47	10.03	15.42	1 -1
20	16.38	11.47	16.33	11.54	16.28	11.61	16.23	1 . 1
21	17.20	12.05	17 15	12 12	17.10	12.19	17:04	12.27
22	18.02	12.62	17.97	12.70	17.91	12.78	17.85	12,35
23	1884	13.19	18.78	13.27	18.72	13.36	18.67	13.44
24	19.66	13.77	19.60	13.85	19.54	13.94	19.48	14.00
25	20.48	14.34	20.42	14.43	20.35	14.52	20 29	14 61
26	21.30	14.91	21.23	15.01	\$1.17	15 10	21.10	1 6-19
27	22.12	15.49	22.0;	15.58	21.98	15.68	21.91	15.77
28	22 94	16.06	22.87	16.16	22.80	16 26	22.72	16-36
29	23 76	16 63	23.68	16.74	23.61	16.84	23.54	16 94
30	24.57	17.21	24.50	17.31	24.42	17.42	24 35	17-53
31			25.32	117.89	25.24	18.00	25.16	18.11
32	26.21	18.35	26.13	18.47	26.05	18.58		18.70
33		18.93	26.95	19.05	26.87	19.16	36 78	19 28
34	27.85	19.50 20.08	27.77	19.62	1 27 68 1 28.49	19.74	27.59 28.41	19.86 20.45
35					,			
36	30.31	20.65	29.4C 30 22	20.78	30 12	20.91	29.22 30.03	21.63
37 38	31.13	,21.80	31.03	21.93	30.94	21.49	30.84	22.20
39	31.95	28.37	31.85	22 51	1 31 75	22.65	31.65	22.79
40	32.77	:22.94	32.67	23.09		23.23	32.46	23:37
141	33.59	2,.52	33.48	23.66	33.38	23 81	33.27	23.95
42	34.40	24.09	34.30	24 24	34.19	24.39	34.09	24.54
43	35.22	24.66	35 12	24.82	35.01	24.97	34.90	25.12
. 44	36.04	25.24	35.93	25.39	35.82	25.55	35.71	25.71
• 45	36.86	25.81	36 75	25.97	36.64	26.13	36.52	26:29
:46	37.68	26.38	37.57	26.55	37.45	26.71	37-33	26.88
.47	38.50	26.96	38.38	27.13	38 26	27.29	38.14	27.46
48	39 32	27.53	39.20	27 70	39.08	27.87	38-96	28 04
49	40.14	28.11	40.02	28.28	39.89	28.45	39.77	28.63
50	40.96	28.68	40.83	.;	40.71	29.04	40.58	29.21
51		29.25		29.43	41.52	29.62	41.39	29.80
52	42.60	29.83	42 47	30.01	42.33	30.20	42.20	30.38
53	43.42	30.40	43.28	30.59	43.15	30.78	43.01	30.97 31.55
.54 55	45.05	31.55	44.92	31.74	44.78	31 94	44.64	32.13
-	45.87	32.12	45.73	32.32		32.52	45.45	
56	46.69	32.69	46.55	32.90	45.59	32.52	46.26	32.72 33:30
57 58	47.51	33.27	47.37	33.47	47.22	33.68		33.89
59	48.33	33.84	48 18	3405	48.03	34.26	47.88	34-47
66	49.15	34-41	49.50	34 63	48.85	34.84	48.69	35.06
1	Dep	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
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110	Dist.	Let.	Dep.		Dep.	Lat.	Dep.	Lat.	Dep
0.0	61	49.97	34.99	49.82	35 21	49.66	35.42	49.51	35.64
1.15 0.81 2.11 1.63 1.11	62	50.79	35 56	50.63	35.78	50.48	36.00	50.32	36.22
1.73 244 17	63	51.61	36.14	\$1.45	36.36	\$1.29	36.58	\$1.13	36.81
2.31 3.26 11	64	52.43	36.71	52.27	36.94	52.10	37.16	51.94	37.39
2.89 407 146	65	53-24	37.86	53.08	37.51	52 92	37.75 38.33	52.75	37.98
46 488 141 04 5.70 461	66 .67	54.88	37.00	53.9° 54.71	38.67	\$3.73° \$4.55	38.91	53.56 54.38	39.14
62 651 461 1	68	55.70	39.00	55-53	30.25	\$5.36 \$0 17	39.49	\$5.19	39-73
9 7.33 621	69	56.52	39.58	56.35	39.82		40.07	56.00	40.31
7 8.14 (3)	70	\$8.16	49.15	57.16	40.40	56.99	40 65	56.81	40.90
8.96 6.39 t	71	58.98	40.72	57.98 58.80	40.98	57.80 58.62	41.23	57 62	41.48
9.77 6.97 4	73	59.80	41.87	59.61	42.13	59 43	42.39	59-24	42.65
10.58 755 2	74	60.63	42.44	60 43	42.71	60.24	42.97	60.06	43.23
12.21 1.71 111	75	61.44	43.02	6.L.25	43 29	61.06	43.55	60.87	43.82
13.03 9.39 10	76	62.26 63.07	43.59	62.06 62.88	43.86	61 87 62.69	44.13	61.68	44.40
13.84 987 111	77 78	63.89	44-17	63.70	44.44	63.50	44.71	63.30	44 99 45 57
14.65 10.45 14	79	64.71	45.31	64.51	45.59	64.32	15.88	64.11	46.16
15-47 10.03 112 1 1 1 1 1 1 1 1	.8ó	65.53	45.89	05.33	46.17	.65.13	46.46	64.93	46 74
	81	66.35	46.46	66.15	+6.75	65.94	47.04	65.74	47 32
91 12.78 rt	82	67.17	47.03	66.96 67.78	47.33	66.76	47.62 48 20	66.55 67.36	47 9 t 48.49
72 13.26 , ilit	83	68.81	47.61	68.60	47.90 48.48	68 39	48.78	68.17	49.08
54 13.94 · Int	85	69,63	48.75	69 41	49.06	69 20	19.36	68.98	49.66
15 1452 22	86	70.45	49.33	70.23	49.63	70.01	49-94	69.80	50.25
7 15 10 115	87	71.27	49.90	71.05	50.21	70.83	50.52	70.61	50.83
16.68 117 16.08 117 1	88	72.09	50.47	71.86	50.79	71.64 72.46	51.10	71.42	51.41
16.84 213	90	73.72	51 62	73.50	51.94	73.27	52.26	73.04	52.58,
17.42 245	91	74-54	52 20	74-31	52.52	74.08	52.84	73 85	53.17.
18.00 3581	92	75.36	52.77	75.13	53.10	74.90	53.42	74.66	53.75
18.58 15.4")	93	76.18	53.34	75.95	53.67	7,5.71	54.01	75.48	54-34
9.16 #141	94	77.82	54.49	76.76	54.25	76.53. 77.34	54.59	75.29 77.10	54.92
1 32 14:	96	78.64	55.06	78.40	55.41	78.16	55.75	77.91	56.09
91 2411 2	97	79.46	55.64	79 21	55.98	78.97	56.33	78.72	56.67
49 30.00	98	80.28	56.21	80.03	56.56	79.78	56.92	79 53	57.26
27 32.45	99	81.10	56.78	80:85 81.66	57.14	80.60 81.41	57.49	80.35 81.16	57.84
1 31.615 1 32.415	100	82.73	57.36	82 48	57 71	82.23	58.65	81.97	59.01
33.27	101	83.55	57.93	83 30	58.87	83.04	59.23	82.78	59.59
/ 3439 E	103	84.37	59.08	84.11	59.45	83.85	59.81	83.59	60.18
1 34 6 5	104	85.19	59.65	84.93	60.02	84.67	60.39	84 40	60.76
35.71 5	104	86.01	60.23	85.75	60.60	85.48	60.97	85.22	61.35
36.72 20	106	86.83 87.65	60.80	86.56 87.38	61.18	86.30 87.11	62.14	86.84	64.93
37-31 mg	108	88.47	61.37	88.20	62.33	87.92	62.72	87.65	63.10
8-66 112	109	89.39	62.52	80.01	62.91	88 74	63.30	88.46	63.68
177號	110	90.11	63.09	89.83	63.44	89.55	63.88	89.27	64.27
19 mil	1111,	90.93	63.67	90.65	64.06	90.37	64 46	90.08	64.85
79 Jack	112	91.74	64.81	yr.46 92.28	64,64	92.00	65.64 65.62	91.71	
0 (2) 1 (2)	114	93.38	65.39	93.10	65.79	92.81	66.20	92.52	
- luii	115	94.20	65.96	. 93.91	1.6.37	93 62	66.78	93.33	67.19
11 ·	116	95.02	66.53	94-73	66,95	94-44	67.36	94.14	67.77
157	117	95.84	67.11	95.55	67.53	95.25 96.07	67.94 68.52	94.95	68.36 68.94
5.2 14	118	96.66 97.48	67.68 68.26	96.36 97.18	68.63	96.88	69,10	96.58	69 53
# ·	120	98.30	68.83	98.40	69.26	97.69	69.68	97-39	7011
4 2	1	Dep.	Lat.	D, p	Lat.	Dep	Lat.	Dep.	Lat.
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7	<u>D</u> .	. 0/		15	1	30)/	4	51
ı	Dist	Lat.	Dep	Lat.	Dep.	Lat	De .	List.	Dep
1	-	0.86	0.51	0.85	0.52	0.85	0.52	0.85	0.53
I	2 9	1.71	1.03	1.71	1.04	1.71	1.04	1.70 2.55	1.05
ı	3	2.57 3.43	2.06	2.56 3.42	1.56	2-56 341	2.09	3.40	2.10
ı	4 5	4.89	2.58	4.27	2.59	4.26	2.61	4-25	2.63
ľ	6	5.14	3.09		3.11	5.12	3 13	5.10	3.16
1	7	6.00	3.61	5.48	3.63	5.97	3-66 4-18	5.95 6.80	3.68 4.21
ı	8	6.56 7.71	4.12 4.64	7.69	415	7.67	4.70	7.65	4-74
ł	10	8.57	5.15	8 55	5.19	8.53	5.22	8.50	5 26
ľ	11	9.43	5.67	9.40	5.71	9 38	5.75	9-35	5.79
ł	12	10.29	6.18	10.26	6.23 6.74	10.23	6.27	10.20 11.0¢	6.84
ı	13	11.14	6.70 7 21	1611	7.26	11.08	7.32	11.90	7.37
ı	15	12.86	7.73	12.82	7.78	12 79	7-84	12.76	7.89
1	16	13.71	8 24	13-68	8.30	13.64	8.36	13.61	8.42
۱	17	14-57	8.76	14-53	8.83.	14.49	9.40	14.46	8.95 9-47
ı	18	15.43 16.29	9.27 9.79	15.39	9·34 9·86	16.20	9.93	15-31	10.00
1	20	17.14	10.30	17.10	10.38	17.05	1045	17.01	10.52
ľ	21	18.00	10 82	17.95	10.89	17.91	10-97	17.86	11:05
1	22	18,86	11.330	18.81	11.41	18.76	11.50	18.71	11.58
ı	24	19.71	11.85	19.66	11.93	19 61 20.46	12.54	19.56	12 63
1	25	20 57 21 43	12 88	21 37	12.97	21.32	13.06	21.26	13.16
1	26	22.29	13.39	22.23	13.49	22 17	13.59	22,11	13.68
ł	27	23.14	13.91	23.08	14-01	23.02	14.11	22.96	14-21
ı	18	· 24.00 · 24.86	14.48	23.94	14.53	23.87 24.73	14.63	24.66	14-73 15.26
ı	30	25.71	15.45	25.65	15.56	25.58	15.68	25.51	15.79
ŀ	31	26 57	15.97	26 ;0	16.08	26.43	16 20	26.36	16.31
ı	32	27:43	16.48	27.36	16.60	27.28	16.72	27.21 28.06	16.84 17.37
1	33 34	28.29 29.14	17.00	28.21	17.12	28.14	17.24	28.91	17.80
1	35	30.00	18.03	29.92	18.16	29.84	18.29	29.76	18.42
ľ	36	30.86	18.54	30.78	18 68	30,70	18.81	30.61	18.94
1	37	31.72	19.06	31.63	19.19	31.55	19.33	31.46	19.47
ı	38 39	32.57 33.43	19.57	32-49	19.71	32 40	20.38	32.31 33.16	20.52
1	40	34.29	20.60	34.20	20.75	. 34.11	20.90	34.01	21.05
ľ	41	35.14	21.12	35.05	21.27	34.96	21.42	34-86	21.37
I	42	36.00	21.63	35-91	21.79	35.81 36.66	21.94	35.71	22.10
ı	43 ·	36.86 37.72	22.15	36.76 37.62	22.83	37.52	22.47	-37 42	23.15
1	45	38.57	23.18	38.47	23.34	38.37	23.51	38.27	23.68
.r	46	39.43	23.69	39-33	23.86	39,22	24.03	39.12	24.21
I	47.	40.29	24.21	40.18	24 38	40.07	24.56 25.08	39.97 40.82	24.73 25.26
	48. 49	41.14	24.72	41.04	24 90	40.93 41.78	25.60	41.67	25.78
	40	42.86	25.75	42-75	25.94	42.63	26.12	42.52	26.31
ŗ	51	43.72	26.27	43.60	26.46	43.48	26.65	43-37	26.84
1	52	44-57	26.78	44.46	26.98	44-34	27.17 27.69	44.22	27.36 27.89
ı	55 54	45.43	27.30	45.31	27.50 28.01	45.19 46.04	28.21	45.92	28.42
I	95	47.14	28,33	47.02	28.53	46 90	28.74	46.77	28.94
r	56	48.00	28.84	47.88	29.05	47-75	29.26	47.62	29.47
I	57	: 48.86	29.56	48.73.	29-57	48.60	29.78 30.30	48.47	29.99
ı	58 59	49.74 50.57	29.87 30.39	49.58	30.61	50.31	30.83	49.32	30.52
1	60	51.43	30.90	51.20	31.13	51.16	31.35	51.02	31.57
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Dig.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
61	52.29	31.42	52.15	31.65	(2.01	31.87	51.87	32.10
62	53.14	31.93	53.00	32 16	52.86	32.39	52.72	32.63
63	54.00	32 45	53.86	3 2.68	53.72	34.92	53-57	33. 15
64	54.86 55.72	32.96 33.48	54-71	33.20 33.72	54 57	33.44 33.96	\$4.42° 55 27	33.68 34.20
66	56.57	33.99	55.57	34.24	55.42	34.48	56.12	34.73
67	\$7:43	34.51	57.28	34.76	57.13	36.01	56.98	35.25
68	58.29	35.02	58.13	35.28	57.98	35 53	57.82	35.78
69	59 14	35.54	58.99	35.80	58.83	36.05	58.67	36.3v
70	60.00	36.05	59.84	36.31	59:68	36.57	59.52	36 84
71 72	60.86 61:72	36 57 37.08	60.70	36.83 37-35	61.39	37.10	60 37	37.36 37.8g
73	62 57	37.60	62.41	37.87	62,24	38.14	62.08	38.41
74	63-43	38.61	63.26	38.39	63.ro	38 66	62.93	38.94
75	64.29	38 63	64.12	38.91	63.95	39.19	63.78	39-47
76	65:14	39.14	64.97	39:43	64.80	39.71	64:63	39.99
77	66.86	39 66 49.17	65.83	39.95 40.48	65.65	49.23	65.48	40 53
79	67.72	40.69	67.54	42.98	67.36	41.28	67.18	41.57
80	68.57	41.40	68.39	41.50	68.21	41.80	68.03	41.10
81	69 43	41.72	69.25	42.02	69.06	44.32	68.88	42.62
82	70.29	42.33	10.10	42 54 4	69.92	42.84	69.73	43 15
83	71.14	42.75	70.96	43.56 43.58	71.62	43.37	70.58	44.20
85	.72 86	43 78	72.67	44.10	72.47	44.4.1	72.28	44.73
86	73.72	44.49	73.52	44.61	73,33	14.93	73.13	45.25
87	74-57	44.81	74 38	46.13	74.18	45.46	73.98	45.78
88.	75.43	45.32	75.23	45.65		45.98	74-83	40 3F
89	76.29 77.85	45.84 46 35	76.09 76.94	46.17 46.69	175.89 76.74	46.50	75.68 76.53	46.83 47.36
1	78.00	46.87	77.80	47.21	77.59	47 55	77.38	47.80
91	78.86	47.38	78.65	47.73	78.44	48.07	178,23	18.46
93	79.72	47.90	79.51	48.25	79.30	48.59	79.08	48.94
94	\$0.58	48.41	80.36 81.22	48.76 49.28	80,15	49.61 ·	79.93 80.78	49.47
95	81.43		82:07	49 80	81,85	50.16	81.63	19.99
96	\$2.29 \$3.15	49 44 49.96	82.93	50 32	82.74	53.68	82.48	50.52
97.	84.00	50.47	83.78	50.84	83 56.	51.20	83.33.	5 4.57
99	84.86	50.99	84.64	51.36	8441	51 73	81-18	51.40
100	85.72	51.50	85.49	51.88	85.26	52 25	85.04.	51.62
101	86.57	52.02	86.35	52 40	86.12 86.97	53.77 53.29	.85.89 -86.74	53.15 53.67
102	87.43 88.29	58.53 53.05	487.20 88.06	52.91 53.43	87 82	53 82	87-59	54.40
104	89:15	53.56	\$8.91	53.95	88167	154.34	88.44	54 7.3
105	90.00	54.08	89.77	54-47	89-53	54.86	89 29	55.29
106	90.86	54-59	90.62	54 99	90.38	55.38	90.14	55.78
128	91.72	55.62	91.48	55,51 56.03	91.23	56.43	90.99	56.83 56.83
100	93.43	56.14	93.19	56.55	92,94	\$6.05	92.69	57.36
110	94-29	56.65	94.04	57.06	93 79	57.47	93-54	57.88
111	95.15	57.17	94-90		94.64	58.00	94.39	58.41
112	96.00	57.68	95.75	58.10	95.50	58.52	95.24	58.94
113	96.86	58.20 58.71	96.61 97.46	,8.62 59.14	96 35	59.04 59.56	96.09 -96.94	59.46
114	98.57	59.23	98.31	59.66	98.05	60.09	97.79	60.51
116	99.43	59.74	99-17	60.18	98.91	60 61	98.64	61.04
117	100.3	60.26	100.0	60.70	99:76	61.13	99-49	61.57
811		60.77	108/9	61.12	109.6	61.65	100.3	61 09
119	102.9	61.29 61.80	101.7	61.73	101.5	62.70	101.2	63.15
i'	Dep.	Lat	Dep.	Liat.	Dep.	Lat.	Dep	Lat.
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	Lat.	Dep	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
	0.85	0.53	0.85	0.53	0.84	0.54	0.84	0.54
1 :	1.70	1.06	1.69	1.07	1.69	1.07	1,68 2.42	1.62
3 4	3-39	1.59 3.12	2.54 3.38	1.60	2.53	2.15	3.36	2.16
3	4.24	2.65	4.23	2.67	4.22	2.69	4.21	2.70
6	5.09	3.18	5.07	3.20	5.06	3.22	5.05	3-25
2	6 78	3.71 4-74	5.92 6.77	3.74	5- 9 0 6-75	3.76 4.30	5.89 6.73	3-79 4-33
	7.63	477	7.61	4.80	7.59	4.84	7.57	4.87
100	8.48	5.30	8.46	5-34	8.43	5.37	8.41	5.48
111	9-33	5.83	9.30	5.87	9,28	5.9E	9.25	5-95 6-49
12	10.18	6.89	10.15	6.40	10,12	6.98	10-93	7.03
14	11.87	7.42	11.84	7.47	11.81	7.52	11.77	7.57
15	1272	7.95	12.69	8.00	12.65	8.06	12.62	8.11
16	13.57	\$.48 9.01	13.53	9.07	13-49	8.60 9.13	13.46	9.30
1 18		9-54	15.22	9.61	15.18	9.67	15.14	9.74
19	16 11	10.07	16.07	10.14	16.02	10.21	15.98	10.82
20	16.96	10 60	16.91	10.67	16.87	11.28	17.66	
21 22	17.81	11.13	17.76	11.74	17.71	11.82	18.50	11.36
23		14.19	19 45	12.27	19.40	14.36	19.34	12.44
1 24		13.25	20.30	12.81.	20.24	13.43	20.18	12.98
25	21.20	13.78	21 14	13.34	21.93	13.97	21.87	14.07
27		14.31	11.99	14.48	12.77	14.51	22-71	14.61
28	1	14.84	23.68	14-94	23.61	15.04	23.55	15.15
30		15.37	24·53 25·37	15.47	24.46	16.12	45.23	16.23
31	26.29	16.43	26.22	16.54	26 15	16.66	26.07	16.77
32	27.14	16.96	27.06	17.05	26.99	17.19	26,91	17.31
33	1 . 5 5	17.49	27.9L	17.62	27.83 28.68	17.73	27.75 28.60	17.85
34	29.68	18.02	28.75	18.68	29.52	18.81	29.44	18.93
36	30.53	19.08	30.45	19.21	30.36	19.34	30.28	19.48
37	31.38	19.61	31.29	19.74	31.21		31.12	20.01
38 39	32.23	20.14	32 14	20.28	32.05	20.95	31.96	21.10
40		21.20	33.83	21.34	33.74	21.49	33.64	21.64
41		21.73	34.67	21.88	34.58	22.03	34 48	22.18
42		22.20	35.52	23.41	35 42	23 57 23.10	35.32	22.72
43	1 -	23.79	36.37 37.24	23.48	37.31	23.64	37.01	23.80
45	38.16	23.85	38.06	24.01	37.95	24.18	37.85	24.34
46		24.38	38 90	24-55	38.80	24.72	-38.69	24.88
47		24-91 25-44	39.75 40.50	25.08	39.64 40.48	25.79	39.53 40.37	25.43 25.97
49		25.97	41.44	26.15	41.33	26 33	41.22	26.51
50	42.40	26 50	42.29	26.68	42.17	26.87	42 05	27.05
51	43.25	27.03 27.56	43.13	27.21	43.01 43.86	27.40	42.89	27.59
53	44-10	28.09	43.98 44.84	27.75	44.70	27.94 24.48	44 58	28.67
54	45.79	28.62	45.67	28.82	45.54	29.01	45-44	29.21
95	46.64	29.15	46 52	29.35		29.55	46.26	29.75
57	47.49 48 34	29.68 30.21	47.36 48.21	29.88 30.42		:30.09 :30.63	47.10 47.94	30.29. 30.84
3	49.19	30.74	49.05	30.95	48.92		48.78	32.38
. 60	50.88	31.27	49.90	31.48	49.76	31.70	49.61	31.92 31.46
-	Dep.	31.80	Dep	32.02 Lat.	50.60 Dep.	32.24 Let	90.46 Dep.	Lat
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Dist	Lat.	Dep.	Lat.	Dep	Lat.	Dep.	Lat.	Dep.
61	51.73	32.33	51.59	32-55	51.45	32.78	51.30	33.00
63	52.58	32.86	52.44 53.28	33.08 33.62	52.29	33.31	52.14	33-54
64	53-43 54-88	33.91	54-13	34.15	53.13	33.85	52.99 53.83	34 08 34.62
65	55.12	34-44	54-97	34.68	44.82	34.93	54-67	35.16
66	55-97	34-97	55.82	35.22	55.66	35.46	55.51.	35.70
67	56 82 57.67	35. 50 36.03	57-51	35.75 36.29	\$7.35	36.00 36.54	56 35 57-19	36.25 36 79
69	58.52	36.56	58.36	36.82	58 19	37.07	\$8.03	37 33
70	59.36	37.09	59.20	37.35	59-04	37.61	59.87	34.87
71 72	61.06	37.62	60.84	37.89	60.72	38.15 38.69	\$9471 60,55	38.41 38.95
73	61.91	38.68	61.74	38.95	61.57	39.12	1.40	39.49
74	62.76	39.31	63.43	39-49 40.02	62.41	39.76 40 30	62.24 63.08	40.03
75	64.45	39·74 40·37	64.28	40.55	64.10	40.83	\$3.92	40.57
77	65.30	40.80	65:12	41.09	64.94	41.37	44 76	41.66
78	66.15	41.33	65.97	41.62	65.78	41.91	65.60	42.20
79 80	67.00 67.84	41.86	66.81 67.66	41.69	66.63 67.47	42.45	66.44	42.74 43.28
81	68.69	41.93	68.50	43.22	68.31	43.52	68.12	43.82
82	69 54	43.45	69:35	43.76	69.16	44.06	69.97	44.36
93 84	70.39	43.98	70.20	,44.29 .44.82	70.00	44.60 45.13	69.81 70.65	44.90 45.44
85	72.08	45.04		44.36	71.69	45.67	71.49	45.98
86	72.93	45.57		45.89	72.53	46.21	72.33	46.52
87 88	73.78	46.10	73.58	46.43	73.38	46.75 47.28	73.17	47.06 47 61
89	75-48	47.16		147-49	75.06	47.82	74.85	48.15
90	76.32	47.69	76.13	48.03	75.91	48.36	75.69	48.69
91	77.17	48.22	76 96 77.81	48.56	76.75	48.89	76.53	49.23
92 93	78.87	48.75	78.65	49.09 49.63	77.59	49-43	77.38	49.77
94	79 72	49.81	79.50	50.16	79.28	50.51	79.06	50.85
95	80 56	50.24	80.34	50.69	80.13	5 1.04	79.90	51.39
96 97	\$1.41 \$2.26	50.87	81.19	51.76	80 97 81.81	51.58	80.74 81.58	51.93 52.47
98	83.11	51.93	82.88	52.20	82.65	52.66	82.42	53.02
100	83 96 84.80	52 46	83.73 84.57	52.83 53.36	83.50 84.34	53.19	83.26 84.10	53.56.
101	85.65	53.52	85.42	53 90	85.18	53.73	84.94	54.10
102	86.50	54.05	86.26	54.43	86.03	54 80	85.79	54.18
103	7.35	54.58	87.11	54.96	86 87 87.74	55.34	86.63	54.73
104	\$8.20 \$9.04	55.88 55.64	87.96 88.80	56.03.	88.56	55.88 56.42	87.47 88 31	50.26 50 80
106	19.80	56.17	84.65	56.56	89.40	56.95	89.15	57.34
107	90.74	50.70	90.49	57.10	90.24	57-49	89 99	57.88
108	91.59	57 23	91.34	57.63 58.16	g1.09	58.57	90.83	58.42 58.97
1 10	93.29	58.29	93.01	58.70	92 77	59.10	92.51	59.51
111	94-13	58.82	93 88	59.23	93.62	59.64	93.36	60.05
112	94.98	59-35 59.88	94.72 95.57	59.7 6 60. 30	94.46	60.18	94 20	60.59
314	96.68	60.41	96.41	60.83	96.15	61.25	95.04	61.67
115	97-53	60.94	97.26	61.37	96.99	61.79	96 72	62.21
116	98.37	61.47	98.10	61.90	97.83	6233	97.56	62.75
117	99.22 100.1	61.00	98.95 99.80	62.43 62.97	98.68	62.86 63.40	9840 99.24	63.2g
2 59	100.9	63.06	100.6	63.50	1004	63.94	100.1	64.38
120		63.50	101.5	64.03	101.2	64.48	100.9	64.92
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-	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	
1	0.84	0.54	0.84	1.10	0.83 7:67	0.55	0.83 1.66	0.56
2	1.68 2.52	1.09	1.67 2.51	1.64	2.50	1.66	2.49	1.67
3 4	3.35	2.18	3.35	2.19	3.34	2 21	3.33	2.22
3	4.19	2.72	4 18	2.74	4 17	2.76	4.16	2.78
6	5.03	3.27	5.02	3.29	5.00	3.34	4-99	3.33
7 8	5.87	3.81	5.85	3.84	5.84	3.86	5.82	3.89
	6.71	4.36	6,69	4.39	6.67	4.42	6.65 7.48	4-44 5.00
9	7.55	4.90 5.45	7.53 8.36	4.93 5.48	7.51	4.97 5.52	8.31	5.56
10	8.39		9.20	6.03	9417	6.07	9.15	611
112	9.23	5.99 6.54	10.04	6.58	10.01	6.62	9498	6.67
13	10.90	7.58	10.87	7.13	10/84	7.18	10.81	7.22
14	11174	7.63	11.71	2.68	11967	7.73	11.64	7.78
15	12.58	8.17	12.54	8.22	12.51	8.88	12.47	8.33
r6	13.42	8.71	13.38	8.77	13.34	8.83	43,30	8.89
17	14.26	9.26	14:22	9.32	14.18	9.38 9.93	14-14	9-44
18	15.93	9 80	15.89	10.42	15.84	10.49	15.80	10.56
19	16.77	10.89	16.73	10.97	16.68	11.04	16.63	11.tt
21	17.61	11.44	17.56	11.51	17.51	11.59	17.46	11.67
22	18.45	11.98	18.40	12.06	18.35	12.14	18.29	12.22
23	19.29	12.53	19.13	12.61	19.18	11.69	19.12	12.78
24	20.13	13.07	20 07	13.16	20.85	13.35	19 .96 20.79	13.89
25	20.97	13.62	20.91	13.71	-		31.62	14.44
26	21 81	14.16	21.74	14.26	21.68	14.35	;22.45	15.00
27	23.48	15.25	23.42	15.35	23:35	15.45	23.28	15.56
20	24.32	15.79	24 25	15.90	24.14	1601	24.11	16.11
30	25.16	16 34	25.09	16.45	25.02	16.56	24:94	16.67
31	26.00	16.88	.25.92	17.00	25.85	17.11	25.78	17 22
32	26.84	17.43	26.76	17 55	26/68	17.66	26.61	17.78
33	27.68	17.97	27.60	18.09	27.52	18.21	27.44°	18.8g
34	28.51 29.35	18.52	29.27	19.19	19.19	19.32	19170	19.44
35	30.19	19.61	30.14	19.74	10.02	19.87	29:53	20.00
37	31.03	20.15	30.94	20 29	30:85	20.43	30.76	20.56
38	31.87	20.70	31.78	20 84	31.69	20.97	31760	21.14
39	32.71	21.24	32162	21.38	32:52	21.53	32 43	21.67 22.22
40	33.55	21.79	33.45	21.93	33 36	22.08	33.26	
41	34-39	22.33	34.29	22.48	34.49	22.63 23.18	34-09 34-92	22.78 23.33
42	35.23	22 87	35.12	23.58	35.86	23.73	35.75	23.89
43	36.06 36.90	23.42 23.96	36.80	24.12	36.69	24.29	36.58	24.45
45	37.74	24 51	37.53	24.67	37.52	24.84	37:42	25.00
46	38.58	25.05	38.47	25.22	38.36	25.39	38.25	25.56
47	39.42	25.60	39.81	25.77	39119	25.94	39.08	26.67
48	40.26	26.14	40.14	26.32	40.86	27.04	39.91 · 40.74	27.22
. 49	41.09 4493	27.23	41.81	27.41	141.50	27.60	41.57	27.78
50			42.65	27.96		28.15	42.40	28.33
. 51 . 52	42.77 43.61	27.78	43.49	28.51	42.53 43.36	28.70	43.24	28.89
53		28.87	44.32	29.06	44.20	29.25	44.07	2g 45
54	45.29	29 41	45.16	29.61	45.03	29.80	44.90	30.00
55	46.13	29.96	46.00	30.16	45.86	30.36	45.73	30.56
56	46.97	30.50	46.83	30.70	46.70	30.91	46.56	31.11
57		31.04	47.67	31.25 35.80	47.53 48.37	31.46 32.01	47.39 48.23	34.67
58	.48.64 49.48	31.59	48.50	32.35	49.20	32.56	49.06	32.78
59	50.32	32.68	50.18	32.90	50.03	33.12	49.89	33-33
1		Lat.	Dep.	Lat.	Dep.	Lat	Dep.	Lut.
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7	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
61	51.16	33.22	51.01	33.45	50.87	33.67	50.72	33.89
62	52.84	33-77 34-31 -	51.85	33.99	51.70	34.22	51.55	34-45
64	53.67	34.86	53-52	34-54	52 53	34.77	52.38	35.56
65	54-51	35.40	54.36	35.64	54.20	35.88	54 05	36.11
66	55.35	15.95	55.19	36.19	55.04	36.43	54.88	36.67
67	57.03	36.49 37.04	56.87	36.74 37.28	55.87 56.70	36.98 37-53	55.7.1	37.22
69	57.87	37.58	57.70	37.83	57-54	38.08	56.54 57.37	38.33
70	58.71	38.12	58.54	38.38	58-37	38.64	58.20	18.89
71	59 55	38.67	59.38	38.93	59.21	39.19	59 03	39.45
72	60.38	39.24 39.76	61.05	39.48 J 40.03	60.04	39.74	59.87 60.70	40.00
74	62.06	40.30	61.89	40.57	61.71	40.84	61.53	41.11
75	62.90	40,85	62.73	41 12	62.54	41 40	62 36	41.67
76	63.74 64.58	41.39	63.56.	41.67	63.38	41.95	63.19	42.22
77 -	65.42	41.94	64.39, 65.23	42.22	64 21	42.50	64.85	43.33
79	66.25	43.03	66.07	43-32	65.88	43.60	65.60	43.89
80	67.09	43.57	66.90	43,86	66.71	44.16	66.52	44-45
81 82	67.93 68.77	44 12	67.74. 68.58	44.41	67.54 68.38	44.71	67.35 68.18	45.00
83	09.61	45 21	69.41	44.96	69.21	45.84	69.01	45.56
84	70.45	45-75	70.25	46 06	70.05	46.36	69.84	46.67
85	71.29	46.29	71 08	46.60	70 88	46.91	70.67	47.22
86 87	72.13° 72.96	46.84	71.92	47.15	71-71	47 47 48.02	71.51	47.78 48 33
88	73.80	47.93	73-59	48.25	73.38	48.57	72-34	48.89
. 89	74.64	48.47	74-43	48.80	74.22	49.12	74.00	49.45
90	75.48	49.02	75.27	49.35	75.05	49.67	7483	50.00
91	76.33	49.56 50.11	76.94	49.89	75.88 76.72	50.23 50.78	75.66. 76.50	51.11
93	78.00	50 65	77.77	50.99	77-55	51.33	77.33.	51.67
94	78.84	\$1.20	78.61	\$1.54	78.39	51.88	78.16	52.22
95	79 67 80.51	\$1.74	79.45 80.28	52.09	80.05	52.43	78.99	52.78
96 97	84.35	52.29 52.83	81.12	52.64 53-18	80.89	52.99 53.54	79.82 80.65	53.33 53.89
98	84 19	53.37	81.96	53.73	81.72	54.09	81.48	54.45
99	83.03	53 92	82.79 83.63	54.28 54.83	82 55	54.64	82.32	55.00
101	84.71	54.46	84 46		83.39	55.19	83.15	55.56
102	85.54	55 OI	85.30	55.93	85.06	55.75 56.30	84.81	56.67
103	86.38	56.10	86.14	56.47	8589	₫6.85	85.64	57.22
104	87.22 88.06	56.64 57.10	86.97 87.81	57-57	86.72 87.56	57 40 57 9 5•	86.47 87.30	57.78 58 33
106	88.90	57.73	88.65	58.12	88 39	58.51	88.14	58.80
107	89.74	58.28	: 89 4 9	58.67	89.23	59 06	88 97	59 45
108	90.58	58.82	90.32	59.22	90.06	59.61	89.80	60.00
109	91.42	59-37 59-91	91 99 ·	59.76 60.31	90.89	60.16 60.71	90.63	60. ₆ 6
111	93.09	60.45	92.83	60.86	92.56	61.26	92.29	61.67
112	.03-03	61.00	93.66	61.41	93.40	61.82	97.12	62.22
113	94-77	61.54	94.50	61.96	94 23	62 37	93.96	62.78
114	95.61 96.45	62.63	95.34	62.51 63.05	95.96 95.90	б2.92 бв.47	94 79 95.62	63.34 63.89
116	97.29	63.18	97.01	63.60	96.73	64.02	96.45	64.45
117	98.12	63.72	97.85	64.15	97.56	64.58	97.28	65.00
811	98:96	64.27 64.81	98,68 s	64.70 65. 35	98.40	65.68	98.11	65 56 65 11
120	100.6	65.36	100.4	65 80	99-43 100.1	66.23	98.94 99.78	65.67
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat
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7	Lat.	Dep.	Lat	Dep.	Lat.	Dep.	Let.	Dep.
1	0.83	0.56	0.83	0.56	0.81	0.57	0.81	0.57
1 2	1.66	1.13	1.65	1.13	1.65	1.13	1.64	1.14
3	2.49	1.68	2.48	1 69	2.47	1.70	2.46	1.71
4 4	3.32	2.24	3.31	2.25	3.30	2.27	3.29	2.88
15	4.15	2.80	4-13	2.81	4.12	283	411	
1 6	4.97	3.36	4.96	3.38	4-94	3-40	493	3.42
2	5.80	391	5.79	3-94	5.77	3 96 4-53	6.57	3.99 4.56
1 8	6.63 7.46	5 03	6.61 7.44	4.50 5.07	6.59 7.43	5 10	7.39	5.13
10	8.29	5.59	8.27	5.63	8.24	.5.66	8.22	5.70
i	9.12	6.15	9.09	6.19	9.07	6.23	9.04	6.27
112	9.95	671	9.09	6.75	9.89	686	9.86	6.84
13	10.78	7.27	1075	7.32	10.71	7.36	10.68	7-41
14	11.61	7.83	11.57	7.88	11.54	7.93	11.50	7-98
15	12 44	8.39	12.40	8.44	12 36	8.50	12.32	8.55
16	13.26	8.95	13.23	.9.20	13.19	9.06	13.15	9.12
17	14 09	9.51	14.05	9-57	14.01	9.63.	13-97	9.69
18	14.92	10.07	14.88	10.13	14.83	10.76	14-79	10.85
19	15 75	10.62	15.71	10,69 11.26	15.66 16 48	11.33	16-43	11.40
20	16.58		16.53			rt.80		11.97
21	17.41	11.74	17.36	11.52	17.31	12.46	17.25	12.54
22	18.24	12.86	19.01	12.94	18.95	13.03	18.90	13 11
24	19.90	13.42	19.84	13.51	19.78	13.59	19.72	13.68
25	20.73	13.98	20.66	14.07	20.60	14.16	20.54	14-25
26	21 55	14 54	21.49	14.63	21 43	14-73	21.36	14.82
87	22 38	15.10	22.32	15.20	22.25	15.29	22 18	15.39
28	23.21	15.66	23.14	15 76	23.08	15.86	23.01	15.96
29	24.04	16.12	€3.97	16.32	23 90	16.43	23.83	16 53
30	24.87	16 78	24.80	16.88	24.72	16.99	2465	17.10
31	25.70	17.33	25.62	17-45	25.55	17.56	25 47	17.67 18.24
32	26.53	17.89	26.45	18.01	29.37	18.13	26.29	18.81
33 34	27.35	18.45	27.28	18 57	28.03	19.26	27.94	19.38
35	29.02	19.57	28 93	19 70	28.84	19.\$2	28.76	19.95
36	29.85	20.13	29.76	30.36	29.67	20.39	29.58	20.52
57	30.67	20.69	30.58	20.32	30 49	20.96	3040	21.09
38	31.50	21.25	31 41	21 39	31.32	31 52	31.22	21.66
19	32.33	21.81	32.24	21.95	38.14	22.00	32.04	12.23
40	33.16	22.37	33.06	22.51	32.97	22.66	32.87	22.80
41	33 99	22.93	33.89	23.07	33-79	23.22	33.69	23.37
42	34.82	23 49	34.72	23.64	34.61	23.79		23.94
43	35.65	24.05	35.54	24.20	35.44 36.26	24.36 24.92	35.33 36.15	24.51
1 44	36.48	24.60	36-37	24.76	37 09	25.49	36.97	25.65
45	37.31		37.20		37.91	26.05	37.80	20.22
46	38.14	25 72 26.28	38 02 38.85	25.89	38.73	26.62	38.62	26.79
47 48	38.96	26.84	39.68	27.01	39.56	27.19	39-44	27.36
49	40.62	27.40	40.50	27.58	40.38	27.75	45 16	27.93
50	41.45	27 96	41.33	28.14	41.81	28.32	4108	28.50
51	42.28	28.52	42.16	28.70		28.89	41.90	29.07
52	43.11	29 08	42 98	29.27		29.45	4273	29,64
53	43.94	29.64	,43.81	29.83		30.02	43.55	30.31
54	4+77	30.20	44.64	30 39		30.59	44-37	30.78
55	45.60	30.76	45.46	30.95		31 15	45.19	38.35
56	46.43	31 31	46.29	31.52	46 15		46.01	31 92
57	47.26	31.87	47.12	32.08 32.64	46.98	32.89 32.85	47.66	32.49 33.06
58	48.68 48,91	32.43 32.99	47·94 48.97	32.21	48.62	38.48	48.48	33.63
59 60	49.74	33.55	49.60	33-77	49-45	33.98	49.30	34 20
1	Dep.	Let	Dep.	Lat.	Dep.	Lat.	Dep.	TAL
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D. P.	Lat.	Dep.	Lat	Dep.	Lat.	Dep.	Lat.	Dep.
1	52.57	34-11	50.42	34-33	50.27	34-55	50.12	34-77
62	51.40.	34-67	51.25	34.89	21.10	35.12	50-94	35.34 35.91
63	52.23 · 53.06	35.23	52.90	35.46	56.92	35.68 36.25	51.76	36.48
64	53.89	36.35	53.73	36.58	53-57	36.82	53.41	37.05
66	5473	36.91	54-55	37.15	54-39	37.38	54.23	37.62
67	55.55	37-47	55.38	37.71	55.22	37.95	55.05	38.19
1 .68	56.37	38.03	56.21	38.87	56.86	38.52	55.87	38.76 39-33
70	57.80 £8.03	38.58 39.14	57.86	39.40	57-69	39.65	57.52	39.90
71	\$8.86	39.70	58.69	39.96	58.51	40.21	58.34	40.47
72	59.60	40.86	\$9.51	40.52	59.34	40.78	59.16	41.04
73	60,52	40.83	60.34	41.08	60.16	41.35	59.98	41.61 42 18
74 75	62.18	41.38	61.17 61.99	43.95	61.81	42.48	61.62	42.75
-	63.01	42.50	62,82	42.77	62.63	43.05	62.45	43.32
76 77	63.84	43.96	63.65	43.34	63.46	43.61	63.27	43.89
78	64.66	48.62	64.47	43.90	64.28	44.18	64.09	44.46
79 80	66.32	44.18	65.30 66.13	44.46	65.31 65.93	44.75	64.91	45.60
81	67.15	44.74	66.95	45.59	66.75	45.88	66.55	46.17
82	67.98	45.85	67.78	46.15	67.58	46.45	67.37	46.74
82	68.81	46.41	68.61	46.71	68.40	47.01	68.20	47.31
84 85	69.64	46.97	69.43 70,26	47.28 47.84	70.05	47.58	69.02	47.88 48.45
86	70.47	47-53	71.09	48.40	70.87	48.71	70 06	49.02
87	71.30	48.0g 48.65	71.91	48.96	71.70	49 28	71.48	49.59
88	72.96	49.21	72.74	49.53	72.52	49.84	72.30	61.02
-89	73.78	19 ·77	73.57	50.09	73-35	50.41	73.13 73-95	50.73
90	74-61	50.33	74-39	50.65	75.00	31.54	74.77	51.87
94	75.44	50.89	75.22	51.78	75-82	52-11	75.59	57.44
98	77.30	52.00	76.87	52.34	76.64	52.68	76.41	53.01
94	77.93	52.56	77.70	52 90	77-47	53.8a	77.23 . 78.06	53 58 54.15
95	78.76	53.12	78.53	53-47	79.12	-	78 88	54.72
96	79.59 80.42	53.68 54.44	79-35 80.18	54.03 54. 5 9	79-94	54-37	79.70	55.29
98	81.25	54.80	10.18	55.15	80.76	55.61	80.52	55 86
99	82.07	55.36	81.83	55.72	81.59	56.07	81.34 82.16	56.43 57.00
100	82.90	55.92	82.66	·	83.24	56.64	82.99	57-57
101	83.73 84.56	56.48	83.49 84.31	56.84 57.41	84.06	57.31	83.81	58.14
102	85.39	57.60	-85.14	57.97	84.88	58.34	84.63	58.7 i
104	86.22	58.16	85.97	58.53	85.71	58.91	85.45 86.27	59.28
105	87.05	58.72	86.79	59.09	86.53	59.47	87.00	59.85
106	87.98 88.71	59.27	87.62 88.45	59 66 60.22	87.36 88.18	60.64 60.64	87.92	60.42
107	89.54	59.83 60.39	89.27	60.78	10.68	61.17	88.74	61.56
109	90.37	60.95	90.10	61.35	89.83	61.74	89.56	62.13
110	91.19	61.51	90.92	61.91	90.65	62.30	90.38	62.70
111	92.02	62.07	91 75	62.47	91.45	63.44	91.20	63.27 63.84
E13	92.85 93.68	62.63	92.68 93.40	63.60	93.12	64.00	92.85	64.41
114	94-51	63.75	94.23	64.16	93.96	64.57	93.67	64.98
115	95.34	64.31	95.06	64.72	94-77	65.14	94-49	65.55
Z16	96.17 -	64.87	95.88	65.20	95.60	65.70	95.31	66.12 66.69
117	97.00	65.98	96.71 97·54	65.85 66.41	96.42	66.27 66.84	96.95	67.26
119	98.66	66.54	98.36	66.97	98.07	67.40	97.78	67 83
120	99.48	67.10	99.19	67.54	99.90	67.97	98.60	68.40
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55 DECREES

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Dist	0'		13	,	• 30)'	4.5	5'
2 2	Lat	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0 82	0.57	. 0.82	0.58	0.81	0.58	0.81	0.58
	1.64	1.15	1.63	1.15	1.63	1.16	1.62	1.17
3	246	1.72	2.45	1.73	2.44	1.74	2.43	1.75
1 4	3.28	2 29	3.27	2.31	3.26	2.32	3.25	2.34
5	4.10	2.87	4.08	2.89	4-07	2.90	4.06	2.92
6	4.91	3.44	4.90	3.46	4.88	3.48	4.87	3.51
2	5.73 6 55	4.01	5.78	4.04	5.70	4.06	ş.68	4.09
8		4.59	6.53	4.62	6.51	4.65	6.49	4.67
10	7·37 8.16	5.16	7.35 8.37	5.19	7-33 8,14	5.23 5.81	7.3° 8.12	5.84
1		5.74						
11	9.Q1 9.83	6.88	8.98 9.80	6.35 6.93	8.96 9.77	6.39 6.97	8.93	6.43 7.01
13	10.65	7.46	10.62	7.50	10-58	7 55	974	7.60
14	11.47	8.03	11.43	8 08	11.40	8.13	11.36	8.18
15	12.29	8.60	12.25	8.66	12.21	8.71	12.17	8.76
16	13.11	9.18	13.07	9.23	13.03	9.29	12.99	9-35
17	13.93	9.75	13.88	9.81	13.84	9.87	13.80	9.93
18	14.74	10.32	14.70	10.39	14.65	10.45	14.61	10.52
19	15.56	10.90	15.52	10.97	15.47	10.03	15.42	IFIG
20	16.38	11.47	16.33	11.54	16.28	11.61	16.23	11.69
21	17.20	12.05	17 15	12 12	17.10	12.19	17.04	12.27
22	18.02	12.62	17.97	12.70	17.91	18.78	17.85	12.85
23	18.84	13.19	18.78	13.27	18.72	13.36	18.67	13.44
24	19.66	13.77	19.60	13.85	19.54	13.94	19.48	14.08
25		14.34	20.42	,				
26	21.30	14.91 15.49	21.23	15.58	#1.17 #1.98	15.10	21.10 21.91	15-19
27 28	22 94	16.06	22.0;	16.16	22.80	16 26	22.72	16-36
29	23 76	16.63	23.68	16.74	23.61	16.84	13.54	16-94
30	24.57	17.21	24.50	17.31	24.42	17.42	34.35	17-53
31	25.39	17.78	25.32	117.89	25.24	18.00	25.16	18.11
32	26.21	18.35	26.13	18.47	26.05	18.58		18.70
33	27.03	18.93	26.95	19.05	26.87	19.16	46 78	1928
34	27.85	19.50	27.77	19.62	27 68	19.74	47.59	19.86
35	28.67	20.08	28.58	20 20	28.49	20.32	28.41	20.45
. 36	29.49	20.65	29.4C	20.78	29.31	20.91	29.22	21.03
37	30.31	21.23	30.22	21.35	30 12	21.49	30.03	21.62
38	31.13	21.80	31.03	21.93	30.94	22.07	30.84	22,20
39	31.95	22.94	31.85	23.09	31.75	22.65	32.46	23:37
1	I			·				
141	33.59	2,52 24.09	33.48	23.66	33.38	23 81 24-39	33.27	23.95 24.54
42 43	34.40	24.66	34.30	24.82	34.19	24.97	34.90	25.18
44	36.04	25.24	35.93	25.39	35.82	25.55	35.71	25.71
45	36.86	25.81	36 75	25.97	36.64	26.13	36.52	26:29
46	37.68	26.38	37.57	26.55	37.45	26.71	37-33	26.88
47	38.50	26.96	38.38	27.13	38.26	27.29	38.14	27.46
48	39 32	27.53	39.20	27 70	39.08	27.87	38-96	28 04
.49	40.14	28.11	40.02	28.28	39.89	28.45	39.77	28.63
50	40.96	28.68	40.83	28.86	40.71	29.04	40.58	29.21
51	41.78	29.25	41.65	29.43	41.52	29.62	41.39	29.80
52	42.60	29.83		30.01	42.33	30.20	42.20	30.38
53	43.42	30.40		30.59	43.15	30.78	43.01	30.97
,54	44.23	30.97	44.10	31117	43.96 44.78	31.36	43.83 44.64	31.55
55					_			
56	45.87 46.69	32.12 32.69	45.73	32.32	45.59	32.52	45.45 46.26	\$2.72 35:30
57 58	47.51	33.27	47.37	33-47	47.22	33.68	47.07	33.89
59	48.33	33.84	48 18	3405	48.03	34.26	47.88	34-47
66	49.15	3441	49.00	34 63	48.85	34.84	48.69	35.06
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114 93.38 65.39 93.10 b5 79 92.81 b6.20 92.52 06.60 115 94.20 65.96 93.91 16.37 93.62 66.78 93.33 67.79 176.37 93.62 66.78 93.33 67.79 93.62 66.78 93.33 67.79 93.62 66.78 93.33 67.79 93.62 66.78 93.33 67.79 93.62 66.78 93.33 67.79 93.62 66.78 93.33 67.79 93.62 66.78 93.33 67.79 93.62 66.78 93.33 67.79 93.62 66.78 93.33 67.79 93.33 67.79 93.62 66.78 93.33 67.79 93.33 67.79 93.33 67.79 93.33 67.79 93.33 67.79 93.33 67.79 93.33 67.79 93.33 67.79 93.33 67.79 93.33 67.79 93.33 67.79 93.33 67.79 93.33 67.79 93.33 67.79 93.33 67.79 93.33 67.79 93.33 67.79 93.33 67.79 93.33 66.78 93.33 67.79 93.	ı	113	92.56	64.81	92.28	65,22	92.00	65.62	91.71	66.02
116 95.02 66.53 94.73 66.95 94.44 67.36 94.14 67.77 117 95.84 67.11 95.55 67.53 95.25 67.94 94.95 68.36 118 96.66 67.68 96.36 68.10 96.07 68.52 95.77 68.94 119 97.48 68.26 97.18 68.63 96.88 69.10 96.58 69.53 120 98.30 68.83 98.00 69.26 97.69 69.68 97.39 70.14 140 140 140 140 140 140 140 140 141 140 140 140 140 140 140 141 140 140 140 140 140 141 140 140 140 140 140 141 140 140 140 140 140 141 140 140 140 140 140 141 140 140 140 140 141 140 140 140 140 140 141 140 140 140 140 141 140 140 140 140 141 140 140 140 140 141 140 140 140 140 141 140 140 140 140 141 140 140 140 140 141 140 140 140 140 140 141 140 140 140 140 140 141 140 140 140 140 140 141 140 140 140 140 140 140 141 140 140 140 140 140 140 141 140 140 140 140 140 140 140 141 140 140 140 140 140 140 140 140 141 140						05 79	92.81			
117 95.84 67.11 95.55 67.53 95.25 67.94 94.95 68.36 118 96.66 67.68 96.36 68.10 96.07 68.52 95.77 68.94 119 97.48 68.26 97.18 68.63 96.88 69.10 96.58 69.50 98.30 68.83 98.00 69.26 97.69 69.68 97.39 70.11	Ŀ									-
119 97.48 68.26 97.18 68.63 96.88 69.10 96.58 69.53 120 98.30 68.83 98.00 69.26 97.69 69.68 97.39 70.11		117	95.84	67.11	95.55	67.53	95.25	67.94	94-95	
120 98.30 68.83 98.00 69.26 97.69 69.68 97.39 70.11										
Don Tot Den Lat										
0' 45' 30' 15'	ı						Dep	Lat.	Dep.	Lat.
	1	Dis	0		45	1		<u> </u>	13	5'

790		07		15/		307		45	
Di at	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep	
<u> </u>	6.81	0.59	0.81	0.59	0.80	0.59	0.80	3.60	
	1.62	1.18	1.61	1.18	1.61	1.19	1.60	143	
3	2.43	1.75	2.42	1.77	2.41	1.78	3.40	79	
4	3.24	2.35	3.23	2.37 2.96	3.22 4.02	2.97	3.20 4.01	2.39 2.99	
1.5	4.05	2.94	4.03		4.82	3-57	4.81	3.59	
6,	4.85	3.53	4.84 5.65	3.55 4.14	5.63	416	5.61	4.19	
7	5.66 6.47	4.70	6.45	4-73	6.43	4.76	6.41	4-79	
9	7.28	5.29	7.26	5.32	7.23	5-35	7.21	5.38	
10	8.09	5.88	8.06	5.91	8.04	1.25	10.8	5.98	
11	8.90	6.47	8.87	6.50	8.84	6.54 7.14	8,81 9.61	7.18	
12	9.71	7.05	9 68	7.10	9.65	7.73	10.41	7.78	
13	10.52	8.23	11.29	8.28	11.25	3.33	71.22	8.38	
15	12.14	8.82	12.10	8.87	12.00	8.92	12.02	8.97	
16	12.94	9.40	12.90	9.46	12.86	9.54	12.82	9-57	
17	13 75	9.99	13.71	10.05	13.67	10.11	13.62	10.17	
18	14.56	10.58	14.52	10.64	14-47 15-27	10.71	15.22	11.37	
19	15.37	11.76	16.13	1187	16.08	11.90	16.03	11.07	
21	16.99	12.34	16.94	12.42	16.88	12.49	14.83	12.50	
22	19.80	12.93	17.74	13.01	17.68	14.09	17.63	19.16	
23	18.61	13.52	18.55	13.60	18.49	13.68	18.43	13-70	
24	19.42	14.11	19.35	14.19	19.29 29.10	14.28	20.03	14.96	
25	20.23	14.69	20.16			15.47	20.83	15.58	
26	21.03	15.28	20.9	15.37	20.90	16.06	21.63	16.16	
27	22.65	16 46	22.58	16.56	22.51	16.65	22.44	16.79	
29	23.46	17.05	33.39	17.14	23.31	17.25		17.35	
30	24.27	17.63	24.19	17.74	24.12	17.84	24 04	17.95	
31	25.08	18.22	25.00	18.33	24.92	18.44		18-55	
32	25.89	19.40	25.81 26.61	18.92.	25.72	19.03	26.44	19.74	
33 34	25.70	19.98	27.42	20.10	27.33	20.22	27.24	20.34	
35	28.32	20.57	28.23	20 70	28.13	26.82	28.04	20.94	
36	29.12	21.16	29 03	21.29	28.94	21.41	28.85	21.54	
37	29.93	21.75	29.84	21.88	29.74	22.05	29.65 30.45	22.14	
38	30.74	22.34 22.92	30.64	23.06	30.55	23.20	31.25	23.74	
39	37.55 32.36	23.51	32.26	23.65	32.15	23.79	32.05	23.93	
41	33-17	84.10	33.06	24.24	32.96	24.39	32.85	24.53	
42	33.98	24.69	33.87	B4-83	33.76	24.98	33.65	25.13	
43	34.79	25 27	34.68	25.43	34-57	25.58	34-45 35.26	25.73	
44	35.60	25.86	35.48 36.20	26.02 26.61	35-37 36.17	26.17	36.06	26.33 26.92	
45	30.41	26.45	37.10	17.20	36.98	27 36	36.86	27-52	
46	37.22 38,02	27.63	37.10	17-79	37.78	27.96	37.66	28.12	
47 -	38.83	12.84	38.71	18.38	38.59	28.55	38.46	28.72	
49	39.64	28.80	39.52	28.97	39.39	29.15	39.26 40.06	29.32	
50	40.45	29.39	40.32	19.57	40.19	29.74	40.86	29.92	
52	41.26	29.98	41.13	10.16	41.80	30.34	41.67	30.51	
52 53	42.07 42.88	30.56 31.15	41.94	11.34	42.60	31.53	42.47	31.71	
54	43.69	32-74	43.55	31.93	43.41	32.12	43.27	32.31	
55	44.50	32.23	44.35	32.52	44.21	32.72	44.07	32.91	
.56	45.30	32.92	45.16	33.11	45.02	33-31	44.87	33-51	
57	46.11	33.50	45.97	33.70	45.82	33.90	45.67	34.70	
58	46.92 47.73	34.09 34.68	45.77	34.89	47.43	34.50	47.27	35 30	
59 60	48.54	35.27	48.39	35.48	48.23	35.69	48.08	35.90	
	Dep.	Lat.	Dep.	Lat	Dep.	Lat.	Dep.	Lat.	
Dist.	0,	₁	45	7	30)/	1	51	
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ľ	-	0	-	1.	5*	3	01	45	7
1	Dist.	Lat.	Dep.	Lat	Dep	Lat.	Dep.	Lat.	Dep.
ŀ	61	49.35	35.85	49.19	36.07	49.04	\$6.26	48.88	36 50
ı	62	50.16	35.44	20.00	36.66	49.84	30.88	49.63	87 10
ı	63 64	50.97	\$7-03 \$7-62	52.61	37.25	51.45	\$7.47	51.28	37.69 28.29
1	65	52.59	38.21	52.42	38.44	52.25	8.66	54 08	38.89
I	66	53.40	\$8.79	53.23	39.03	53.09	\$9.36	58.88	39 49
1	67 68	54.20	39.38	54.03 54.84	39.62 40.21	53.85 54.66	40.45	53.68 54-49	40.09 40.69
1	69	55.82	40.56	55 64	40.00	55.47	41.34	55.29	41.28
1	70	56.63	4 r. 14	56.45	41.39	56.27	41.64	56 09	41.88
	71	57.44	41.73	57.26 5806	41.98	57.88	42.23	56.89 57.69.	#2.48 #3.68
1	72 73	59.06	42.9F	58.87	43.17	58.68	43.42	58.49	43.68
١	74	59.87	43.50	59:68	43.76	59-49	44.02	59.29	44.28
ŀ	75	60.68	44.08	60.48	44.35	69.00	44.61	60.09	44.87
1	76 77.	64.49	44.67	64.10	44-94	62.90	45.80	60.95	45.47
ŧ	78	63:10	45.85	62.90	46.12	62.70	46.40	62.50	46.67
ł	79.	63.94° 64.73	46.43	64.52	46.71	63.50	46.99	64.10	47.27
F	81	65.53	47.61	65.32	47.90	64.31	47.59	64.90	47 87
ł	82	66.34	48.20	66.143	48.49	65.98	48.78	65.70	19.06
1	83	67.05	48.79	66.93	49.08	65.72	49-37	66.50	49.66
1	84 85	68.77	49.37	68.55	\$0.26	68.33	49.97 50.56	68.14	50.26·
ł	86	69.48	50.55	69.35	50.85	69.13	51,15	68.91	51.46
I	87.	70.38	\$1.14	70.16	\$1.44	69.94	\$1.75	69.71	\$2.05
1	88 89	71.19	\$1.73 \$2.31	70.97	52.62	70.74	52-34	70.51 71.31	52.65
ł	90	72.81	52.00	72.58	\$3.22	72.35	53.53	78.18	\$3.85
ľ	91	73.62	53.49	78-39	\$3.81	73.15	54.13	79.92	\$4.45
1	92	74-43	\$4.08 \$4.66	74.19	\$4.40	73.95	54.72	75.72 74.52	\$5.05
1	93 94	76.03	55.25	75.81	\$5.58	75.56	55.32	75.32	\$5.64
Į.	95	75.86	55.84	76 61	\$6,17	76.37	\$6.51	75.12	\$6 84
l	96	77.67 78.47	\$6.43	77.42	56.77	77.17	57.10	76.92	57-44
Į	97 98	79.28	57.60	78.25	57.36	77.97 78.78	57.70 58.20	78.52	58.64 58.64
I.	99	80.09	58.19	79.84	\$8.54	79.58	58.89	79.32	\$9.23
4-	100	80.go 81.71	58.78	80.64	59.13	80.39	59.48	80 73	59.83
	101	82.52	59-37	81.45	\$9.72 60.31	81.19	60.08	80.93 81.75	60.43 61.03
ŀ	105	83.33	60.54	83.06	60.90	82.80	61.27	84.53	61.63
	104 105	84.14	61,72	83.87 84.58	62.00	89.60	62.46	89.35	62.23 62.82
-	06	85.76	62.31	85.48	62,68	85.21	63.05	84.93	3.42
ŀ	107	86.56	62.89	86.29	63-27	86.01	63.65	85.73	64.02
	106 109	87.37 88.48	63.49	87.90	63.86	86.82 87.61	64.24	86.54	64.62 .
	סד	88.99	64.66	88.71	65.04	88.41	64.84 65.43	87.34 88.14	65.22 65.82
1	11	89.80	65.24	89.52	65.64	89.23	66.03		66.41
	12	99.61	65.83	90.32	66.23	90.03	66.62	89 74	67.01
	13	91.42	67.01	91.13	66.82	90.84	67. 22 67.81	90.54	67.61
	15	93.04	67.60		68.00	92 44	68 40	92.14	18.86
1	16	93.85	68.48		68.59	93:25	69.00	91.95	69.41
	17		68.77 69.36		69.18 69.77	94.86	69.59 70.19	93.75	70.00 70.60
ŀ	19	96.87	69.95	95.97	70.37	95.66	70.78		71 20
F-	20	97.08	70.53	96177	70.96	96.46	71.38	95.15	71.80
1.		Dep.	Lqt.	Dep.	Lat.	Dep.	Lat.		Lat
1_	٠.'	Ú		45	DECD	30/		15	

18	07		15	7	30)7	45'	
ğ	Lat	Dep.	Lat	Dep.	Lat.	Dep.	Lat.	Dep.
1	0.80	0.60	0.80	0.61	0.79	,0,61	0.79	0.61.
.2	1.60	1.20	1.59	1.82	1.59 2.38	1.83	€.5¥ 2.37	1.32
3	2.40. 3.19	2-41	2.39 3.18	2.42	3.17	243	3.16	
3	3.99	3.01	3.98	3.03	3.97	3.04	3.95	3.06
6	479	3.61	4 78	3.63	4-76	3.65	4-74	3.67
7	ş.59	4.21	₹·57	4.24	5:55 6.35	4.26	5.53 6.33	4-29
9	6.39 7.19	4.81 5.42	9.16	5-45	7-14	5.48	7.12	5.51
10	7.99	6.02	7.96	6.05	7-93	6.09.	7.91	6.12
11	8.78	6.62	8.76	6.66	8.73	6.70	8.70	6.73
12	9.58 10.38	7.22	9.55	7.26 7.87	9.52	7.21	9.49 10.28	7.35
14	11.18	8.43	11.14	8-47	11.11	8.52	11.07	8.57
15	1198	9.03	11.94	9.08	11.90	9.13	11.86	9.18
16	12.78	9 63	12.74	9.68	12169	9-74	12.65	9.20
17	13.58 14.38	10.23	13.53	10.29	13.49 14.28	10.35	13-44	10.41
19	15.17	11.43	15.12	11.50	15.07	11.57	15.02	11.63
20	15.97	12.04	15.92	12.11	15.87	12.18	15.81	12.24
21	16.77	12.64	16.72	12.71	16.66	12.78	16.60	13.47
22	17.57	13.24	17.51	13.32	17.45	13.39	17.40	14.08
24	18.37	14-44	18.31 19.10	14-53	19.04	14.61	18.98	14.69
25	19.97	15.05	19.90	15.13	19.83	15.22	19.77	15.31
26	20,76	15.65	20,70	15:74	20.63	15.83	20.56	15.92
27	21.56	16.25	21.49	16.34 16.95	21.42	16.44	21.35	16.53
29	23.16	17.45	22.29 23.08	17.55	23.01	17.65	22.93	17.75
30	23.96	18.05	23.88	18.16	23.80	18.26.	23.72	18.37
31	24.76	18.66	24 68	18.76	24.59	18.87	24.51	18.98
32	25.56	19.26	25.47 26.27	19.37	25.39 26.18	19.48 20.09	25.30 26.00	19.59
33	26.35 27.15		27.06	20 58	26.97	20.70	26.88	20.82
35	27.95	21.06	27.86	21.19	27.77	21.31	27.67	21.43
36	28.75	21.67	28.66	21.79	28.56	21 92	28 46	22.04
37	29-55 30.35	22.27 22.87	29.45 30.25	22.40 23.00	29,35 · 30.15	22.52	29.26 30.05	22.95 23.26
39	31.15	43.47	31.04	23.61	30.94	23.74	30.84	23.88
40	31.95	24.07	31.84	24.21	31.73	24.35	31.63	24.49
41	32.74	24.67	32.64	24.82	32.53	24.96	32 42 33.21	25.10
42 43	33·54 34·34	25.28 25.88	33-43 34-23	25.42 26.03	33.33*	25.57	34.00	25.71 26.33
44	35.14	26.48	35.02	26.63.	34-91	26.79	34-79 -	26.94
45	35.94	27.08	35.82	27.24	39.70	27.39	35.58	27.55
46	36.74	27.68	36.62	27 84	36.49	28.00 28.61	36.37 37.16	28.16 28.77
47 48	37·54 38·33	28.29 28.89	37.41 38.21	28.45 29.05	37-29 38.08	19.22	37.10	29.39
49	39.13	29 49	39.00	29.66	38-87	29.83	38.74	30.00
50	39.93	30.09	39.80	30.26	39.67	30.44	39-53	30.61
54	40.73	30.69	40.60	30.87	49.46	31.66	40.33	31.22
52 53	41.53	31.29	41.39	31.48 32.08		32.26	41.12	32.45
54	43.13	32.50	42.98	32.69	42.84	32.87	42.70	33.06
55	43.93	33.10	43.78	33.29	43.63	33.48	43.49	33.67
56	44-72	33.70	44.58	33.90	44-43	34 09	44.28	34.28
57 58		34.30 34.91	45.37 46.17	34.50	45.22 46.01	`34.70 35.31	45.86	34.90
59		35.51	46.96	35.71	46 81	35.92	46.65	36.12
60	47.92	36.11	47.76	36.32	47.60	36.53	47.44	36.73
Dist	Dep.	Lat.	Dep.	Lat.	Dep	Lat	Dep.	Lat-
18	0/	i	45	,	30	,	1.	5/ _

		l v			5/	1 30			5'
1	Dist.			Lat.	D p:	1			
		Lat	Dep.			Lat.	Dep.	Lat.	Dep.
	61	48.72	36 71 37-31	48.56	36.92 37.53	48.39	37.13 37.74	48.23 49.02	37·35 37·96
1	63	50.31	37.91	20.12.	38.13	49.98	38.35	49.81	38.57
	64	51.11	38.52	50.94	38.74	50.77	38 96	50.60	39.18
-	65	51.91	39.12	51.74	39-34	51.57	39.57	51.39	39-79
	66	52.71	39.72	52.54	39.95	52.36	40.18	52.19	40.41
1	67 68	53.51 54.31	40.32	53·33 54·13	40.55	\$3.15 \$3.95	40.79	52.98 53.77	41.02
	69	55.11	41.53	54.92	41.77	54 74	43.00	54.56	42.24
	<i>7</i> 0	55.90	43.13	55.72	44.37	55.53	42.61	55.35	42.86
-	71	56.70	42.73	56.52	42.98	56.33	43.22	56.14	43-47
1	72	57 50	43.33	57.31	43.58	57.12	43.83	56.93	44.08
1	73 74	58.30 59 10	43 93 44-53	58.11 58.90	44-19 44-79	57.91 58.71	44-44	57.72	44-69 45-30
1	75	59.90	45.14	59.70.	45.40	59.50	45.66	59.30	45.92
1	76	60.70	45.74	60.50	46.00	60.29	46.27	60.09	46.53
1	77	61 49	46.34	61.29	46.61	61.09	46.87	60.88	47.14
1	78	62.29	46.94	62.09	47.21	61.88	47.48	61.67	47-75
1	79	63.89	47.54	62.88	47.82 48.42	62.67 63.47	48.09 48.70	62.46 63.26	48.37 48.98
1	81	64.69	48.75	64.48	49.03	64.26	49.31	64.05	
	82	65.49	49.35	65,27	49.63	65.05	49.93	64.84	49-59 50.20
1	83	66.29	49-95	65.07	50.24	65.85	50.53	65.63	50.81
1	84	67.09	50.55	*66.86	50.84	66.64	94.14	66 42	51.43
-	85	67.88	51,15	67.66	51.45	67.43	51.74	67.21	52.04
1	86 87	69.48	51.76 53.26	68.46 · 69.25	52.66	68.23 69.02	52.35 52.96	68.00 68.79	52.65 53.26
1	88	70.28	52.96	69.04	53.27	69.62	53-57	69.58	53.88
١.	89	71.08	53.56	70.84	53.87	70.61	54-18	70.37	54-49
1	90	71 88	54.16	71.64	34.48	71.40	54-79	71.16	55.10
	91	72.68	54-77	72 44	55.08	72.20	55.40	71.95	55.71
1	92 93	7347 · 74-27	55.37	73-23 74.03	55.69	72.99	56.61	72.74	56.32
1	94	75.07	56.57	74.82	56.90	73.78	57.22	73.53 74.32	56.94 57.55
	95	75.87	57.17	75.62	57.50	75.37	57.83	75.12	58.16
1	96	76.67	57.77	76.42	58.14	76.16	58.44	75.91	58.77
1	.97	.77-47	58.38	77.21	58.71	76.96	59.05	76.70	59-39
1	98 99	78.27 79.06	58.98	78.01 78.80	59.32	77.75 78.54	59.66 60.27	77-49 78.28	60.61
1	100	79.86	60.18	79.60	60153		60.88	79.07	61.22
1	101	80.66	60.78	80.40	61.13	80.13	61.48	79.86	61.83
1	101	81.46	61.39	81.19	61.74	#D.92	62.09	80.65	62.45
1	103	82.26 83.06	61.99	81.99	62.35		62.70	81.44	63.06
	104	83.86	62.59	82.78 4 83.58	62.95 63.55	8251 83 30	63.31	82.23	63.67 64.28
ł	106	84.66	63.79	84.38	64.16		64.53		
-	107	85.45	64.39	85.16	64.77		65.14	83.81 84.60	64.89 65.51
1	108	86.25	65.00	85.97	65.37	85.68	65.75	85.39	66.12
J	109	87.05	65.60	86.76	65 98		66.36	86.19	66.73
1	110	87.85	66.20	87.56	66.58	87 27	66.96	86 98	67.34
١	111	89.45	67.40	88.36 89.15	67.19 67.79	88.86	67.57	87:77	67.96
1	113	90.25	68.11	89.95	68.40		68.79	88. 56 89.35	48.57 89.18
-	114	91.04	68.61	90.74	69.00	90.44	69.40	90.14	69.79
ļ	115		69.21	91.54	19.61	91.24	70.01	90.93	70.40
.	116	92.64	69.81	91.34	70.21	92.03	70 62	91.72	71.02
	117	93·44 94·24	70.41	93.13	70.82	92.82	71.23	92.51	71.63
ļ	149	95.04	71.62	94.72	72 03	94.41	72.44	93.30	72.24 72.85
	120	95.84	72 22	95.52	72.64	95.20	73.05	94.88	73.47
i	ايد	Dep.	Lat	Dep.	Lat.	Dep.	Lat.	Dep	Lat.
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52 DEGREES,

	_		15	,	34	.,	1 2	37
Dist	0							
7	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
	0.79	0.63	0.79	0.62	0.78	0.62	0.78	0.63
2	1.58	1.33	1457	1.86	1.57	1.87	1.56 2.34	1.88
3	2,36	1.85	2.36 3.14	2.48	2.35 3.13	1.49	3.12	2.50
. \$	3.25 °	1.08	3.93	3.10	3.91	3.12	3,90	3.13
6	473	1.69	4.74	3.71	4.70	3.74	4.68	3.76
7	5.58	4.32	5.50	4.33	5.48	4.36	5.46	4.38
8	6 30	4-93	6.28	4.95	6.26	498	6.24	5.01
.9	7.00	5.54	7.07	5.57	7.04	5.60 6.23	7.80	5.63 6.36
10	7 88	6.16	7.85	6.19	7.83	6.8;	8.58	6.89
11	8.67	6.77	8.64	6.81 7.43	9.39	7.47	9.36	7.51
12	9.46	7-39 8.00	9.42	8.05	10.17	8.00	10.14	8.14
14	11.03	8.62	10.99	8.67	10.96	8.72	10.92	8.76
15	12.82	9.23	11.78	9.29	11,74	9.34	11.70	9.39
16	12.61	9.8;	12.57	9.91	12.52	9.96	12.48	10.01
17	13.40	10.47	13.35	10.52	13.30	10.58	13.26	10.64
18	14.18	80 11	14.14	11.14	14.09	11.21	14.04	11.80
19	14 97	1170	14.92	11.76	15.65	11.45	15.60	12.58
20	15.76		16 40	43.00	16.43	13.07	16.38	13.14
21	16.65 17.34	12.93	17.28	43.62	17.22	13.70	17.16	13.77
23	18.12	14.16	. 18 06	14.24	18.00	14.52	17.94	14-40
24	18.91	14.78	18.85	14.86	18.78	14-94	18.73	15.08
25	19.70	15.39	19.63	15.48	19.57	15.56	49.50	15.65
26	20.49	16.01	20.43	16.10	20.35	16.19	20.48	16.27 16.99
27	21.28	16.62	21.20	16.72	21.05	17.43	21.84	17.53
28	22.8¢	17.85	22.77	17.95	22.70	18.05	22.62	18.15
30	23.64	18.47	23.56	18.57	23.48	18.68	23.40	18.78
731	24.48	19.02	24-34	19.10	24.26	19.30	24.18	19.40
38	25.22	19.70	25.13	19.81	25.04	19.91	84.96	20.0g 20.66
33	26.00	20.32	25.92	20.43	25.83 26.61	20 54	26.54	21.28
34	26.79	20.93	26.70 27.49	21.05	27.59	81.79	27.90	21.91
35	27.58	27.55	28.27	22.29	28.17	22.41	28.08	22.58
36 37	20.16	22.78	29.06	2291	28.96	23.03	18.86	23.16
38	29.94	23 40	29.84	23.53	89.74	23.66	29.64	23.79
39	30.73	24.01	30.63	24.14	30.52	24.28	30.43	34.43 85.04
40	31.52	24.63	31.41	24.76	31.30	24.90		25.66
41	32.31	25.24	32.20	25.38	32.09 32.87	25.52	31.98	26.29
42	33.10	25.86 26 47	32.98	26.62	33.65	26.77	33-53	26.91
43	34.67	27.09	34.55	87.24	3443	27-39	34 31	27.54
45	35 46	27 70	35-34	87.86	35 22	28.01	35.09	28.17
46	36.25	28.32	36.12	28.48	36.00	28.64	35.87	28.79
47	37.94	28.94	36.9 t	29.10	36.78	29.26	36.65	29.43
48	37.82	29.55	37.70	29.72	37.57	29.88 30.50	37-43 38.21	30.04 30.67
49	38.61	30.17	38.48 39.27	30.34 30.95	38.35 39.13	31.13	38.99	3:-30
50	39.40				39.91	31.75	39.77	31.92
51 53	40.19 40.98	31.40 32.01	40.05 40.84	31.57	40.70	32.37	40.55	32.55
53	41.76	3263	41.62	32.81	41.48	32.99	41.33	33.17
54	42.55	33.25	42.41	33.43	42.26	33.62	42.11	33.80
35	43-34	33.86	43.19	34.05	43.04	34.24	42.89	34-43
56	44-13	34.48	43.98	34.67	43.82	34.86	43.67	35.05 35.68
67		35.09	44.76	35.29	44.61 45.39	35.48 36.11	44 45 45.23	36.30
58	45.70 46.49	35.71 36 32	45.55 46.33	36.53	46.17	36.73	46.01	36.93
59 60	47.28	36.94	47.13	37.15	46.96	37.35	46.79	37 56
	Dep.	Lat.	Dep	Lat.	Dep.	Lat	Dep	Lat.
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9	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
64	48.07	37.56	47.90	37.76	47.74	37.97	47.57	38.18
61			48.69	38.38	48.52 49.30	38.60 39.22	48.35	38.81 39.43
64	50.43		50.26	39.62	50.09	39.84	49.91	40.06
65		-	51.05	40.24	50.87	40 46	50.69	40.68
66	,	40.63	51.83	40.86	51.65	41.71	51.47 52.25	41.31 41.94
68	53.58	41.25	53.40	42.10	52 43 53.22	42.33	53.03	42.56
69	54-37	42.48	54.19	42.72	54.00	42.95	53 81	43.19 43.81
70		43.10	54.97	43.34	54.78	43.58	54-59 55-37	44-44
71	55.95 56.74	43.71	55.76	43.96 44.57	55.57 56.35	44.82	56.15	45.07
73	57.52	44-94	57 33	45.19	57.13	45-44	56.93	45.69
74		46.17	58.11	45.81 46 43	57.91 58.70	46.67 46.69	57.71 58.49	46.32 46.94
76	_	46.79	59.68	47,05	59.48	47.31	59.27	47.57
77	60.68	47.41	60.47	47.67	60.26	47-93	60.05	48,20
78			61.25	48.29 48.91	61.04	48.56	60.83	48.82
79 80			62.83	49.53	62.61	49.80	62 39	50.07
87	63.83		63.61	50.15	63.39	50.42	63.17	50.20
82			64.40	50 77	64.17	51.05	63.93	51:33
83 84		51.10	65.18	51.38 52.00	64 96 65.74	51.67	64 73	51.95
85	66.98		66.75	52.62	66.52	52.91	66.29	53.20
•86		52.95	67.54	53.24	67.30	53.54	67.07	53.83
87 88	68.56 69.34		68.32	53.86 54.48	68.09 68.87	54.16	68.63	54.46
89	70.13	54-79	69.89	55.10	69.65	55.40	69.41	55.71
90	70.92		70 68	55.72	70.43	56.03	70.19	56.33
91	71.71		71.46	56.34 56.96	71.22	56 65	70.97	56.96
92			73.03	57.58	72.78	57.89	72.53	58.21
94	74.07	\$7.87	73.82	58.19	73.57	58.52	73.31	58.84
95		58.49	74.61	58.81	74.35	59.76	74.09	59.46 60.29
96 97	75.65	59.10	75.39 76 18	59.43	75.13 75.91	60 38	75.65	60.71
98	77.22	60.33	76.96	60.67	76.70	61.01	76.43	61.34
100		61.57	77.75	61.29 61.91	77.48 78.26	61.63	77.21	62.59
101	79.59	62.18	79.32	62.53	79.04	62.87	78.77	63.22
102	80.38	62.80	80.10	63.15	79.83	63.50	79-55	63.84
103	81.17	63.41	80.89 81.67	63.77 64.39	80.61 81.39	64.12	80.33	64.47
104	81.95	64.64	82.46	65.00	82.17	65.36	\$1.89	65 72
106		65.26	83.24	65 62	82.96	65.99	82.67	66 35
107	84.32	65.88	84 03	66.24 66.86	83.74	66.61 67.23	83.45 84.23	66.97 67.60
109	1	66.49	84.81 85.60	67.48	85.50	67.85	85.01	68.23
110		67.72	86.38	68.10	86.09	68.48	85.79	68.85
1111	87.47	68.34	87 17	68.72	86.87	69.10	86.57	69.48
113		68.95	87.96 88.74	69.34 69.96	87.65 88.43	69.72 70.34	87,35	70.10
1114		70.19	89.53	70.58	89.22	70.97	88 91	71.36
1115		70.80	90.31	71.20	90.00	71.59	89.69	71.98
116			91.10	71.84	90.78	72.21	90.47	72.61
117			92.67	73.05	92-35	73.46	92.03	73.86
1119	93.77	73.26	93.45	73.67	93.13	74.08	92.81	74.48
120		- I	94-24	74-19 Lat	93.91 Dep.	74 70	93·59. Dep.	75.11
List.	Dep	Late	D-p. 4.		30 30			5/
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T E	- 0,	,	ı -	1	30)/	45	<u> </u>
Dist.	Lat.	Dep	Lat.	Dep.	lais !	Dep.	Lat.	Dep.
	0.78	0.63	0.77	0.63	0.77	0.64	0.77	0.64
2	1.55	1.26	1.55	1.27	1.54	1.27	1.54	1.28
3	2.33	1.89	2.32	1.90	2.31	191	2.31	1.92
4	3.11	2.52	3.10	2.53	3.09	2.54	4.08	2.56
_5	3.89	3.15	3.87	3.16	3.86	3 18	1.84	3.20
6	4.66	3.78	4.65 5.42	3.80 443	4.63 5.40	3.82. 4.45	4.61 5138	3.84 4.48
7 8	5.44 6.22	5.03	6.20	5.06	6.17	5.09	6.15	5.12
9	6.99	5.66	6.97	5.69	6.94	5.72	6.92	5.75
10	7.77	6.29	7.74	6.33	. 7.72	6.36	7.69	6 39
11	8.55	6.92	8.52	6.96	8.49	7.00	8.46	7.03
. 12	9 3 3	7.55	9.29	7.59	9.26	7.63	9.23	7.67
13	10.10	8.18	10.07	8.23 8.86	10.03	8.27	9.99	8.31
14	10.88	8.81 9.44	10.84	9.49	10.80	8.91 9.54	10.76	8.95
15		10.07		10.12		10.18	12.30	9.59
16	12.43	10.70	12.39	10.76	12 35	10.13	13.07	10.23
18	13.99	11.33	13.94	11.39	13.89	11.45	13.84	11.51
19	14.77	11.96	14.71	12.02	14 66	12.09	14.61	12.75
20	15.54	12.59	15.49	1265	15.43	12.72	15.38	12.79
21	16.32	13.22	16.26	13.29	16.20	13.36	16.15	13.43
22	17.10	13.84	17.04	13.92	16.98	13.99	16.91	14.07
23	17.87	14.47	17.81	14.55	17.75	14.63	17.68	14.71
24 25	19.43	15.73	19.36	15.82	19.29	15.90	19.22	15.35
26	20.21	16.36	20.13.	16.45	20.06	16.54	19.99	10.63
27	20 98	16.99	20.91	17.08	20.83	17.17	20.76	17.26
28	21 76	17.62	21 68	17.72	21.61	17.81	21.53	17.90
29	22.54	18.25	22.46	18.35	22 38	18.45	22.30	18.54
30	23.31	18.88	23.23	18.98	23.15	19.08	23.07	19.18
31	24.09	19.51	24.01	19.61	23.92	19.72	23.83	19.82
32	24.87	20.14	2.1 78	20.25	24.69	20.35	24.60	20.46
33	25 65	20.77	25.55 26 33	20.88	25.46	20,99	25.37 · 26.14	21.10 21.74
34 35	27.20	22.03	27.10	22.14	27.01	22.20	26.91	32.38
36	27.98	22.66	27.88	22.78	27.78	22.90	27.68	23.02
37	28.75	23.28	28.65	23.41	28.55	23.53	28.45	23.66
38	29.53	23.91	29.43	24 04	29.32	24.17	29.22	24.50
39	30.31	24.54	30.20	24.68	30.09	24.31	29.98	24.94
40	31.09	25.17	30.98	25.31	39.86	24.44	30.75	25.58
41	31.86	25.80	31.75	25.94	31.64	26.08	31.52	26.22
42	32.64	26.43 27.06	32.52	26.57	32.41	26.72 27.35	32.29	26.86
43	33.42	27.69	33.30	27.84	33.95	27.99	33.83	27.50
45	34.97	28.32	34.85	28.47	34.72	28.62	34.60	28.77
46	35.75	28.95	35.62	29.10	35 49	29.26	35-37	29.41
47	36.53	29.58	36.40	29.74	36.27	29.90	36.14	30.05
48	37.30	30.21	37.17	30.37	37.04	30.53	36.90	30.69
49	38.08	30.84	37.95	131.00	37.81	31 17	37.67	31.33
50	38.86	31.47	38.72	31.64	38.58	31.80	38.44	31.97
51	39.63	32.10	39.49	32.27	39.35	32.44	39.21	32.61
52 53	40.41	32.72	4C.27	32.90 33.53	40.12	33.08	39.98	33.25 33 84
54	41.97	33 98	41.82	34.17	41.67	34-35	41.52	34.53
55	42.74	34.61	42.59	34.80	42.44	34.98	42.29	35.17
56	43.52	35 24	43.37	35.43	43.21	35.62	43.06	35.87
57	44.30	35.87	44.14	36.c6	43.98	36.26	43.82	36.41
58	45.07	36.50	44.91	36.70	44-75	36.89	44.59	37 69
60	45.85	37.13	45.69	37.33	45.53	37.53	45.36	37-73
	46.63	-	46.46	37.96	46.30	38.16		38.37
Dist.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
<u>' </u>	1 (y/	1 4:	5/	\$ 3	07	1 1.	\$ '

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Dist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
61	47.41	38.39	47.24	38.60	47.07	38.80	46.90	39.01
62 63	48.18 48.96	39.02	48.01 48.79	39 23 39.86	47.84 48.61	39.44 40 07	47.67 48.44	39.65 j 40.28 j
64	49.74	40 18	49.56	42.49	49.38	40.71	49.21	40 92
65	50.51	40.91	50.34	41.13	50.16	41.35	49.97	41.56
66	51.29	41-54	51.11	41.76	50.93	41.98	50.74	42.20
67 68	52.07	42.16	51 88 52.66	42.39 43.02	51.70 52.4 7	42.62 43.25	51.51	42.84
69	52.85	42.79	53.43	43.66	53.24	43.89	53.05	44.12
73	54.40	44.05	54.21	44.29	54.01	44-53	53.82	44.76
71	55.18	44.68	54.98	44.92	54 79	45.16	54.59	45.40
72	55.95	45.31		45.55 46.19	55.56	45.80	55.36	46.68
73 74	56.73 57.51	45.94 46.57	56.53 57.31	46.82	57.10	47.07	56.89	47.32
75	58.29	47.20	- A -	47-45	57 87	47.71	57.66	496
76	59.06	47.83	58.85	48.09	58.64	48.34	58.43	48.60
77	59 84	48.46	59.63	48.72	59 42	48.98	59.20	49.24
78 70	60.62 61.39	49.09	60.40	49.35	60.19 60.96	49.61	59.97 60.74	50.52
79 80	62.17	50 35	61.95	50.62	61.63	50.89	61.51	51.16
. 81	62.95	50.97	62.73	51.25	64.50	51.52	62.28	51.79
82	63.73	51.60	63.50	51.88	63.27	52.16	63.04	52.43
83	64.50	52.23	64.27	52.51	64.04 64.82°	52.79	64.58	53.07
84 85	65.28 66.06	52 86	65.82	53.15	65.59	53.43	05.35	54-35
86	66.83	54.12	66.60	54.41	66.36	54.70	66.12	54.99
87	67 61	54.75	67.37	55.05	67.13	55.44	66.89	55.63
88	68.39	55.38	68.15	55.68	67.90	55.97	67.66	56.27
89	69.17	56.64	68.92 69.70	56.32	68.67 69.45	56.61 57.25	68.43 69.20	56.9 t 57.55
90		57.27	70.47	57.58	70.22	57.88	64.96	58.19
91	70.72	57.90	71.24	58.21	70.99	58.52	70.73	58.83
93	72.27	.58.53		58.84	71.76	59.16	71.50	59.47
9 🛊	73.05	59.16	72.79	59.47 60 11	72.53	59.79 60 43	72.27 73 04	60.11
95	73.83	59.79	73.57	60.74	73 30	61.06	73.81	61.39
96 97	74.61	60.41	74.34	61.37	74.85	61.70	74.58	62.03
98	76.16	61.67	75.89	62.01	75.62	62.34	75.35	62.06
99	16.94	62.30	76.60	62.64	76.39	62 97	76.12	63.30
100	7771	61.93	77.44	63:27	77.16	64.24	77.65	64.58
101	78.49 79:27	63 56	78.21 78.99	63. 90 64.54	77.93	64.88		65.22
103	80.05	64 82	79.76	65.17	79.48	69.52	79.19	65.86
104	80.82	65.45	80.54	65.80	80.25	66.15	79.96 80.73	66.50
105	81.60	66.08	81.31	66 43	81.79	67.42	81.50	67.14
100	82.38 83.15	66 71	82.09 82.80	67.70	82.56	68.06	82.27	68.42
108	83.93	67 97	83.63	68.33	83.34	68.70	83.04	69.06
109	84.71	68 60	84.41	63.96	84.11	69.33	83.80	69.70
110	85.49	69.23	85.18	69.60	84 88	69.97	84.57	70.34
111	86.26 87.04	69.85	85.96 86.73	70.23 70.86	86.42	70.60 71.24	85.34 86.11	70.98
113	87.82	71.11	87.51	71.50	87.19	71.88	86.88	72.26
114	88.59	71.74	88.28	72.13	87.97	72.51		72 90
119	89.37	72.37	89.06	72.76	88.74	73.15	88.42	73.54
116	90.15	73.00	89.83	73.39	89 51 90.28	73.79	89.95	74-17
117	90 93	73.63	90.60	74.03	91.25	74.42		74.81 75.45
119	92 48	74.89	92.15	75 29	9182	75.69	91.49	76 09
120	93.26	75.52	92.93	71.92	92.59	76.33	92 26	76.73
, st	Dep.	Lat.	Dep.	Lat.	Dep.	Lat	Dep.	Lat.
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14	Lat.	Dep	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0.77	0.64	0.76	0.65	0.76	0.65	0.76	0.65
2	1.53	1.29	1.53	1.29	1.52	1.30	1.52	1.31
3 4	2.30 3.06	1.93 2.57	3.29 3.05	1 94 2.58	2,28	1.95	2.27	1.96
5	3.83	3.21	3.82	3.23	3.80	3.25	3.03 3.79	2.61 3.26
6	4.60	3.86	4.58	3.88	4.56	3.90	4-55	3.92
7	5.36	4.50	5.34	4.52	5.32	4-55	9.30	457
8	6.13 6.89	5.14	6.11	5-17	6.08	5.20	6.06	5.22
10	7.66	5.79 6.43	7.63	5.82 6.46	6.84 7.60	5.84 6.49	6.82 7.58	5-87 6-53
11	8.43	7.07	8.40	7.11	8.36	7.14	8.33	7.18
12	9.19	7.71	9.19	7.75	9.12	7.70	9.09	7.83
13	9.96	8.36	9.92	8.40	9.89	8.44	9.85	8.49
14	11.49	9.00 9.64	10.69 11.45	9.69	10.65	9.09	10.61	9-14
16	12.26	10.28	12.25	10.34	12.17	9-74	12.13	9.72
17	13.02	10.93	12-97	10.98	12.93	11.04	12.88	11.10
18	13.79	11.57	13.74	11.63	23.69	11.69	13.64	3 1.75
19	14.55	12.21	14.50	12.28	14.45	12.35	1439	12.40
21	16.09		15.26	12.92	15.21	12.99	15.15	13.06
22	16.85	13.50	16.03 16.79	13-57	15.97	13.64	15 92 16.67	13.71
23	17.62	1478	47.55	14.86	17.49	14.94	17.48	15.01
24	18.39	15.43	18.32	15.51	18.25	15.59	18.18	15.67
25	19.15	16.07	19.08	16.15	19.01	16.24	18.94	10.32
27	19.92 20.68	16.71	19.84 20.61	16.80	19.77	16.89	19.70	16.97
28	21.45	18.00	21.37	18.09	31.20	18.18	21.25	18.28
29	22.22	18.64	22.13	18.74	22.05	18.83	21.97	18.93.
30	22.98	19.28	22.90	19.38	22.81	19.48	22.73	19.58
31	23.75 24.51	19-93	23.66	20.03	23-97	20.13	23,48	20.24
33	25.28	20.57	24.43	21.32	24-33	20.78	24-24 35 00	20.89
34	26.05	21.85	25.95	21.97	25.85	22.08	25.76	22.19
35	26.81	22.50	26.71	22.61	26.61	22.73	26.51	22.85
36 37	27.58 28.34	23.14	27.48	23.26	27.37	23.38	27.27	23.50
38	29.11	24.43	28.24	24.55	28.12	24.03 24.68	28.03	24.15
39	29.88	25.07	29-77	25.20	29,66	25.33	29.54	25.46
40	30.64	25.71	30.53	25.84	30 42	25.98	30.30	26, 11
41	31.41	26.35	31 29	26-49	31.18	26.63	31.06	26.76
42 43	32.17	27.64	32.06	27.14	31.94	27.28	31.82	27.42 28.07
44	33.71	28.18	33.58	28.43	32.46	28.58	33-33	28.78
45	34-47	28.93	34-35	29.08	34.22	29.23	34.09	29-37
46	35.24	29.57	35.11	29.72	34-98	29.87	34.85	30.03
47 48	36.00	30.84	35.87 36.64	30.37	35.74 36.50	30.52	35.61 36.36	30.68
49	37.54	31.50	37.40	31.66	17 26	31.82	37.12	31-33 31-99
50	38.30	32.14	38.16	32.31	38.02	32.47	37.88	32.64
51	39.07	32.78	38.92	32.95	38.78	33.12	38.64	33.29
52	39.83 40.60	33-42	39.69	33.60	39.54	33.77	39-39	33.94
54	41 37	34-07 34-71	40.45 41.21	34.24 34.89	40.30	34.42	40.15	34.60
55	42.13	35.35	41.98	35.54	41.82	35.72	41.67	35.90
56	42.90	36.00	42.74	36.18	42.58	36-37	4245	36.55
57 58	43.66	36.64	43.50	36.83	43-34	37.02	43.18	37.21
59	44.43	37.28 37.92	44-27	37.48	44-10 44-86	37.67	43-94 44-70	37.86
60	45.96	38.57	45.79	38.77	45.62	38.97	45.45	38.51
보	Dep.	Lat.	Dep.	Lat.	Dep.	Lut.	Dep.	Lat.
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78.00	!	ď		15		30		45	
-	╝.	Lat.	Dep.	Lat.	Dep	Lat.	Dep.	Lat.	Dep.
6		46.73	39.21		39.41	46.38	39.62	46.21	39.82
6		47-49 48.26	39.85		40.06 40.71	47·15 47·91	40.27 40.92	46.97 47.73	40.47
6		49.03	41.14		41.35	48.67	41.56	48.48	41.78
6		49.79	41.78	49.61	42.00	49-43	42.21	49.24	42.43
6	6	50.56	42.42		42.64	50. 19	42.86	50.00	43.08
6		51.32	43.07	51.14	43.29	50.95	43.51	50.76	43-73
6	- 1	52.09 52.86	43.71	51.90 52.66	43.94 44.58	51.71 52.47	44.81	52.27	45.04
7	3	53.62	45.00	53-43	45.23	53.43	45.46	53.03	45.69
17		54-39	45.64	54-19	45.87	53-99	46.11	53.79	46.35
	2	55.16	46.28	54-95	46.52	54.75	46.76	54-54	47.00
	3	55.92 56 69	46.92	55.72 56.48	47.81	55.5 P 56.27	47.41	55.30	47.65
	5	57.45	48.21	57.24	48.46	57.03	48.71	56.82	48.96
-	6	58.22	48.85	10.82	49.11	57-79	49.36	57-57	49.61
	7	58.99	49-49	58.77	49-75	58.55	50.01	58.33	50.26
	*	59-75	50.14	59-53	50.40	59.31	50.66	59.09	50.92
		60.52	50.78	60.30	51.69	60.07	51.31	59.85	51.57
	=	62.05	52.07	61.82	52.34	61.59	52.01	61.36	52.87
	32	62.82	52.71	62.59	\$2.98	62.35	53.25	62.12	53.53
1 8	3	63.58	53.35	63.35	53.63	63.11	53.90	62.88	54-18
13	34	64.35	53.99	64.11	54.27	63.87	54-55	63.64	54.83
	85	65.11	54.64	65.64	54.92		55.85	65,15	55.48
	86 87	65.88 66.65	55.28	66.40	55.57	65.39	56.50	65.91	56.79
	88	67.41	56.57	67.16	56.86	66.92	57.15	66.67	57.44
-	89	68.18	57 21	67.93	57.50	67.68	57.80	67.42	58.10
	90	68.94	57.85	68.69	58.25	68.44	58.45	68.18	58.75
	gt	70.48	58.49	70.22	58.80	69.20	59.10	68.94	59.40
	92 93	71.24	59.78	70.98	60.09	70.72	60.40	70.45	60/71
	94	72.01	60.42	71.74	60.74	71.48	61.05	71.21	61.36
	95	72.77	61.06	72.51	61.38	72.24	61.70	71.97	62.01
	96	73-54	61:71	73.27	62.03	73.00	62.35	72.73	62.66
Ŧ	97 98	74-31	62.35	74-80	63.32	73.76	63.65	73.48	63.32
	99	75.84	63.64	75.56	63.97	75.28	64.30	75.00	64.62
	00	76.60	64.28	76 32	64.61	76.05	64.94		65.28
	101	77.37	64.92	77.09	65.26	76.80		76.51	65.93
	02	78.14		77.85	66.55	77.56	66.24	77.27	66 58
	103 104	79.67	66.85	79.38	67.20	79.08	67.54	78.79	67.89
- 1	105	80.43	67.49	80.14	67 84	79.84	68.19	79-54	68.54
Ţ	106	81.20		80.90	68.49	80.60		80.30	69.19
	107	81.97		81.67	69. 14	81.36	69.49	81.82	69.85
	109 109	82.50		82.43	70.43	82.88	70.14	82.57	70.50
	110	84.26	79.71	83.96	71.07	83.64	71.44	83.33	71.8c
1	111	85.03	71.36	84.72	71.72	84-41	72.09	84.09	72.46
•	112	85.80	71.99	85.48		85.17	72.74	84.85	73-11
	113 114	86.56		86.25	73.66	85.93	73-39	85.60	73-76
	115	88.10	73.92	87.77	74.30	87.45		87.12	7.5 07
- 4-	116	88.86	-			88.21	75.34	87.88	75.72
_ [1	117	89.63	75.21	89-30	75.60	88.97	25.99	88 64	76.37
	118	90.39		90.06		89-73		89.39	77.03
	119	91.93	1		,	90.49		90.15	77.68
J.		Dep.	Lat.		Lat.	Dep.	Lat.	Dep.	Lat
1	Dist.	1	04		157		27	-	5'
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Dist.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
	0.75	0.66	0.75	0.66	0.75	0.66	0.75	3.67
2	1.51	1.31	1.50	1.32	1.50	1.33	1.49	1.33 2.00
3	2.26 3.02	1.97 2.62	2.26 3.01	1.98 2.64	2.25 3.00	1.99 2.65	2.24 2.98	2.66
4 5	3.77	3.28	3.76	3 30	3.74	3.31	3 73	3.33
6	4.53	3.94	4.51	3.96	4.49	3.98	4.48	4.00
7	5.28	4-59	5.26	4.62	5.24	4.64	5.22	4.66 5.33
	6.04 6.79	5.25 5.90	6.77	5.27 5.93	5.99 6.74	5.30 5.96	5.97 6.71	5.99
9	7.55	6.56	7.52	6.59	7.49	6.63	7.46	6.66
	8.30	7.22	8.27	7.25	8 24	7 29	8.21	7.32
12	9.06	7.87 8.53	9.02	7.91 8.57	8.99 9.74	7.95 8.61	8. 9 5 9.70	7.99 8 66
13	9.81 10.57	9.18	9.77	9.23	10.49	9.28	10.44	9.32
14	11.32	9.84	11.28	9.89	11.23	9.94	11.19	9.99
16	12.08	10,50	12.03	10.55	11.98	10.60	11.94	10.65
17	12.83	11.15	12.78	11.21	12.73	11.26	12.68	11.32
18	13.58	12.47	14.28	12.53	14.23	12.59	14.18	12.65
19 20	15.09	13.12	15.04	13.19	14 98	13.25	14.92	17.32
21	15.85	13.78	15.79	13.85	5.73	13.91	15.67	13.98
22	16.60 17.36	14.43	16.54	14.51	26.48 17.23	14.58	17.16	15.32
23	18.11	15.75	18.04	15.82	17.97	15.90	17.91	15.98
24 25	1887	16.40	18 80	16.48	18.72	16.57	18.65	16.65
26	19.62	17.06	19.55	17.14	19.47	17.23 17.89	19.40	17.31
27	20.38	17.71	20.30 21.05	17.80 18.46	20.22	18.55	20.89	18.64
28	21.13	19.03	21.80	19.12	21.72	19.22	21.64	19.31
29 30	22.64	19.68	22.56	19.78	22.47	19.88	22.38	19.98
31	23 40	20.34	33.31	20.44	23.22	20.54	23.13 23.87	20.64 21.31
32	24 15	20.99	24.06	21.10	23.97 24.72	21.20	24.62	21.97
33	24.91 25.66	22.31	25.56	22 42	25.46	22.53	25.37	22.64
34 35	26.41	22 96	26.31	23.08	26.21	23.19	26.11	23.31
36	27.17	23.62	27.07	23.74	26.96	23.85		23.97 24.64
37	27.92 28.68	24 ² 7 24.93	27.82 28.57	24 40 25.06	27.71 28 46	24.52	28.35	25.30
38 39	29.43	25.59	29.32	25.71	29.21	25.84	29.10	25.97
40	30.19	26.24	- 30.07	26.37	29.96	26.50	29.84	26.64
41	30.94	26.90	30.83	27.03	30.71	27 17 27.83	30.59 31.33	27 30 27.97
42	31.70 3 2. 45	27.55 28.21	31.58	27 69 28.35	32.21	28.49	32.08	28.63
43 44	33.21	28.87	33.08	29.01	32.95	29.16	32.83	29.30
45	33.96	29.52	33.83	29.67	33.70	29.82	33.57	29.97
46	34-72	30 18	34.58	30.33	34.45 35.20	30.48 31.14	34.32 35.06	30.63
47	35.47 36.23	30.83 31.49	35.34 36.09	30.99	35.95	31.81-	35.81	31.96
48 49	36.98	32.15	36.84	32.31	36.70	32.47		32.63
50	37.74	32.80	37.59	32.97	37 45	33 13	37.30	33 29
51		33.46	38 34 39.10	33.63 34.29	38.20 38.95	33:79 34.46	38.79	34.63
52	39.24 40.00	34.12 34.77	39.85	34.95	.39.69	35.12	39.54	35.29
53 54	40.75	35-43	40.60	\$5.60	40.44	35.78	40.29	35.96 36.62
55	41.51	36 08	41.35	36.26	41.19	36.44	41.03	37.29
56	42.26	36.74	42.10	36.92 37.58	41.94 42.69	37.41 37.77	41.78	37.29 37 96
57	43.02 43.77	37.40 38.05	42.85	38.24	43.44	38.43	43.27	38.62
58 59	44.53	38.71	44.36	38.90	44.19	39.09	44.02	39.29
60	45.28	39.36	45.11	39 56	44.99	39.76	44.76	39.95 Lat-
Dist.	De p.	Lat.	Dep	Lat.	Dep.	Lat .	Dep.	5/
しぎし	U'	,	4:	j'	30) (1. 1.	

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Dist	0		15		3	0'	4	5'
	Lat	Deo.	Lat.	Dep	1.81	Dep.	Lat	Det
61	46.04	40.02	45 86	40.22	45.19	40.42	45.51	40.62
62 63	46 79 47·55	40.68	46.61 47.37	40.88		41.08	46.26	41.28
64	48.30	41.99	48.12	41.54	47.18 47.93	41.75	47.00 47.75	41.95
6;	49.06	42.64	48.87	42.86	48.68	43.07	48.49	43.28
66	49.81	43.30	49.62	43 52	49.43	43.73	49.24	43.95
67 68	50.57	43.96	50 37	44.18	50.18	44.40	49.99	44.6 r
69	51.32 52.07	44.6 t 45.27	51.12	44.84	50.9 3 51.68	45.72	50.73	45.28
70	52.83	45.92	52.63	46.15	52.43	46.38	51.48 52.22	45.95 46.61
71	53.58	46.58	53.38	46.81	53 18	47.05	52.97	47.28
72	54-34	47 24	54.13	47 47	53.92	47.71	53.72	47.94
73	55.09 55.85	47.89	54.88	48 13	54.67	48.37	.54.46	48.61
7.4 7.5	56.60	48.55	55.64 56.39	48.79 49.45	55.42 55 17	49.03 49.70	55.21 55.95	49.28 49.94
76	57.36	49.86	57.14	50.11	56.92	50.36	56.70	50.61
77	58.11	50.52	57.89	50.77	57.67	51.02	57.45	51.27
78	58.87	\$1.17	58.64	51 43	58.42	51.68	58.19	54.94
7.9 80	59.62.	51.83	59.40	52.09	59-17	52.35	58.94	52.60
81	61.13	12 48	60.15	52.75	59.92	53.01	59.68	53.27
82	61.13	53.14.	60.90 61.65	53.41 54.07	60.67	53.67 54.33	60.43 61.18	53.94 54.60
83	62.64	\$4.45	62.40	54.73	62 16	55.00	61.92	55.27
84	63.40	55.11	63.15	55.38	62.91	55.66	62.67	55.93
85	64.15	55.76	63.91	56.04	63.66	56.32	63.41	56.60
86	64.90 65.66	56.42	64.66	56.70	64.41	56.99	64.16	57.27
88	66.41	57.73	66.16	57.36	65.16	57.65	64.91 65.65	57.93 58.60
89	67.17	58.39	66.91	58.68	66.66	58.97	66.40	59.26
90	67.92	59.05	67.67	59.34	67.41	59 64	67.15	59.93
91	68.68	59.70	68.42	60.00	68.15	60.30	67.89	60.60
93	69.43 70.19	60.36	69.17	60.66	68 90	60 96	68 64	61.29
94	70.94	61.67	69.92 70.67	61.32	69.65 70.40	61.62	69.38 70.13	61.93
95	71.70	02.33	71.42	62.64	71.15	62.95	70.88	63.26
96	72.45	62.98	72.18	63.30	71.90	63 61	71.62	63.92
97	73.21	63.64	72.93	63.96	72.65	64 27	72.37	64.59
98	73.96 74.72	64.29 64.95	73.68	64.62	73.40	64.94	73.11 73.86	65.26
100	75 47	65.61	74.43	65.93	74.15	65.60 66.26	74.61	65 92
101	76.23	66.26	75.94	66.59	75.64	66.92	75.35	67.25
102	76.98	66.92	76.69	57.25	76.39	67.59	76.10	67.92
103	77.74	67.57	77.44	67.91	77-14	68.25	76.84	68.59
104	78.49 79.24	68.23 68.89	78.19 78.94	68.57	77.89 78. 6.4	68.91 69.58	77.59 78.34	69.25
106	80.00	69.54	79 70	69.89		70.24	79.03	69.92
107	80.75	70.20	85.45	70.55	79.39 80.14	70.24	79.83	70.58
103	81.51	70.85	81.20	71.21	85.89	71.56	80.57	71.92
109	82.26	71.51	81.95	71.87	81.64	72.23	81.32	72.58
110	83.02	72.17	82.70	72 53	82.38	72.89	83.07	73 25
111	83.77	72.82 73.48	83.45	73 19 73.85	83.13 83.88	73.55	82.81	73.91
113	85.28	74.13	84.96	74.51	84.63	74.88	83.56 84.30	74.58
114	86.04	74-79	85.71	75.17	85.38	75.54	85.05	75.91
1112	86.79	75.45	86.46	75.82	86 13	76.20	85.80	76.59
116	87.55	76.10	87.21	76.48	86.88	76.86	\$6.54	77.24
117	88.30 89.06	76.76 77.42	87.97 88.7 2	77.14 77.80	87.63 88.38	77.53	87 .29 88.03	77.91
119	8981	78.07	89.47	78.46	89.13	78.85	88.78	78.57
120	90.57	78.73	90.22	79.12	89.87	79.51	89.53	79.91
ید	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat
Dıst.	0	<i>'</i> .	45	51	30	,,	1.	5'
				Draw				

18	1 6	0'		15/		30/	, 46,	
) g	Lat.	Dep.	Lat.	Dep.		Dep.		Dep.
-	0.74	0.67	0.74	0.67	0.74	متنت سمارا –	0.73	0.68
1 2		1.34	1.48	1.34	1.47	1.35	1.47	1.36
3 4	2.97	2.68	2.96	2.60	2.21		2.20	2.04
5	3.72	3.35	3.70	3.36	3.69		3.67	3.39
6	4.46	4.01	4.44	4.03	4-42		4-41	4.07
7 8	5.20	5.35	5.18	5.38	5.16		5.14	4-75 5-43
9	6.69	6.02	6.66	6.05	6.64		6.4	6.11
10	7 43	6.69	7.40	6.72	7.37	-	7.34	6.79
1 !!	8.17 8.92	7.36	8.14 8.88	8.07	8.11	7-43	80.8	7-47
1 13	9.66	8.70	9.61	8.74	0.58	8.78	9-55	8.82
14	10.40	9 37	10.36	9.41	10.32	9.46	10.28	9.50
15	11.15	10.04	11.10	10.09	11.06	10.13	11.01	10.18
16	11.89	10.71	11.84	10.76	11.80	10.81	11.75	11.54
18	13.38	12.04	13.32	12.10	13.27	12.16	13.23	12.22
19	14.13	12.71	14.06	12.77	14-01	12.84	13.95	12.90
20	14.86	13.38	14.80	13:45	14.75	13.51	14.69	13.58
22	15.6t	14.05	15.54	14.79	15.48	14.19	15.42	14.25
23	17.09	15.39	17.02	15.46	16.96	15.54	16.89	15.61
25	17.84	16.73	17.77	16.14	17.69	16.21	17.62	16.29
26	19.32	17.40	19.25	17.48	19.17	17.57	19.09	17.65
27	20.06	18.07	19.99	18.15	19.91	18.24	19.83	18.33
28	20.81	18.74	20.73	18.83	20.64	28.92	20.56	19.01
39 30	21 55	19.40 20.07	21.47	19.50	22.12	19.59 20.27	21.30	19.69 30.36
31	23.04	20.74	82.95	20.84	22.86	20.94	22.76	21.04
32	23.78	21.41	23.69	21.52	23.59	21.62	23.50	21.72
33 34	24.52 25.27	22.08 22.75	24 43 25.17	22.19 22.86	24.33	22.29 22.97	24-23 24-97	23.08
35	26.01	23.42	25.91	23.53	25.80	23.65	25.70	23.76
36	26.75	24.09	26.65	24.21	26.54	24.32	26.44	24.44
37	27.50	24.76	27.39	24.88	27.28	25.00	87.17	25.12
38 39	28.24 28 98	25.43 26.10	28.13 28.87	25.55 26.22	28.04 28.75	25.67 26 35	27.90 28.64	25.79 26.47
40	29.73	26.77	29.61	26.89	29.40	27.02	29.37	27.15
41	30.47	27.43	30.35	27.57	30.23	27.70	30.11	27.83
42	31.21 34.96	28.10 28.77	31.83	28.24 28.91	30.97	28.37	30.84 31.58	28.51 29.19
43 44	32.70	29.44	32.57	29.58	31.70 32.44	29.05 29.73	32-31	29.87
45	33-44	30.11	33.31	30.26	33.18	30.40	33.04	30.55
46	34.18	30.78	34.05	30.93	33.91	31.08		31.22
47 48	34.93 35.67	31.45	34·79 35·53	31.60	34.65 35.39	31.75		31.90
49	36.41	32.79	36.27	32.95	36.13	33.10	35.98	33.26
50	37.16	33.46	37.01	33.62	36.80	33.78		33.94
51		34.13		34.29 34.96		34.46		34-62
52 53		34-79 35.46		34.90 35.64		35.13 35.81	38.92	35.98
54	40.13	16.13	39.97	36.31	39.81	36.48	39.65	36.66
55		36.80		36.98		37.16	I	37.33
56 57		37·47 38.14		37.65 38.32		37.83 38.51		38.01 38.69
38		38.81	42.93	39.00		39.18	42.59	9-37
59	43.85	39.48	43.67	39.67	43.50	39.86	43.32	loos
60		40.15		40.34		40.54		10.73
Die Die Die Die Die Die Die Die Die Die	Dep.	Lat.	Dep.	Lat.	Dep. 30'	Lat.	Dep.	Lat.
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שו	0	<u></u>	1	5/	3	9/	1 4	57
Di si	<u>lut</u>	Dep.	Lat	Dep.	Lat.	Dep	Lat.	Dep.
61	:45-33	40.82	45.15	41.01 .	44.97	41.21	44.79	41.41
62	46.07	41.49	45.89	41.69	45.71	41.89	45.53	42 09
63	46.82 47.56	42,16	45.63 47.37	42.36	46.45	42.56	45.26 47.00	42.76 43.44
6,	48.30	43.49	- 48.1 T	43.03 43.70	47.92	43.24 43.91	.47.73	44.12
66	49 05	44.16	48.85	44.38	48.66	44.59	48.47	44.80
67	49.79	44.83	49.59	45.05	49.40	45.26	49.20	45.48
68	50.53	45.50	50.33	45.72	50.13	45.94	49.93	46.16
69	51.28 52.02	46.17	51.07	46.39 47. 07	50.87	46.62 47.20	50.67 51.40	46.84 47.52
70	52.76	47.51	52.50	47.74	52.35		52.14	43.19
71 72	53.51	48.18	53.30	48.41	53.08	47:97 48.64	52.87	48 87
73	54.25	48.85	54.04	49.08	53.82	49 32	:53.61	49.55
74	54 99.	49.52	54-78	49.76	54-56	49.99	54-34	50.23
7.5	55.74	50.18	55.52	50.43	55.30	50.67	55.07	50.91
76	56.48 57.22	50.85	56.26 57.00	51.10	56.03 56.77	51.34 52.02	55.81 59.54.	\$1.59 \$2.27
7.7	57.97	52.19	57.74	52.44	57-51	52.70	57.28	52.95
79	58.71	52.86	58.48	53.12	58.24	53 37	58.01	53.63
80	59-45	53 53	59.22	53.79	58.98	54.05	58.75	54.30
81	60.19	54.20	59.96	54.46	59.72	54-72	99.48	54.98
82	60.94	54.87	60.70	55.81	61.10	55.40	60.21	55 66 56.34
84	62.42	56.21	62.18	56.48	61.93	56.07 56.75	61.68	57.02
85	63.17	56 88	62.92	57.15	.62.67	57:43	62.42	57.70
86	63.91	57-55	63 66	57.82	63.41	58 10	63.15	58.38
87	64.65	58.24	64.40	58.50	64.14	58.78	63.89	59.06
88	65.40	59.55	65 14 65.88	59.17	64.88	59-45	64.62	59.73 60.41
95	66.88	60.22	66.62	59.54 60.51	66.35	60.13 60.80	66.09	61.00
91	67.63	60.89	67.36	61.19	67.09	61.48	66.82	61.77
93	68.37	61.56	68.10	61.86	67.83	62.15	. 67.56	62.45
93	69.11 69.86	62.23	68 84	62.53	68.57	62.83	68.29	63.13
94	70 60	62.90 63.57	69.58 70.32	63 20 63.87		63.51	69.03 69.76	63.81 · 64.49
96	71.34	64.24	71.06	64.55	70.78	64.86	70-49	65.16
97	72.08	64.91	71.80	65.22	71.52	65.53	71:23	65.84
98	72.83	65.57	72.54	65.89	72.25	66.21	7196	66.52
99	73.57	66.24	73.28	66 56	72.99	66.88	72.70	67.20
100	74.31	66.91	74.02	67.14	73:73	67,56	73.43	67.88
101	75.06 75.80	67.58	74.76 75.50	67.91 68.58	74.46	68.23 68.91	74.17	68 56
103	76.54	6×.92	76.24	69.25	75-94	69.59	75 64	69 92
104	77.29	69.59	76.98	69.93	76.68	70.26	76.37	70.60
105	78.03	70.26	77.72	70.60	77.41	70.94	77.10	71.27
106	78.77	70.93	78.46 79.20	71.27	78.15	71.61	7.7.84	71.95
107	79.51 80.26	71.60	79.20	71.94	78.89 79.63	72.29	78.57 79.31	72.63
109	82.00	72.94	80.68	73.29	80.36	73.64	80.04	73.99
110	81.75	73 60	81.42	73.98	81.10	74 31	80 78	74-67
111	82,49	74-27	82.46	74-63	81.84	74-99	81.51	75.35
112	83.23	74-94	82.90 83.64	75.31	82.57	75.67	82.24	76.03
113	83.98 84.72	75.61	84.38	75.98 76.65	83.31 84.05	76.34	82.98	76.70
115	85:46	76.95	85 12	77 32	84.79	77.69	84.45	78.06
116	86.20	77.62	85.87	77.99	85.52	78.37	85.18	78.74
117	86.95	78.29	19.98	78.67	86.96	79.04	85.92	79.42
118	87.69 88.43	78.96 79.63	87 35 88 09	79.34	87.00	79.72	86.65	80.10
120	89.18	80 30		80.68	87.74	80.40	87.38	80.78
	Hep	Late	1)p_	Lat.	υ ε ρ.	Lat	Dep.	Lat
Dist,		V					1/cp.	·
			45, 30/ 47 DEGREES.				17	

1	0		15	•	36		,	-
1	Lat.	Dep.	Lat	Dep.	Let.	Dep.	Lat.	Dep.
1	Q.73°	0.68	0.73	0.69	6.73	0.69	0.72	0.69
3	3.46 2.19	1.36	1.46	1.37 2.06	2.18	1.38	2.17	1.38
4	4.93	2.73	2.91	2.74	1.90	2.75	2.89	2.77
5	3.66	3.41	3.64	3·43 4:1+	4-35	3:44 4:23	4-33	3.46 4.15
	439 5.12	4.09 4.77	4-37	4.80	5.08	4.82	5.06	4.84
7	5.85	5.46 6.1#	5.83	5.48 6.17	5. 8 0	6.50 5.51	6.50	5.53 6.22
9	6.58 7 31	6.82	7.28	6.85	7.25	6.88	7.22	6.92
ī	8.04	7.5%	8,01	7.54 8 22	7.98	7-57 8.26	7.95	7.61
13	8.78 9.51	8.18 8.87	8.74 9.47	8.91	8.70 9-43	8.95	8.67 9-39	8.30 8.99
14	10.24	9.55	10.20	9.59	10.16	9.64	10.11	9.68
15	10.97	10.23	10.93	10.28	10.88	10.33	10.84	10.37
17	12.43	11.59	12.38	11.65.	12.33	11.70	12.28	11.76
18	13.16	12.28	13.11	12.33	13.78	12.39 13.08	13.00	13.14
10	r4.63	13.64	14.57	13.70	14.51	13.77	14-45	13.83.
21	P5.36	14:32	15.30	14.39	15.23	14.46	15.17	14.52
12 13	16.82	15.00	16.03	15.75	15.96	15.14	15.89	15.21 15.90
24	17.55	16.37	17.48	16.44	17-41	16 52	17.34	16.60
25	18.28	17.05	18-21	17.13	18.86	17.90	18.06	17.29
17	19.75	18.41	19.67	18.50	19.59	18.59	19.50	18.67
28 29	20.48	19.10	20.39	19.19	20.31	19.27 19.96	20.23	19.36 20.05
30	21.94	20.46	21.85	20.56	21.76	20.65	21.67	20.75
7	22 67	31.14	22.58	31.24	22.49	21.34	22.39	21.44 22.13
32 13	23 40 24.13	21.82 22.51	23.31	21.93 22.61	23.21 23.94	12.03 12.72	23.12 . 23.84	12.82
14	24 87	23.19	24.76	23.30	24.66	23.40	24.56	23.51 24.20
16.	25.60	24.55	25.49	23.98	25.39	24.09 24.78	26.01	24.89
17	27.06	25.23	26:95	25.35	26.84	25.47	26.73	45.99
19	27.79	25.92 26.60	27:68 28.41	26.04 26.72	27.56 28.29	26.26 26.85	27.45 28.17	26.28 26.97
ρ	29.25	27.28	29.13	27.41	29.01	27-53	28.89	27.66
11	29.99	27.96	29.86	28.09 28.78	29.74	28.22 28.91	29.62 30.34	28.35
2 3	30.72 31.45	28.64 29.33	30.59	29.46	30 47. 31.19	29.60	31.06	29.04 29.74
14	32:18	30.01 30.69	32.05 32.78	30.83	31 92 32.64	30.29 30.98	34.78 32.51	30-43 31-12
10	32.91 33.64	34.37	33.51	31.52	33.37	31.66	33.93	31.81
17	374-37	32.05	34.23	32.20	34.09	32.35	33.95	32.50
8 9	35.10 35.84	32.74 33.42	34.96 35.69	32.89	34.82 35.54	33.04 33.73	34·67 35·40	35.19 33.88
;0	36.57	34.10	36.42	34,26	36.27	34.43	36.12	34.58
;I	37.30. 38.03.	34.78 35.46	37.15 37:88	34-94 35.63	36.99. 37.72	35.11 35.79	36.84 37\96	35.27 35.96
;2 ;3	38.76	36.15	38.60	36.31	38.44	36.48		36.65
i4	39 49 40.22	36.83	39-33 40.06	37.00 37.69	39.17 39.90	37.17 37.86	39.01 39.73	37·34 38 03
<u>5</u>	40.96	37.51	40.79	38.37	40.62	38.55	40.45	38.72
17	41.69	38.87	41.58	39.06	41.35	39.24	41.57	39.42
8	42.42 43.15	39.56 40.24	42.25	39·74 40.43	42.80	39 92 40.61	41.90 42.62	40.1T 40.80
19	43.88	40.92	43.70	41.11	43.52	41 30	43.34	41 49
180	Dep.	Lat.	Dep.	Let.	Dep.	Lat.	Dep.	Lat.
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Di Di	Lat	Dep	Lat	Dep.	Lat.	Dep.	Lat.	Dep.		
61	44.61	41.60	44-43	41.80	44-25	41.99	44.06	42.18		
63 63	45-34 46.08	42.28	45.16	42.48	44-97 45.70	42.68	44-79 45-51	42.87 43.57		
64	46.81	43.65	46.62	43.85	46.42	44.05	46.23	44.26		
65	47-54	44-33	47-34	44-54	47.15	44.74	46.95	44.95		
66	48.27	45.01	48.07	45.22	47.87	45.43	47.68	45.64		
67 68	49.00	45.69 46.38	48.80 49-53	45.91 46.59;	48.60 49.33	46.12 46.81	48.40 49.12	46.33 47.02		
69	50.46	47.06	50.26	47.28	50.05	47.50	49.84	47.71		
70	\$1.19	47.74	50.99	47.96	50.7B	48.18	50.57	48.41		
71	\$1.93	48,42	51.71	48.65	\$1.50	48.87	51.29	49.10		
72 73	52.6 6 53-39	49.10 49.79	52.44 53.17	49-33 50.02	,52.23 ,52.95	49.56 50.25	52.01 - 52.73	49.79 50.48		
74	54.13	\$0.47	\$3.90	50.70	\$3.68	50.94	53-45	51.17		
75	54.85	51.15	54.63	51.39	54 40	51.63	54.18	51.86		
76 77	55.5 8 56.31	51.83 52.51	56.08	52.76	55.85	52.31 53.00	54.90 55.62	52.55		
78	\$7.05	53.20	56.81	53.44	\$6.58	63.69	56.34	53.94		
79	57.78	53.88	57-54	44.13	. 67.20	54.38	57.07	54.63		
80	58.51	54-56	58.27	54.84	18.03	55.07	57.79	55.32		
81	59 4 4 59-97	55.24 55.92	59.00 59.73	55 50 56.18	58.76 59.48	55.76 56.45	58.51 59.23	56.01		
83	60.70	56.61	60.45	\$6.87	60.21	57.13	59.96	\$7.40		
84	61-43	57-29	81.16	57.56	60.93	57.82	60.68	58.09		
85	62.17	57·97	62.64	58.24	61.66	58.51	61.40	\$8.78		
86	62.90	58.65 59.33	63.37	58.93 59.61	62.38	59.20 59.89	62.85	69.47		
88	64.36	60.02	64 10	60.30	63.83	60.58	63.57	60.85		
89	65.09	60.70 61.38	64.81	60.98 61.67	64.56	61.26	64.29	61.54		
90	66.55	62.06	65.55	62.35	66.01	61.95 62.64	65.74	62 93		
91	67.28	62.74	67.01	63.04	66.73	63 33	66 46	63.62		
93	68.01	63.43	67 74	63.72	67.46	64 02	67.18	64.31		
94	69.48	64.11 64.79	68.47 69.23	64.41	68. 19	64.71 65. 59	67.90 68.62	65.00 65.69		
95	70.21	65.47	69.92	65.78	69.64	66.08	69.35	66.39		
97	70.94	66.15	70.65	66.46	70.36	66.77	70.07	67.08		
98	71 67	66.84	71.38	67.15	71.09	67.46	70.79	67.77		
100	72 40	67.52 68.20	72.11	67.83 68.52	71.81 72.54	68.15 68 84	71.51 79.84	68.46 69 15		
101	73.87	68.88	73.57	69.20	72.26	69.52	7296	69.84		
102	74-60	69.56	74.29	69.89	73.99	70.21	73.68	70.53		
103	75.33	70.25	75.02	70.57	74.71	70 9 0 71.59	74.40	71.23		
104	76.06	70.93	75.75	71.94	76.16	72 28	75.13	72.61		
106	77.53	72.29	77.21	72.63	76.89	72.97	76.57	73.3C		
107	78.24	72.97	77-94	73.31	77.61	73.65	77.29	73 .9 9 74.68		
108	78.99	73.66 74.34	78.66	74.68	78.34	74-34	78.02	74.08		
110	80.45	75.02	80.12	75:37	79.70	75.72	79.46	76.01		
şie.	81.18	75.70	80.85	76.06	80.52	76 41	80.18	76.70		
112	81.91	76 38	\$1.58 \$2.51	76.74	81.24	77.10	80.90	77.4		
113	82.64 83 37	77.75	83.03	77.43	82.69	18.47	81.03	78.8		
115	84.11	78.43	83.76	78.80	8542	79.16	83.07	79 5		
116	84.84	79 11	84.49	79.48	84.14	79.85	83.79	80.2		
118	86.30	79.79	85.22	80.17	84.87	80.54	84.52	80.9		
119	\$7.03	81.16	86.68	81.54	86.32	81.91	85.96	82.2		
120	87.76	81.84	87.40	82.22	87 04	82.60	86 68	82.9		
1 1	Dep.	Lat	Dep.	Lut	Dep	Lat.	Dep.	<u> </u>		
I a	à 0' 45' 30'									
	FO DEGREES.									

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3				5/.	30	<i>μ</i>	4-	, 	lat-
Dist.	Lat.	Dep	Lat	Dep.	Lat.	Dep.	Lat	Dep	Dep.
-	0.72	0.69	-0.72	0.70	0.71	0.70	0.71	0.70	0.71
2	1.44	1.39	1.43	1.40	1:43	1.40	1.42	1.41	1.41
3	2.16	2.08	2.15	2.09	2:14	2.10	2.13	2.11	2.12 2.83
4	2.88 3.60	2.78 3.47	2.87 3.58	2.79 3.49	2 8 ₅ 3 57	2.80 3.50	3.55	3.52	3-54
5	4.32	4.17	4.30	4.19	4.28	4.21	4.26	4-22	4-34
	5.04	4.86	5.01	4.88	4.99	491	4-97	4.93	4-95
7	5.75	5.56	5.73	5.58	5.71	5.61	5.68	5.63	5.66
9	6.47	6.25	7.16	6.28	6.42 7.13	6.31 7.01	6.39 7.10	7.04	6.36 7.07
11	7.19	7.64	7.88	7.68	7.85	7.71	7.81	7.74	7.78
12	8.63	8.34	8.60	8.37	8.56	8.41	8.52	8.45	8.49
13	9.35	9.03	931	9.07	9.27	9.11	9.23	9.15	9.19
14	10.07	9.73	10.74	9.77 10.47	9.99	9.81 10.51	9.94	10.56	9.90
16	11.51	11.11	11.46	11.16	11.41	11.21	11.36	11.26	11.31
17	12.23	1181	12.18	11.86	12.13	11.92.	12.07	11.97	12.02
18	13.95	12.50	12.89	12.56	12.84	12.62	12.78	12.67	12.73
10	19.67	13.20 13.89	13.61	13.26 13.96	13.55	13.32	13.49	13.38	13-44 14-14
20	15.11	14-59	19.04	1465	14.98	14.72	14 91	1478	14-85
22	15.83	15.28	15.76	15.35	15.69	15 42	15.61	75.49	15.56
23	16.54	15:98	16.47	16.05	16.40	16.12	16.33	16.19	16.26
24	17.26	16.67	17.19	16.75 17.44	17.13	16.82 17.52	17.04	16.90 17.60 °	16.97
25	17.98	17.37	17.91	18.14	18.54	18 22	18.46	18.30	18.38
27	19.42	18 76	19 34	18.84	19.26	18.02	19.17	19.01	19.09
28	20.14	19.45	20.06	19.54	19.97	19.63	19.89	19.71	19.80
29	20 86	20.15	29.77	20.24	20.68	20 33,	20.60	31.12	20.51
30	21.58	20.84	21 49	20.93	21 40	21.03	21.31	21.82	21.92
3 i 32	22.30 23.02	21.53	22.21	21.63	22.11	21.73	22.73	12.53	22.63
33,	23.74	23.92	23.64	23.03	23.54	23.13	23.44	23.23	23.33
34	14.46	23.62	24.35	23.72	24.25	23,83	24.15	23.94	124.75
35,	25.18	24.31	25.07	24.42	24196	<u>24.53</u>	24.86	24.64	25-46
36: 37.	-25.90 26.62	25.01 25.70	25.79 26.50	25.12	25 68 26.39	25.23	25.57	25.34	26.16
383	27 33	26 40	27.22	26.52	27.10	26.63	26.99	26.75	26.87
39.	28.05	27.09	27.94	27, 21	27.82	27.34	27.70	27.46	27.38 28.28
40	28.77	27 79	28 65	27.91	28.53	28.04	28.41	28.16	28.99
41	29:49 30 21	28.48 29.18	29.37 30.08	28.61 29 31	29.24 29.96	28.74 29.44	29.12	28.86 29.57	29.70
434	130.93	29.87	30.80	30.01	30.67	30.14	30,54.	30.27	30.41
44	31.65	30.56	31:52	30.70	31.38	30.84	31.25	30.98	31.T1 31.B2
45	32.37	31:26	32.23	31.40	32.10	31.54	31.96	3:.68	
46 47	33.09- 33.81	31,95 32.65	32 95 33.67	32.10: 32.80	32.81	32.24 32.94	32.67	32.38 33.09	32 53 33 23
48	34.53	33.34	34.38	33.49	34.24	33.64	34.00	33.79	33.94
49	35.25	34.04	35.10	34.19	34 95	34-34	34 80	34.50	34 65
50	35.97	34 73	35 82	34.89	35 66	35.05	35.51	35.20	35.36
51	36.69	35.43	36.53	35.59	36.38	35.73	36.22	35 90 36.61	36.06 36.77
52 53	37.41	36.12 36.82	37.25 37.96	36.29 36.98	37.00	36.45	36.93 37.64	37.31	37-48
54	38 84	37.51	38.68	37.68	38.52	37.85	38.35	38:02	38.48
55	39:56	38.21	39.40	38.38	39.23	38.55	39.06	18.72	38.89
56	40.28	38.90	40.11	39.08	39.94	39.25	39.77	39-42	39.60 40.31
57 58	41.00	39.60 40. 29	40.83	4 9.77	40.66	39.95 40.65	40.48	40.13	41.01
59	42.44	40 98	42.26	41.17	42.08	41-35	41.90	41.54	41.72
50	43.16	41.68	42.98	41.87	42 80	42 05	42.61	42.24	42.43
Dist.	Dep.	Lat.	Dep	Lat.	Dep.	Lat	Dep.	Lat	DL
<u>ā</u>	0	/	45	<i>′</i>	30/	-	1	5 <i>1</i>	0 M.

					GREES.				17.
모	0	/	15	<i>y</i>	30	· 1	4	5'	0'
Dist	Lat.	Dep.	Lat.	Dep.	Tat	Dep.	Lat_	Dep.	L. D.
61	43:88	42.37	43.69	42.57	43.51	42.76	43.32	42.94	43.13
62	44.60	43.07	44.41	43.26	44.22	43.46	44.03	43.65	43.84
63	45.32	43.76	45.13	43.96	44 93	44.16	·44-74*	44-35	44.55
64	46.04	44.46	45.84	44.66	45 65	44.86	45.45	45.06	c45.25
65.	46.76	45.15	46.56	45.36	.46.36	45.56	46.161	45.75	45.96
66	47.48	45.85	47.28	46.05	47.07	46.26	46.87	46.47	46.67
67	48.20	45.54	47.99	46.75	47.79	46.96	47.48	47-17	47.38
68	48.92	47.24.	48.71	47.45	48.50	47.66	48.19 49.00	47.87 48.58	48.08 48.79
69. 70	49.63 50.35	47.93	49.42 50.14	48.85	49.21	48.36 49. 0 6	49.71	49.28	49.50
1	ببنبنت		50.86						50.20
71 72	.54 07 .5479 -	49.32 50.02	51.67	49·54 50·24	51.35	49.76	50.42 54.13	49.99 50.69	10 02
73	52.51	50.71	52.29	50.94	52.07	51.17	51.84	51.39	51.62
74.	53.23	51.40	53.01	51 64	52.78	51.87	52.55	52.10	54-33
75.	53.95	52.10	53.72	52.33	53.49	52.57	53.26	52.80	53.03
76	54.67	52.79	-54-44	53.03	54-34	53-87	52-97	53.51	53.74
77	55.39	53.49	59.16	53.73	54.92	53.97	54.68	54.21.	54-45
78.	56.14	54.18	55.87	54-43	55.63	54.67	56.39	54.91	55.15
79	56,83	54.88	.56.59	55-13-	56 35	55.37	56.10	55.62	53.86
80	57,55	55.97	57.30	55.82	\$7.06	56.07	56.81	56.32	59.57
81	58.27	56.27	58.02	56.52	57 77	56.77	57.52	57-03	57.28
82 83	58.99 59.71	56.96 ·	58.74	57.22	58.49	57.47	58.24	57.73	57.98 58.69
84	60,48	58.35	59.45 50.17	57.92	59.20	58.88	58.95°.	5843. 59.14.	.59.40
85	61.14	50.05	60.89	58,61 59.31	59.91. 60.63	59.58	60,37	59,84	60.10
86	62.86	59.74	61.60	60 01	61.34	60.28	61:08	60.55	60.81
87	62.58	60.44	6232	60.71	68.05	60.48	61.79	61.25	-61.52
88	63:30	61.13	63.03	61.41	61.77	61.68	61.50	61.95	62-23
89	64.02	61.82	63.75	62.10	63.48	62.38	63.24	62.66	64.93
90	6474	68.52	6447	62.80	64.19	63.08	63.92	63.36	63.64
91	65.46	63,21	65.18	63.50	64.9i	63.78	64.63	64.97	64.35
92	66.18	63.dt -		64.20	65.62.	64.48	65.34	64-77	65.05
93	66.90	64.60	66.02	64.89	66.33	65.18	66.05	65.47	65.76 66.47
94	63.34	65.99	68.05	65.59	67.76	65.89 66.59	66.76. 67.47	66.88 ·	67.18
95	69,06	-					68,18	·	67.88
96 97	59.78	66 65 67.38	58.75	66 99 67.69	68 47,	67.29 67.99	68.8g	69.59 68.29	68.59
98	70.50	68.08		68.38	69.10	68.69	69.60	68.99	-69.30
99	71,21	68 77	70.91	69.08	70.61	69.39	70.54	69.70	70.00
100	71.93	69.47	71.63	69.78	74.33,	70.09	71,02	70.40	70.71
101	72.05	70.16	72.35	70.48	72.04:	70.79	7473	74,14	74.42
102	. 73,37 :	70.86	73.00	71.17	72.75	71.49	73,44	71.81	72.12
103	74.09	71.55	73.78	71-87	7.3.40	72.19	73.15	72.51	74.83
104	74 81	74,24	74.50	72.57	74.18	72.89	73.86	73 22-	73-54
105	15:53	73.94	75:21	73.27	74.89	73.60	74.57	73.92	74.25
106	76.25	73.63	75.98	73-97	75.60	74.30	75.28	74.63	7495 75.66
108	76.97 :77.69	74.33 74.02	76.64	74.66 ±	76.32.	75.00 75.70	75.99	75.33	76.37
109	78.44	7572	78.08	76,06	27-74:	76.40	77-48	76.74	77.07
1110	79113			76.76	78.46	77.10	78,18	77.44	77.78
1111	79.85			77.45	79.17	77.80	78.83	78.15	78.49
112	80,57	77 80		78.45	79.88	78.50	79.54	78.85	79.20
113	81,29	78,5Q.	80.94	78.85	8e.60	79.20	80,25	79.55	79.90
114	82.00	79-19	\$1.66	79 55 1	81.31	79.90	80,96	80.26	80,61
115	82.71	79.89		80.25	82.02	80.60	81.67	80.96	81.32
116	83.44	80.58	83.09	80.94	82.74	81.31	82.38	81.67	82.02
117	84.16 84.88	81.28		81.64	83.45	82.01	83.09	82.37	82.73 83.44
1119	85.60	81.97	84.52	82.34 83.04	84 16 84 88	82.71 83.41	83,80	83.07 83.78	84,15
120	86.32	83.36	85.96	83.73		84 14	85.22	84.48	84.85
	Dep.	Lat	Dep.	Lat	Dep.	Lat	Dep.	Lat.	L D.
Dist.	==0		4		3(51	0'
	<u> </u>		*	,	ડા	,		J.	

TABLE 6.

MEAN REFRACTION.

-	-	_	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
App.	Re	fr.	Ap	p.	Re	rr.	Ap	p.]	Re	r.	Ap		Re	n.	A	p.	Re	Ir.
Alt.	1		A	It.	5		A	it.		10	A	lt.			A	t.		18
0 /	7	B	0	-	-	10	0	-	1	-	0	7	7	-	0	7	- 7	. 13
10	1	-		'	1		4		15			1	25			13		10
0 0	33	0	5	5	9	54	10	0	5		20	0	2		34	0	·F	24
0 5	32	10	5	5	9	46	10	10	5	10	20	10	2	34	34	30	E	23
0 10	3.1	22	5	10	9	38	10	20	5	5	20	20	2		35	0	. 1	21
0 15	30	35	5	15	9	30	10	30	5	Ó	20	30	2	31		30		20
0 20	29	50	5	20	9	23	10	40	4	56	20	40	2	20	36	0	1	18
A COLUMN TO A COLU	-						-			3"			2	28	36	30	i	17
0 25	29	6	5	25	9	15	10	50	4	51	20	50	100				Don't Co	- 2
0 30	28	23	5	30	9	8	11	0	4	47	21	0	2	27	37	0	1	16
0 35	27	41	5	35	9	1	11	10	4	43	21	10	2		37	30	57	*4
0 40	27	0	5	40	_	54	EF	20	4	39	21	20	2	25	38	0	1	13
0 45	26	20	5	45	8	47	11	30	4	34	21	30	2	24	38	30	1	15
-	-	-	-	-	8	-	11	40	+	31	21	40	2	23	39	0	1	10
0 50	25	42	5	50		4.	100		4	-	7.4		100			- 4	10.1	€ 2 40
0 55	25	5	5	55	- 8	34	11	50	4	27	21	50	2,	21	39	30	I	9
1 0	24	29	6	0	8	28	12	0	4	23	22	0	2		40	0		- 8
1 5	100	54	6	5	8	21	12	10	4	20	22	10	2	19	41	0		5
1 10		20	6	10	8	15	12	20	4	16	22	20	2	18	42	.0		3
	22	47	6	15	8	9	12	30	4	13		30	2	17	43			41
			6	20	8		12	40		9	22	40	2	16	44	0	0	59
1 20	22	15			100	3			4							0	0	57
1 25	21	44	6	25	7	57	rz.	50	4	6	22	50	2		45	-	Limber.	-
1 30	21	15	6	30	7	51	13	0	14	3	23	0	-2,	14	46	0	-0	55
1 35	20	46	6	35	7	45	1.3	10	4	0	23	10	2	13	47	0	0	53
1 40	20	18	6	40	7	40	13	20	3	57	23	20	2	12	48	To	0	51
	100	1					17	100	-	-	23		2	11	49	0	0	49
1 45	19	51	6	45	7	35	-	30	3	54		30				0	0	48
1 50	19	25	6	50	7	30	13	40	3	51	23	40	2	100000	50		M 100 PM	
1 55	19	0	6	55	7	25	13	50	3	48	23	50	2	900	51	0	0	46
2 0	18	35	7	0	7	20	14	0	3	45	24	0	2	2.0	52	0	0	44
2 5	18	11	7	5	7	35	14	10	3	43	24	10	2.	7	53	0	a	43
2 10	17	48	7	10	7	11	14	20	3	40	24	20	2	6	54	0	0	41
		26		15	7	6	14	30	3	38	24	30	2		55	0	0	40
1	17	-55	7	20		2		-	-	-	24	40	2		56	0	0	38
2 20	17	4	7		7		14	40	3	35			2	- 3			0	3
2 25	16	44	7	25	6	57	14	50	3	33	24	50	-	3	57	0	6	37
2 30	16	24	7	30	6	53	15	0	3	30	25	0	2	2	58	0	0	35
2 35	16	A	7	35	6	49	15	10	3	28	25	10	2	1	59	0	0	34
4 4	15		7	40	6	45	1.5	20	3	26	25	20	2	0	60	0	0	33
and the second		45			6					24	25	30	1	1.7	61	0	0	32
2 45	15	27	7	45		41	15	30	3				1		62		0	17. 4
2 50	15	9	7	50	6	37	15	40	3	21	25	40				0		30
2 55		52	7 8	55	6	33	15	50	3	19	25	50	1		63	0	0	29
3 0		36		0	6	29	16	10	3	17	26	0	1		64	0	0	28
3 5	14	20	8	5	6	25	16	10	3	15	26	10	1		65	0	0	26
3 10	14	4	8	10	6	22	16	20	3	12	26	20	1		66	0	0	25
			8	15	6	18	16	30	3	10	26	30	1		67	0	0	24
3 15	13	49	_	-	-	-	-	-	-		-	-	_	-		-	-	-
3 20	13	34	8	20	6	15	16	40	3	3	26	40	1	53	68	0	0	23
3 25	13	20	8	25	6	11	16	50	3	6	26	50	1		69	0	0	22
3 30	13	6	8	30	6	8	17	0	3	4	27	0	1	51	70	0	0	21
3 30	12		8	35	6	-5	17	10	3	3	27	15	1		71	0	0	19
	10	33	8	40	6	1	17	20	3	1	27	30	1	100	72	0	0	18
	12	40							2	59	27	-	i	48	73	0	0	100
3 45	12	27	8	45	5	58	17	30	1			45	1			1 1 1 1	0	16
3 50	12	15	8	50	5	55	17	40	2	57	28	0			74	0		
3 55	12	3	8	55	5	52	17	50	2	55	28	15	1	46		0		15
4 0	11	51	9	0	5	48	18	0	2	54	28	30	1		76	0	0	14
4 5	11	40	9	5	5	45	18	10	2	52	28	45	1	44	77	0	0	13
-	_		-	-	-		18	20	2	51	20	0	1	-	78	0	0	12
4 10	11	29	9	10	5	42									100		0	11
4 15	11	18	9	15	5	39	18	30	2	49	29	30	-1		79	0		300
4 20	TI	8	9	20	5	36	18	40	2	47	30	0	1		80	0	0	10
4 25	10	58	9	25	5	34	18	50	2	46	30	30	1		81	0	0	9
		48	9	30	5	31	19	0	2	44	3.1	Ó	1		82	0	0	8
			-	_		28	19	10	2	43	31	30	1		83	0	0	7
4 35	10	39	9	35	5			20	2	41	32	0	r	31	-	0	0	6
4 40	10	29	9	40	5	25	19				-					100		
4 45	10	20	9	45	5	23	19	30	2	40	32	30			86	0	0	4
4 50	10	11	9	50	5	20	19	40	2	38	33	0	1		88	0	0	2
4 55	10	2	9	55	5	18	19	50	2	37	33	30	1	26	90	0	0	0
4 11	-	_		-	_	_	_	-	_	-	_	_		_	-	-	_	-

Bun's	Paral-				Hori		1	Đ		t di	ffer.		tanc	
7.01	in Alt.	Height	D	ip	Height	D	ip	1.80		ght	of	the		
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10	9	4		56	22	4	30	4	4	8	12	15	19	17
20	8	5	2	9	23	4	36	1	3	5	17	10	12	14
30	7	6	2	21	24	4	42	12	3	4	6	18	10	12
50	6	7	2	33	28	5	52	2	2	4	5.	12	8	9
55	5	9	2	43	30	5	15	22	2	3	. 5	6	7	8
60	4	10	3	2	3.5	5	39	31	2	3	4	1 2	6	6
65	4	11	3	10	40	6	.4	4	2	3	4	5	25"	6
70	3	12	3	19	45	6	27	5	2	3	4	4	5	,6
80	2	14	3	26	60	2	25	6	2	3	4	4	5	1.5
85	1	15	3	42		8	i	1			111	(No.		1
90	0	16	3	50		8	34	2 -	1		No	100	31	-
1	2/01/	17	3	57	90	9	6		1,0				Ab	nd

TABLE: 10.

The Semi-diameter of the Sun-

	•							
Mostb	Day.	Sun's Semi-di-		-Day.	Sun's Semi-di.	Menth	Day.	San's Semi-di-
100	7 13 19	16' 19'1 26 19 16 19 16 18 16 17	May.	7 13 19 25	15/54" 15*53 25 52 15 51 15 50	September. Month	7 13 19 25	19' 55" 15 56 15 58 15 59 16 1
ebruary.	1 7 33 29 25	26 16 16 15 16 14 16 13 16 12	Jane	1 7 13 19, 25	15 49 15 48 15 47 85 47 15 47	October	1 7 13 19 25	16 3 16 4 16 6 15 8 16 9
ف	7 3 19 25	16 10 16 9 16 7 16 8 16 4	July.	7. 13 19 25	15 47 15 47 15 47 15 48 15 48	December. Nov ember.	7 13 19 25	16 11 16 13 16 14 16 15 16 16
Tient.	7 13 19 25	16 2 16 1 15 59 15 57 15 \$6	August.	1 7 13 19 25	15 49 15 50 15 51 15 52 15 53	December.	7 13 19 25	16 17 16 18 16 18 16 19 16 19

TARLE IL

Apparent Time of Transit of Polc Star.

This table is adapted to leap year, particularly 1808. In order to make it serve for other years, the time of transit must be taken for the day following that given in the months of January and February. For the first year after leap year, one minute is to be added to the time of transit given in the table; two minutes for the second, and three minutes for the third after leap year.

Again, to reduce this table to a different meridian than that to which it is adapted, viz. Greenwich; if the longitude is between 45° E, and 45° W, there is no correction to be applied. If the longitude is between 45° and 135° E, one minute is to be added; but if it is between 45° and 135° W, one minute is to be subtracted. If the longitude is between 135° E, and 180°, two minutes are to be added, but subtracted if the given longitude is between 135° W, and 180°.

This table is useful to find the time when the altitude of the pole star ought to be observed, to find the latitude by its meridian altitude; it is also useful in finding the variation of the compass by the pole star.

15	, ,	an.	Feb.	Marc	April.	May.	June.	July.	Aug. Se	ot. / Oct.	Nov.	Dec
18		. M	P. M.	P. M·	P. M.	A. M.	A. M.		A. M. A.	M. A. M.	P. M.	P. A.
Г	6	b 97	3h56/	2h 4'	oh o'	10h19/	8h17'	6h 13'	4h 9' 2h	3' Ob25'	10h25'	81.22
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3	6		3 48	E 57	0 3	10 12	8 9	6 5	4 1 2	6 0 18	10 17	8 13
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14			3 4	1 16	11 23	9 29	7 24	5 20	1	7 11 34	9 33	7 25
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27	, -	17	2 15	0 29	10 34	8 38	6 20	4 28		0 10 44	8 39	6 27
28		13	2 11	0 25	10 31	8 34	6 26	4 24		6 10 41	8 35	6 23
29	4	8	2 8	0 21	10 27	8 30	6 22	4 20		3 10 37	8 31	6 19
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31	4	0		0 14		8 22	1	4 12	2 17	10 29	i	6 10

Difference of Altitude of the Pole Star and the Pole, at different distances of the Star from the Meridian.

As the pole star is generally known, that no opportunity, therefore, may be lost for determining the latitude, this table is inserted, the use of which is as follows:—

Find the interval between the time of observation of the altitude of the pole star, and that of its passing the meridian, and take out the corresponding equation from the table; which added to, or subtracted from the true altitude of the pole star, will give the latitude of the place of observation.

EXAMPLES.

I. Let the corrected altitude of the pole star be 46° 10' N, observed 8h. 30' before its passage over the meridian. Required the latitude?

True altitude of the pole star
Equation from table 12 to 8h. 30'
+ 46° 10' N

Latitude
- 47° 15 N.

II. At 1h. 10' after the passage of the pole star over the meridian, its altitude corrected was 58° 51' N. Required the latitude?

True altitude of the pole star - 58° 51' N. Equation from table 12 to 1h. 10' - 1 42

Latitude - 57 9 N.

TABLE 12.

Difference of Altitude of Pole Star and Pole.

Argument. Distance of the Star from the Meridian, in Sidereal Time
Subtract.

Min.	0	Hour.		Hour.	12	Hours.	13 F	lours.	41	lours.		lours.	
0	1,	46'9	1	43,3	1,	32,6	1,0	15'6	0	53,4	00	27.7	1 60
5	1	46.9	1	42.7	1 .	31.4	I	13.9	0	51.4	0	25.4	55
10	1	46.8	1	42.0	1	30.2	I	12.2	0	49.4	0	23.2	50
15	1	46 7	1	41.2	1	28.9	I	10.5	10	47.3	0	20.9	45
20	1	46.5	I	40.4	I	27.6	I	8.7	0	45.2	0	18.6	40
25	. 1	46.3	1	39.6	1	26.2	1	6.9	0	43. I	0	16.3	35
30		46.0	E	38.8	I	24.8	1	5.1	0	40.9	0	14.0	30
35	1	45.7	1	37.9	I	23.4	I	3.2	0	38.8	0	11.6	25
40	1	45.3	1	36.9	I I	21.9	ĸ	1.3	0	36.6	0	9.3	20
45	1	449	T	35.9	I	20.4	0	59.4	0	34.4	0	7.0	15
50	1	44-4	1	34.8	I	18.8	0	57.4	0	32.2	٥	4.7	10
55	I	43.9	1	33.7	1	17.2	0	55.4	0	29.9	0	2.3	5
60	1	43.3	I	32.6	1	15.6	0	53.4	0	27.7	0	0.0	0
	11	Hours	10	Hours.	9 1	lours.	8 I	lours	7 H	lours.	6 H	ours.	Min.

Sun's Declination for the Years 1808, 1812, 1816, 1820.

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EXPLANATION AND USE OF THIS TABLE.

The Declination of the Sun is an arch of a meridian contained between its centre and the equinoctial, which arch is reckoned in

degrees, minutes, &c.

In the first quadrant of the ecliptic, from about the 21st of March, to the 21st of June, the Sun's declination is North, and increasing; and in the third quadrant, between the 22d of September and 21st of December, the Sun's declination is South, and increasing In the second quadrant of the ecliptic, from about the 21st of June to the 22d of September, the Sun's declination is North, and decreasing; and in the fourth quadrant, between the 21st of December and the 21st of March, the Sun's declination is South, and decreasing; which will be readily perceived by inspecting the table.

In this table, the Sun's declination is given, from the year 1808 to 1823 inclusive, calculated for the instant of noon, each day, at

Sun's Declination for the Years 1809, 1813, 1817, 1821.

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2	2:		56	16	50	7	14	4	53	15		22	11	23		17	50		0	3	31	14	43	21	58
3			51	16	33	6	51	5		15	-		18	23		17	35	7	38		54	-	2	22	7
1 4	2		45		15	0	28	5			55		€6		55		19		16	4	•	, ,	21	22	- 1
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the Meridian of Greenwich, or the meridian, at which we begin to reckon the Longitude. It is to be taken out with the month ut the top, and the day in the left hand column, at the same time, noting whether it be North, or South, as expressed at the top of each column. The declination being here given to the nearest minute, it will be found sufficiently exact for the most common and useful problems, wherein it is concerned.

The sun's declination is necessary to find the latitude, whether at sea or land, from the meridian altitude observed; it is also requisite for finding the latitude from two altitudes observed with the interval of time measured by a watch; it serves for computing the sun's azimuth, having his altitude and the latitude of the place given, in order to find the variation of the compass; it is required, jointly with the latitude of the place and the sun's horary angle, to compute his altitude, if neglected to be observed at the time of taking the moon's distance from the sun for finding the longitude, being useful to facilitate the calculation of the effect

Sun's Declination for the Years 1810, 1814, 1818, 1822.

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31	17	28	l	_	14	1	i		21	52	l	(18	24	8	49	١		14	0		_ {	23	8

of refraction and parallax upon the distance; it is also necessary to calculate the apparent time from an obsered altitude of the sun at a distance from the meridian, the latitude being given; or to compute the time of the sun's setting or rising; which, though a less accurate method than the former of obtaining the time, may yet be useful when that cannot be had. For any of these purposes the sun's declination must be found to the time given nearly, reduced to the meridian of *Greenwich*, making proportion according to its daily increase, or decrease, by the help of table 14, as in the following examples.

1st Required the Sun's Declination at noon in New-York, in Ljongitude 74° 8' West, on the 1st of April, 1811.

Dec. for April 1st, 1811, at Greenwich, in Tab. 13 = 4° 18' N. Equation for Long. Table 14. = +4 50"

. Required Declination = 4° 22' 50".N.

Sun's Declination for the Years 1811, 1815, 1819, 1823.

	Ja	n j	Fe	b.	M	ar.	Αp	ril	М	ay.	Ju	ne.	Ju	ly.	Αu	g.	3	ept	Oc	t.	No	v.	1)e	c.
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3	32	54	16	41	7	3	5		15			15			17	42		49	3 4	43	14	53 12	22	11
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N. B. To find the equations in Table 14,—seek the Sun's declination to the nearest degree in the top line of the table; then, under this declination and against the given Lon. in the left hand column, is found the equation for Lon. and in the same column with the dec. and against the given time from Noon, in the right hand column, is found the equation for time; both which equations must be added, or subtracted, according to the directions at the head of the Table.

2d Required the Sun's Declination on the 1st of May, 1811, at 5 h. 48 min. P. M. in Longitude 72° W.

When Sun's dec. increases.

Add in W. lon. | Add af noon. | Sub. in W. lon. | Sub. af noon.

Sub. in E. lon. | Sub. be. noon. | Add in E. lon. | Add be. noon.

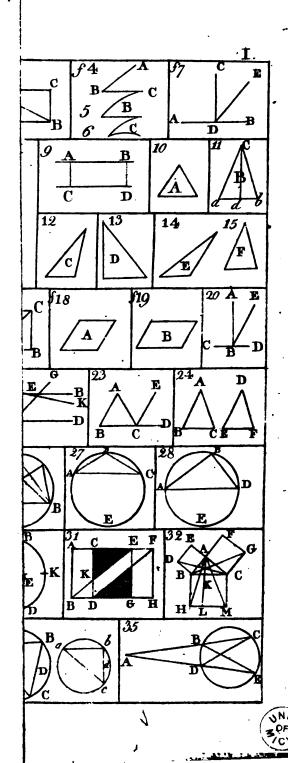
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9	٥	35	0	35	0	35	٥	34	0	34	0	33		32	0	32	0	36
12	0	47	٥	47	0	47	0	46	٥	45	0	44	0	43	0	42	o	48
15	٥	59	٥	59	0	58	O	57	0	56	0	55	0	54	0	53	1	0
18	1	11	1	10	1	10	1	9	1	7	I	6	1	5	1	3	1	12
21	1	22	I	22	1	22	I	21	1	18	1	17	1	16	1	14	1	24
24	1	34	1	34	1	33	1	32	I	29	1	28	1	27	1	24	1	36
27	1	46		45	1	44	1	43	I	41	1	39		38	1	35	1	48
30		58		57		56	1	54		51	1	49	ᆜ	48	1	45	2	0
33	2	, 10	2	10	2	8	2	6	2	3	2	1	1	59	1	55	2	12
36	2	22	2	21	2	19	2	17	2	14	2	12	2	10	2	6	2	24
39	2	33	2	32	2	31	2	39	2	25	2	23	2	20	2	16	2	36
42	2	45	2	44	2	43	2	40	2	36	2	34	2	31	2	27	2	48
45	2	57	2	56	2	54	3	51	2	47	2	44	2	4.1	2	38	3	0
48	3	9	3	8	3	18	3	3	2	59	2	55	2	52	2	49	3	12
51	3	20	3	19	3		3	15 26	3	10	3	6	3	3	3	.~	3	24
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81	5 5	18	5	17	5	14	5	9	5	20	4	56	4	51	4	44	5	12
84	3	30	5	28	5	26	5	20	5	12	3	7	5	2	4	55	5	24 36
87	3	41	5	40	5	37	3	31	5	23	5	18	5	13	5	33	5	48
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102	6	40	6	39	6	35	6	28	6	19	6	14	6	7	5	58	6	36 48
105	6	52	6	51	6	46	6	39	6	30	6	24	6	17	6	9	7	70
108	7	4	7	2	6	58	6	51	6	41	6	35	6	28	6	19	7	12
111	7	15	7	14	7	10	7	3	6	52	6	46	6	39	6	30	7	24
114	7	27	7	26	7	22	7	15	7	3	6	57	6	50	6	40	7	36
117	7	39	7	37	7	33	7	26	7	14	7	8	7	ī	6	51	7	48
120	7	51	7	49	7	44	7	37	7	25	7	48	7	11	7	1	8	0
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126	8	14	8	13	7 8	8	7 8	ó	7	48	7	4Ó	7	33	,	22	8	24
129	8	26		24	8	20	8	11	7	59		51	7	43	7	33	8	36
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144	9	25	9	23	9	18	9	8	8	55	8	46	8	37	8	26	9	36
147	9	37	9	35	9	29	9	19	9	6	8	57	8	48	8	36	9	48
150	9	48	_9_	45	9	40	9	30	9	17	9	8	8	58	8	47	10	0
153	10	0	9	57		52	9	42	9	28	9	19	9	9	8	57	0	12
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159	10	24		21	10	10	10	5	9	50	9	41	9	31	9	18	10	36
162	10	30		33	10	27	10	16	10	1	9	52	9	42	9	29	10	48
165	10	47	10	44	10	38	10	27	10	12	10	3	9	52	9	39	11	0
168	10	59		56		50	10	39	10	24	10	14	10	3	9	şo		12
171	11	11	11	8	11	2	10	51	10	35	10	25	10	14	10	0	11	24
174	11	23	11	20	11	14	11	3	10	46	10	36	10	25	10	11	11	36
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180	11	401	11	43	11	57	11	25	£ £	ō	10	58	10	46	ıo	32	12	0

When Sun's dec. increases. When Sun's dec. decreases.

Add in W. lon. Add af. noon. Sub. in W. lon. Sub.af.noon.

Sub. in E. lon. Sub. be. noon Add in E. lon. Addbe.noon.

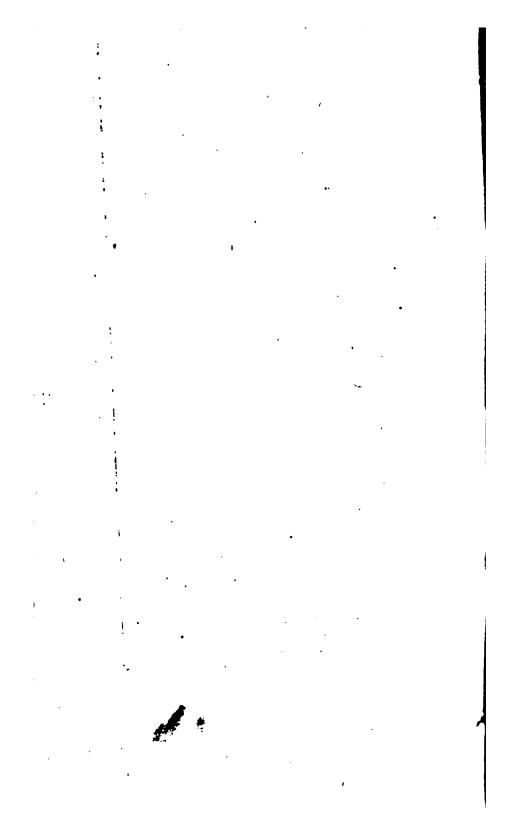
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15	0 51	0 50	0 48	0 46	0 44	0 32	0 31	0 28	0 48
18	1 1	1 0	0 58	0 55	0 53	0 49	0 46	0 35	1 12
21	1 12	1 9	1 7	1 5	1 2	0 57	0 54	0 49	1 24
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45	2 34	1	2 24	2 19	2 12	2 5	1 57	I 39	3 0
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72	4 6		3 51	3 41	3 32	3 10	3 7	2 43	4 48
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108	5 59	100	5 37	5 23	5 8	4 52	4 33	4 9	7 0
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144	8 13	7 58	7 42	7 23	7 3		6 14	5 42	9 36
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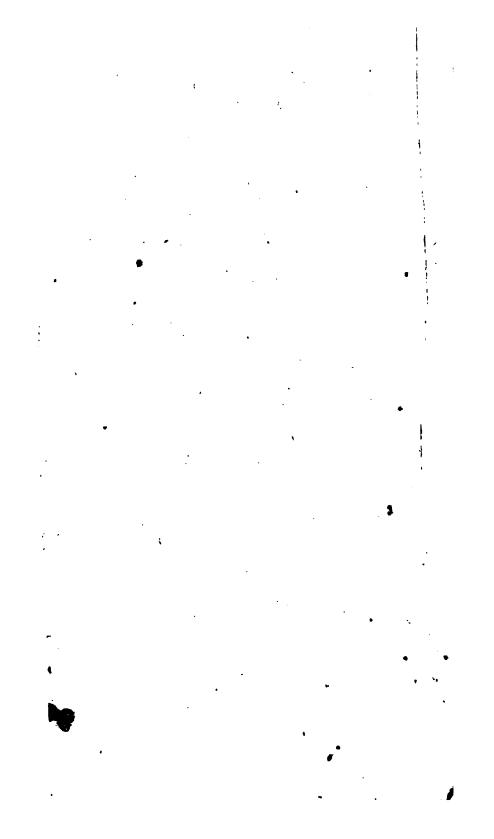


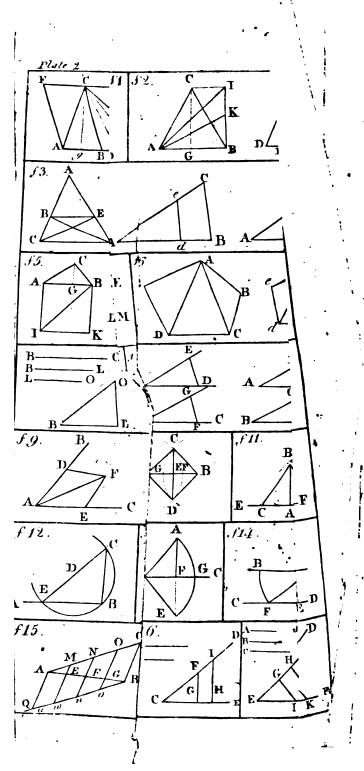
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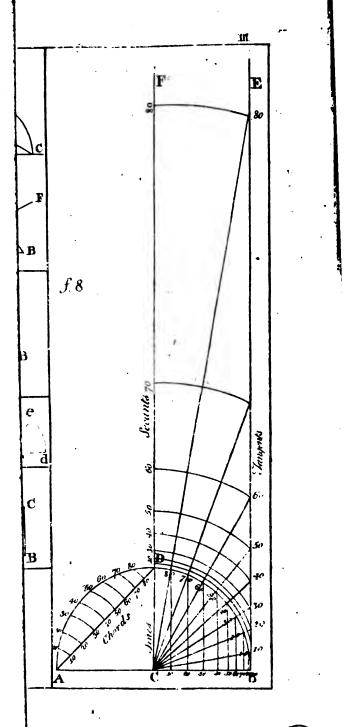


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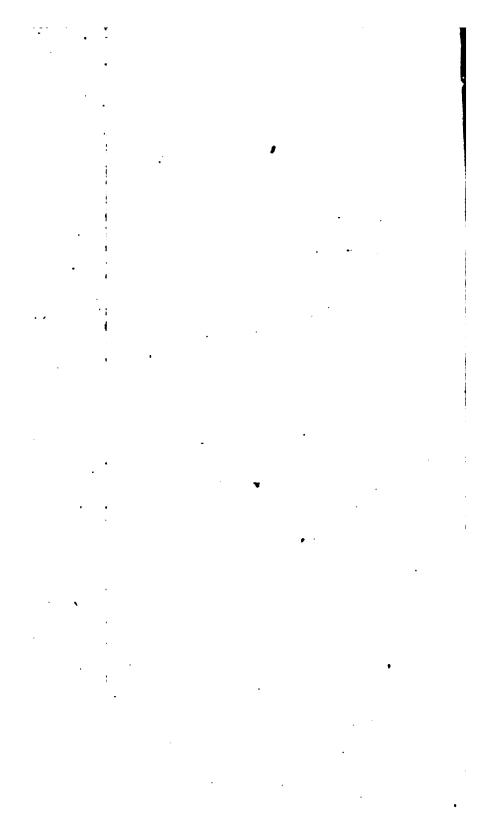








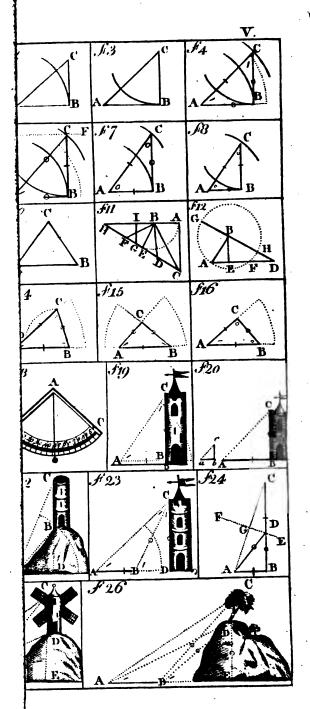
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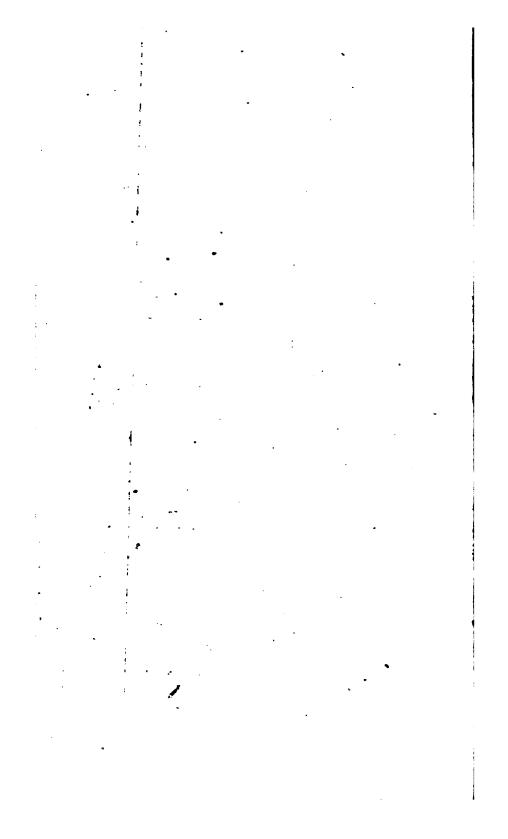
The Proportions for the Solution of 6 Cases of Right Angled Plain Triangles TA S. 'A. AC :: R AB Sc'C AC TC AB Ser'C:AC::R:BC Jee A. A.C. TA:BC R: Al: SA: BC R: ac::SC: AB B R TC:AB::SecC:AC SA:BC::SC:AB SA:BC::R:AC TA:BC::R:AB TA:BC:Ja'A:AC TC:AB:: R:BC Case 3. TA AB:R: AC: Sec'A BC:R::AC: Sec.C AC:R::BC: SA R:AB:: TA:BC R:AC::SC:AB R:BC::TC:AB Case 5.

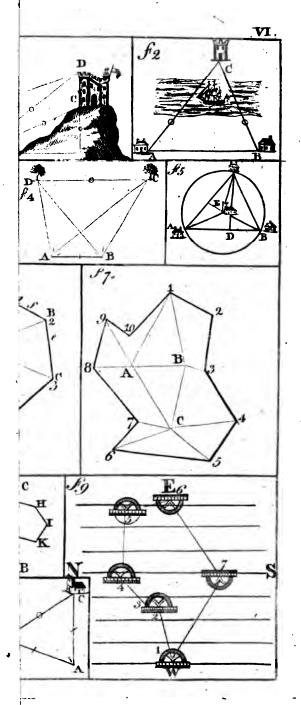
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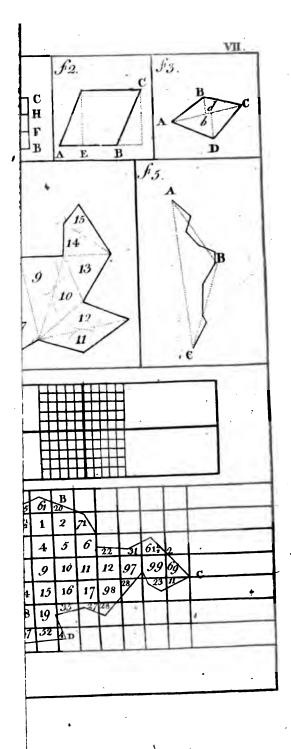




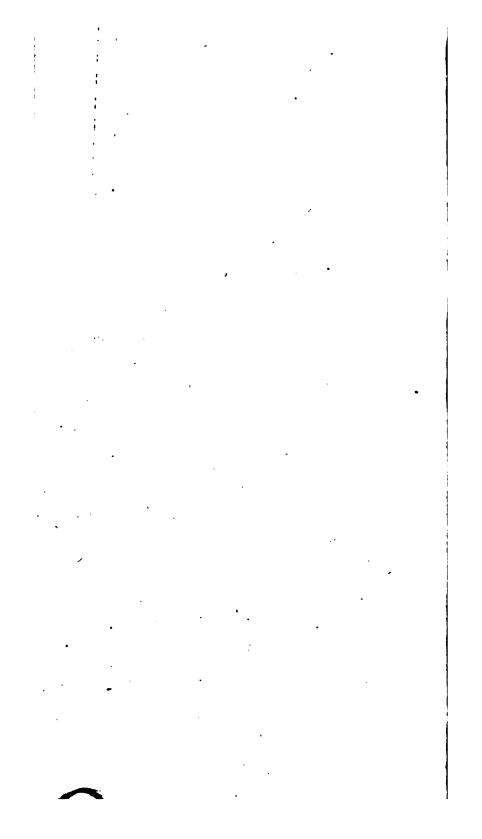


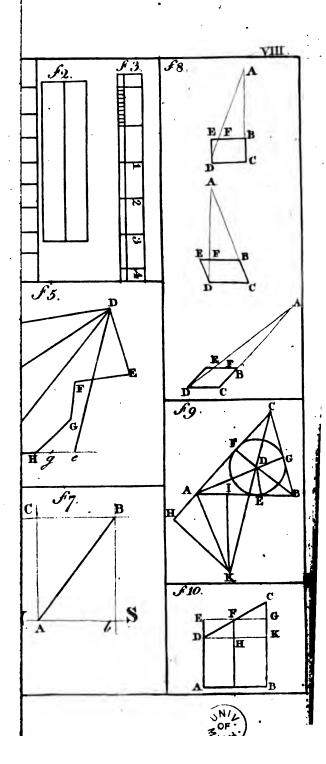


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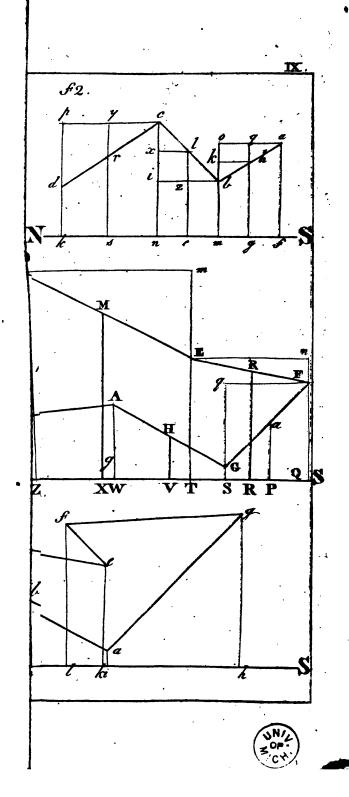


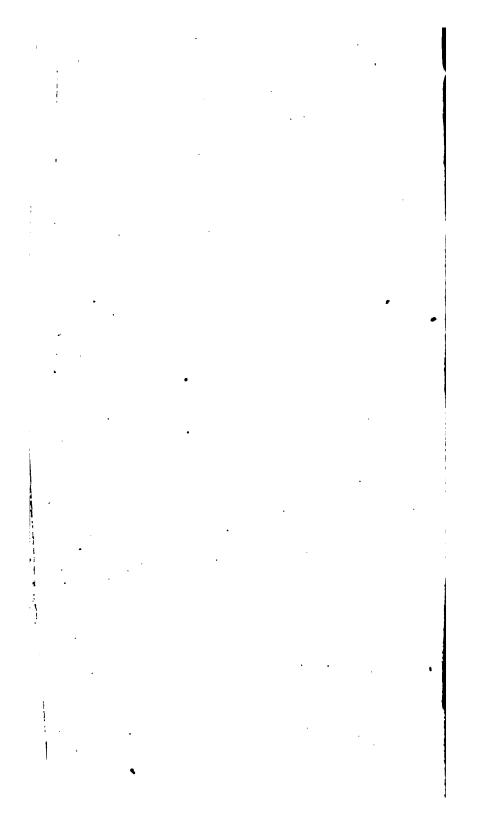
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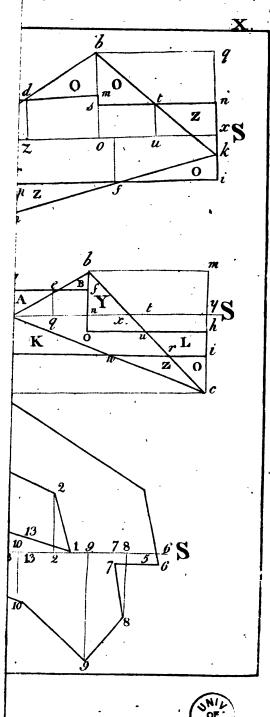


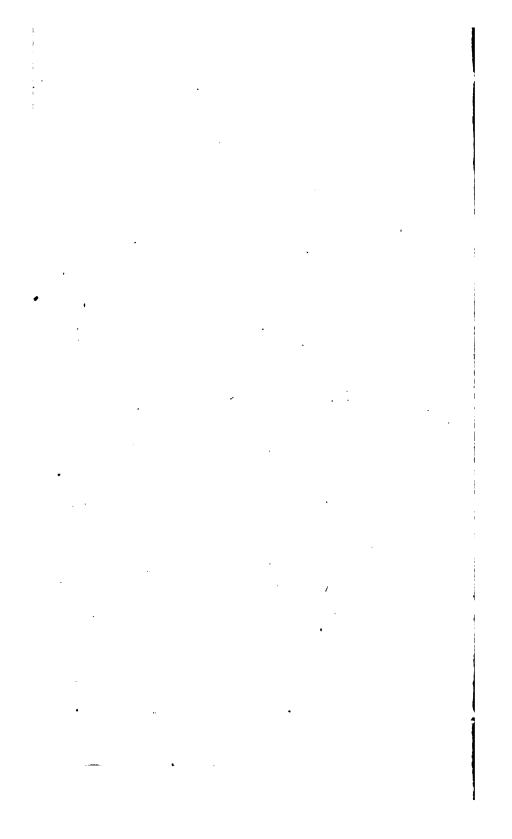


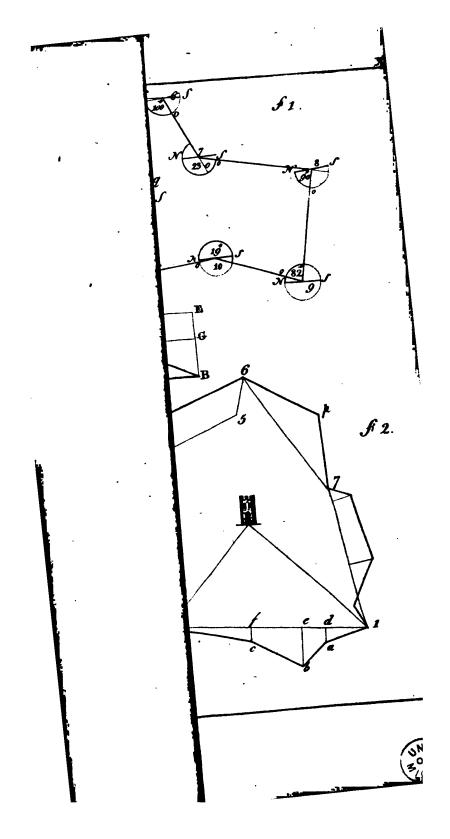
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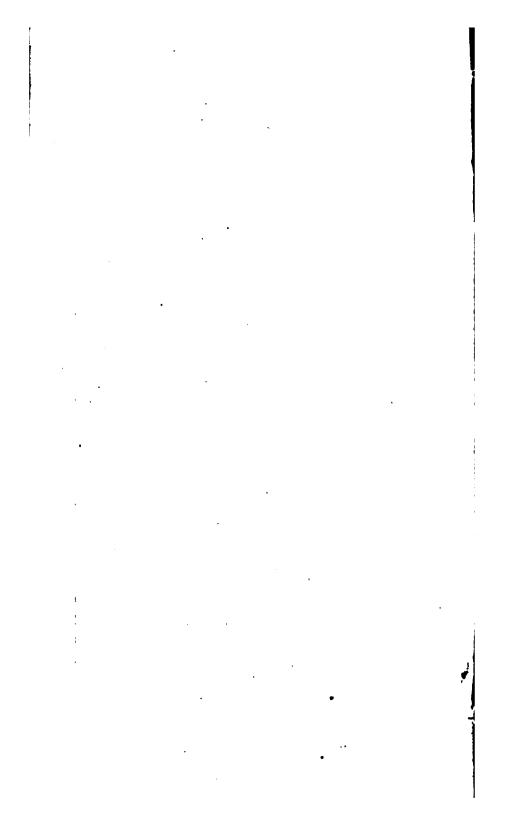


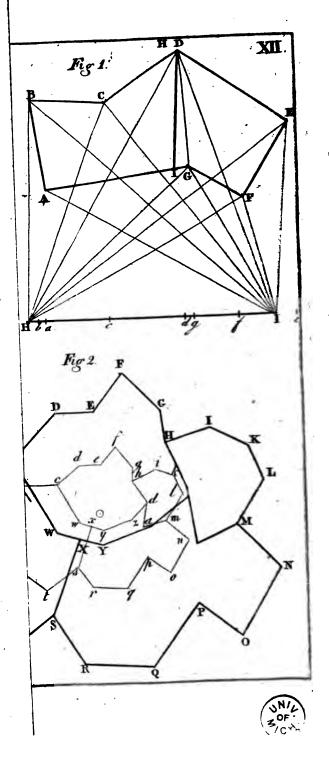


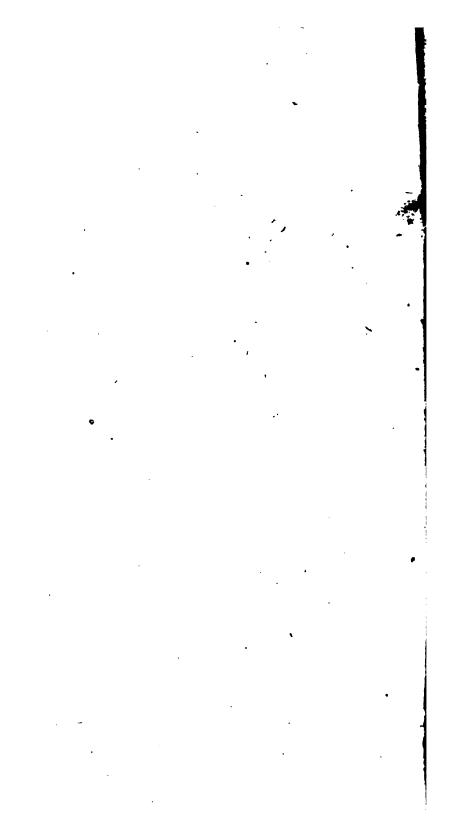


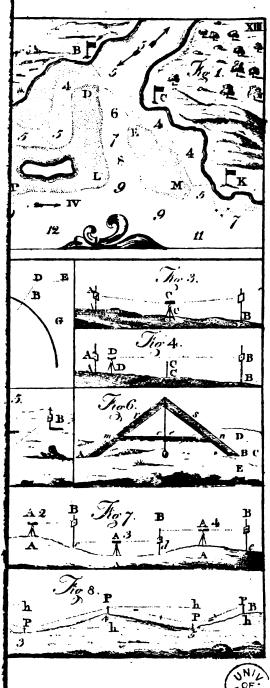














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